

**Document Status Control Record**

**Section 16 Planning Application for Proposed Hotel  
at 16 Kimberley Road, Tsim Sha Tsui  
K.I.L. 6022 s.B R.P.**

**Traffic Impact Assessment Report**

|  |                  |     |                                 |
|--|------------------|-----|---------------------------------|
|  |                  |     |                                 |
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## **1 INTRODUCTION**

### **1.1 Background**

- 1.1.1 The owner of 16 Kimberley Road, Tsim Sha Tsui (hereafter, referred to as “the Site”) intends to demolish the existing building and redevelop the Site into a non-domestic building for hotel use (hereafter, referred to as “the proposed hotel”) with a relaxation in plot ratio. The location of the Site is shown in **Figure 1.1**.
- 1.1.2 LLA Consultancy Limited has been commissioned by the owner to undertake a traffic impact assessment study to support the planning application. This report presents the findings of the study.

### **1.2 Study Objectives**

- 1.2.1 The objectives of this study can be summarised as follows:
- to review the existing traffic conditions in vicinity of the proposed hotel;
  - to estimate the volume of traffic that will be induced by the proposed hotel;
  - to assess the future traffic situation of the surrounding network in vicinity of the proposed hotel;
  - to appraise the potential traffic impact of the proposed hotel;
  - to quantify the internal transport facilities for the proposed hotel.

## 2 THE PROPOSED DEVELOPMENT

### 2.1 The Development Site Location

2.1.1 As shown in **Figure 1.1**, the Site is located at 16 Kimberley Road, Tsim Sha Tsui and has a site area of about 1,141m<sup>2</sup>.

### 2.2 Proposed Development Content

2.2.1 It is understood that a set of GBP was approved in September 2024 for a development of 99 guestrooms hotel cum retail use (hereafter, referred to as “the approved scheme”). The development content of the approved scheme is summarized in **Table 2.1**.

**Table 2.1 Development Parameters of the Approved Scheme and the Proposed Hotel**

| Use                               | Development Parameters   |                          |
|-----------------------------------|--------------------------|--------------------------|
|                                   | Approved Scheme          | Proposed Hotel           |
| Hotel                             | 99 guestrooms            | 159 guestrooms           |
| Conference and Banquet Facilities | 4,123.684 m <sup>2</sup> | 5,917.629 m <sup>2</sup> |
| Retail                            | 888.403 m <sup>2</sup>   | Nil                      |

2.2.2 The proposed hotel will be mainly for hotel use with supporting hotel facilities. Due to an increase in hotel room numbers, no retail area will be provided. **Table 2.1** also summarizes the development parameters of the proposed hotel.

### 3 EXISTING TRAFFIC SITUATION

#### 3.1 Existing Traffic Conditions

- 3.1.1 The Application Site is located on the southern kerbside of Kimberley Road. With reference to the Annual Traffic Census (ATC) published by the Transport Department (TD) in 2023, Kimberley Road is a two-lane local distributor road connecting Nathan Road and Observatory Road. It recorded an average annual daily traffic (AADT) of 17,230 vehicles in the section between Nathan Road and Observatory Road in 2023.
- 3.1.2 Nathan Road is a dual three-lane primary distributor road connecting Salisbury Road and Boundary Street. It recorded an AADT of 28,220 vehicles in the section between Hillwood Road and Kimberley Road in 2023.

#### 3.2 Traffic Count Survey

- 3.2.1 In order to assess the existing traffic conditions, a traffic count survey was carried out at the following locations in the vicinity of the Application Site on 18 September 2025 (Thursday) during the peak hour period, i.e., from 07:30 to 09:30 and 17:00 to 19:00. The locations of the surveyed junctions are as follows and presented in **Figure 3.1**.

J1 – Nathan Road / Kimberley Road;

J2 – Nathan Road / Austin Road;

J3 – Chatham Road South / Austin Road / Cheong Wan Road;

J4 – Chatham Road South / Observatory Road; and

J5 – Kimberley Road / Observatory Road

- 3.2.2 The identified AM and PM peak hours are 08:30 – 09:30 and 17:45 – 18:45, respectively. The recorded peak hour traffic flows are presented in **Figure 3.2**.

#### 3.3 Junction Capacity Assessment

- 3.3.1 Junction capacity assessment was carried out to reveal the existing performance of the key junctions with the 2025 surveyed traffic flows. The assessment results are tabulated in **Table 3.1** and the detailed calculation sheets are presented in **Appendix A**.

**Table 3.1 Existing Junction Performance**

| No. | Junction   | Type/ Capacity Index <sup>(1)</sup> | AM Peak | PM Peak |
|-----|--|-------------------------------------|---------|---------|
| J1  | Nathan Road / Kimberley Road                       | Priority/DFC                        | 0.11    | 0.16    |
| J2  | Nathan Road / Austin Road                          | Signalized/RC                       | 54%     | 55%     |
| J3  | Chatham Road South / Austin Road / Cheong Wan Road | Signalized/RC                       | 49%     | 52%     |
| J4  | Chatham Road South / Observatory Road              | Priority/DFC                        | 0.39    | 0.70    |
| J5  | Kimberley Road / Observatory Road                  | Priority/DFC                        | 0.35    | 0.52    |

Note: (1) RC = Reserve Capacity for signalized junction; DFC = Design Flow to Capacity ratio for priority junction.

- 3.3.2 **Table 3.1** has indicated that the concerned junctions operate satisfactorily during both AM and PM peak hours.

### 3.4 Existing Public Transport Facilities

3.4.1 The Site enjoys extremely high accessibility to public transport facilities, including MTR and bus services. Tsim Sha Tsui MTR Station Entrance is located about 260m south of the Site. Furthermore, there are over 70 bus routes running along Nathan Road. **Table 3.2** and **Figure 3.3** show the existing bus routes serving the vicinity of the Site.

**Table 3.2 Existing Public Transport Routes**

| Mode | Route No.  | Origin - Destination  | Frequency (min) |
|------|--|---|-----------------|
| Bus  | 1  | Chuk Yuen Estate – Star Ferry                                     | 8 – 25          |
|      | 1A   | Sau Mau Ping (Central) – Star Ferry                               | 7 – 20          |
|      | 1R   | Hung Hom (Hung Luen Road) – Ngong Ping                            | 3 trips per day |
|      | 2  | Star Ferry – Cheung Sha Wan (So Uk Estate)                        | 15 – 25         |
|      | 3X   | Tsz Wan Shan (North) – China Ferry Terminal (Via Fu Shan)         | 9 trips per day |
|      | 6  | Star Ferry – Lai Chi Kok  | 8 – 25          |
|      | 7  | Star Ferry – Lok Fu   | 15 – 30         |
|      | 9  | Choi Fook – Tsim Sha Tsui East (Mody Road)                        | 15 – 30         |
|      | 13X  | Po Tat – Tsim Sha Tsui East                                       | 10 – 30         |
|      | 14X  | Yau Tong (Shung Tak Wai) – Tsim Sha Tsui (Circular)               | 15 – 30         |
|      | 26   | Shun Tin – Tsim Sha Tsui East                                     | 8 – 25          |
|      | 26X  | Tsim Sha Tsui East – Shun Tin                                     | 4 trips per day |
|      | 35A  | Kwai Chung (On Yam Estate) – Tsim Sha Tsui East                   | 5 – 20          |
|      | 35X  | Kwai Chung (On Yam Estate) – Tsim Sha Tsui East                   | 20 – 30         |
|      | 36X  | Lei Muk Shue – Tsim Sha Tsui East (Mody Road)                     | 5 trips per day |
|      | 37X  | Chi Fu Fa Yuen – Central (Circular)                               | 15 – 20         |
|      | 41A  | Tsing Yi (Cheung On Estate) – Tsim Sha Tsui East                  | 10 – 25         |
|      | 50   | Tuen Mun (Ching Tin And Wo Tin) – Tsim Sha Tsui (Kowloon Station) | 20 – 30         |
|      | 79P  | Queen'S Hill Fanling – Hsr West Kowloon Station                   | 4 trips per day |
|      | 81C  | Yiu On – Tsim Sha Tsui East (Mody Road)                           | 10 – 30         |
|      | 87D  | Kam Ying Court – Hung Hom Station                                 | 6 – 25          |
|      | 87E  | Nai Chung – Tsim Sha Tsui   | 2 trips per day |
|      | 87C  | Kam Ying Court – Hung Hom Station                                 | 12 – 20         |
|      | 98D  | Hang Hau (North) (Tseung Kwan O Hospital) – Tsim Sha Tsui East    | 6 – 30          |
|      | 98P  | Hong Sing Garden – Tsim Sha Tsui East                             | 5 trips per day |
|      | 203C   | Sham Shui Po (Tai Hang Tung) – Tsim Sha Tsui East (Mody Road)     | 20 – 30         |
|      | 203S   | Chak On Estate – Tsim Sha Tsui East (Mody Road)                   | 1 trip per day  |
|      | 208  | Broadcast Drive – Tsim Sha Tsui East                              | 25 – 30         |
| 213X | On Tai (South) (Hang Tai House) – Tsim Sha Tsui (Circular) | 12 – 30   |                 |
| 219X | Laguna City – Tsim Sha Tsui(Circular)                      | 16 – 40   |                 |

| Mode | Route No. | Origin - Destination  | Frequency (min)  |
|------|-----------|---|------------------|
|      | 224X      | Kai Yip – Tsim Sha Tsui East (Circular)                             | 25 – 30          |
|      | 230X      | Tsuen Wan (Allway Gardens) – Whampoa Garden                         | 3 trips per day  |
|      | 234P      | Tsuen Wan (Bayview Garden) – Star Ferry                             | 1 trip per day   |
|      | 234X      | Tsim Sha Tsui East (Mody Road) – Tsuen Wan (Bayview Garden)         | 15 – 25          |
|      | 242X      | Tsing Yi (Cheung Hang Estate) – Tsim Sha Tsui                       | 4 trips per day  |
|      | 252B      | Handsome Court – Tsim Sha Tsui                                      | 3 trips per day  |
|      | 259C      | Sun Tuen Mun Centre – Tsim Sha Tsui                                 | 2 trips per day  |
|      | 259B      | Tuen Mun Pier Head – Tsim Sha Tsui                                  | 3 trips per day  |
|      | 260X      | Tuen Mun (Po Tin Estate) – Hung Hom Station                         | 5 – 20           |
|      | 260B      | Tuen Mun Central – Tsim Sha Tsui                                    | 4 trips per day  |
|      | 261B      | Tuen Mun (Sam Shing Estate) – Kowloon Station                       | 3 trips per day  |
|      | 268B      | Long Ping Station – Hung Hom (Hung Luen Road)                       | 5 trips per day  |
|      | 269B      | Tin Shui Wai Town Centre – Hung Hom (Hung Luen Road)                | 12 – 30          |
|      | 270A      | Sheung Shui – Tsim Sha Tsui East (Mody Road)                        | 10 – 30          |
|      | 270S      | Tsim Sha Tsui East (Mody Road) – Fanling (Luen Wo Hui)              | 4 trips per day  |
|      | 270C      | Fanling (Luen Wo Hui) – Tsim Sha Tsui East (Mody Road)              | 2 trips per day  |
|      | 271       | Tai Po (Fu Heng) – Jordan (West Kowloon Station)                    | 6 – 60           |
|      | 271B      | Tai Po (Fu Heng) – Jordan (West Kowloon Station)                    | 8 trips per day  |
|      | 271X      | Jordan (West Kowloon Station) – Tai Po (Fu Heng)                    | 5 trips per day  |
|      | 271S      | Hung Hom Station – Tai Po (Tai Wo)                                  | 1 trip per day   |
|      | 271P      | Kau Lung Hang – Tsim Sha Tsui (Canton Road)                         | 2 trips per day  |
|      | 280X      | Sui Wo Court – Tsim Sha Tsui East (Mody Road)                       | 15 – 30          |
|      | 281B      | Shek Mun Estate – Tsim Sha Tsui East (Mody Road)                    | 15 – 30          |
|      | 281X      | Yiu On – Tsim Sha Tsui East (Mody Road)                             | 15 – 25          |
|      | 281A      | Kwong Yuen – Kowloon Station  | 10 – 25          |
|      | 281E      | Haiphong Road Tsim Sha Tsui – Kwong Yuen                            | 2 trips per day  |
|      | 287D      | Hung Hom Station – Kam Ying Court                                   | 2 trips per day  |
|      | 296D      | Sheung Tak – Kowloon Station (Via M+)                               | 15 – 30          |
|      | 790       | Oscar By The Sea – Tsim Sha Tsui (Mody Road)                        | 20               |
|      | 796P      | Tseung Kwan O Station – Tsim Sha Tsui (East)                        | 20 – 30          |
|      | A21       | Hung Hom Station – Airport (Ground Transportation Centre)           | 8 – 30           |
|      | H2K       | Central (Star Ferry) – West Kowloon Cultural (Circular)             | 14 trips per day |
|      | N21       | Tsim Sha Tsui (Star Ferry) – Airport (Ground Transportation Centre) | 20 – 30          |
|      | N21A      | Tsim Sha Tsui (Star Ferry) – Airport (Via Yat Tung Estate)          | 3 trips per day  |
|      | N41X      | Hung Hom Station – Tsing Yi (Cheung Wang Estate)                    | 2 trips per day  |
|      | N50       | Tuen Mun (Ching Tin And Wo Tin) – Tsim Sha Tsui (Kowloon Station)   | 4 trips per day  |

| <b>Mode</b> | <b>Route No.</b> | <b>Origin - Destination</b>                          | <b>Frequency (min)</b> |
|-------------|------------------|--|------------------------|
|             | N213             | Tsim Sha Tsui East (Mody Road) – On Tai (West)       | 2 trips per day        |
|             | N216             | Yau Tong – Hung Hom Station                          | 25 – 30                |
|             | N241             | Hung Hom Station – Tsing Yi (Cheung Wang Estate)     | 25 – 30                |
|             | N271             | Tai Po (Fu Heng) – Hung Hom Station                  | 20 – 30                |
|             | N281             | Kam Ying Court – Hung Hom Station                    | 25 – 30                |
|             | N283             | Tsim Sha Tsui East (Mody Road) – Wong Nai Tau        | 3 trips per day        |
|             | N287             | Tsim Sha Tsui East (Mody Road) – Wu Kai Sha Station  | 3 trips per day        |
|             | N796             | Tsim Sha Tsui East (Chatham Road South) – Lohas Park | 20 – 30                |
|             | NA20             | Whampoa Garden – HZMB Hong Kong Port                 | 2 trips per day        |

## 4 FUTURE TRAFFIC SITUATION

### 4.1 Design Year

4.1.1 It is anticipated that the proposed hotel can be operated by 2030. To consider 3 years after the planned completion of the proposed hotel, a design year of 2033 will be adopted in this study.

### 4.2 Traffic Generation of the Approved Scheme

4.2.1 For the approved scheme in September 2024, the traffic volume that would be induced can be estimated based on the trip rates documented in the Transport Planning Design Manual (“TPDM”), Volume 1, Chapter 3 – Transport Considerations of Town Plans and summarized in **Table 4.1**.

**Table 4.1 Traffic Generation of the Approved Scheme**

|  | Unit/Content             | AM Peak Hour |           |           | PM Peak Hour |           |           |
|--|--------------------------|--------------|-----------|-----------|--------------|-----------|-----------|
|  |                          | Gen.         | Att.      | 2-way     | Gen.         | Att.      | 2-way     |
| <b>Adopted Trip Rates <sup>(1)</sup></b> |                          |              |           |           |              |           |           |
| Hotel (99 rooms)                         | pcu/hr/room              | 0.1329       | 0.1457    | -         | 0.1290       | 0.1546    | -         |
| Retail (888.403 m <sup>2</sup> GFA)      | pcu/hr/100m <sup>2</sup> | 0.2296       | 0.2434    | -         | 0.3100       | 0.3563    | -         |
| <b>Traffic Generation (pcu/hr)</b>       |                          |              |           |           |              |           |           |
| Hotel                                    | 99 rooms                 | 14           | 15        | 29        | 13           | 16        | 29        |
| Retail                                   | 888.403 m <sup>2</sup>   | 3            | 3         | 6         | 3            | 4         | 7         |
| <b>Total</b>                             |                          | <b>17</b>    | <b>18</b> | <b>35</b> | <b>16</b>    | <b>20</b> | <b>36</b> |

Note: Gen. – Generation; Att. – Attraction  
(1) TPDM mean trip rates are adopted.

### 4.3 Traffic Generation of the Proposed Hotel

4.3.1 Based on the development parameters as listed in **Table 2.1**, the development traffic generation of the proposed hotel were estimated and summarized in **Table 4.2**, based on the trip rates documented in TPDM Volume 1 Chapter 3 – Transport Considerations of Town Plans.

**Table 4.2 Traffic Generation of the Proposed Hotel**

| 159 guestrooms      | Unit/Content | AM Peak Hour |        |       | PM Peak Hour |        |       |
|---------------------|--------------|--------------|--------|-------|--------------|--------|-------|
|                     |              | Gen.         | Att.   | 2-way | Gen.         | Att.   | 2-way |
| Adopted Trip Rates  | pcu/hr/room  | 0.1329       | 0.1457 | -     | 0.1290       | 0.1546 | -     |
| Traffic Generations | pcu/hr       | 22           | 24     | 46    | 21           | 25     | 46    |

Note: Gen. – Generation; Att. - Attraction

### 4.4 Comparison of Traffic Generation between the Proposed Hotel and the Approved Scheme

4.4.1 As shown in **Table 4.2**, the proposed hotel will generate a two-way traffic of 46 pcu/hr in both AM and PM peak hour, respectively. As compared with the traffic generation of the approved scheme estimated in **Table 4.1**, the comparison result is presented in **Table 4.3**.

**Table 4.3 Comparison of Development Traffic Generation**

| Use                           | AM Peak Hour |          |           | PM Peak Hour |          |           |
|-------------------------------|--------------|----------|-----------|--------------|----------|-----------|
|                               | Gen.         | Att.     | Total     | Gen.         | Att.     | Total     |
| Approved Scheme (A)           | 17           | 18       | 35        | 16           | 20       | 36        |
| Proposed Hotel (B)            | 22           | 24       | 46        | 21           | 25       | 46        |
| <b>Net Increase (B) – (A)</b> | <b>5</b>     | <b>6</b> | <b>11</b> | <b>5</b>     | <b>5</b> | <b>10</b> |

Note: Gen. – Generation; Att. - Attraction

4.4.2 Based on the comparison result with the approved scheme, the proposed hotel will only induce additional two-way traffic of 11 and 10 pcu/hr during the AM and the PM peak hour, respectively. Even the cumulative impact of 46 and 46 pcu/hr in the two peak hours is considered insignificant to the surrounding road network, in particular with the high accessibility of public transport services. The development traffic flows are distributed onto the road network as shown in **Figure 4.1**.

Other Planned and Approved Developments

- To estimate the future traffic flows generated and attracted by the nearby planned and approved developments, updated information has been obtained from available information regarding the planned and approved developments in the vicinity of the proposed hotel, the details of these developments are listed in **Table 4.4**.

**Table 4.4 Planned and Approved Developments**

| Site | Location  | Parameters                 |
|------|---|----------------------------|
| S1   | Proposed Minor Relaxation of Building Height and Site Coverage Restrictions for the Expansion of Hong Kong Science Museum and Hong Kong Museum of History at 2 Science Museum Road and 100 Chatham Road South, Tsim Sha Tsui<br>(Planning Application No. A/K1/267) | 66,438 m <sup>2</sup> GFA  |
| S2   | Proposed Minor Relaxation of Building Height Restriction for Permitted Educational Institution Use at Main Campus of the Hong Kong Polytechnic University, Kowloon Inland Lot No. 9853 RP & Ext. (Part)<br>(Planning Application No. A/K1/268)                      | 33,299 m <sup>2</sup> GFA  |
| S3   | Proposed Flat with Permitted Office, Shop and Services/Eating Place at 43-49A Hankow Road, Tsim Sha Tsui, Kowloon<br>(Planning Application No. A/K1/269)  | 9,210.6 m <sup>2</sup> GFA |
| S4   | Proposed Hotel Redevelopment at 11 Middle Road, Tsim Sha Tsui<br>(Kimpton Tsim Sha Tsui Hong Kong)  | 495 guestrooms             |

4.4.3 Based on the latest set of traffic generation and attraction rates documented in Chapter 3 “Transport Considerations of Town Plans” of the Transport Planning and Design Manual (TPDM), the traffic generated by these developments were estimated and are taken into account in the following assessments.

## 4.5 Traffic Forecast

### Historical ATC Data

4.5.1 In order to establish the traffic growth rate in the vicinity of the Site, reference was made to the 2019 to 2023 Annual Traffic Census Reports published by the Transport Department, reporting on the annual average daily traffic (AADT) flows at the counting stations in the territory. Details of the counting stations in the study area and the corresponding counts are shown in **Table 4.5**.

**Table 4.5 Annual Traffic Census Data**

| Stn. No.     | Road Section   |                           |                           | AADT <sup>(1)</sup> |                            |                           |                            |                           | Avg. Growth% |
|--------------|----------------|---------------------------|---------------------------|---------------------|----------------------------|---------------------------|----------------------------|---------------------------|--------------|
|              | Road           | From                      | To                        | 2019                | 2020                       | 2021                      | 2022                       | 2023                      |              |
| 3013         | Austin Rd      | Cox's Rd                  | Chatham Rd S              | 30,030              | 27,400<br>(-8.8%)          | 25,010<br>(-8.7%)         | 25,350<br>(1.4%)           | 27,690<br>(9.2%)          | -2.0%        |
| 3242         | Cheong Wan Rd  | Yuk Choi Rd up-ramp       | Chatham Rd S              | 33,840              | 31,670<br>(-6.4%)          | 33,020<br>(4.3%)          | 31,470<br>(-4.7%)          | 33,840<br>(7.5%)          | 0.0%         |
| 3445         | Austin Rd      | Canton Rd                 | Nathan Rd                 | 36,200              | 31,490<br>(-13%)           | 32,840<br>(4.3%)          | 31,290<br>(-4.7%)          | 33,010<br>(5.5%)          | -2.3%        |
| 3608         | Chatham Rd S   | Observatory Rd            | Austin Rd & Cheong Wan Rd | 41,350              | 35,310<br>(-14.6%)         | 35,580<br>(0.8%)          | 33,910<br>(-4.7%)          | 35,770<br>(5.5%)          | -3.6%        |
| 3610         | Nathan Rd      | Hillwood Rd               | Kimberley Rd              | 30,600              | 29,220<br>(-4.5%)          | 28,080<br>(-3.9%)         | 26,750<br>(-4.7%)          | 28,220<br>(5.5%)          | -2.0%        |
| 3646         | Austin Rd      | Nathan Rd                 | Cox's Rd                  | 22,510              | 22,190<br>(-1.4%)          | 22,690<br>(2.3%)          | 21,620<br>(-4.7%)          | 22,810<br>(5.5%)          | 0.3%         |
| 3688         | Observatory Rd | Chatham Rd S              | Kimberley Rd              | 9,220               | 10,530<br>(14.2%)          | 12,710<br>(20.7%)         | 12,110<br>(-4.7%)          | 12,780<br>(5.5%)          | 8.5%         |
| 3809         | Chatham Rd S   | Austin Rd & Cheong Wan Rd | Gascoigne Rd              | 53,790              | 50,350<br>(-6.4%)          | 45,900<br>(-8.8%)         | 43,200<br>(-5.9%)          | 45,580<br>(5.5%)          | -4.1%        |
| 3810         | Nathan Rd      | Jordan Rd                 | Hillwood Rd               | 24,030              | 22,490<br>(-6.4%)          | 18,840<br>(-16.2%)        | 18,140<br>(-3.7%)          | 19,140<br>(5.5%)          | -5.5%        |
| 4620         | Kimberley Rd   | Nathan Rd                 | Observatory Rd            | 13,560              | 10,160<br>(-25.1%)         | 17,030<br>(67.6%)         | 13,520<br>(-20.6%)         | 17,230<br>(27.4%)         | 6.2%         |
| <b>Total</b> |                |                           |                           | <b>295,130</b>      | <b>270,810<br/>(-8.2%)</b> | <b>271,700<br/>(0.3%)</b> | <b>257,360<br/>(-5.3%)</b> | <b>276,070<br/>(7.3%)</b> | <b>-1.7%</b> |

Note: (1) Figures in bracket indicated the % increase between two years.

4.5.2 **Table 4.5** showed that the recorded average annual growth rate of the concerned counting stations is -1.7% between years 2019 to 2023.

### TPEDM Data for Future Years

4.5.3 Reference was also made to the 2021 – based Territorial Population and Employment Data Matrix (TPEDM) published by the Planning Department. The population and employment data of year 2019 and 2031 are summarized in **Table 4.6**.

**Table 4.6 TPEDM Data – Yai Tsim Mong**

| Year                           | 2021    | 2026                 | 2031                 |
|--------------------------------|---------|----------------------|----------------------|
| Population                     | 310,650 | 291,700              | 267,100              |
| Employment                     | 413,950 | 439,300              | 428,850              |
| Total                          | 724,600 | 731,000              | 695,950              |
| <b>Average Annual Growth %</b> |         | +0.2% (2021 to 2026) | -1.0% (2026 to 2031) |

4.5.4 As shown in **Table 4.6**, the average annual growth rate for the population and the employment total between 2021–2026 and 2026–2031 is +0.2% and -1.0% respectively. Having considered that the annual growth rates derived from the ATC data and the TPEDM data, a nominal growth rate of +0.5% will be adopted for the subsequent traffic forecast on a conservative approach.

#### 4.6 2033 Reference and Design Flows

4.6.1 The 2033 Reference Flows, i.e. the traffic flows in the vicinity without the proposed hotel, were estimated based on the following equation.

$$\text{2033 Reference Flows} = \text{2025 Traffic Flows} \times (1 + 0.5\%)^8 + \text{Traffic Flows Generated by the Planned and Approved developments}$$

4.6.2 The 2033 Design Flows, i.e. the traffic flows in the local road network with the traffic generated by the proposed hotel, were estimated based on the following equation:

$$\text{2033 Design Flows} = \text{2033 Reference Flows} + \text{Traffic Flows Generated by the Proposed Hotel}$$

4.6.3 The 2033 Reference and Design Flows are shown in **Figures 4.2 and 4.3**, respectively.

#### 4.7 Junction Capacity Assessment

4.7.1 Junction capacity analysis was carried out for the assessment year 2033. The assessment results are shown in **Table 4.7** and the detailed calculation sheets are attached in **Appendix B**.

**Table 4.7 2033 Junction Capacity Assessment**

| No. | Junction   | Type/Capacity Index <sup>(1)</sup> | 2033 Reference |      | 2033 Design |      |
|-----|--|------------------------------------|----------------|------|-------------|------|
|     |  |                                    | AM             | PM   | AM          | PM   |
| J1  | Nathan Road / Kimberley Road                       | Priority/DFC                       | 0.12           | 0.17 | 0.12        | 0.17 |
| J2  | Nathan Road / Austin Road                          | Signalized/RC                      | 45%            | 49%  | 44%         | 47%  |
| J3  | Chatham Road South / Austin Road / Cheong Wan Road | Signalized/RC                      | 41%            | 46%  | 40%         | 45%  |
| J4  | Chatham Road South / Observatory Road              | Priority/DFC                       | 0.42           | 0.75 | 0.45        | 0.79 |
| J5  | Kimberley Road / Observatory Road                  | Priority/DFC                       | 0.36           | 0.54 | 0.40        | 0.57 |

Note: (1) RC = Reserve Capacity for signalized junction; DFC = Design Flow to Capacity ratio for priority junction.

4.7.2 As shown in **Table 4.7**, the assessed junctions will operate with capacities during the peak hours in 2033 with the expected traffic growth and the additional traffic flows generated by the proposed hotel.

## 5 PROVISION OF TRANSPORT FACILITIES

### 5.1 Vehicular Access

5.1.1 In the proposed hotel, the vehicular access remains the same position as the approved scheme at Kimberly Road in order to provide access to internal transport facilities. The width of the vehicular access will be of 6.0m and the access's sightline is demonstrated in **Figure 5.1**.

### 5.2 HKPSG Requirements in Car Parking and Loading/Unloading Provisions

5.2.1 The requirements of car parking and loading/unloading facilities should be estimated, taking into consideration of the latest Hong Kong Planning Standards and Guidelines (HKPSG) requirements. The required car parking and loading/unloading facilities for the proposed hotel as required under the HKPSG is listed in **Table 5.1**.

**Table 5.1 Car Parking and Loading/Unloading Facilities as Required by HKPSG**

| Component  | HKPSG Requirements   | Required Provision Under HKPSG |  | Proposed Provision |   |
|--|--|--------------------------------|--|--------------------|---|
|  |  | Nos.                           | Dimension  | Nos.               | Dimension   |
| <b>Hotel – 159 guestrooms and 5,917.629 m<sup>2</sup> GFA for Conference and Banquet Facilities;</b> |  |                                |  |                    |   |
| Car Parking Space  | <u>Guestroom:</u><br>1 car space per 100 rooms                                       | 2                              |  | 2                  |   |
|  | <u>Conference and banquet facilities:</u><br>0.5 – 1 car space per 200m <sup>2</sup> | 15 – 30                        |  | 28 <sup>(1)</sup>  |   |
| <b>TOTAL CAR PARKING</b>   |  | <b>17 – 32</b>                 | 16 – 31 @ 5.0m(L) x 2.5m(W) x 2.4m (L)<br>1 @ 5.0m(L) x 3.5m(W) x 2.4m (L) | 30                 | 29 @ 5.0m(L) x 2.5m(W) x 2.4m (L)<br>1 @ 5.0m(L) x 3.5m(W) x 2.4m (L) |
| Loading/Unloading Space  | 1 goods vehicle bay per 100 rooms  | 2                              | 1 @ 11.0m(L) x 3.5m(W) x 4.7m (L)<br>1 @ 7.0m(L) x 3.5m(W) x 3.6m (L)      | 2                  | 2 @ 8.0m(L) x 3.5m(W) x 3.6m (L)<br><sub>(2)(3)</sub>                 |
| Motorcycle Parking Space   | 5 – 10 % of total provision for private cars   | <b>1 – 3</b>                   | 1 – 3 @ 2.0m(L) x 1.0m(W)  | 3                  | 3 @ 2.0m(L) x 1.0m(W)   |
| Lay-by for Taxi and Private Car  | 2 spaces for ≤ 299 rooms   | <b>2</b>                       | 2 @ 5.0m(L) x 2.5m(W) x 2.4m (L)   | 2                  | 2 @ 5.0m(L) x 2.5m(W) x 2.4m (L)                                      |
| Lay-by for Single-Deck Tour Bus  | 1 space for ≤ 299 rooms  | <b>1</b>                       | 1 @ 12.0m(L) x 3.5m(W) x 3.8m (L)  | 1                  | 1 @ 8.0m(L) x 3.5m(W) x 3.6m (L)<br><sub>(3)(4)</sub>                 |

- Notes: (1) 0.93 car space per 200m<sup>2</sup> is adopted for Conference and Banquet Facilities.  
(2) In view of the size of the Site, only LGV loading/unloading bays are provided.  
(3) The spaces can be share-used by goods vehicles and light buses and are therefore proposed to be 8.0m (L) x 3.5m (W).  
(4) In view of the size of the Site, only light bus parking space are provided.

5.2.2 The proposed hotel will provide a total of 30 car parking spaces, 2 LGV loading/unloading bays, 3 motorcycle parking spaces, 2 lay-bys for taxi and private cars and 1 light bus lay-by to meet the HKPSG requirements. The car park layout plan is enclosed in **Appendix C** and it is clearly demonstrated that two basement floors are fully utilized to provide internal transport facilities which are serving by two carlifts.

5.2.3 In formulating the ground floor layout, the 2 nos. of taxi and private car lay-by is being arranged in the most effective and efficient manner such that the vehicles will conduct the pick-up/drop-off activities within the proposed hotel instead of along the Kimberley Road kerbside. As a result, it is not anticipated to induce additional pick-up/drop-off demand on public road. Furthermore, to ensure the internal circulation of vehicles on ground floor will not be affected, a waiting zone of 15m is provided as shown on **Figure 5.2** and can avoid vehicles queuing back onto public road.

**5.3 Practical Dimensions of Loading/Unloading Bays and Single Deck Tour Bus Lay-by**

5.3.1 Due to site constraints, it is proposed to limit the use of LGV loading/unloading bays (8m in length) and light bus lay-by (8m in length) only and to replace the HGV loading/unloading bays (11m in length) and lay-by for single deck tour bus (12m in length) with full justifications listed in **Table 5.2**. Traffic management plan will be set up in place by the hotel operator to reject HGV and large tour bus during the operational phase.

**Table 5.2 Justifications on Dimensions of the Internal Transport Facilities**

| No.                             | Considerations                      | Justifications for Proposed Dimension of Loading/unloading Space  |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |
|---------------------------------|-------------------------------------|---|----------|--------------------------|-------------------|---------------------------------|-------------------------|-----------|----------------------------|-----------------|------------|-------|-------------------------------|---|
| 1                               | Area and shape of Site              | The dimension of the Site is about 21m (W) x 50m (L). Given the small site area, after providing the necessary floor space to accommodate the ramp, entrance lobby, staircases, lift core and M&E facilities etc., the remaining area is not sufficient to provide a 11m long loading/unloading space because the 11m long HGV cannot make a 3-point turn manoeuvring at the remaining area. Please refer to the swept path analysis in <b>Appendix D</b> demonstrating that a HGV cannot make a 3-point turn within the Site.  |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |
| 2                               | No tour group                       | The proposed small hotel with 159 rooms is not targeted for large tour groups with coaches as transportation. The provision of light bus lay-by will be sufficient to meet the demand.  |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |
| 3                               | Negligible Loading/unloading Demand | <p>According to the operating of similar hotels with less than 200 rooms, the loading/unloading demand for these hotels was very minimal. In general, the normal operation of a small hotel will induce loading/unloading demand because of the activities as shown below. The subsequent recorded/estimated loading/unloading trips are also shown below.</p> <table border="1"> <thead> <tr> <th>Activity</th> <th>Loading/unloading Demand</th> <th>Required Duration</th> </tr> </thead> <tbody> <tr> <td>Regular Delivery of Consumables</td> <td>Maximum 1 trips per day</td> <td>5 minutes</td> </tr> <tr> <td>Out-source Laundry Service</td> <td>1 trips per day</td> <td>10 minutes</td> </tr> <tr> <td>Total</td> <td>Not more than 2 trips per day</td> <td>-</td> </tr> </tbody> </table> <p>In view of the small loading/unloading frequency, the provision of LGV bays will be sufficient to meet the demand of the proposed building.</p> | Activity | Loading/unloading Demand | Required Duration | Regular Delivery of Consumables | Maximum 1 trips per day | 5 minutes | Out-source Laundry Service | 1 trips per day | 10 minutes | Total | Not more than 2 trips per day | - |
| Activity                        | Loading/unloading Demand            | Required Duration   |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |
| Regular Delivery of Consumables | Maximum 1 trips per day             | 5 minutes   |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |
| Out-source Laundry Service      | 1 trips per day                     | 10 minutes  |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |
| Total                           | Not more than 2 trips per day       | -   |          |                          |                   |                                 |                         |           |                            |                 |            |       |                               |   |

#### **5.4 Car Lift Assessment**

- 5.4.1 To assess the performance of the car lift system, it is necessary to adopt an appropriate arrival rate (attraction rate) in the assessment. With reference to the trip rates as documented in the latest Transport Planning and Design Manual, Volume 1, Chapter 3 prepared by the Transport Department, the peak traffic attraction rate of the proposed hotel is estimated.
- 5.4.2 The servicing rate of the car lift system is estimated based on the operation data provided by the car lift supplier.
- 5.4.3 A M/M/N queuing model is adopted to assess the probability of nos. of vehicle queuing in the car lift system. In case only 3 vehicles in the system, this implies that the 2 car lifts and the waiting space(s) are being occupied. If 4 or above vehicles in the system, there will be traffic queuing onto the public road and the system performance is undesirable.
- 5.4.4 From the assessment result, the probability of queuing onto the public road is about 1%. In other words, there is 99% confidence level that no traffic queue will occur in the public road and the system performance is found to be satisfactory. The details of the car lift assessment calculation are shown in **Appendix E**.

#### **5.5 Swept Path Analysis**

- 5.5.1 To ensure smooth manoeuvring of the parking area, swept path analysis was conducted to demonstrate that adequate space is provided for the vehicles for manoeuvring as shown in **Appendix F**.

#### **5.6 Building Setback**

- 5.6.1 At present, the footpath width along the site frontage is about 2.5 m. In the proposed hotel development, 4.3 m setback will be provided to increase the footpath width to 6.8 m to enhance the pedestrian walking environment.

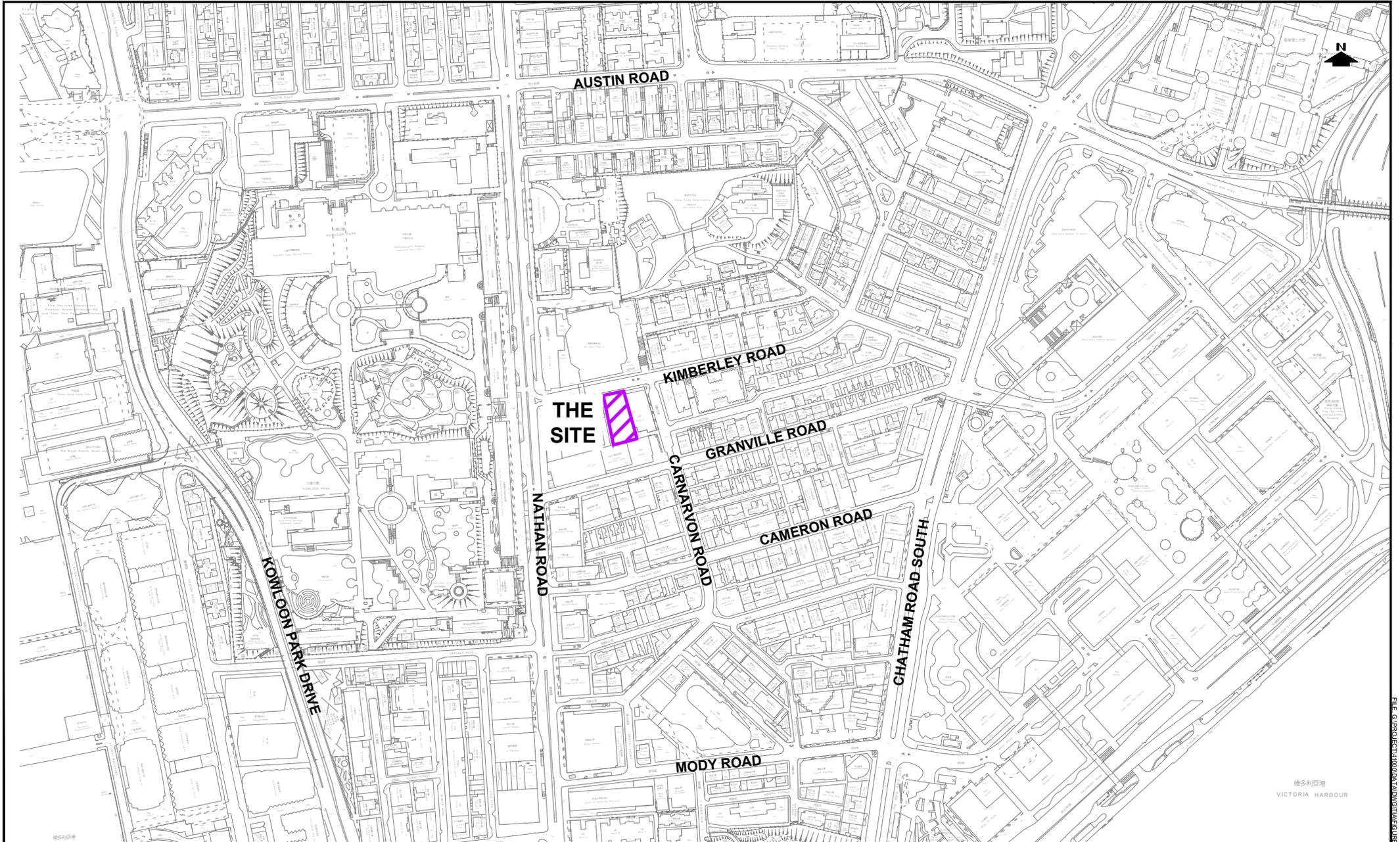
## **6 SUMMARY AND CONCLUSION**

### **6.1 Summary**

- 6.1.1 The owner of the Site at 16 Kimberley Road, Tsim Sha Tsui intends to redevelop the Site into a non-domestic building as a hotel.
- 6.1.2 In order to assess the existing traffic conditions, a traffic count survey was carried out at the key junctions in the vicinity of the Application Site on 18 September 2025 (Thursday) during the peak hour period. The identified AM and PM peak hours are 08:30 – 09:30 and 17:45 – 18:45, respectively. The capacity of the key junctions in the vicinity of the Site was analysed and the results show that the concerned junctions are operating satisfactorily in the AM and PM peak hours. The proposed hotel enjoys excellent accessibility to public transport facilities, including MTR, bus and minibus services. Tsim Sha Tsui MTR Station Entrance is located about 260m south of the Site.
- 6.1.3 The proposed hotel will generate a two-way traffic of 46 pcu and 46 pcu during AM peak hour and PM peak hour, respectively. As compared with the approved GBP submission in September 2024, the proposed hotel will only induce additional two-way traffic of 11 and 10 pcu/hr during the AM and the PM peak hour respectively. By assigning the development traffic to the 2033 Reference Flows, the 2033 Design Flows were obtained.
- 6.1.4 The cumulative traffic impact is considered insignificant to the surrounding road network. For the proposed hotel, the same vehicular access as the approved GBP scheme is adopted at Kimberly Road. The proposed hotel will provide a total of 30 car parking spaces, 2 LGV loading/unloading bays, 3 motorcycle parking spaces, 2 lay-bys for taxi and private cars and 1 light bus parking space to meet the HKPSG requirements. Two basement floors are parking spaces to serve the proposed hotel.
- 6.1.5 Due to the Site constraint, for the small hotel (159 rooms only), relaxation is required and the provision of the LGV loading/unloading bays and light bus lay-bys would be sufficient to meet the guests' demand.
- 6.1.6 Car lift assessment was conducted and the result shows that the probability of queuing onto the public road is about 1%. In other words, there is 99% confidence level that no traffic queue will be incurred in Kimberly Road and the system performance is found to be satisfactory.

### **6.2 Conclusion**

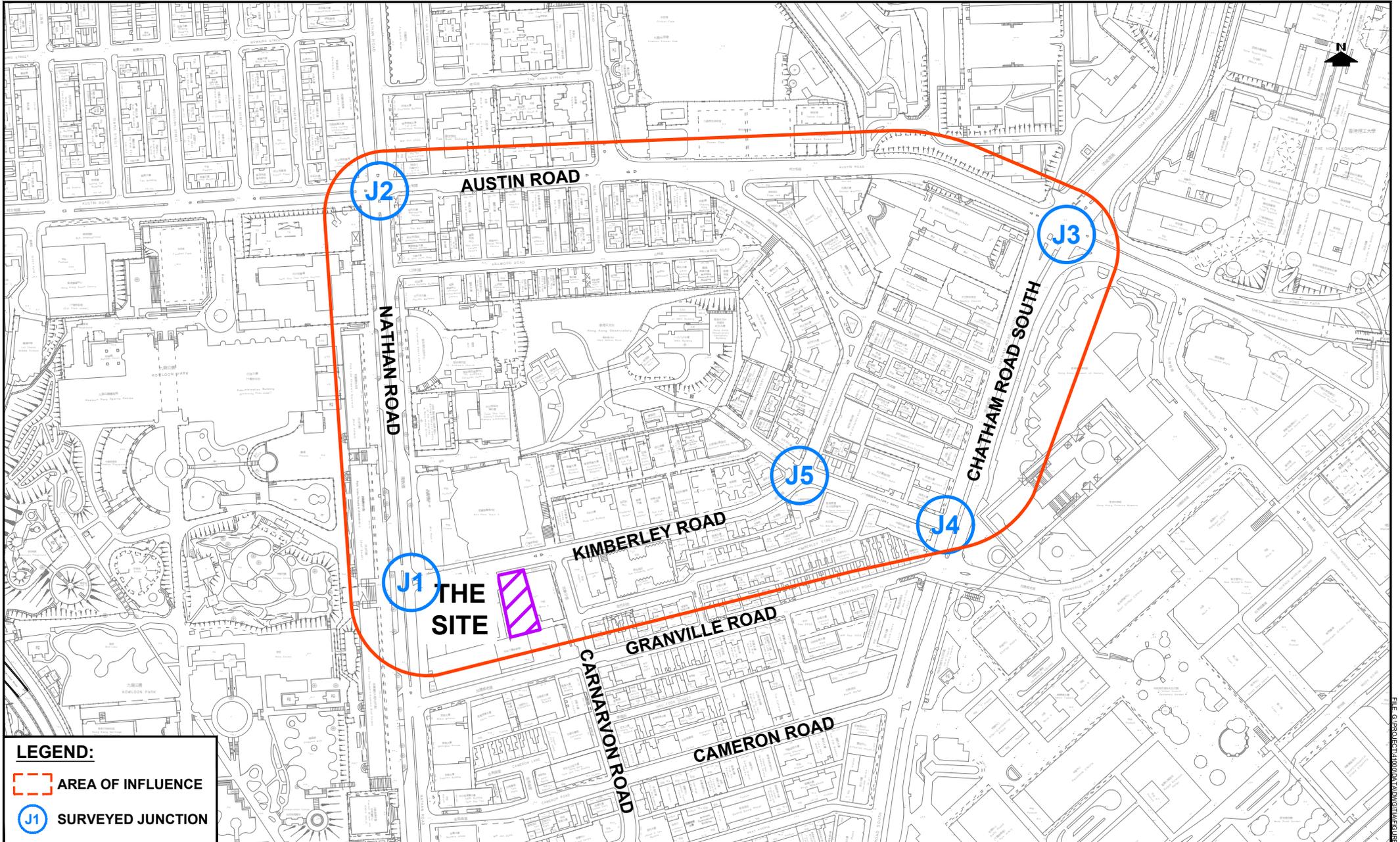
- 6.2.1 Based on the findings of the traffic impact assessment study, it can be concluded that the proposed hotel development, with the provision of adequate internal transport facilities, will not induce significant adverse traffic impact and is acceptable from traffic engineering perspective.



|             |       |               |
|-------------|-------|---------------|
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| DESIGNED    | SKL   | DATE SEP 2025 |
| DRAWN       | CLL   | SCALE 1:5000  |
| CHECKED     | SLN   |               |

|               |  |  |
|---------------|--|--|
| PROJECT TITLE | SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B.R.P. |  |
| DRAWING TITLE | <b>LOCATION PLAN</b>   |  |

|                   |            |                     |   |
|-------------------|------------|---------------------|---|
| DRAWING NO.       | FIGURE 1.1 | REV.                | . |
| <b>LLA</b> 顧問有限公司 |            | Consultancy Limited |   |



**LEGEND:**

AREA OF INFLUENCE

SURVEYED JUNCTION

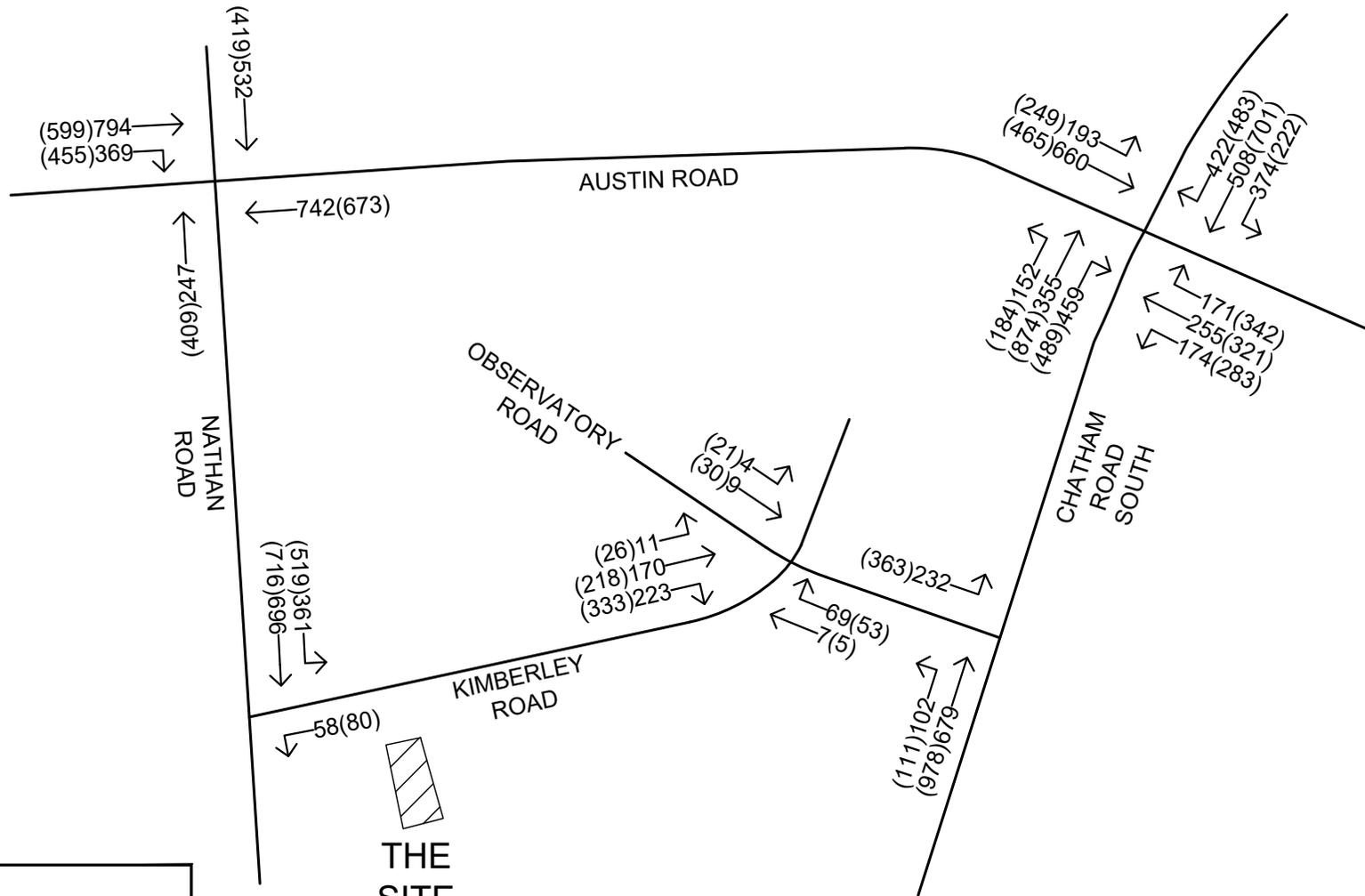
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| CHECKED     | SLN   |               |

PROJECT TITLE SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B.R.P.

DRAWING TITLE **LOCATION OF SURVEYED JUNCTIONS AND AREA OF INFLUENCE**

|             |            |      |   |
|-------------|------------|------|---|
| DRAWING NO. | FIGURE 3.1 | REV. | . |
|-------------|------------|------|---|

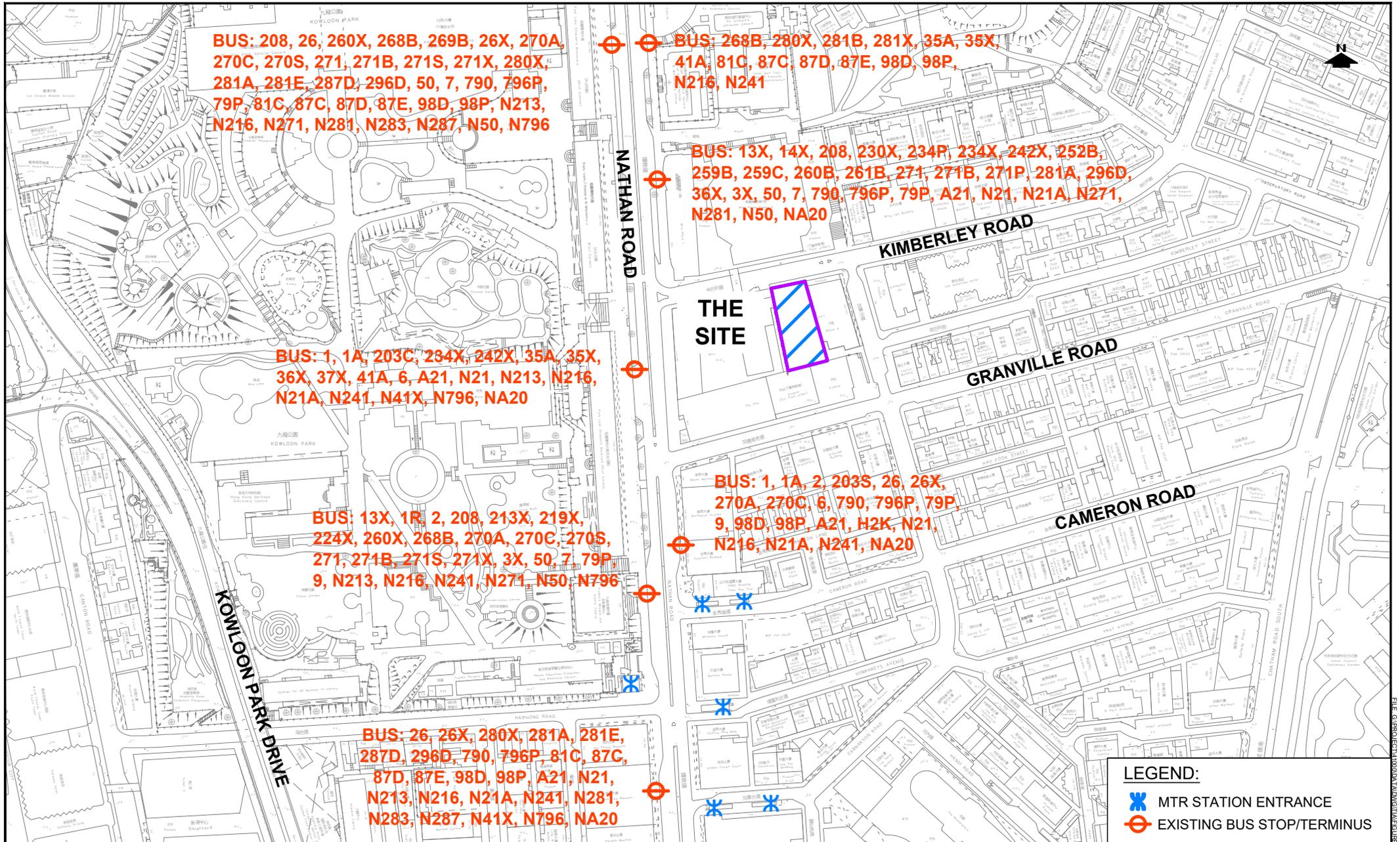
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**LEGEND:**  
 123 (456) ← PM PEAK HOUR TRAFFIC FLOW  
 ↑ AM PEAK HOUR TRAFFIC FLOW

**NOTE:**  
 1. ALL TRAFFIC FLOWS ARE IN PCU/HOUR  
 2. MINOR ROADS ARE NOT SHOWN FOR CLARITY

|                   |               |  |  |  |  |        |  |
|-------------------|---------------|--|--|--|--|--------|--|
| PROJECT NO. 41000 |               | PROJECT TITLE SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B R.P. |  | DRAWING NO. FIGURE 3.2                   |  | REV. . |  |
| DESIGNED SKL      | DATE SEP 2025 | DRAWING TITLE  |  |  |  |        |  |
| DRAWN CLL         | SCALE N.T.S.  | <b>2025 EXISTING TRAFFIC FLOW</b>  |  |  |  |        |  |
| CHECKED SLN       |               |  |  |  |  |        |  |
|                   |               |  |  | <b>LLA</b> 顧問有限公司<br>Consultancy Limited |  |        |  |

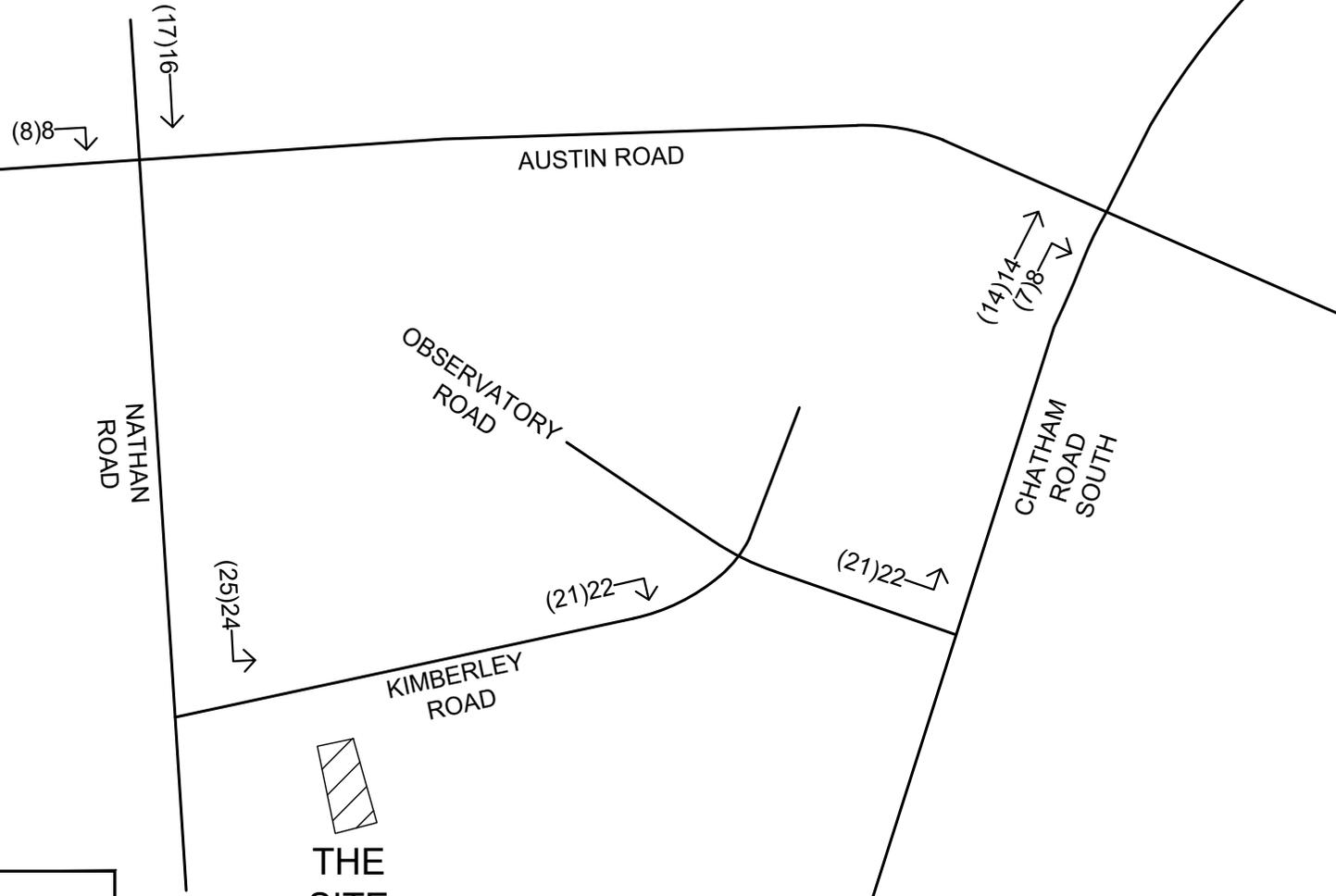


|             |       |               |
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| DRAWN       | CLL   | SCALE 1:3000  |
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PROJECT TITLE SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B R.P.

|               |   |  |
|---------------|---|--|
| DRAWING TITLE | PUBLIC TRANSPORT SERVICES ALONG NATHAN ROAD |  |
| DRAWING NO.   | FIGURE 3.3                                  |  |
| REV.          |   |  |

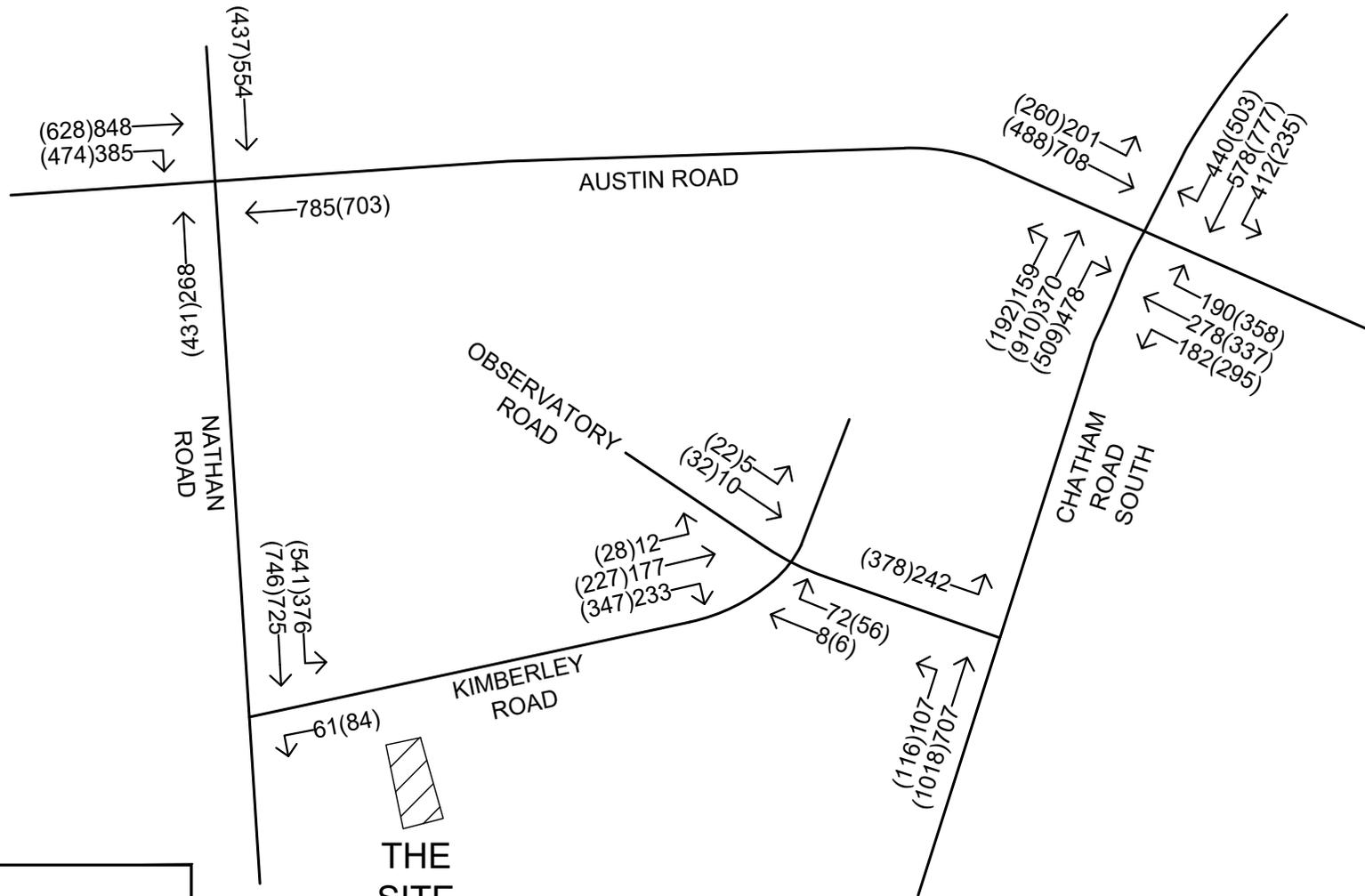
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**LEGEND:**  
 123 (456) ← PM PEAK HOUR TRAFFIC FLOW  
 ↑ AM PEAK HOUR TRAFFIC FLOW

**NOTE:**  
 1. ALL TRAFFIC FLOWS ARE IN PCU/HOUR  
 2. MINOR ROADS ARE NOT SHOWN FOR CLARITY

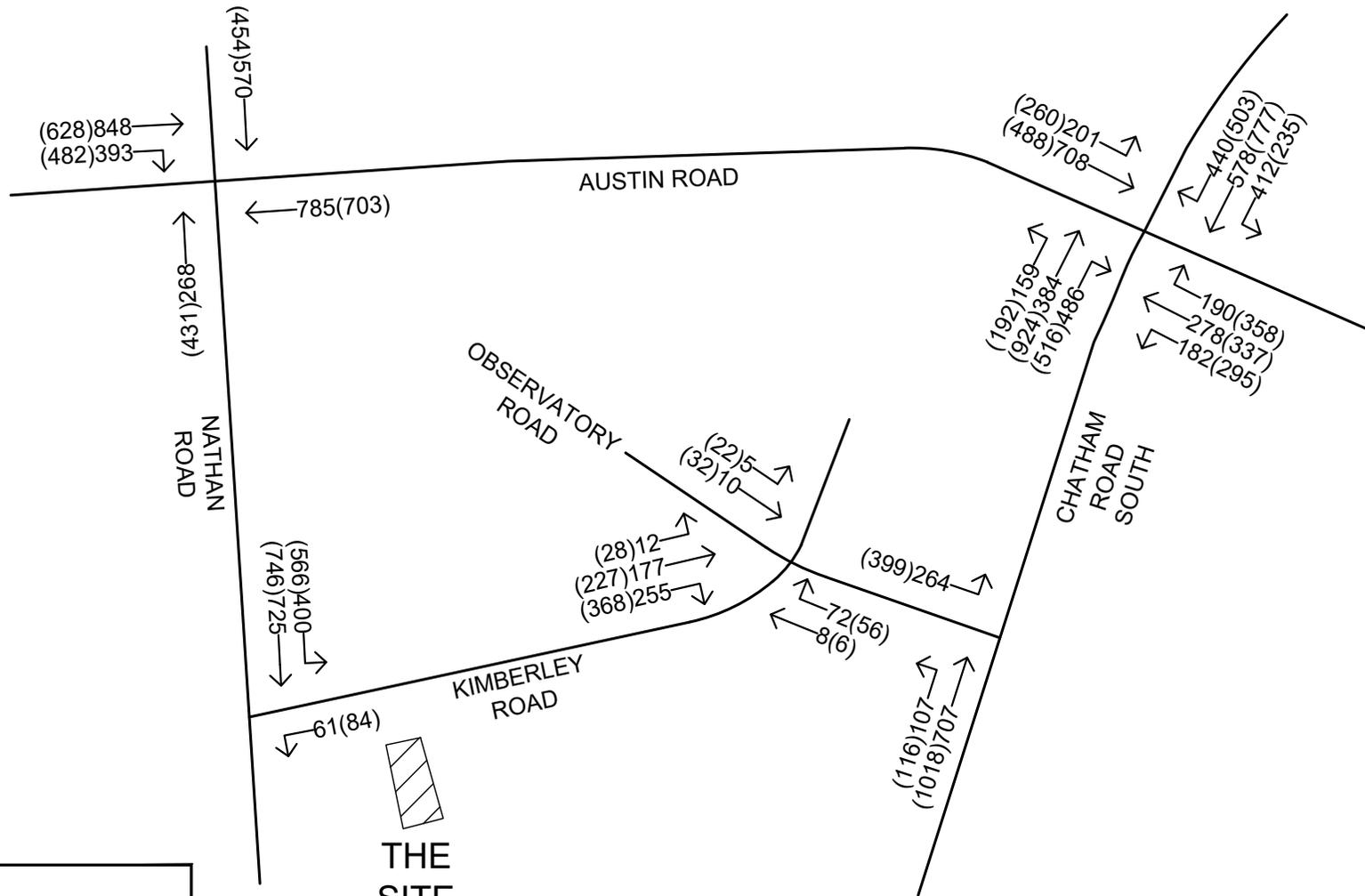
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| DESIGNED SKL                             | DATE SEP 2025 | DRAWING TITLE DEVELOPMENT TRAFFIC FLOW   |  |                        |        |
| DRAWN CLL                                | SCALE N.T.S.  |  |  |                        |        |
| CHECKED SLN                              |               |  |  |                        |        |
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**LEGEND:**  
 123 (456) ← PM PEAK HOUR TRAFFIC FLOW  
 ↑ AM PEAK HOUR TRAFFIC FLOW

**NOTE:**  
 1. ALL TRAFFIC FLOWS ARE IN PCU/HOUR  
 2. MINOR ROADS ARE NOT SHOWN FOR CLARITY

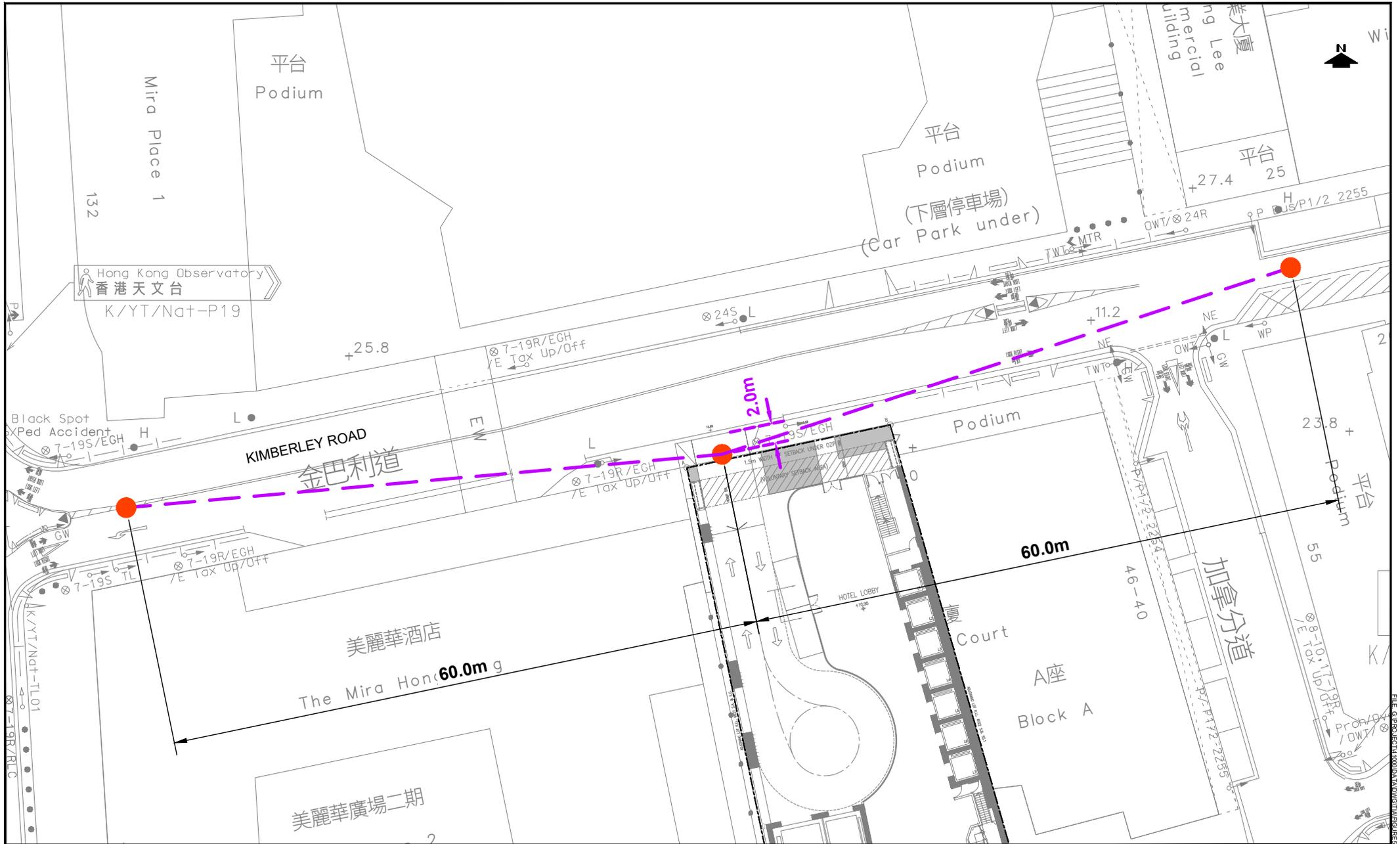
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| PROJECT NO. 41000 |               | PROJECT TITLE SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B R.P. |  | DRAWING NO. FIGURE 4.2        |  | REV. . |  |
| DESIGNED SKL      | DATE SEP 2025 | DRAWING TITLE 2033 REFERENCE TRAFFIC FLOW  |  |                               |  |        |  |
| DRAWN CLL         | SCALE N.T.S.  |  |  |                               |  |        |  |
| CHECKED SLN       |               |  |  |                               |  |        |  |
|                   |               |  |  | 顧問有限公司<br>Consultancy Limited |  |        |  |



**LEGEND:**  
 123 (456) ← PM PEAK HOUR TRAFFIC FLOW  
 ↑ AM PEAK HOUR TRAFFIC FLOW

**NOTE:**  
 1. ALL TRAFFIC FLOWS ARE IN PCU/HOUR  
 2. MINOR ROADS ARE NOT SHOWN FOR CLARITY

|                   |               |  |  |                        |  |  |
|-------------------|---------------|--|--|------------------------|--|--|
| PROJECT NO. 41000 |               | PROJECT TITLE SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B R.P. |  | DRAWING NO. FIGURE 4.3 |  | REV. .   |
| DESIGNED SKL      | DATE SEP 2025 | DRAWING TITLE  |  |                        |  | <br>顧問有限公司<br>Consultancy Limited |
| DRAWN CLL         | SCALE N.T.S.  | <b>2033 DESIGN TRAFFIC FLOW</b>  |  |                        |  |  |
| CHECKED SLN       |               |  |  |                        |  |  |



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| PROJECT NO. | 41000    |
| DESIGNED    | SKL      |
| DRAWN       | CLL      |
| CHECKED     | SLN      |
| DATE        | JUL 2025 |
| SCALE       | 1:500    |

PROJECT TITLE SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, K.I.L. 6022 S.B R.P.

|               |   |
|---------------|---|
| DRAWING TITLE | SIGHTLINE ANALYSIS OF PROPOSED VEHICULAR ACCESS |
| DRAWING NO.   | FIGURE 5.1                                      |
| REV.          | B   |

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**Appendix A**  
**Junction Calculation Sheets**  
**- Existing Scenario**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J1 Nathan Road / Kimberley Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

Sep-25

SKL

PREPARED BY:

PROJECT NO.: 41000

Sep-25

SLN

CHECKED BY:

FILENAME: J1\_NR\_KR.xls

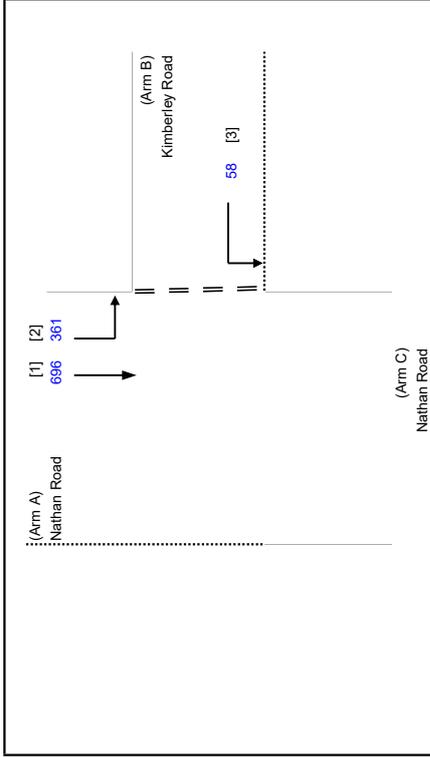
Sep-25

SLN

REVIEWED BY:

REFERENCE NO.:

## 2025 Existing AM



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |                   |
|---------------------------|-------------------|
| <b>MAJOR ROAD (ARM A)</b> |                   |
| W = 6.8 (metres)          | D = 0.53322       |
| W cr = 0 (metres)         | E = 1.02732       |
| q a-b = 361 (pcu/hr)      | F = 0.56595       |
| q a-c = 696 (pcu/hr)      | Y = 0.76540       |
| <b>MAJOR ROAD (ARM C)</b> |                   |
| W c-b = 0.00 (metres)     | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)      |                   |
| q c-a = 0 (pcu/hr)        |                   |
| q c-b = 0 (pcu/hr)        |                   |
| <b>MINOR ROAD (ARM B)</b> |                   |
| W b-a = 0.00 (metres)     |                   |
| W b-c = 4.80 (metres)     |                   |
| V l b-a = 0 (metres)      |                   |
| V r b-a = 0 (metres)      |                   |
| V r b-c = 39 (metres)     |                   |
| q b-a = 0 (pcu/hr)        |                   |
| q b-c = 58 (pcu/hr)       |                   |

### GEOMETRIC FACTORS :

|             |              |                            |
|-------------|--------------|----------------------------|
| D = 0.53322 | Q b-a = 210  | TOTAL FLOW = 1115 (PCU/HR) |
| E = 1.02732 | Q b-c = 525  |                            |
| F = 0.56595 | Q c-b = 264  |                            |
| Y = 0.76540 | Q b-ac = 525 |                            |

### THE CAPACITY OF MOVEMENT :

|              |                   |
|--------------|-------------------|
| Q b-a = 210  | DFC b-a = 0.0000  |
| Q b-c = 525  | DFC b-c = 0.1105  |
| Q c-b = 264  | DFC c-b = 0.0000  |
| Q b-ac = 525 | DFC b-ac = 0.1105 |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

**CRITICAL DFC = 0.11**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J1 Nathan Road / Kimberley Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

PREPARED BY: SKL

Sep-25

CHECKED BY: SLN

Sep-25

REVIEWED BY: SLN

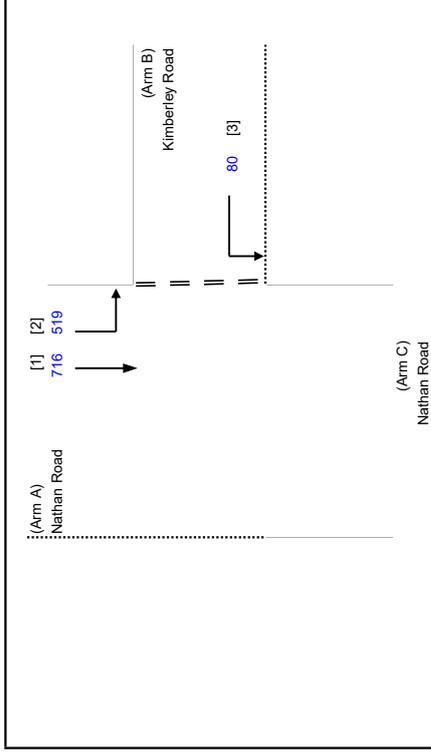
Sep-25

PROJECT NO.: 41000

FILENAME: J1\_NR\_KR.xls

REFERENCE NO.:

## 2025 Existing PM



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
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- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |                   |
|---------------------------|-------------------|
| <b>MAJOR ROAD (ARM A)</b> |                   |
| W = 6.8 (metres)          | D = 0.53322       |
| W cr = 0 (metres)         | E = 1.02732       |
| q a-b = 519 (pcu/hr)      | F = 0.56595       |
| q a-c = 716 (pcu/hr)      | Y = 0.76540       |
| <b>MAJOR ROAD (ARM C)</b> |                   |
| W c-b = 0.00 (metres)     | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)      |                   |
| q c-a = 0 (pcu/hr)        |                   |
| q c-b = 0 (pcu/hr)        |                   |
| <b>MINOR ROAD (ARM B)</b> |                   |
| W b-a = 0.00 (metres)     |                   |
| W b-c = 4.80 (metres)     |                   |
| V l b-a = 0 (metres)      |                   |
| V r b-a = 0 (metres)      |                   |
| V r b-c = 39 (metres)     |                   |
| q b-a = 0 (pcu/hr)        |                   |
| q b-c = 80 (pcu/hr)       |                   |

### GEOMETRIC FACTORS :

|                   |                            |
|-------------------|----------------------------|
| D = 0.53322       | Q b-a = 197                |
| E = 1.02732       | Q b-c = 502                |
| F = 0.56595       | Q c-b = 235                |
| Y = 0.76540       | Q b-ac = 502               |
| F for (Qb-ac) = 1 | TOTAL FLOW = 1315 (PCU/HR) |

### THE CAPACITY OF MOVEMENT :

|              |                   |
|--------------|-------------------|
| Q b-a = 197  | DFC b-a = 0.0000  |
| Q b-c = 502  | DFC b-c = 0.1594  |
| Q c-b = 235  | DFC c-b = 0.0000  |
| Q b-ac = 502 | DFC b-ac = 0.1594 |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

**CRITICAL DFC = 0.16**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J2 Nathan Road / Austin Road

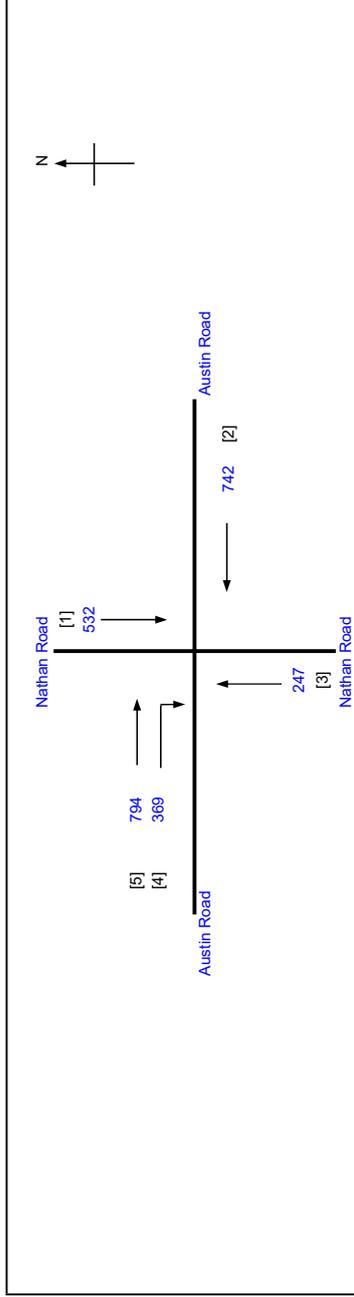
# TRAFFIC SIGNAL CALCULATION

2025 Existing AM

PROJECT NO.: 41000  
 FILENAME: J2\_AR\_NR.xlsx

Prepared By:  
 Checked By:  
 Reviewed By:

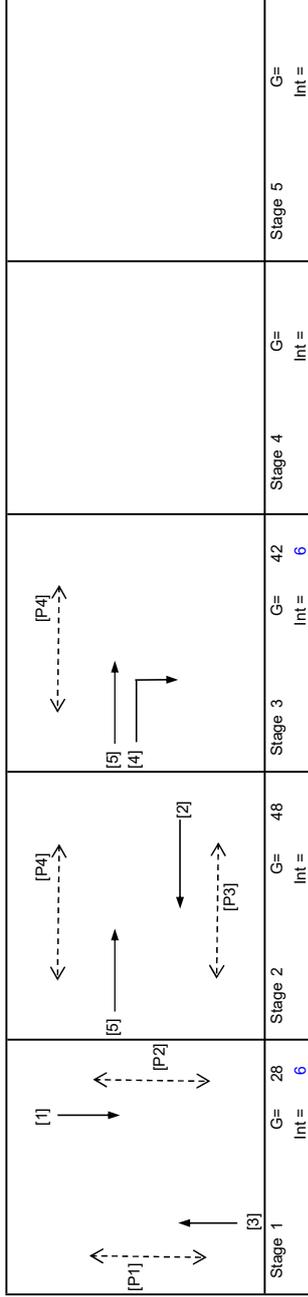
INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle N = 3

Cycle time C = 130 sec  
 Sum(y) Y = 0.539  
 Loss time L = 10 sec  
 Total Flow = 2684 pcu  
 Co = (1.5\*L+5)/(1-Y) = 43.4 sec  
 Cm = L/(1-Y) = 21.7 sec  
 Yult = 0.825  
 R.C.ult = (Yult-Y)\*100% = 53.1 %  
 Cp = 0.9\*L/(0.9-Y) = 24.9 sec  
 Ymax = 1-L/C = 0.923

**R.C.(C) = (0.9\*Ymax-Y)\*100% = 54 %**



| Pedestrian Phase | Stage | Green Time SG | Green Time FG | Delay | Green Time Provided SG | Green Time Provided FG |
|------------------|-------|---------------|---------------|-------|------------------------|------------------------|
| P1               | 1     | 8             | 7             | 3     | 24                     | 7                      |
| P2               | 1     | 5             | 10            | 7     | 17                     | 10                     |
| P3               | 2     | 8             | 7             | 6     | 35                     | 7                      |
| P4               | 2,3   | 8             | 7             | 7     | 82                     | 7                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.50          | 2           |           |   | N | 4070                     | 532                 | 247                     |                      | 532              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.131 | 0.131     | 10    | 29               | 29            | 0.584                  | 42                      | 43                      |
| 3         | 1     | 3.50          | 2           |           |   | N | 4070                     | 247                 |                         |                      | 247              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.061 | 0.061     |       | 14               | 29            | 0.584                  | 21                      | 55                      |
| 2         | 2     | 3.00          | 2           |           |   | N | 3970                     | 742                 | 742                     |                      | 742              | 0.00                           | 3970            |               |                     |             |                    |            |                        | 3970                    | 0.187 | 0.187     |       | 42               | 48            | 0.584                  | 54                      | 35                      |
| 5         | 2,3   | 3.30          | 1           | 15        |   | N | 1945                     | 794                 | 794                     |                      | 794              | 0.00                           | 1945            |               |                     |             |                    |            |                        | 1945                    | 0.408 | 0.408     |       | 91               | 91            | 0.584                  | 48                      | 11                      |
| 4         | 3     | 3.30          | 1           | 15        |   | N | 2085                     | 369                 | 369                     |                      | 369              | 1.00                           | 1895            |               |                     |             |                    |            |                        | 1895                    | 0.195 | 0.195     |       | 43               | 43            | 0.584                  | 48                      | 36                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J2 Nathan Road / Austin Road

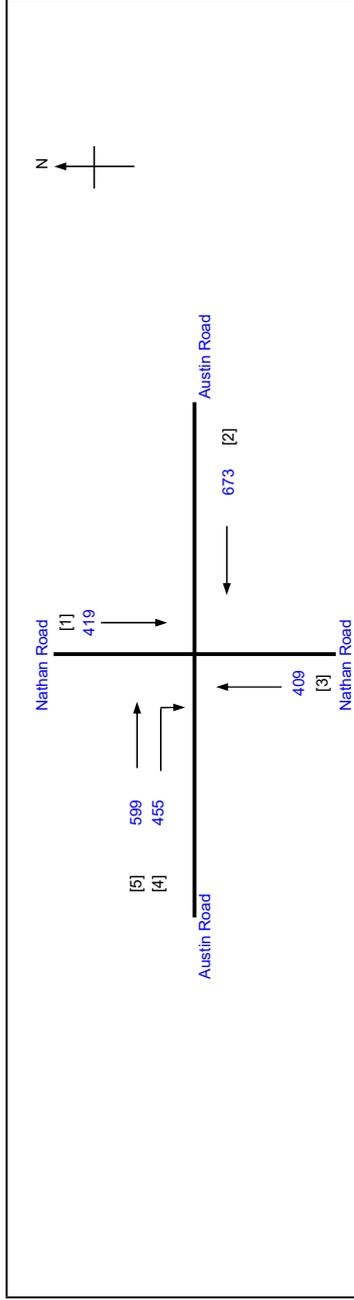
# TRAFFIC SIGNAL CALCULATION

2025 Existing PM

PROJECT NO.: 41000  
 FILENAME: J2\_AR\_NR.xlsx

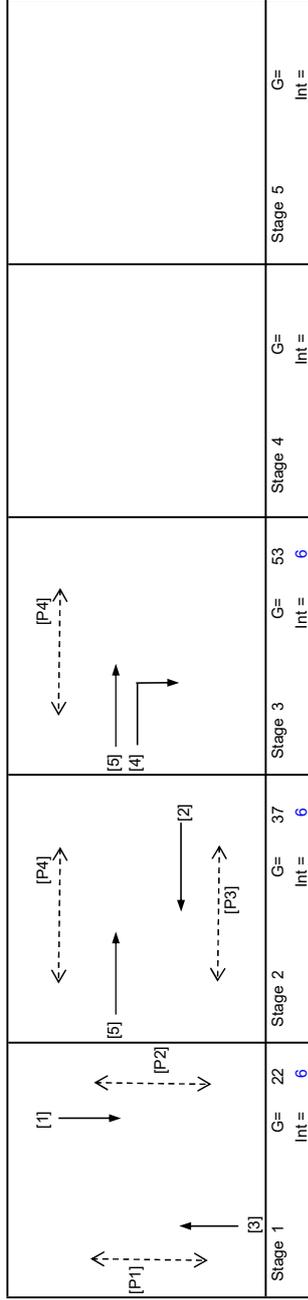
Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle N = 3  
 Cycle time C = 130 sec  
 Sum(y) Y = 0.513  
 Loss time L = 15 sec  
 Total Flow = 2555 pcu  
 Co = (1.5\*L+5)/(1-Y) = 56.4 sec  
 Cm = L/(1-Y) = 30.8 sec  
 Yult = 0.788  
 R.C.ult = (Yult-Y)\*100% = 53.7 %  
 Cp = 0.9\*L/(0.9-Y) = 34.8 sec  
 Ymax = 1-L/C = 0.885

**R.C.(C) = (0.9\*Ymax-Y)\*100% = 55 %**



| Pedestrian Phase | Stage | Green Time SG | Green Time FG | Delay | Green Time Provided SG | Green Time Provided FG |
|------------------|-------|---------------|---------------|-------|------------------------|------------------------|
| P1               | 1     | 8             | 7             | 3     | 18                     | 7                      |
| P2               | 1     | 5             | 10            | 7     | 11                     | 10                     |
| P3               | 2     | 8             | 7             | 6     | 30                     | 7                      |
| P4               | 2,3   | 8             | 7             | 7     | 88                     | 7                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.50          | 2           |           |   | N | 4070                     | 419                 | 419                     | 419                  | 419              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.103 | 0.103     | 15    | 23               | 23            | 0.579                  | 36                      | 47                      |
| 3         | 1     | 3.50          | 2           |           |   | N | 4070                     | 409                 | 409                     | 409                  | 409              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.100 | 0.100     |       | 23               | 23            | 0.579                  | 36                      | 48                      |
| 2         | 2     | 3.00          | 2           |           |   | N | 3970                     | 673                 | 673                     | 673                  | 673              | 0.00                           | 3970            |               |                     |             |                    |            |                        | 3970                    | 0.170 | 0.170     |       | 38               | 38            | 0.579                  | 51                      | 37                      |
| 5         | 2,3   | 3.30          | 1           | 15        |   | N | 1945                     | 599                 | 599                     | 599                  | 599              | 0.00                           | 1945            |               |                     |             |                    |            |                        | 1945                    | 0.308 | 0.308     |       | 69               | 92            | 0.579                  | 60                      | 21                      |
| 4         | 3     | 3.30          | 1           | 15        |   | N | 2085                     | 455                 | 455                     | 455                  | 455              | 1.00                           | 1895            |               |                     |             |                    |            |                        | 1895                    | 0.240 | 0.240     |       | 54               | 54            | 0.579                  | 54                      | 29                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

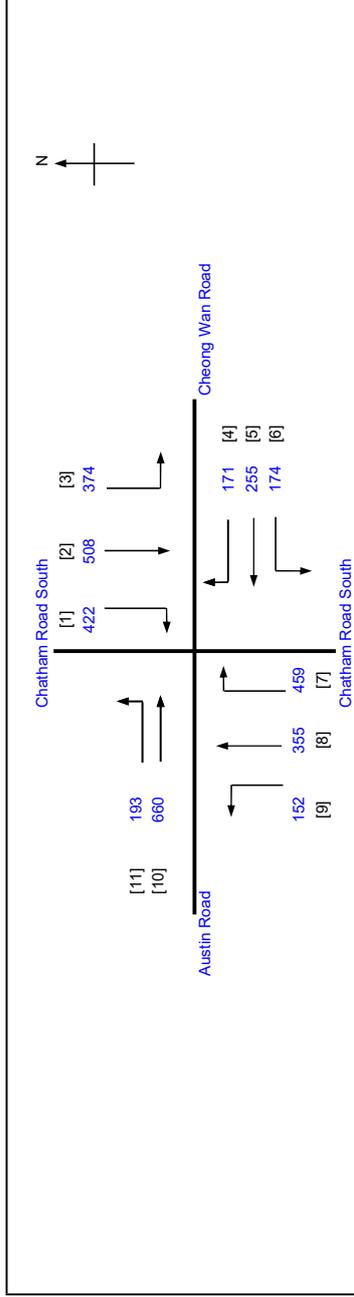
Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J3 Chatham Road South / Austin Road / Cheong Wan Road

# TRAFFIC SIGNAL CALCULATION

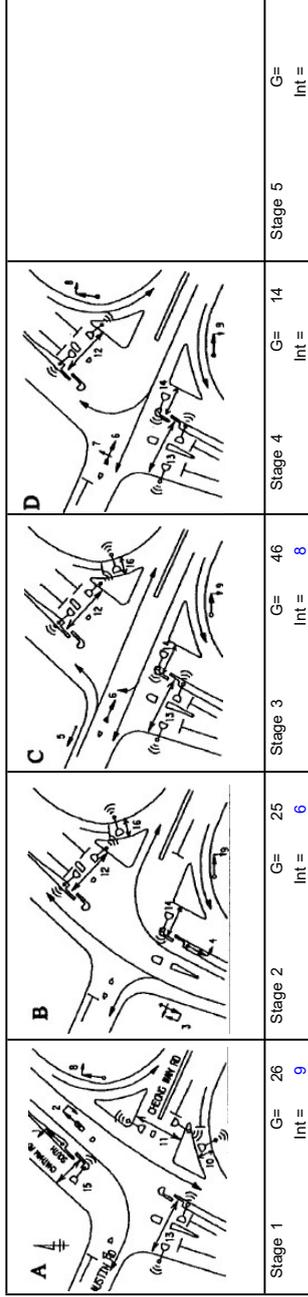
2025 Existing AM

PROJECT NO.: 41000  
 FILENAME: J3\_CRS\_AR\_CWR.xlsx  
 Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



|                         |                                  |
|-------------------------|----------------------------------|
| No. of stages per cycle | N = 4                            |
| Cycle time              | C = 130 sec                      |
| Sum(y)                  | Y = 0.447                        |
| Loss time               | L = 34 sec                       |
| Total Flow              | = 3723 pcu                       |
| Co                      | = (1.5*L+5)/(1-Y)                |
| Cm                      | = L/(1-Y)                        |
| Yult                    | =                                |
| R.C.ult                 | = (Yult-Y)*100%                  |
| Cp                      | = 0.9*L/(0.9-Y)                  |
| Ymax                    | = 1-L/C                          |
| <b>R.C.(C)</b>          | <b>= 0.9*Ymax-Y)*100% = 49 %</b> |



| Stage   | Green Time Required SG | Green Time Provided SG |
|---------|------------------------|------------------------|
| Stage 1 | 5                      | 7                      |
| Stage 2 | 11                     | 10                     |
| Stage 3 | 10                     | 9                      |
| Stage 4 | 12                     | 10                     |
| Stage 5 | 5                      | 10                     |
| Stage 6 | 5                      | 10                     |
| Stage 7 | 5                      | 6                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.00          | 2           | 25        |   |   | 4110                     |                     | 422                     | 422                  | 422              | 1.00                           | 3877            |               |                     |             |                    |            | 3877                   | 0.109                   | 0.109 | 20        | 23    | 27               | 0.806         | 36                     | 48                      |                         |
| 2         | 1     | 3.00          | 2           | 25        |   |   | 4110                     |                     | 508                     | 508                  | 508              | 0.00                           | 4110            |               |                     |             |                    |            | 4110                   | 0.124                   | 0.124 |           | 27    | 27               | 0.806         | 42                     | 45                      |                         |
| 3         | 1,4   | 3.00          | 1           | 20        |   | N | 1915                     | 374                 | 374                     | 374                  | 1.00             | 1.00                           | 1781            |               |                     |             |                    |            | 1781                   | 0.210                   | 0.210 |           | 45    | 45               | 0.806         | 48                     | 36                      |                         |
| 8,9       | 2     | 3.00          | 1           | 10        |   | N | 1915                     | 152                 | 0                       | 152                  | 152              | 1.00                           | 1665            |               |                     |             |                    |            | 1665                   | 0.091                   | 0.091 |           | 20    | 26               | 0.806         | 24                     | 56                      |                         |
| 8         | 2     | 3.00          | 2           | 25        | O |   | 4110                     | 355                 | 355                     | 355                  | 0.00             | 0.00                           | 4110            | 36            | 1080                |             |                    |            | 4110                   | 0.086                   | 0.086 |           | 19    | 26               | 0.806         | 30                     | 51                      |                         |
| 7         | 2     | 3.00          | 2           | 20        | O |   | 4110                     | 459                 | 459                     | 459                  | 1.00             | 1.00                           | 3823            |               |                     |             |                    |            | 3823                   | 0.120                   | 0.120 |           | 26    | 26               | 0.806         | 39                     | 46                      |                         |
| 6         | 2,3,4 | 3.00          | 1           | 25        |   | N | 1915                     | 174                 | 174                     | 174                  | 1.00             | 1.00                           | 1807            |               |                     |             |                    |            | 1807                   | 0.096                   | 0.096 |           | 21    | 21               | 0.806         | 30                     | 54                      |                         |
| 4,5       | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | 255                 | 255                     | 264                  | 0.03             | 0.03                           | 1821            |               |                     |             |                    |            | 2901                   | 0.091                   | 0.091 |           | 20    | 20               | 0.806         | 48                     | 52                      |                         |
| 4         | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | 162                 | 162                     | 162                  | 1.00             | 1.00                           | 1722            |               |                     |             |                    |            | 1722                   | 0.094                   | 0.094 |           | 20    | 20               | 0.806         | 24                     | 55                      |                         |
| 10,11     | 3     | 3.00          | 1           | 20        |   | N | 1915                     | 193                 | 211                     | 404                  | 0.48             | 0.48                           | 1849            |               |                     |             |                    |            | 1849                   | 0.219                   | 0.219 | 14        | 47    | 47               | 0.806         | 54                     | 34                      |                         |
| 10        | 3     | 3.00          | 1           | 20        |   |   | 2055                     | 449                 | 449                     | 449                  | 0.00             | 0.00                           | 2055            |               |                     |             |                    |            | 2055                   | 0.218                   | 0.218 |           | 47    | 47               | 0.806         | 60                     | 34                      |                         |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUEING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

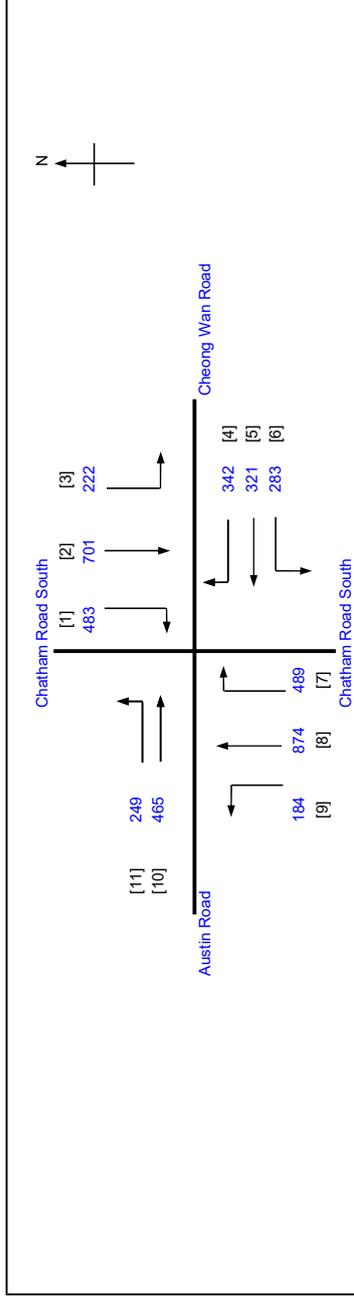
J3 Chatham Road South / Austin Road / Cheong Wan Road

# TRAFFIC SIGNAL CALCULATION

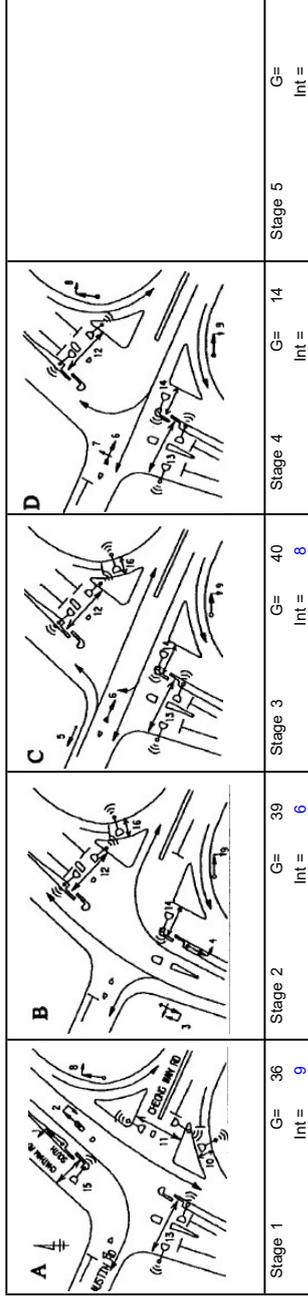
2025 Existing PM

PROJECT NO.: 41000  
 FILENAME: J3\_CRS\_AR\_CWR.xlsx  
 Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



|                         |                                  |
|-------------------------|----------------------------------|
| No. of stages per cycle | N = 4                            |
| Cycle time              | C = 130 sec                      |
| Sum(y)                  | Y = 0.437                        |
| Loss time               | L = 34 sec                       |
| Total Flow              | = 4613 pcu                       |
| Co                      | = (1.5*L+5)/(1-Y)                |
| Cm                      | = L/(1-Y)                        |
| Yult                    | =                                |
| R.C.ult                 | = (Yult-Y)*100%                  |
| Cp                      | = 0.9*L/(0.9-Y)                  |
| Ymax                    | = 1-L/C                          |
| <b>R.C.(C)</b>          | <b>= 0.9*Ymax-Y)*100% = 52 %</b> |



| Stage | Stage | Green Time Required SG | Green Time Provided SG |
|-------|-------|------------------------|------------------------|
| 1     | 1     | 5                      | 7                      |
| 2     | 1     | 11                     | 10                     |
| 3     | 2,3,4 | 10                     | 9                      |
| 4     | 1,3,4 | 12                     | 10                     |
| 5     | 2,3,4 | 5                      | 10                     |
| 6     | 1     | 5                      | 10                     |
| 7     | 2,3   | 5                      | 6                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Movement  | Total Flow | Proportion of Turning Vehicles | Sat. Flow | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/hr | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|-----------|------------|--------------------------------|-----------|---------------|---------------------|-------------|--------------------|------------|------------------------|--------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.00          | 2           | 25        |   |   | 4110                     | Left 222  | 483        | 1.00                           | 3877      |               |                     |             |                    |            |                        | 3877                     | 0.125 | 0.125     | 20    | 27               | 37            | 0.592                  | 39                      | 45                      |
| 2         | 1     | 3.00          | 2           | 25        |   |   | 4110                     | Right 701 | 701        | 0.00                           | 4110      |               |                     |             |                    |            |                        | 4110                     | 0.171 | 0.171     |       | 37               | 37            | 0.592                  | 54                      | 38                      |
| 3         | 1,4   | 3.00          | 1           | 20        |   |   | 1915                     | Left 222  | 222        | 1.00                           | 1781      |               |                     |             |                    |            |                        | 1781                     | 0.125 | 0.125     |       | 27               | 27            | 0.592                  | 36                      | 48                      |
| 8,9       | 2     | 3.00          | 1           | 10        |   | N | 1915                     | Left 184  | 317        | 0.58                           | 1762      |               |                     |             |                    |            |                        | 1762                     | 0.180 | 0.180     |       | 40               | 40            | 0.592                  | 42                      | 39                      |
| 8         | 2     | 3.00          | 2           | 25        | O |   | 4110                     | Right 741 | 741        | 0.00                           | 4110      |               |                     |             |                    |            |                        | 4110                     | 0.180 | 0.180     |       | 40               | 40            | 0.592                  | 54                      | 36                      |
| 7         | 2     | 3.00          | 2           | 20        |   |   | 4110                     | Left 489  | 489        | 1.00                           | 3823      |               |                     |             |                    |            |                        | 3823                     | 0.128 | 0.128     |       | 28               | 40            | 0.592                  | 39                      | 44                      |
| 6         | 2,3,4 | 3.00          | 1           | 25        |   | N | 1915                     | Left 283  | 283        | 1.00                           | 1807      |               |                     |             |                    |            |                        | 1807                     | 0.157 | 0.157     |       | 34               | 34            | 0.592                  | 42                      | 42                      |
| 4,5       | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | Right 66  | 387        | 0.17                           | 1807      | 36            | 617                 |             |                    |            |                        | 2424                     | 0.160 | 0.160     |       | 35               | 35            | 0.592                  | 60                      | 41                      |
| 4         | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | Left 276  | 276        | 1.00                           | 1722      |               |                     |             |                    |            |                        | 1722                     | 0.160 | 0.160     |       | 35               | 35            | 0.592                  | 42                      | 42                      |
| 10,11     | 3     | 3.00          | 1           | 20        |   | N | 1915                     | Left 86   | 335        | 0.74                           | 1814      |               |                     |             |                    |            |                        | 1814                     | 0.185 | 0.185     |       | 41               | 41            | 0.592                  | 48                      | 38                      |
| 10        | 3     | 3.00          | 1           | 20        |   |   | 2055                     | Right 379 | 379        | 0.00                           | 2055      |               |                     |             |                    |            |                        | 2055                     | 0.184 | 0.184     | 14    | 41               | 41            | 0.592                  | 54                      | 38                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J4 Chatham Road South / Observatory Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

SKL

Sep-25

SLN

Sep-25

SLN

Sep-25

PROJECT NO.: 41000

PREPARED BY:

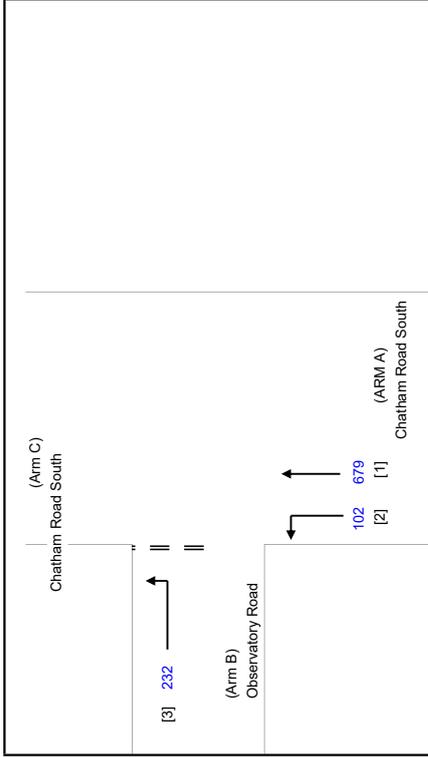
FILENAME: J4\_CRS\_OR

CHECKED BY:

REFERENCE NO.:

REVIEWED BY:

## 2025 Existing AM



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH

W cr = CENTRAL RESERVE WIDTH

W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a

W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c

W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b

V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a

V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a

V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c

V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c

V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b

V r c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b

D = STREAM-SPECIFIC B-A

E = STREAM-SPECIFIC B-C

F = STREAM-SPECIFIC C-B

Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                       |                   |
|-----------------------|-------------------|
| MAJOR ROAD (ARM A)    |                   |
| W = 10.50 (metres)    | D = 0.53322       |
| W cr = 0 (metres)     | E = 1.01663       |
| q a-b = 102 (pcu/hr)  | F = 0.56595       |
| q a-c = 679 (pcu/hr)  | Y = 0.63775       |
| MAJOR ROAD (ARM C)    |                   |
| W c-b = 0.00 (metres) | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)  |                   |
| q c-a = 0 (pcu/hr)    |                   |
| q c-b = 0 (pcu/hr)    |                   |
| MINOR ROAD (ARM B)    |                   |
| W b-a = 0.00 (metres) |                   |
| W b-c = 4.70 (metres) |                   |
| V l b-a = 0 (metres)  |                   |
| V r b-a = 0 (metres)  |                   |
| V r b-c = 37 (metres) |                   |
| q b-a = 0 (pcu/hr)    |                   |
| q b-c = 232 (pcu/hr)  |                   |

### GEOMETRIC FACTORS :

|                            |                 |
|----------------------------|-----------------|
| Q b-a = 245                | Q b-c (O) = 588 |
| Q b-c = 588                | Q c-b = 330     |
| Q c-b = 330                | Q b-ac = 588    |
| TOTAL FLOW = 1013 (PCU/HR) |                 |

### THE CAPACITY OF MOVEMENT :

|                  |                  |                  |                               |
|------------------|------------------|------------------|-------------------------------|
| DFC b-a = 0.0000 | DFC b-c = 0.3946 | DFC c-b = 0.0000 | DFC b-c (share lane) = 0.3946 |
|------------------|------------------|------------------|-------------------------------|

### COMPARISON OF DESIGN FLOW TO CAPACITY:

**CRITICAL DFC = 0.39**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J4 Chatham Road South / Observatory Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

Sep-25

SKL

PREPARED BY:

Sep-25

SLN

CHECKED BY:

Sep-25

SLN

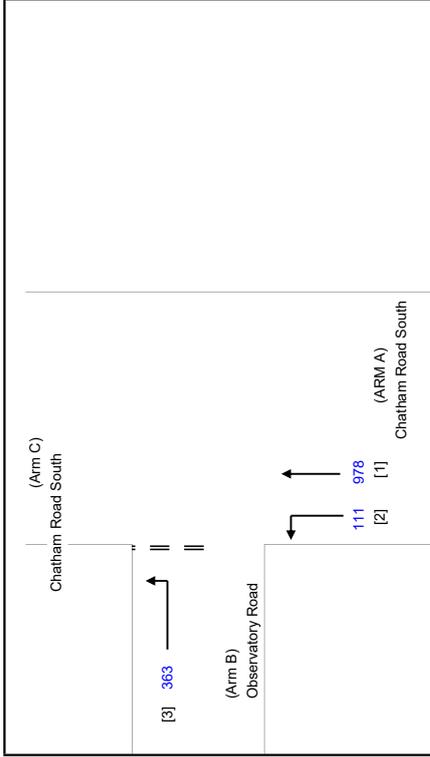
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**2025 Existing PM**

PROJECT NO.: 41000

FILENAME: J4\_CRS\_OR

REFERENCE NO.:



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH

W cr = CENTRAL RESERVE WIDTH

W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a

W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c

W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b

Vr b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a

Vr b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a

Vr b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c

Vr b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c

Vr c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b

Vr c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b

D = STREAM-SPECIFIC B-A

E = STREAM-SPECIFIC B-C

F = STREAM-SPECIFIC C-B

Y = (1-0.0345W)

## GEOMETRIC DETAILS:

### MAJOR ROAD (ARM A)

W = 10.50 (metres)

W cr = 0 (metres)

q a-b = 111 (pcu/hr)

q a-c = 978 (pcu/hr)

### MAJOR ROAD (ARM C)

W c-b = 0.00 (metres)

Vr c-b = 0 (metres)

q c-a = 0 (pcu/hr)

q c-b = 0 (pcu/hr)

### MINOR ROAD (ARM B)

W b-a = 0.00 (metres)

W b-c = 4.70 (metres)

Vr b-a = 0 (metres)

Vr b-a = 0 (metres)

Vr b-c = 37 (metres)

q b-a = 0 (pcu/hr)

q b-c = 363 (pcu/hr)

## GEOMETRIC FACTORS :

D = 0.53322

E = 1.01663

F = 0.58595

Y = 0.63775

F for (Qb-ac) = 1

## THE CAPACITY OF MOVEMENT :

Q b-a = 208

Q b-c = 516

Q c-b = 288

Q b-ac = 516

TOTAL FLOW = 1452 (PCU/HR)

## COMPARISON OF DESIGN FLOW TO CAPACITY:

DFC b-a = 0.0000

DFC b-c = 0.7035

DFC c-b = 0.0000

DFC b-c (share lane) = 0.7035

**CRITICAL DFC = 0.70**



# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J5 Kimberley Road / Observatory Road

# PRIORITY JUNCTION CALCULATION

**2025 Existing PM**

PROJECT NO.: 41000

FILENAME: J5\_KR\_OR.xls

REFERENCE NO.:

INITIALS

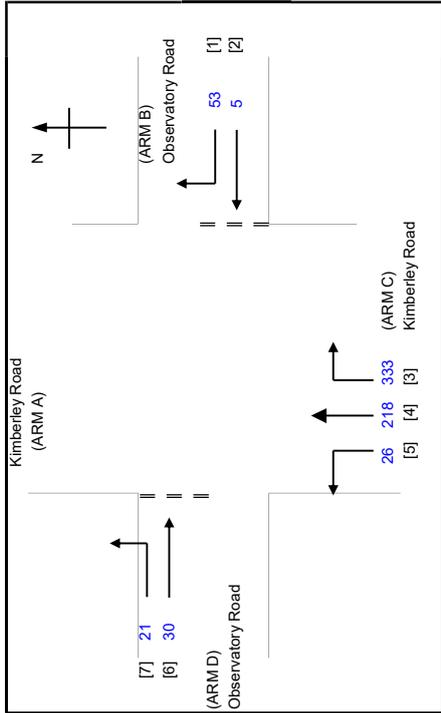
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DATE

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Sep-25



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH  
 W cr = CENTRAL RESERVE WIDTH  
 W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a  
 W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c  
 W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b  
 V b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a  
 V r-b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a  
 V r-b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
 V r-c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b  
 X a = STREAM-SPECIFIC (RIGHT TURN FROM A)  
 X b = STREAM-SPECIFIC (RIGHT TURN FROM B)  
 Z b = STREAM-SPECIFIC (LEFT TURN FROM B)  
 M b = STREAM-SPECIFIC (STRAIGHT AHEAD FROM B - LEFT LANE)  
 Y = (1-0.0345W)  
 r b-a = RATIO OF FLOW TO CAPACITY IN STREAM b-a

## GEOMETRIC DETAILS:

|                    |                 |                       |
|--------------------|-----------------|-----------------------|
| GENERAL            |                 | Y = 0.745             |
| W                  | = 7.4 (metres)  |                       |
| W cr               | = 0 (metres)    |                       |
| MAJOR ROAD (ARM A) |                 |                       |
| W a-d              | = 0.00 (metres) | MAJOR ROAD (ARM C)    |
| V r-a-d            | = 0 (metres)    | W c-b = 3.10 (metres) |
| q a-b              | = 0 (pcu/hr)    | V r-c-b = 22 (metres) |
| q a-c              | = 0 (pcu/hr)    | q c-a = 218 (pcu/hr)  |
| q a-d              | = 0 (pcu/hr)    | q c-b = 333 (pcu/hr)  |
|                    |                 | q c-d = 26 (pcu/hr)   |
| MINOR ROAD (ARM B) |                 |                       |
| W b-a              | = 5.00 (metres) | MINOR ROAD (ARM D)    |
| W b-c              | = 0.00 (metres) | W d-c = 0.00 (metres) |
| V l-b-a            | = 23 (metres)   | W d-a = 3.00 (metres) |
| V r-b-a            | = 100 (metres)  | V l-d-c = 0 (metres)  |
| q b-a              | = 53 (pcu/hr)   | V r-d-a = 0 (metres)  |
| q b-c              | = 0 (pcu/hr)    | q d-c = 0 (pcu/hr)    |
| q b-d              | = 5 (pcu/hr)    | q d-a = 21 (pcu/hr)   |
|                    |                 | q d-b = 30 (pcu/hr)   |

## GEOMETRIC FACTORS :

|  |                   |              |                |
|--|-------------------|--------------|----------------|
| X b  | = 1.022           | X a          | = 0.586        |
| X c  | = 0.865           | X d          | = 0.533        |
| Z b  | = 0.586           | Z d          | = 0.857        |
| M b  | = 0.541           | M d          | = 0.780        |
| PROPORTION OF MINOR STRAIGHT AHEAD TRAFFIC : |                   |              |                |
| r b-a  | = 0.2129          | r d-c        | = 0.000        |
| q l b-d                                      | = 3.0321 (pcu/hr) | q l d-b      | = 15 (pcu/hr)  |
| q r b-d                                      | = 1.9679 (pcu/hr) | q r d-b      | = 15 (pcu/hr)  |
| CAPACITY OF MOVEMENT :                       |                   |              |                |
| Q b-a  | = 457 (pcu/hr)    | Q d-c        | = 249 (pcu/hr) |
| Q b-c  | = 413 (pcu/hr)    | Q d-a        | = 585 (pcu/hr) |
| Q c-b  | = 644 (pcu/hr)    | Q a-d        | = 322 (pcu/hr) |
| Q l b-d                                      | = 247 (pcu/hr)    | Q l d-b      | = 370 (pcu/hr) |
| Q r b-d                                      | = 467 (pcu/hr)    | Q r d-b      | = 253 (pcu/hr) |
| Q b-acd                                      | = 457 (pcu/hr)    | Q d-abc      | = 326 (pcu/hr) |
| TOTAL FLOW =                                 |                   | 686 (PCU/HR) |                |

## COMPARISON OF DESIGN FLOW TO CAPACITY:

|                         |          |
|-------------------------|----------|
| DFC b-a                 | = 0.1160 |
| DFC b-c                 | = 0.0000 |
| DFC c-b                 | = 0.5171 |
| DFCI b-d                | = 0.0123 |
| DFCr b-d                | = 0.0042 |
| DFC d-c                 | = 0.0000 |
| DFC d-a                 | = 0.0359 |
| DFC a-d                 | = 0.0000 |
| DFCI d-b                | = 0.0405 |
| DFCr d-b                | = 0.0593 |
| DFC b-acd (shared lane) | = 0.1269 |
| DFC d-abc (shared lane) | = 0.1564 |

**CRITICAL DFC = 0.52**

**Appendix B**  
**Junction Calculation Sheets**  
**- Reference & Design Scenarios**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J1 Nathan Road / Kimberley Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

Sep-25

SKL

PREPARED BY:

Sep-25

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Sep-25

SLN

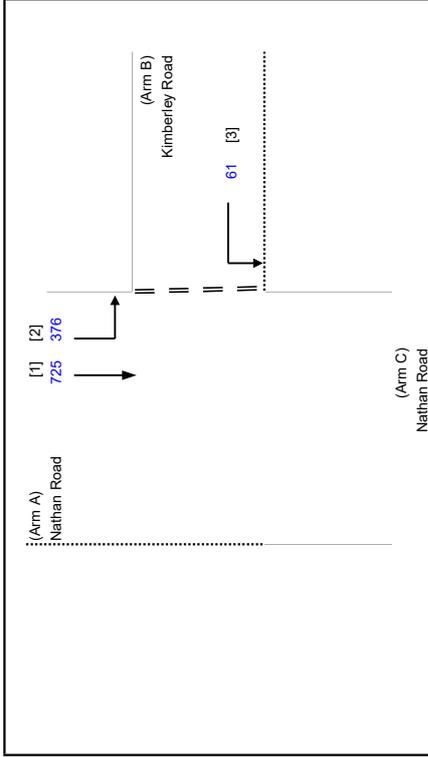
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FILENAME: J1\_NR\_KR.xls

REFERENCE NO.:

## 2033 Reference AM



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |  |
|---------------------------|--|
| <b>MAJOR ROAD (ARM A)</b> |  |
| W = 6.8 (metres)          |  |
| W cr = 0 (metres)         |  |
| q a-b = 376 (pcu/hr)      |  |
| q a-c = 725 (pcu/hr)      |  |
| <b>MAJOR ROAD (ARM C)</b> |  |
| W c-b = 0.00 (metres)     |  |
| V r c-b = 0 (metres)      |  |
| q c-a = 0 (pcu/hr)        |  |
| q c-b = 0 (pcu/hr)        |  |
| <b>MINOR ROAD (ARM B)</b> |  |
| W b-a = 0.00 (metres)     |  |
| W b-c = 4.80 (metres)     |  |
| V l b-a = 0 (metres)      |  |
| V r b-a = 0 (metres)      |  |
| V r b-c = 39 (metres)     |  |
| q b-a = 0 (pcu/hr)        |  |
| q b-c = 61 (pcu/hr)       |  |

### GEOMETRIC FACTORS :

|                   |  |
|-------------------|--|
| D = 0.53322       |  |
| E = 1.02732       |  |
| F = 0.58595       |  |
| Y = 0.76540       |  |
| F for (Qb-ac) = 1 |  |

### THE CAPACITY OF MOVEMENT :

|                   |  |                 |          |
|-------------------|--|-----------------|----------|
| Q b-a = 205       |  |                 |          |
| Q b-c = 515       |  | Q b-c (O) = 515 |          |
| Q c-b = 257       |  |                 |          |
| Q b-ac = 515      |  |                 |          |
| TOTAL FLOW = 1162 |  |                 | (PCU/HR) |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                   |   |
|-------------------|---|
| DFC b-a = 0.0000  | = |
| DFC b-c = 0.1184  | = |
| DFC c-b = 0.0000  | = |
| DFC b-ac = 0.1184 | = |

**CRITICAL DFC = 0.12**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J1 Nathan Road / Kimberley Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

Sep-25

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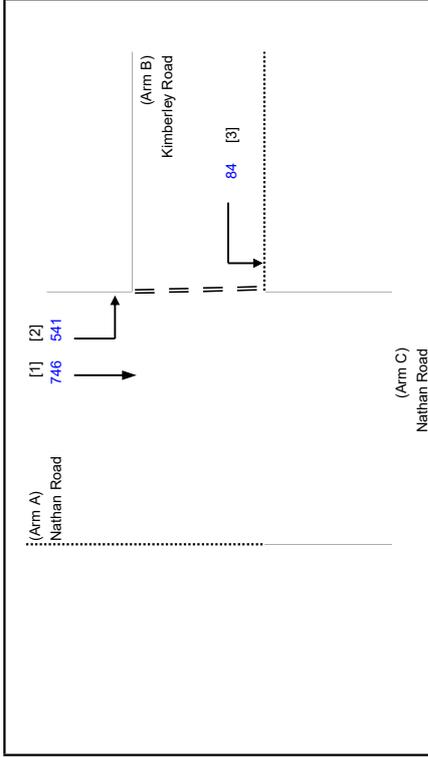
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## 2033 Reference PM



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |                   |
|---------------------------|-------------------|
| <b>MAJOR ROAD (ARM A)</b> |                   |
| W = 6.8 (metres)          | D = 0.53322       |
| W cr = 0 (metres)         | E = 1.02732       |
| q a-b = 541 (pcu/hr)      | F = 0.56595       |
| q a-c = 746 (pcu/hr)      | Y = 0.76540       |
| <b>MAJOR ROAD (ARM C)</b> |                   |
| W c-b = 0.00 (metres)     | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)      |                   |
| q c-a = 0 (pcu/hr)        |                   |
| q c-b = 0 (pcu/hr)        |                   |
| <b>MINOR ROAD (ARM B)</b> |                   |
| W b-a = 0.00 (metres)     |                   |
| W b-c = 4.80 (metres)     |                   |
| V l b-a = 0 (metres)      |                   |
| V r b-a = 0 (metres)      |                   |
| V r b-c = 39 (metres)     |                   |
| q b-a = 0 (pcu/hr)        |                   |
| q b-c = 84 (pcu/hr)       |                   |

### GEOMETRIC FACTORS :

|                   |                            |
|-------------------|----------------------------|
| D = 0.53322       | Q b-a = 192                |
| E = 1.02732       | Q b-c = 491                |
| F = 0.56595       | Q c-b = 226                |
| Y = 0.76540       | Q b-ac = 491               |
| F for (Qb-ac) = 1 | TOTAL FLOW = 1371 (PCU/HR) |

### THE CAPACITY OF MOVEMENT :

|                   |                |
|-------------------|----------------|
| Q b-a = 192       | Q b-c(O) = 491 |
| Q b-c = 491       |                |
| Q c-b = 226       |                |
| Q b-ac = 491      |                |
| TOTAL FLOW = 1371 | (PCU/HR)       |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                   |   |
|-------------------|---|
| DFC b-a = 0.0000  | = |
| DFC b-c = 0.1711  | = |
| DFC c-b = 0.0000  | = |
| DFC b-ac = 0.1711 | = |

**CRITICAL DFC = 0.17**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J1 Nathan Road / Kimberley Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

PREPARED BY: SKL

Sep-25

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Sep-25

REVIEWED BY: SLN

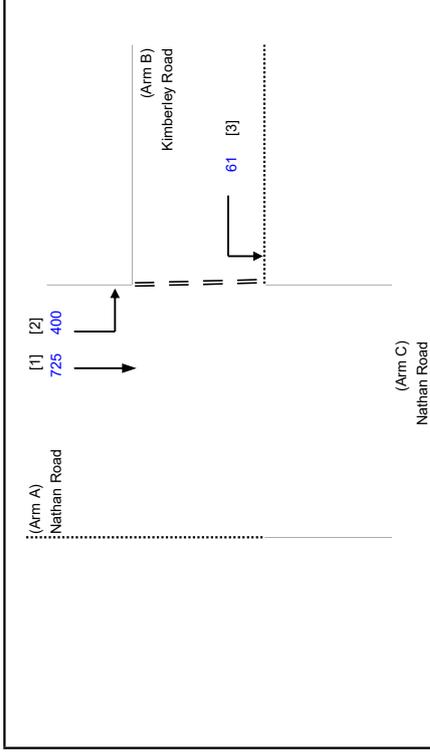
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PROJECT NO.: 41000

FILENAME: J1\_NR\_KR.xls

REFERENCE NO.:

## 2033 Design AM



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |                   |
|---------------------------|-------------------|
| <b>MAJOR ROAD (ARM A)</b> |                   |
| W = 6.8 (metres)          | D = 0.53322       |
| W cr = 0 (metres)         | E = 1.02732       |
| q a-b = 400 (pcu/hr)      | F = 0.58595       |
| q a-c = 725 (pcu/hr)      | Y = 0.76540       |
| <b>MAJOR ROAD (ARM C)</b> |                   |
| W c-b = 0.00 (metres)     | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)      |                   |
| q c-a = 0 (pcu/hr)        |                   |
| q c-b = 0 (pcu/hr)        |                   |
| <b>MINOR ROAD (ARM B)</b> |                   |
| W b-a = 0.00 (metres)     |                   |
| W b-c = 4.80 (metres)     |                   |
| V l b-a = 0 (metres)      |                   |
| V r b-a = 0 (metres)      |                   |
| V r b-c = 39 (metres)     |                   |
| q b-a = 0 (pcu/hr)        |                   |
| q b-c = 61 (pcu/hr)       |                   |

### GEOMETRIC FACTORS :

|                   |                            |
|-------------------|----------------------------|
| D = 0.53322       | Q b-a = 203                |
| E = 1.02732       | Q b-c = 513                |
| F = 0.58595       | Q c-b = 253                |
| Y = 0.76540       | Q b-ac = 513               |
| F for (Qb-ac) = 1 | TOTAL FLOW = 1186 (PCU/HR) |

### THE CAPACITY OF MOVEMENT :

|                   |                |
|-------------------|----------------|
| Q b-a = 203       | Q b-c(O) = 513 |
| Q b-c = 513       |                |
| Q c-b = 253       |                |
| Q b-ac = 513      |                |
| TOTAL FLOW = 1186 | (PCU/HR)       |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                   |   |
|-------------------|---|
| DFC b-a = 0.0000  | = |
| DFC b-c = 0.1189  | = |
| DFC c-b = 0.0000  | = |
| DFC b-ac = 0.1189 | = |

**CRITICAL DFC = 0.12**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J1 Nathan Road / Kimberley Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

PREPARED BY: SKL

Sep-25

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Sep-25

REVIEWED BY: SLN

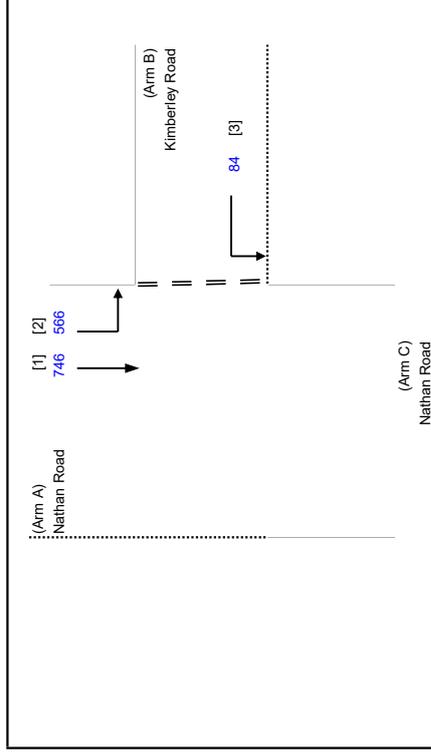
Sep-25

## 2033 Design PM

PROJECT NO.: 41000

FILENAME: J1\_NR\_KR.xls

REFERENCE NO.:



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |  |
|---------------------------|--|
| <b>MAJOR ROAD (ARM A)</b> |  |
| W = 6.8 (metres)          |  |
| W cr = 0 (metres)         |  |
| q a-b = 566 (pcu/hr)      |  |
| q a-c = 746 (pcu/hr)      |  |
| <b>MAJOR ROAD (ARM C)</b> |  |
| W c-b = 0.00 (metres)     |  |
| V r c-b = 0 (metres)      |  |
| q c-a = 0 (pcu/hr)        |  |
| q c-b = 0 (pcu/hr)        |  |
| <b>MINOR ROAD (ARM B)</b> |  |
| W b-a = 0.00 (metres)     |  |
| W b-c = 4.80 (metres)     |  |
| V l b-a = 0 (metres)      |  |
| V r b-a = 0 (metres)      |  |
| V r b-c = 39 (metres)     |  |
| q b-a = 0 (pcu/hr)        |  |
| q b-c = 84 (pcu/hr)       |  |

### GEOMETRIC FACTORS :

|                   |  |
|-------------------|--|
| D = 0.53322       |  |
| E = 1.02732       |  |
| F = 0.56595       |  |
| Y = 0.76540       |  |
| F for (Qb-ac) = 1 |  |

### THE CAPACITY OF MOVEMENT :

|                   |                 |          |
|-------------------|-----------------|----------|
| Q b-a = 190       |                 |          |
| Q b-c = 488       | Q b-c (O) = 488 |          |
| Q c-b = 222       |                 |          |
| Q b-ac = 488      |                 |          |
| TOTAL FLOW = 1396 |                 | (PCU/HR) |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                   |   |
|-------------------|---|
| DFC b-a = 0.0000  | = |
| DFC b-c = 0.1721  | = |
| DFC c-b = 0.0000  | = |
| DFC b-ac = 0.1721 | = |

**CRITICAL DFC = 0.17**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J2 Nathan Road / Austin Road

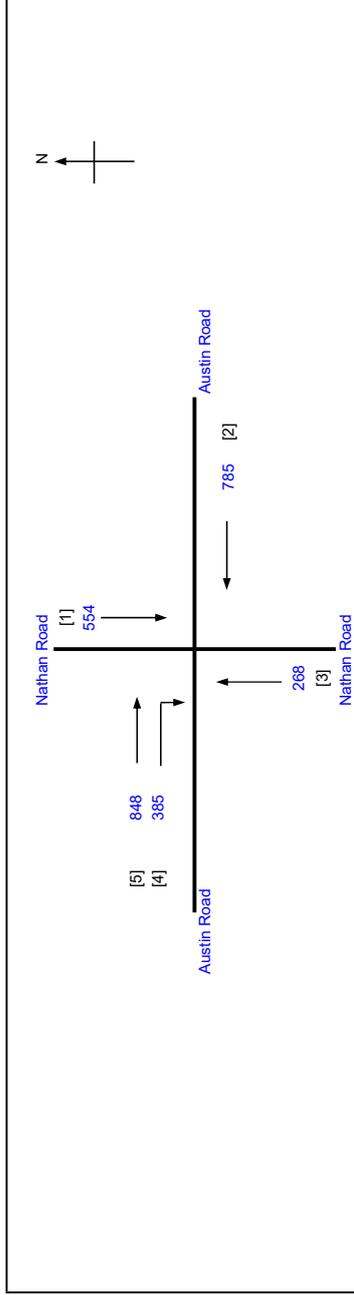
# TRAFFIC SIGNAL CALCULATION

2033 Reference AM

PROJECT NO.: 41000  
 FILENAME: J2\_AR\_NR.xlsx

Prepared By:  
 Checked By:  
 Reviewed By:

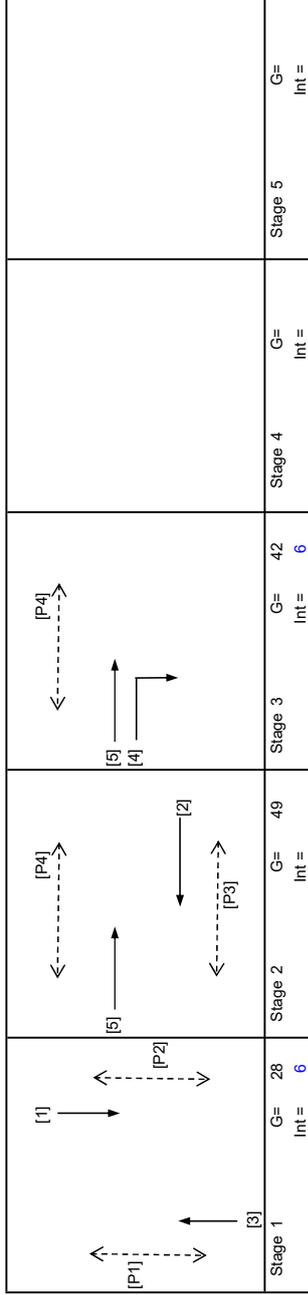
INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle = 3

Cycle time = 130 sec  
 Sum(y) = 0.572  
 Loss time = 10 sec  
 Total Flow = 2840 pcu  
 Co = 46.7 sec  
 Crm = 23.4 sec  
 Yult = 0.825  
 R.C.ult = 44.2 %  
 Cp = 27.4 sec  
 Ymax = 0.923

**R.C.(C) =  $(0.9 * Y_{max} - Y) * 100\%$  = 45 %**



| Pedestrian Phase | Stage | Green Time SG | Green Time FG | Delay | Green Time Provided SG | Green Time Provided FG |
|------------------|-------|---------------|---------------|-------|------------------------|------------------------|
| P1               | 1     | 8             | 7             | 3     | 24                     | 7                      |
| P2               | 1     | 5             | 10            | 7     | 17                     | 10                     |
| P3               | 2     | 8             | 7             | 6     | 36                     | 7                      |
| P4               | 2,3   | 8             | 7             | 7     | 82                     | 7                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.50          | 2           |           |   | N | 4070                     | 554                 | 268                     | 268                  | 554              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.136 | 0.136     | 10    | 29               | 29            | 0.620                  | 45                      | 44                      |
| 3         | 1     | 3.50          | 2           |           |   | N | 4070                     | 268                 | 268                     | 268                  | 268              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.066 | 0.066     |       | 14               | 29            | 0.620                  | 24                      | 56                      |
| 2         | 2     | 3.00          | 2           |           |   | N | 3970                     | 785                 | 785                     | 785                  | 785              | 0.00                           | 3970            |               |                     |             |                    |            |                        | 3970                    | 0.198 | 0.198     |       | 41               | 49            | 0.620                  | 57                      | 36                      |
| 5         | 2,3   | 3.30          | 1           | 15        |   | N | 1945                     | 848                 | 848                     | 848                  | 848              | 0.00                           | 1945            |               |                     |             |                    |            |                        | 1945                    | 0.436 | 0.436     |       | 91               | 91            | 0.620                  | 54                      | 11                      |
| 4         | 3     | 3.30          | 1           | 15        |   | N | 2085                     | 385                 | 385                     | 385                  | 385              | 1.00                           | 1895            |               |                     |             |                    |            |                        | 1895                    | 0.203 | 0.203     |       | 43               | 43            | 0.620                  | 54                      | 37                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J2 Nathan Road / Austin Road

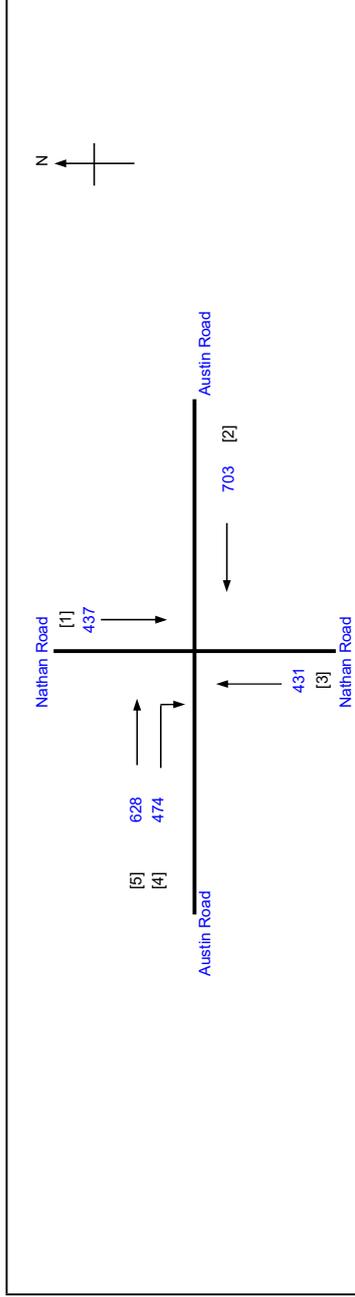
# TRAFFIC SIGNAL CALCULATION

## 2033 Reference PM

PROJECT NO.: 41000  
 FILENAME: J2\_AR\_NR.xlsx

Prepared By:  
 Checked By:  
 Reviewed By:

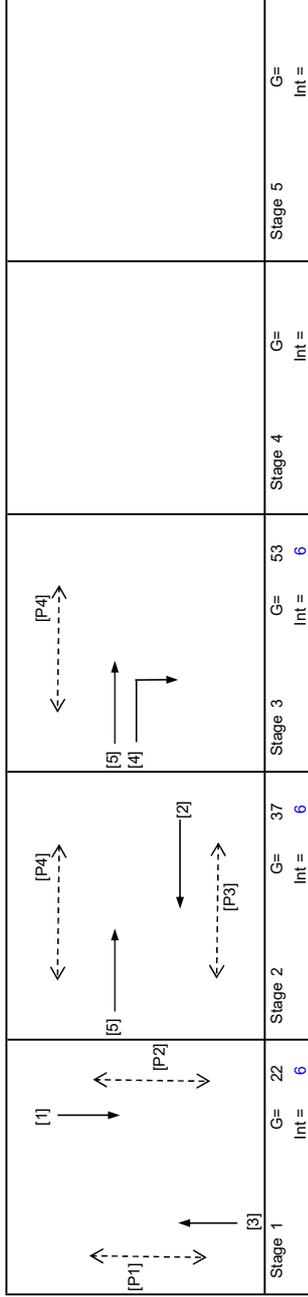
INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle = 3

Cycle time = 130 sec  
 Sum(y) = 0.535  
 Y = 15 sec  
 L = 2673 pcu  
 Co = 59.1 sec  
 Crm = 32.2 sec  
 Yult = 0.788  
 R.C.ult = 47.3 %  
 Cp = 36.9 sec  
 Ymax = 1-L/C = 0.885

**R.C.(C) =  $(0.9 \cdot Y_{max} - Y) / Y \cdot 100\%$  = 49 %**



| Pedestrian Phase | Stage | Green Time SG | Green Time FG | Delay | Green Time Provided SG | Green Time Provided FG |
|------------------|-------|---------------|---------------|-------|------------------------|------------------------|
| P1               | 1     | 8             | 7             | 3     | 18                     | 7                      |
| P2               | 1     | 5             | 10            | 7     | 11                     | 10                     |
| P3               | 2     | 8             | 7             | 6     | 30                     | 7                      |
| P4               | 2,3   | 8             | 7             | 7     | 88                     | 7                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.50          | 2           |           |   | N | 4070                     | 437                 | 437                     | 437                  | 437              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.107 | 0.107     | 15    | 23               | 23            | 0.604                  | 36                      | 48                      |
| 3         | 1     | 3.50          | 2           |           |   | N | 4070                     | 431                 | 431                     | 431                  | 431              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.106 | 0.106     |       | 23               | 23            | 0.604                  | 36                      | 48                      |
| 2         | 2     | 3.00          | 2           |           |   | N | 3970                     | 703                 | 703                     | 703                  | 703              | 0.00                           | 3970            |               |                     |             |                    |            |                        | 3970                    | 0.177 | 0.177     |       | 38               | 38            | 0.604                  | 51                      | 38                      |
| 5         | 2,3   | 3.30          | 1           | 15        |   | N | 1945                     | 628                 | 628                     | 628                  | 628              | 0.00                           | 1945            |               |                     |             |                    |            |                        | 1945                    | 0.323 | 0.323     |       | 69               | 92            | 0.604                  | 60                      | 21                      |
| 4         | 3     | 3.30          | 1           | 15        |   | N | 2085                     | 474                 | 474                     | 474                  | 474              | 1.00                           | 1895            |               |                     |             |                    |            |                        | 1895                    | 0.250 | 0.250     |       | 54               | 54            | 0.604                  | 60                      | 30                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

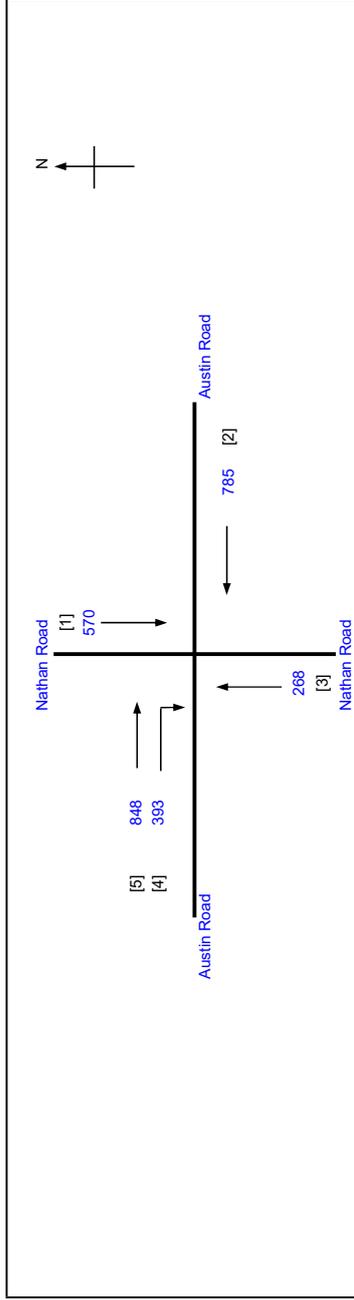
# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J2 Nathan Road / Austin Road

# TRAFFIC SIGNAL CALCULATION

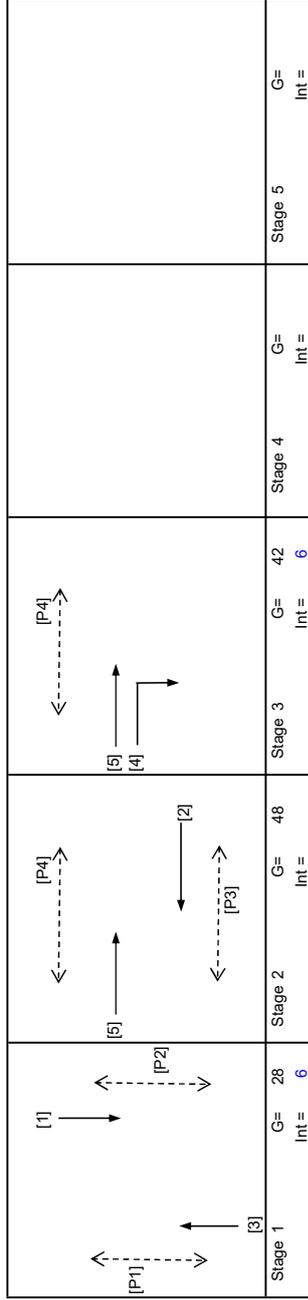
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 FILENAME : J2\_AR\_NR.xlsx  
 Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle N = 3  
 Cycle time C = 130 sec  
 Sum(y) Y = 0.576  
 Loss time L = 10 sec  
 Total Flow = 2864 pcu  
 Co = (1.5\*L+5)/(1-Y) = 47.2 sec  
 Cm = L/(1-Y) = 23.6 sec  
 Yult = 0.825  
 R.C.ult = (Yult-Y)\*100% = 43.2 %  
 Cp = 0.9\*L/(0.9-Y) = 27.8 sec  
 Ymax = 1-L/C = 0.923

**R.C.(C) = 0.9\*Ymax-Y)\*100% = 44 %**



| Pedestrian Phase | Stage | Green Time SG | Green Time FG | Delay | Green Time Provided SG | Green Time Provided FG |
|------------------|-------|---------------|---------------|-------|------------------------|------------------------|
| P1               | 1     | 8             | 7             | 3     | 24                     | 7                      |
| P2               | 1     | 5             | 10            | 7     | 17                     | 10                     |
| P3               | 2     | 8             | 7             | 6     | 35                     | 7                      |
| P4               | 2,3   | 8             | 7             | 7     | 82                     | 7                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m /lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|------------------------|-------------------------|
| 1         | 1     | 3.50          | 2           |           |   | N | 4070                     | 570                 | 570                     |                      | 570              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.140 | 0.140     | 10    | 29               | 29            | 0.624                  | 45                     | 44                      |
| 3         | 1     | 3.50          | 2           |           |   | N | 4070                     | 268                 | 268                     |                      | 268              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.066 | 0.066     |       | 14               | 29            | 0.624                  | 24                     | 56                      |
| 2         | 2     | 3.00          | 2           |           |   | N | 3970                     | 785                 | 785                     |                      | 785              | 0.00                           | 3970            |               |                     |             |                    |            |                        | 3970                    | 0.198 | 0.198     |       | 41               | 48            | 0.624                  | 57                     | 36                      |
| 5         | 2,3   | 3.30          | 1           |           |   | N | 1945                     | 848                 | 848                     |                      | 848              | 0.00                           | 1945            |               |                     |             |                    |            |                        | 1945                    | 0.436 | 0.436     |       | 91               | 91            | 0.624                  | 54                     | 11                      |
| 4         | 3     | 3.30          | 1           | 15        |   |   | 2085                     | 393                 | 393                     | 393                  | 393              | 1.00                           | 1895            |               |                     |             |                    |            |                        | 1895                    | 0.207 | 0.207     |       | 43               | 43            | 0.624                  | 54                     | 37                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J2 Nathan Road / Austin Road

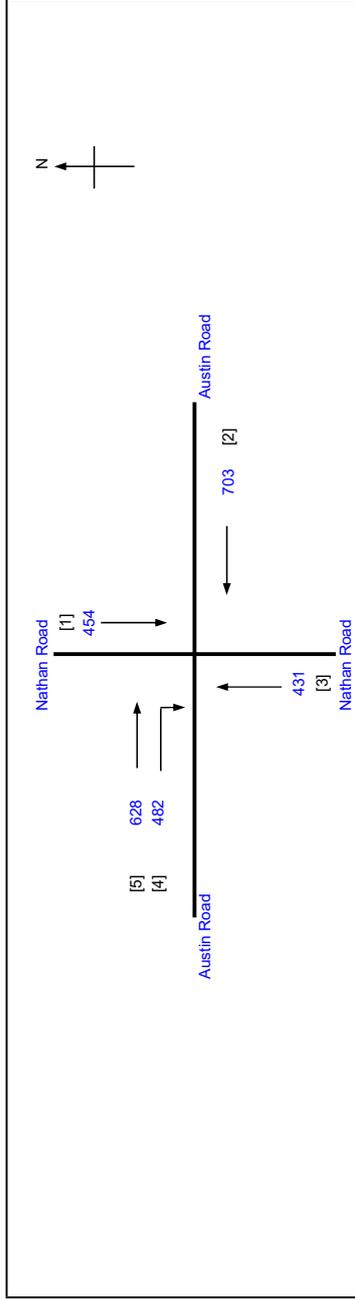
# TRAFFIC SIGNAL CALCULATION

2033 Design PM

PROJECT NO.: 41000  
 FILENAME: J2\_AR\_NR.xlsx

Prepared By:  
 Checked By:  
 Reviewed By:

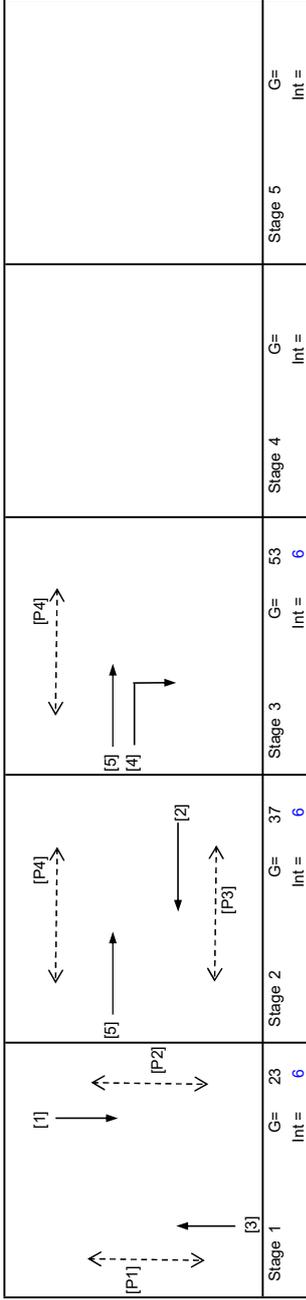
INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle = 3

Cycle time = 130 sec  
 Sum(y) = 0.543  
 Loss time = 15 sec  
 Total Flow = 2698 pcu  
 Co = 60.2 sec  
 Crm = 32.8 sec  
 Yult = 0.788  
 R.C.ult = 45.0 %  
 Cp = 37.8 sec  
 Ymax = 0.885

**R.C.(C) =  $(0.9 * Y_{max} - Y) * 100\%$  = 47 %**



| Pedestrian Phase | Stage | Green Time SG | Green Time FG | Delay | Green Time Provided SG | Green Time Provided FG |
|------------------|-------|---------------|---------------|-------|------------------------|------------------------|
| P1               | 1     | 8             | 7             | 3     | 19                     | 7                      |
| P2               | 1     | 5             | 10            | 7     | 12                     | 10                     |
| P3               | 2     | 8             | 7             | 6     | 30                     | 7                      |
| P4               | 2,3   | 8             | 7             | 7     | 87                     | 7                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement Left pcu/h | Movement Straight pcu/h | Movement Right pcu/h | Total FLOW pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|---------------------|-------------------------|----------------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.50          | 2           |           |   | N | 4070                     | 454                 | 454                     | 454                  | 454              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.112 | 0.112     | 15    | 24               | 24            | 0.614                  | 39                      | 48                      |
| 3         | 1     | 3.50          | 2           |           |   | N | 4070                     | 431                 | 431                     | 431                  | 431              | 0.00                           | 4070            |               |                     |             |                    |            |                        | 4070                    | 0.106 | 0.106     |       | 22               | 24            | 0.614                  | 36                      | 48                      |
| 2         | 2     | 3.00          | 2           |           |   | N | 3970                     | 703                 | 703                     | 703                  | 703              | 0.00                           | 3970            |               |                     |             |                    |            |                        | 3970                    | 0.177 | 0.177     |       | 38               | 38            | 0.614                  | 54                      | 38                      |
| 5         | 2,3   | 3.30          | 1           | 15        |   | N | 1945                     | 628                 | 628                     | 628                  | 628              | 0.00                           | 1945            |               |                     |             |                    |            |                        | 1945                    | 0.323 | 0.323     |       | 68               | 91            | 0.614                  | 60                      | 22                      |
| 4         | 3     | 3.30          | 1           | 15        |   | N | 2085                     | 482                 | 482                     | 482                  | 482              | 1.00                           | 1895            |               |                     |             |                    |            |                        | 1895                    | 0.254 | 0.254     |       | 54               | 54            | 0.614                  | 60                      | 30                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

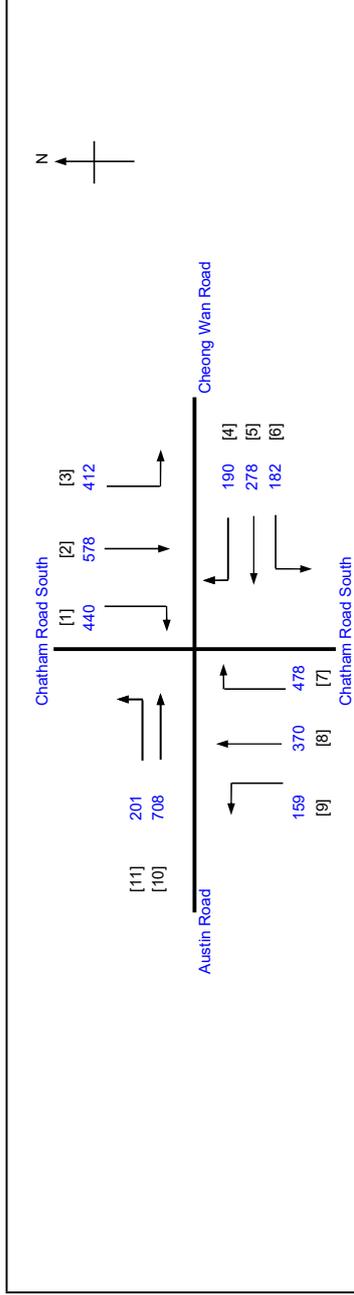
Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J3 Chatham Road South / Austin Road / Cheong Wan Road

# TRAFFIC SIGNAL CALCULATION

2033 Reference AM

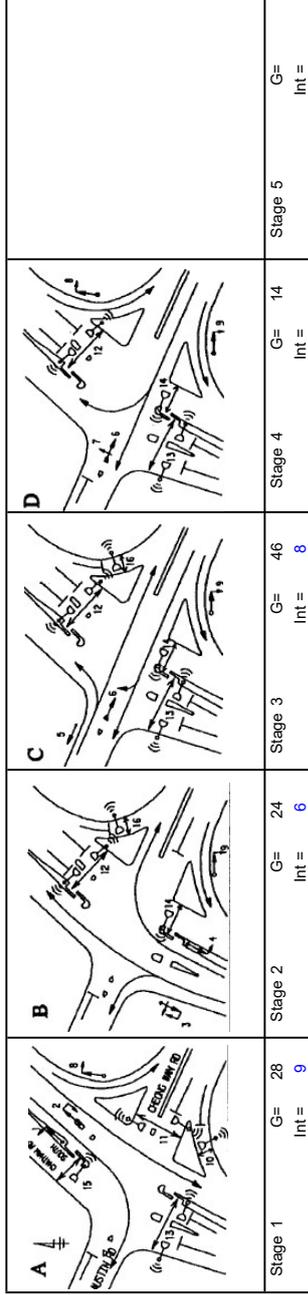
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 FILENAME: J3\_CRS\_AR\_CWR.xlsx  
 Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



No. of stages per cycle = 4  
 Cycle time = 130 sec  
 Sum(y) = 0.471  
 Loss time = 34 sec  
 Total Flow = 3996 pcu  
 Co = 105.9 sec  
 Crm = 64.3 sec  
 Yult = 0.645  
 R.C.ult = 36.8 %  
 Cp = 71.4 sec  
 Ymax = 1-L/C = 0.738

**R.C.(C) = 0.9\*Ymax-y/Y\*100% = 41 %**



| Stage   | Green Time Required SG | Green Time Provided SG |
|---------|------------------------|------------------------|
| Stage 1 | 5                      | 7                      |
| Stage 2 | 11                     | 10                     |
| Stage 3 | 10                     | 9                      |
| Stage 4 | 12                     | 10                     |
| Stage 5 | 5                      | 10                     |
| Stage 6 | 5                      | 10                     |
| Stage 7 | 5                      | 6                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement Left Sat. Flow | Movement Straight Sat. Flow | Movement Right Sat. Flow | Total Flow | Proportion of Turning Vehicles | Sat. Flow | Flare Lane m. | Flare Effect | Site Factor | Site Effect | Gradient % | Gradient Effect | Revised Sat. Flow | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|-------------------------|-----------------------------|--------------------------|------------|--------------------------------|-----------|---------------|--------------|-------------|-------------|------------|-----------------|-------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.00          | 2           | 25        |   |   | 4110                     |                         | 440                         | 440                      | 440        | 1.00                           | 3877      |               |              |             |             |            |                 | 3877              | 0.113 | 0.113     | 20    | 23               | 29            | 0.638                  | 39                      | 49                      |
| 2         | 1     | 3.00          | 2           | 25        |   | N | 4110                     |                         | 578                         | 578                      | 578        | 0.00                           | 4110      |               |              |             |             |            |                 | 4110              | 0.141 | 0.141     |       | 29               | 29            | 0.638                  | 48                      | 45                      |
| 3         | 1,4   | 3.00          | 1           | 20        |   |   | 1915                     |                         | 412                         | 412                      | 412        | 1.00                           | 1781      |               |              |             |             |            |                 | 1781              | 0.231 | 0.231     |       | 47               | 47            | 0.638                  | 54                      | 35                      |
| 8,9       | 2     | 3.00          | 1           | 10        |   | N | 1915                     | 0                       | 159                         | 159                      | 159        | 1.00                           | 1665      |               |              |             |             |            |                 | 1665              | 0.095 | 0.095     |       | 19               | 25            | 0.638                  | 30                      | 58                      |
| 8         | 2     | 3.00          | 2           | 25        | O |   | 4110                     | 370                     | 370                         | 370                      | 370        | 0.00                           | 4110      | 36            | 1029         |             |             |            |                 | 4110              | 0.090 | 0.090     |       | 18               | 25            | 0.638                  | 33                      | 52                      |
| 7         | 2     | 3.00          | 2           | 20        | O |   | 4110                     | 478                     | 478                         | 478                      | 478        | 1.00                           | 3823      |               |              |             |             |            |                 | 3823              | 0.125 | 0.125     |       | 25               | 25            | 0.638                  | 39                      | 47                      |
| 6         | 2,3,4 | 3.00          | 1           | 25        |   | N | 1915                     | 182                     | 182                         | 182                      | 182        | 1.00                           | 1807      |               |              |             |             |            |                 | 1807              | 0.101 | 0.101     |       | 21               | 21            | 0.638                  | 30                      | 56                      |
| 4,5       | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | 278                     | 278                         | 292                      | 292        | 0.05                           | 1820      |               |              |             |             |            |                 | 2848              | 0.103 | 0.103     |       | 21               | 21            | 0.638                  | 48                      | 52                      |
| 4         | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | 176                     | 176                         | 176                      | 176        | 1.00                           | 1722      |               |              |             |             |            |                 | 1722              | 0.102 | 0.102     |       | 21               | 21            | 0.638                  | 30                      | 56                      |
| 10,11     | 3     | 3.00          | 1           | 20        |   | N | 1915                     | 201                     | 201                         | 431                      | 431        | 0.47                           | 1850      |               |              |             |             |            |                 | 1850              | 0.233 | 0.233     | 14    | 47               | 47            | 0.638                  | 54                      | 35                      |
| 10        | 3     | 3.00          | 1           | 20        |   |   | 2055                     | 478                     | 478                         | 478                      | 478        | 0.00                           | 2055      |               |              |             |             |            |                 | 2055              | 0.233 | 0.233     |       | 47               | 47            | 0.638                  | 60                      | 35                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUEING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

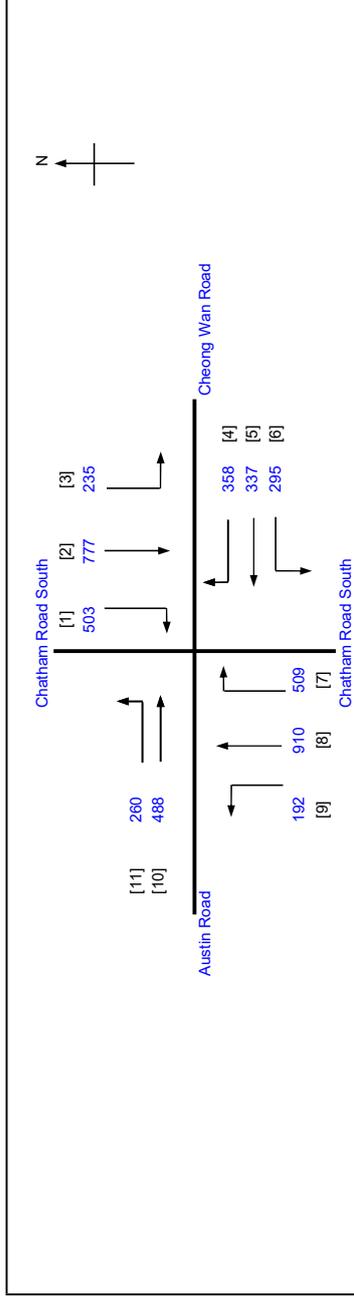
Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui  
 J3 Chatham Road South / Austin Road / Cheong Wan Road

# TRAFFIC SIGNAL CALCULATION

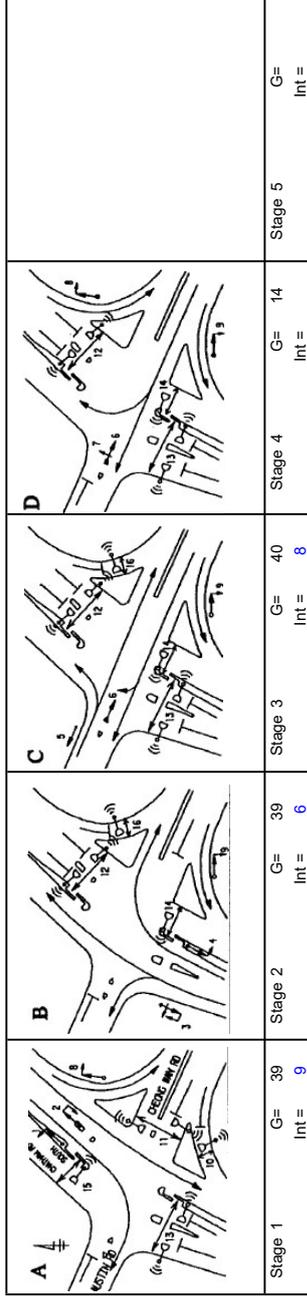
2033 Reference PM

PROJECT NO.: 41000  
 FILENAME: J3\_CRS\_AR\_CWR.xlsx  
 Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



|                         |                                   |
|-------------------------|-----------------------------------|
| No. of stages per cycle | N = 4                             |
| Cycle time              | C = 130 sec                       |
| Sum(y)                  | Y = 0.456                         |
| Loss time               | L = 34 sec                        |
| Total Flow              | 4864 pcu                          |
| Co                      | = (1.5*L+5)/(1-Y) = 103.0 sec     |
| Cm                      | = L/(1-Y) = 62.5 sec              |
| Yult                    | = = 0.645                         |
| R.C.ult                 | = (Yult-Y)*100% = 41.3 %          |
| Cp                      | = 0.9*L/(0.9-Y) = 69.0 sec        |
| Ymax                    | = 1-L/C = 0.738                   |
| <b>R.C.(C)</b>          | <b>= (0.9*Ymax-Y)*100% = 46 %</b> |



| Green Time Required | Green Time Provided |
|---------------------|---------------------|
| SG                  | SG                  |
| FG                  | FG                  |
| Delay               | Delay               |
| 5                   | 7                   |
| 11                  | 10                  |
| 10                  | 9                   |
| 12                  | 10                  |
| 5                   | 10                  |
| 5                   | 10                  |
| 5                   | 6                   |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement   |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|------------|-------------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
|           |       |               |             |           |   |   |                          | Left pcu/h | Right pcu/h |                  |                                |                 |               |                     |             |                    |            |                        |                         |       |           |       |                  |               |                        |                         |                         |
| 1         | 1     | 3.00          | 2           | 25        |   |   | 4110                     |            | 503         | 1.00             | 3877                           |                 |               |                     |             |                    |            | 3877                   | 0.130                   | 0.130 | 20        | 27    | 40               | 0.618         | 42                     | 45                      |                         |
| 2         | 1     | 3.00          | 2           | 25        |   | N | 4110                     |            | 777         | 0.00             | 4110                           |                 |               |                     |             |                    |            | 4110                   | 0.189                   | 0.189 |           | 40    | 40               | 0.618         | 57                     | 37                      |                         |
| 3         | 1,4   | 3.00          | 1           | 20        |   |   | 1915                     |            | 235         | 1.00             | 1781                           |                 |               |                     |             |                    |            | 1781                   | 0.132                   | 0.132 |           | 28    | 28               | 0.618         | 36                     | 49                      |                         |
| 8,9       | 2     | 3.00          | 1           | 10        |   | N | 1915                     |            | 331         | 0.58             | 1762                           |                 |               |                     |             |                    |            | 1762                   | 0.188                   | 0.188 |           | 40    | 40               | 0.618         | 48                     | 40                      |                         |
| 8         | 2     | 3.00          | 2           | 25        | O |   | 4110                     |            | 771         | 0.00             | 4110                           |                 | 36            |                     |             |                    |            | 4110                   | 0.188                   | 0.188 |           | 39    | 40               | 0.618         | 57                     | 37                      |                         |
| 7         | 2     | 3.00          | 2           | 20        |   |   | 4110                     |            | 509         | 1.00             | 3823                           |                 |               |                     |             |                    |            | 3823                   | 0.133                   | 0.133 |           | 28    | 40               | 0.618         | 42                     | 45                      |                         |
| 6         | 2,3,4 | 3.00          | 1           | 25        |   | N | 1915                     |            | 295         | 1.00             | 1807                           |                 |               |                     |             |                    |            | 1807                   | 0.163                   | 0.163 |           | 34    | 34               | 0.618         | 42                     | 43                      |                         |
| 4,5       | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     |            | 406         | 0.17             | 1807                           |                 | 617           |                     |             |                    |            | 2424                   | 0.168                   | 0.168 |           | 35    | 35               | 0.618         | 60                     | 41                      |                         |
| 4         | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     |            | 289         | 1.00             | 1722                           |                 |               |                     |             |                    |            | 1722                   | 0.168                   | 0.168 |           | 35    | 35               | 0.618         | 42                     | 43                      |                         |
| 10,11     | 3     | 3.00          | 1           | 20        |   | N | 1915                     |            | 351         | 0.74             | 1814                           |                 |               |                     |             |                    |            | 1814                   | 0.193                   | 0.193 | 14        | 41    | 41               | 0.618         | 48                     | 39                      |                         |
| 10        | 3     | 3.00          | 1           | 20        |   |   | 2055                     |            | 397         | 0.00             | 2055                           |                 |               |                     |             |                    |            | 2055                   | 0.193                   | 0.193 |           | 41    | 41               | 0.618         | 54                     | 38                      |                         |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUEING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

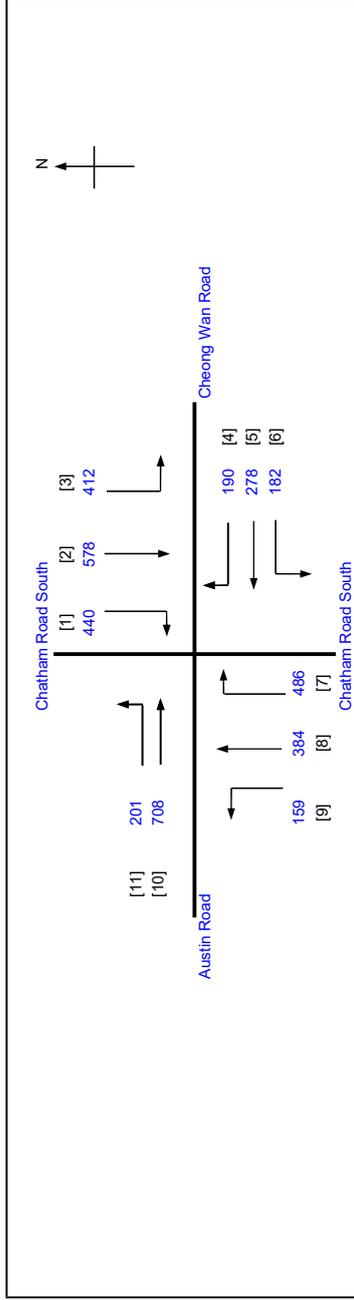
J3 Chatham Road South / Austin Road / Cheong Wan Road

# TRAFFIC SIGNAL CALCULATION

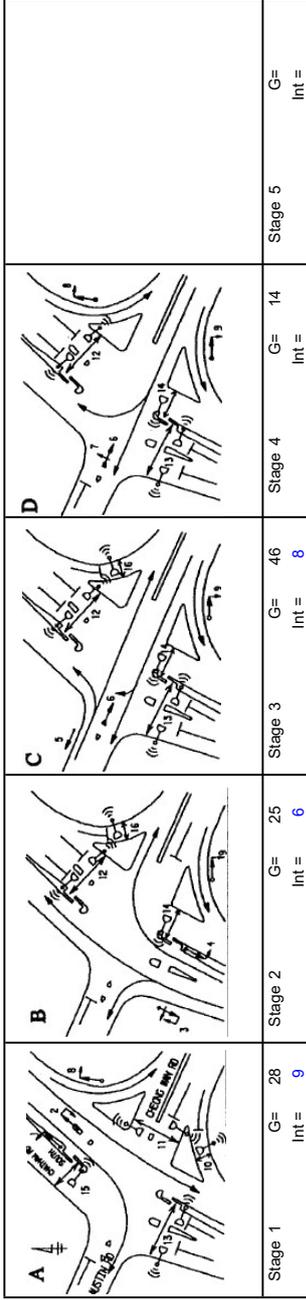
2033 Design AM

PROJECT NO.: 41000  
 FILENAME: J3\_CRS\_AR\_CWR.xlsx  
 Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS DATE  
 SKL Sep-25  
 SLN Sep-25  
 SLN Sep-25



|                         |                                  |
|-------------------------|----------------------------------|
| No. of stages per cycle | N = 4                            |
| Cycle time              | C = 130 sec                      |
| Sum(y)                  | Y = 0.474                        |
| Loss time               | L = 34 sec                       |
| Total Flow              | = 4018 pcu                       |
| Co                      | = (1.5*L+5)/(1-Y)                |
| Cm                      | = L/(1-Y)                        |
| Yult                    | = 0.645                          |
| R.C.ult                 | = (Yult-Y)*100%                  |
| Cp                      | = 0.9*L/(0.9-Y)                  |
| Ymax                    | = 1-L/C                          |
| <b>R.C.(C)</b>          | <b>= 0.9*Ymax-Y)*100% = 40 %</b> |



| Stage | Stage | Green Time Required SG | Green Time Provided SG |
|-------|-------|------------------------|------------------------|
| 1     | 1     | 5                      | 7                      |
| 11p   | 1     | 11                     | 10                     |
| 12p   | 2,3,4 | 10                     | 9                      |
| 13p   | 1,3,4 | 12                     | 10                     |
| 14p   | 2,3,4 | 5                      | 10                     |
| 15p   | 1     | 5                      | 10                     |
| 16p   | 2,3   | 5                      | 6                      |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight Ahead Sat. Flow | Movement | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|----------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.00          | 2           | 25        |   |   | 4110                     | Left     | 440              | 1.00                           | 3877            |               |                     |             |                    |            |                        | 3877                    | 0.113 | 0.113     | 20    | 23               | 29            | 0.641                  | 39                      | 49                      |
| 2         | 1     | 3.00          | 2           | 25        |   |   | 4110                     | Through  | 578              | 0.00                           | 4110            |               |                     |             |                    |            |                        | 4110                    | 0.141 | 0.141     |       | 29               | 29            | 0.641                  | 48                      | 45                      |
| 3         | 1,4   | 3.00          | 1           | 20        |   |   | 1915                     | Right    | 412              | 1.00                           | 1781            |               |                     |             |                    |            |                        | 1781                    | 0.231 | 0.231     |       | 47               | 47            | 0.641                  | 54                      | 36                      |
| 8,9       | 2     | 3.00          | 1           | 10        |   | N | 1915                     | Left     | 159              | 1.00                           | 1665            |               |                     |             |                    |            |                        | 1665                    | 0.095 | 0.095     |       | 19               | 26            | 0.641                  | 30                      | 59                      |
| 8         | 2     | 3.00          | 2           | 25        | O |   | 4110                     | Through  | 384              | 0.00                           | 4110            | 36            | 1029                |             |                    |            |                        | 4110                    | 0.093 | 0.093     |       | 19               | 26            | 0.641                  | 33                      | 52                      |
| 7         | 2     | 3.00          | 2           | 20        |   |   | 4110                     | Right    | 486              | 1.00                           | 3823            |               |                     |             |                    |            |                        | 3823                    | 0.127 | 0.127     |       | 26               | 26            | 0.641                  | 42                      | 47                      |
| 6         | 2,3,4 | 3.00          | 1           | 25        |   | N | 1915                     | Left     | 182              | 1.00                           | 1807            |               |                     |             |                    |            |                        | 1807                    | 0.101 | 0.101     |       | 20               | 20            | 0.641                  | 30                      | 56                      |
| 4,5       | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | Through  | 292              | 0.05                           | 1820            |               |                     |             |                    |            |                        | 2848                    | 0.103 | 0.103     |       | 21               | 21            | 0.641                  | 48                      | 52                      |
| 4         | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | Right    | 176              | 1.00                           | 1722            |               |                     |             |                    |            |                        | 1722                    | 0.102 | 0.102     |       | 21               | 21            | 0.641                  | 30                      | 57                      |
| 10,11     | 3     | 3.00          | 1           | 20        |   | N | 1915                     | Left     | 230              | 0.47                           | 1850            |               |                     |             |                    |            |                        | 1850                    | 0.233 | 0.233     | 14    | 47               | 47            | 0.641                  | 54                      | 35                      |
| 10        | 3     | 3.00          | 1           | 20        |   |   | 2055                     | Through  | 478              | 0.00                           | 2055            |               |                     |             |                    |            |                        | 2055                    | 0.233 | 0.233     |       | 47               | 47            | 0.641                  | 60                      | 35                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

# TRAFFIC SIGNAL CALCULATION

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

2033 Design PM

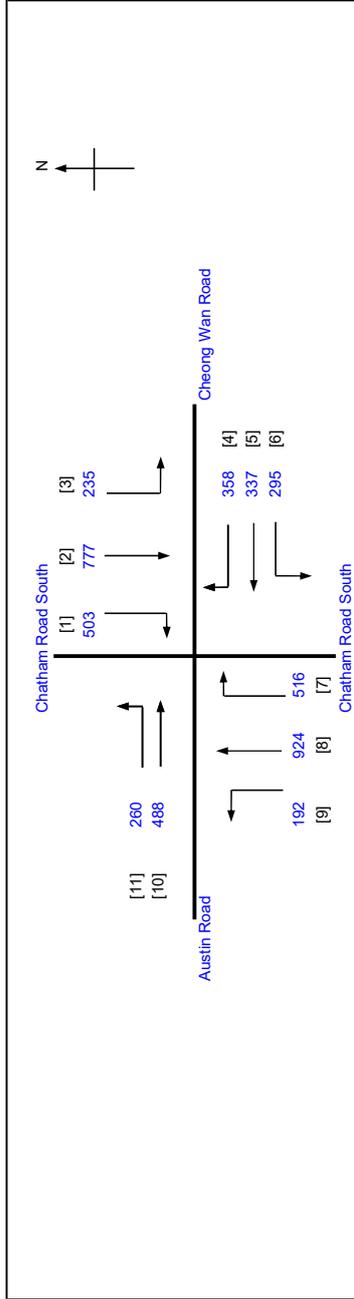
J3 Chatham Road South / Austin Road / Cheong Wan Road

PROJECT NO.: 41000  
 FILENAME: J3\_CRS\_AR\_CWR.xlsx

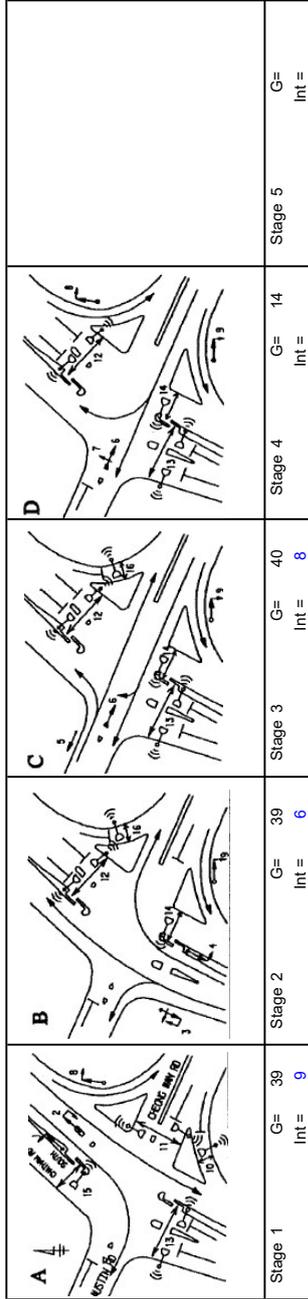
Prepared By:  
 Checked By:  
 Reviewed By:

INITIALS  
 SKL  
 SLN  
 SLN

DATE  
 Sep-25  
 Sep-25  
 Sep-25



|                         |                                  |
|-------------------------|----------------------------------|
| No. of stages per cycle | N = 4                            |
| Cycle time              | C = 130 sec                      |
| Sum(y)                  | Y = 0.458                        |
| Loss time               | L = 34 sec                       |
| Total Flow              | = 4885 pcu                       |
| Co                      | = (1.5*L+5)/(1-Y)                |
| Cm                      | = L/(1-Y)                        |
| Yult                    | = 0.645                          |
| R.C.ult                 | = (Yult-Y)*100%                  |
| Cp                      | = 0.9*L/(0.9-Y)                  |
| Ymax                    | = 1-L/C                          |
| <b>R.C.(C)</b>          | <b>= 0.9*Ymax-Y)*100% = 45 %</b> |



| Stage   | Green Time Required SG | Green Time Provided SG |
|---------|------------------------|------------------------|
| Stage 1 | 5                      | 7                      |
| Stage 2 | 11                     | 10                     |
| Stage 3 | 10                     | 9                      |
| Stage 4 | 12                     | 10                     |
| Stage 5 | 5                      | 10                     |
| Stage 6 | 5                      | 10                     |

| Move-ment | Stage | Lane Width m. | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Movement | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Flare Lane m. | Flare Effect pcu/hr | Site Factor | Site Effect pcu/hr | Gradient % | Gradient Effect pcu/hr | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queue Length (m / lane) | Average Delay (seconds) |
|-----------|-------|---------------|-------------|-----------|---|---|--------------------------|----------|------------------|--------------------------------|-----------------|---------------|---------------------|-------------|--------------------|------------|------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-------------------------|
| 1         | 1     | 3.00          | 2           | 25        |   |   | 4110                     | Left     | 503              | 1.00                           | 3877            |               |                     |             |                    |            |                        | 3877                    | 0.130 | 0.130     | 20    | 27               | 40            | 0.620                  | 42                      | 45                      |
| 2         | 1     | 3.00          | 2           | 25        |   |   | 4110                     | Through  | 777              | 0.00                           | 4110            |               |                     |             |                    |            |                        | 4110                    | 0.189 | 0.189     |       | 40               | 40            | 0.620                  | 57                      | 37                      |
| 3         | 1,4   | 3.00          | 1           | 20        |   |   | 1915                     | Right    | 235              | 1.00                           | 1781            |               |                     |             |                    |            |                        | 1781                    | 0.132 | 0.132     |       | 28               | 28            | 0.620                  | 36                      | 49                      |
| 8,9       | 2     | 3.00          | 1           | 10        |   | N | 1915                     | Left     | 144              | 0.57                           | 1764            |               |                     |             |                    |            |                        | 1764                    | 0.190 | 0.190     |       | 40               | 40            | 0.620                  | 48                      | 40                      |
| 8         | 2     | 3.00          | 2           | 25        | O |   | 4110                     | Through  | 780              | 0.00                           | 4110            | 36            | 617                 |             |                    |            |                        | 4110                    | 0.190 | 0.190     |       | 40               | 40            | 0.620                  | 57                      | 37                      |
| 7         | 2     | 3.00          | 2           | 20        |   |   | 4110                     | Right    | 516              | 1.00                           | 3823            |               |                     |             |                    |            |                        | 3823                    | 0.135 | 0.135     |       | 28               | 40            | 0.620                  | 42                      | 45                      |
| 6         | 2,3,4 | 3.00          | 1           | 25        |   | N | 1915                     | Left     | 295              | 1.00                           | 1807            |               |                     |             |                    |            |                        | 1807                    | 0.163 | 0.163     |       | 34               | 34            | 0.620                  | 42                      | 44                      |
| 4,5       | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | Through  | 406              | 0.17                           | 1807            |               |                     |             |                    |            |                        | 2424                    | 0.168 | 0.168     |       | 35               | 35            | 0.620                  | 60                      | 41                      |
| 4         | 3,4   | 3.00          | 1           | 25        | O |   | 2055                     | Right    | 289              | 1.00                           | 1722            |               |                     |             |                    |            |                        | 1722                    | 0.168 | 0.168     |       | 35               | 35            | 0.620                  | 42                      | 43                      |
| 10,11     | 3     | 3.00          | 1           | 20        |   | N | 1915                     | Left     | 91               | 0.74                           | 1814            |               |                     |             |                    |            |                        | 1814                    | 0.193 | 0.193     | 14    | 41               | 41            | 0.620                  | 48                      | 39                      |
| 10        | 3     | 3.00          | 1           | 20        |   |   | 2055                     | Through  | 397              | 0.00                           | 2055            |               |                     |             |                    |            |                        | 2055                    | 0.193 | 0.193     |       | 40               | 41            | 0.620                  | 54                      | 39                      |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRAIN WALKING SPEED = 1.2m/s QUEUEING LENGTH = AVERAGE QUEUE \* 6m

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J4 Chatham Road South / Observatory Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

Sep-25

SKL

PREPARED BY:

Sep-25

SLN

CHECKED BY:

Sep-25

SLN

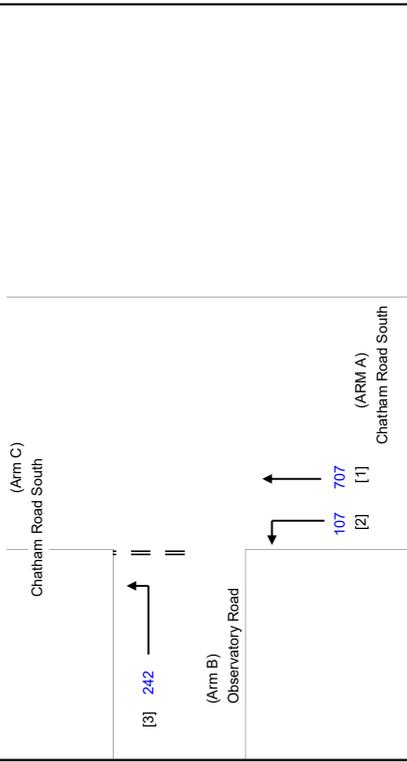
REVIEWED BY:

## 2033 Reference AM

PROJECT NO.: 41000

FILENAME: J4\_CRS\_OR

REFERENCE NO.:



NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V r c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                           |                   |
|---------------------------|-------------------|
| <b>MAJOR ROAD (ARM A)</b> |                   |
| W = 10.50 (metres)        | D = 0.53322       |
| W cr = 0 (metres)         | E = 1.01663       |
| q a-b = 107 (pcu/hr)      | F = 0.58595       |
| q a-c = 707 (pcu/hr)      | Y = 0.63775       |
| <b>MAJOR ROAD (ARM C)</b> |                   |
| W c-b = 0.00 (metres)     | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)      |                   |
| q c-a = 0 (pcu/hr)        |                   |
| q c-b = 0 (pcu/hr)        |                   |
| <b>MINOR ROAD (ARM B)</b> |                   |
| W b-a = 0.00 (metres)     |                   |
| W b-c = 4.70 (metres)     |                   |
| V i b-a = 0 (metres)      |                   |
| V r b-a = 0 (metres)      |                   |
| V r b-c = 37 (metres)     |                   |
| q b-a = 0 (pcu/hr)        |                   |
| q b-c = 242 (pcu/hr)      |                   |

### GEOMETRIC FACTORS :

|                   |                 |
|-------------------|-----------------|
| Q b-a = 242       | Q b-c (O) = 581 |
| Q b-c = 581       | Q c-b = 326     |
| Q c-b = 326       | Q b-ac = 581    |
| TOTAL FLOW = 1056 | (PCU/HR)        |

### THE CAPACITY OF MOVEMENT :

|                  |                  |                  |                               |
|------------------|------------------|------------------|-------------------------------|
| DFC b-a = 0.0000 | DFC b-c = 0.4165 | DFC c-b = 0.0000 | DFC b-c (share lane) = 0.4165 |
|------------------|------------------|------------------|-------------------------------|

### COMPARISON OF DESIGN FLOW TO CAPACITY:

**CRITICAL DFC = 0.42**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J4 Chatham Road South / Observatory Road

# PRIORITY JUNCTION CALCULATION

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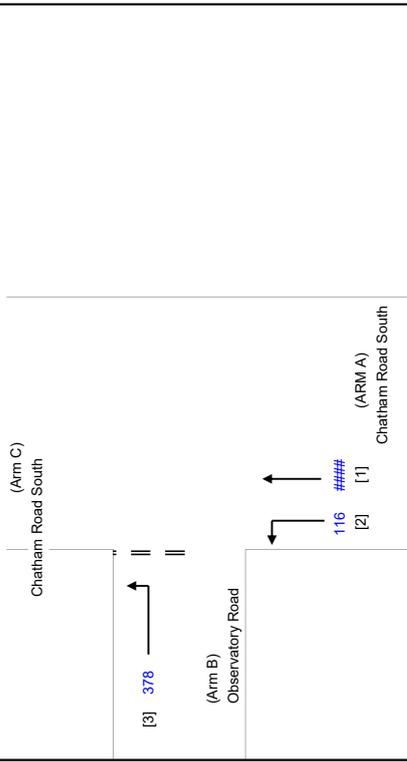
Sep-25

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Sep-25

PROJECT NO.: 41000  
 FILENAME: J4\_CRS\_OR  
 REFERENCE NO.:

## 2033 Reference PM



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH  
 W cr = CENTRAL RESERVE WIDTH  
 W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a  
 W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c  
 W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b  
 V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a  
 V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a  
 V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c  
 V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
 D = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b  
 E = STREAM-SPECIFIC B-A  
 F = STREAM-SPECIFIC B-C  
 Y = STREAM-SPECIFIC C-B  
 (1-0.0345W)

### GEOMETRIC DETAILS:

|                       |                   |
|-----------------------|-------------------|
| MAJOR ROAD (ARM A)    |                   |
| W = 10.50 (metres)    | D = 0.53322       |
| W cr = 0 (metres)     | E = 1.01663       |
| q a-b = 116 (pcu/hr)  | F = 0.58595       |
| q a-c = 1018 (pcu/hr) | Y = 0.63775       |
| MAJOR ROAD (ARM C)    |                   |
| W c-b = 0.00 (metres) | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)  |                   |
| q c-a = 0 (pcu/hr)    |                   |
| q c-b = 0 (pcu/hr)    |                   |
| MINOR ROAD (ARM B)    |                   |
| W b-a = 0.00 (metres) |                   |
| W b-c = 4.70 (metres) |                   |
| V l b-a = 0 (metres)  |                   |
| V r b-a = 0 (metres)  |                   |
| V r b-c = 37 (metres) |                   |
| q b-a = 0 (pcu/hr)    |                   |
| q b-c = 378 (pcu/hr)  |                   |

### GEOMETRIC FACTORS :

|                            |              |
|----------------------------|--------------|
| D = 0.53322                | Q b-a = 203  |
| E = 1.01663                | Q b-c = 506  |
| F = 0.58595                | Q c-b = 282  |
| Y = 0.63775                | Q b-ac = 506 |
| TOTAL FLOW = 1512 (PCU/HR) |              |

### THE CAPACITY OF MOVEMENT :

|              |                 |
|--------------|-----------------|
| Q b-a = 203  | Q b-c (O) = 506 |
| Q b-c = 506  |                 |
| Q c-b = 282  |                 |
| Q b-ac = 506 |                 |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                               |
|-------------------------------|
| DFC b-a = 0.0000              |
| DFC b-c = 0.7470              |
| DFC c-b = 0.0000              |
| DFC b-c (share lane) = 0.7470 |

**CRITICAL DFC = 0.75**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J4 Chatham Road South / Observatory Road

# PRIORITY JUNCTION CALCULATION

INITIALS

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SKL

PREPARED BY:

PROJECT NO.: 41000

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FILENAME: J4\_CRS\_OR

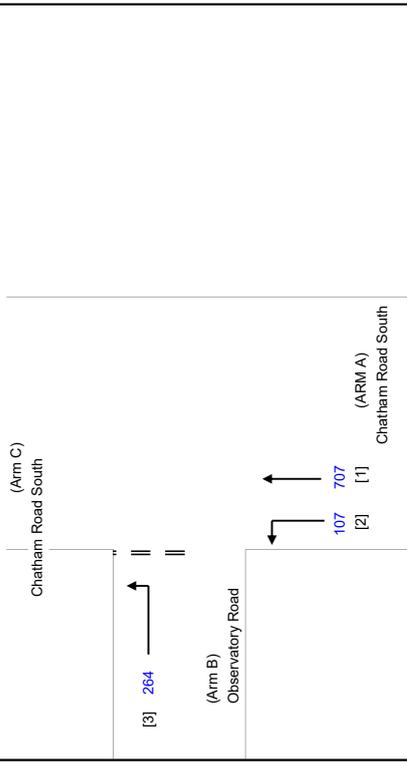
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REFERENCE NO.:

## 2033 Design AM



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH

W cr = CENTRAL RESERVE WIDTH

W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a

W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c

W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b

V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a

V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a

V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c

V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c

V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b

V r c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b

D = STREAM-SPECIFIC B-A

E = STREAM-SPECIFIC B-C

F = STREAM-SPECIFIC C-B

Y = (1-0.0345W)

### GEOMETRIC DETAILS:

|                       |                   |
|-----------------------|-------------------|
| MAJOR ROAD (ARM A)    |                   |
| W = 10.50 (metres)    | D = 0.53322       |
| W cr = 0 (metres)     | E = 1.01663       |
| q a-b = 107 (pcu/hr)  | F = 0.58595       |
| q a-c = 707 (pcu/hr)  | Y = 0.63775       |
| MAJOR ROAD (ARM C)    |                   |
| W c-b = 0.00 (metres) | F for (Qb-ac) = 1 |
| V r c-b = 0 (metres)  |                   |
| q c-a = 0 (pcu/hr)    |                   |
| q c-b = 0 (pcu/hr)    |                   |
| MINOR ROAD (ARM B)    |                   |
| W b-a = 0.00 (metres) |                   |
| W b-c = 4.70 (metres) |                   |
| V l b-a = 0 (metres)  |                   |
| V r b-a = 0 (metres)  |                   |
| V r b-c = 37 (metres) |                   |
| q b-a = 0 (pcu/hr)    |                   |
| q b-c = 264 (pcu/hr)  |                   |

### GEOMETRIC FACTORS :

|             |              |                            |
|-------------|--------------|----------------------------|
| D = 0.53322 | Q b-a = 242  | TOTAL FLOW = 1078 (PCU/HR) |
| E = 1.01663 | Q b-c = 581  |                            |
| F = 0.58595 | Q c-b = 326  |                            |
| Y = 0.63775 | Q b-ac = 581 |                            |

### THE CAPACITY OF MOVEMENT :

|              |                 |
|--------------|-----------------|
| Q b-a = 242  | Q b-c (O) = 581 |
| Q b-c = 581  |                 |
| Q c-b = 326  |                 |
| Q b-ac = 581 |                 |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                               |
|-------------------------------|
| DFC b-a = 0.0000              |
| DFC b-c = 0.4544              |
| DFC c-b = 0.0000              |
| DFC b-c (share lane) = 0.4544 |

**CRITICAL DFC = 0.45**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J4 Chatham Road South / Observatory Road

# PRIORITY JUNCTION CALCULATION

INITIALS

DATE

Sep-25

SKL

PREPARED BY:

Sep-25

SLN

CHECKED BY:

Sep-25

SLN

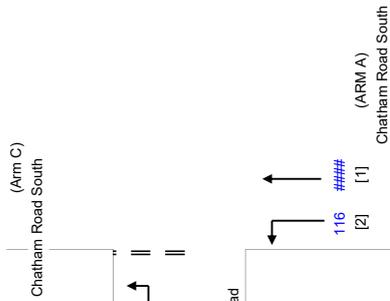
REVIEWED BY:

## 2033 Design PM

PROJECT NO.: 41000

FILENAME: J4\_CRS\_OR

REFERENCE NO.:



### NOTES : ( GEOMETRIC INPUT DATA )

- W = MAJOR ROAD WIDTH
- W cr = CENTRAL RESERVE WIDTH
- W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a
- W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c
- W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b
- V l b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a
- V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a
- V l b-c = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-c
- V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c
- V l c-b = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM c-b
- V r c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b
- D = STREAM-SPECIFIC B-A
- E = STREAM-SPECIFIC B-C
- F = STREAM-SPECIFIC C-B
- Y = (1-0.0345W)

### GEOMETRIC DETAILS:

#### MAJOR ROAD (ARM A)

W = 10.50 (metres)  
 W cr = 0 (metres)  
 q a-b = 116 (pcu/hr)  
 q a-c = 1018 (pcu/hr)

#### MAJOR ROAD (ARM C)

W c-b = 0.00 (metres)  
 V r c-b = 0 (metres)  
 q c-a = 0 (pcu/hr)  
 q c-b = 0 (pcu/hr)

#### MINOR ROAD (ARM B)

W b-a = 0.00 (metres)  
 W b-c = 4.70 (metres)  
 V l b-a = 0 (metres)  
 V r b-a = 0 (metres)  
 V l b-c = 37 (metres)  
 V r b-c = 0 (metres)  
 q b-a = 0 (pcu/hr)  
 q b-c = 399 (pcu/hr)

### GEOMETRIC FACTORS :

D = 0.53322  
 E = 1.01663  
 F = 0.58595  
 Y = 0.63775

F for (Qb-ac) = 1

### THE CAPACITY OF MOVEMENT :

Q b-a = 203  
 Q b-c = 506  
 Q c-b = 282  
 Q b-ac = 506

TOTAL FLOW = 1533 (PCU/HR)

### COMPARISON OF DESIGN FLOW TO CAPACITY:

DFC b-a = 0.0000  
 DFC b-c = 0.7885  
 DFC c-b = 0.0000  
 DFC b-c (share lane) = 0.7885

**CRITICAL DFC = 0.79**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J5 Kimberley Road / Observatory Road

# PRIORITY JUNCTION CALCULATION

**2033 Reference AM**

PROJECT NO.: 41000  
 FILENAME: J5\_KR\_OR.xls  
 REFERENCE NO.:

INITIALS

DATE

PREPARED BY: SKL

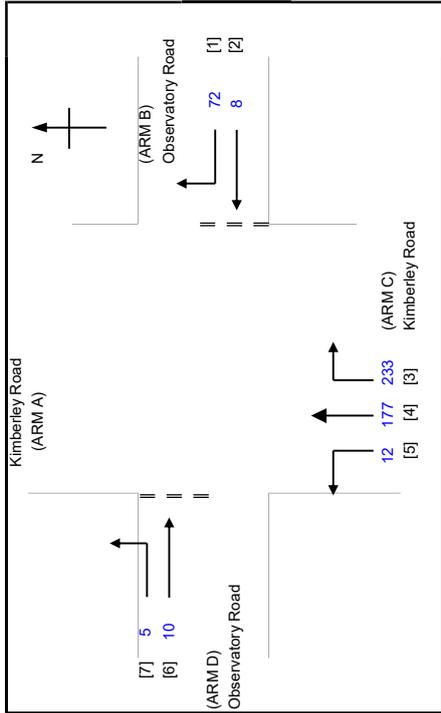
Sep-25

CHECKED BY: SLN

Sep-25

REVIEWED BY: SLN

Sep-25



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH  
 W cr = CENTRAL RESERVE WIDTH  
 W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a  
 W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c  
 W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b  
 V b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a  
 V r-b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a  
 V r-b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
 V r-c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b  
 X a = STREAM-SPECIFIC (RIGHT TURN FROM A)  
 X b = STREAM-SPECIFIC (RIGHT TURN FROM B)  
 Z b = STREAM-SPECIFIC (LEFT TURN FROM B)  
 M b = STREAM-SPECIFIC (STRAIGHT AHEAD FROM B - LEFT LANE)  
 Y = (1-0.0345W)  
 r b-a = RATIO OF FLOW TO CAPACITY IN STREAM b-a

## GEOMETRIC DETAILS:

|                    |   |      |          |                    |                 |
|--------------------|---|------|----------|--------------------|-----------------|
| GENERAL            |   |      |          |                    |                 |
| W                  | = | 7.4  | (metres) |                    |                 |
| W cr               | = | 0    | (metres) | Y                  | = 0.745         |
| MAJOR ROAD (ARM A) |   |      |          | MAJOR ROAD (ARM C) |                 |
| W a-d              | = | 0.00 | (metres) | W c-b              | = 3.10 (metres) |
| V r-a-d            | = | 0    | (metres) | V r-c-b            | = 22 (metres)   |
| q a-b              | = | 0    | (pcu/hr) | q c-a              | = 177 (pcu/hr)  |
| q a-c              | = | 0    | (pcu/hr) | q c-b              | = 233 (pcu/hr)  |
| q a-d              | = | 0    | (pcu/hr) | q c-d              | = 12 (pcu/hr)   |
| MINOR ROAD (ARM B) |   |      |          | MINOR ROAD (ARM D) |                 |
| W b-a              | = | 5.00 | (metres) | W d-c              | = 0.00 (metres) |
| W b-c              | = | 0.00 | (metres) | W d-a              | = 3.00 (metres) |
| V l-b-a            | = | 23   | (metres) | V l-d-c            | = 0 (metres)    |
| V r-b-a            | = | 100  | (metres) | V r-d-a            | = 0 (metres)    |
| q b-a              | = | 72   | (pcu/hr) | q d-c              | = 0 (pcu/hr)    |
| q b-c              | = | 0    | (pcu/hr) | q d-a              | = 5 (pcu/hr)    |
| q b-d              | = | 8    | (pcu/hr) | q d-b              | = 10 (pcu/hr)   |

## GEOMETRIC FACTORS :

|  |   |        |         |              |              |
|--|---|--------|---------|--------------|--------------|
| X b  | = | 1.022  | X a     | =            | 0.586        |
| X c  | = | 0.865  | X d     | =            | 0.533        |
| Z b  | = | 0.586  | Z d     | =            | 0.857        |
| M b  | = | 0.541  | M d     | =            | 0.780        |
| PROPORTION OF MINOR STRAIGHT AHEAD TRAFFIC : |   |        |         |              |              |
| r b-a  | = | 0.2687 | r d-c   | =            | 0.000        |
| q l b-d                                      | = | 5.0746 | q l d-b | =            | 5 (pcu/hr)   |
| q r b-d                                      | = | 2.9254 | q r d-b | =            | 5 (pcu/hr)   |
| CAPACITY OF MOVEMENT :                       |   |        |         |              |              |
| Q b-a  | = | 514    | Q d-c   | =            | 268 (pcu/hr) |
| Q b-c  | = | 407    | Q d-a   | =            | 596 (pcu/hr) |
| Q c-b  | = | 644    | Q a-d   | =            | 354 (pcu/hr) |
| Q l b-d                                      | = | 273    | Q l d-b | =            | 401 (pcu/hr) |
| Q r b-d                                      | = | 516    | Q r d-b | =            | 274 (pcu/hr) |
| Q b-acd                                      | = | 514    | Q d-abc | =            | 328 (pcu/hr) |
|  |   |        |         | TOTAL FLOW = | 517 (PCU/HR) |

## COMPARISON OF DESIGN FLOW TO CAPACITY:

|                         |   |        |
|-------------------------|---|--------|
| DFC b-a                 | = | 0.1401 |
| DFC b-c                 | = | 0.0000 |
| DFC c-b                 | = | 0.3618 |
| DFCI b-d                | = | 0.0186 |
| DFCr b-d                | = | 0.0057 |
| DFC d-c                 | = | 0.0000 |
| DFC d-a                 | = | 0.0084 |
| DFC a-d                 | = | 0.0000 |
| DFCI d-b                | = | 0.0125 |
| DFCr d-b                | = | 0.0182 |
| DFC b-acd (shared lane) | = | 0.1556 |
| DFC d-abc (shared lane) | = | 0.0457 |

**CRITICAL DFC = 0.36**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J5 Kimberley Road / Observatory Road

# PRIORITY JUNCTION CALCULATION

**2033 Reference PM**

PROJECT NO.: 41000  
 FILENAME: J5\_KR\_OR\_xlsx  
 REFERENCE NO.:

INITIALS

DATE

PREPARED BY: SKL

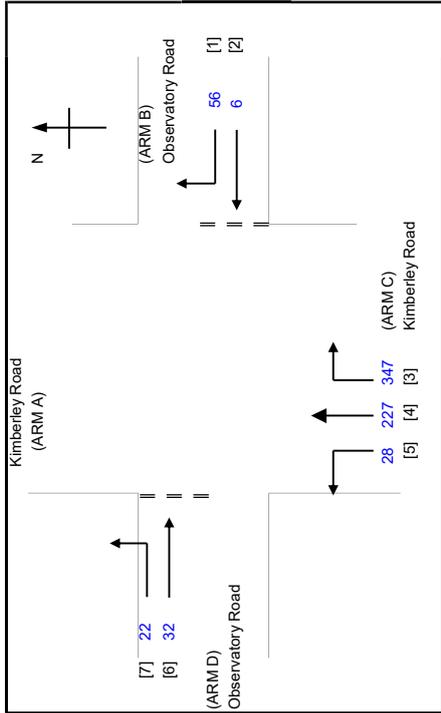
Sep-25

CHECKED BY: SLN

Sep-25

REVIEWED BY: SLN

Sep-25



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH  
 W cr = CENTRAL RESERVE WIDTH  
 W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a  
 W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c  
 W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b  
 V b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a  
 V r-b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a  
 V r-b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
 V r-c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b  
 X a = STREAM-SPECIFIC (RIGHT TURN FROM A)  
 X b = STREAM-SPECIFIC (RIGHT TURN FROM B)  
 Z b = STREAM-SPECIFIC (LEFT TURN FROM B)  
 M b = STREAM-SPECIFIC (STRAIGHT AHEAD FROM B - LEFT LANE)  
 Y = (1-0.0345W)  
 r b-a = RATIO OF FLOW TO CAPACITY IN STREAM b-a

## GEOMETRIC DETAILS:

|                        |                       |           |
|------------------------|-----------------------|-----------|
| GENERAL                |                       | Y = 0.745 |
| W a-d = 7.4 (metres)   | W c-b = 3.10 (metres) |           |
| W cr = 0 (metres)      | V r-c-b = 22 (metres) |           |
| MAJOR ROAD (ARM A)     | q a-b = 0 (pcu/hr)    |           |
| W a-d = 0.00 (metres)  | q a-c = 0 (pcu/hr)    |           |
| V r-a-d = 0 (metres)   | q a-d = 0 (pcu/hr)    |           |
| MINOR ROAD (ARM B)     | W d-c = 0.00 (metres) |           |
| W b-c = 5.00 (metres)  | W d-a = 3.00 (metres) |           |
| V l-b-a = 23 (metres)  | V r-d-c = 0 (metres)  |           |
| V r-b-a = 100 (metres) | V r-d-a = 0 (metres)  |           |
| q b-a = 56 (pcu/hr)    | q d-c = 0 (pcu/hr)    |           |
| q b-c = 0 (pcu/hr)     | q d-a = 22 (pcu/hr)   |           |
| q b-d = 6 (pcu/hr)     | q d-b = 32 (pcu/hr)   |           |

## GEOMETRIC FACTORS :

|  |                        |
|--|------------------------|
| X b = 1.022                                  | X a = 0.586            |
| X c = 0.865                                  | X d = 0.533            |
| Z b = 0.586                                  | Z d = 0.857            |
| M b = 0.541                                  | M d = 0.780            |
| PROPORTION OF MINOR STRAIGHT AHEAD TRAFFIC : |                        |
| r b-a = 0.2286                               | r d-c = 0.000          |
| q l b-d = 3.6857 (pcu/hr)                    | q l d-b = 16 (pcu/hr)  |
| q r b-d = 2.3143 (pcu/hr)                    | q r d-b = 16 (pcu/hr)  |
| CAPACITY OF MOVEMENT :                       |                        |
| Q b-a = 449 (pcu/hr)                         | Q d-c = 245 (pcu/hr)   |
| Q b-c = 412 (pcu/hr)                         | Q d-a = 583 (pcu/hr)   |
| Q c-b = 644 (pcu/hr)                         | Q a-d = 317 (pcu/hr)   |
| Q l b-d = 243 (pcu/hr)                       | Q l d-b = 365 (pcu/hr) |
| Q r b-d = 459 (pcu/hr)                       | Q r d-b = 250 (pcu/hr) |
| Q b-acd = 449 (pcu/hr)                       | Q d-abc = 321 (pcu/hr) |
| TOTAL FLOW = 718 (PCU/HR)                    |                        |

## COMPARISON OF DESIGN FLOW TO CAPACITY:

|                                  |
|----------------------------------|
| DFC b-a = 0.1247                 |
| DFC b-c = 0.0000                 |
| DFC c-b = 0.5388                 |
| DFCI b-d = 0.0152                |
| DFCr b-d = 0.0050                |
| DFC d-c = 0.0000                 |
| DFC d-a = 0.0377                 |
| DFC a-d = 0.0000                 |
| DFCI d-b = 0.0438                |
| DFCr d-b = 0.0640                |
| DFC b-acd (shared lane) = 0.1381 |
| DFC d-abc (shared lane) = 0.1683 |

**CRITICAL DFC = 0.54**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J5 Kimberley Road / Observatory Road

# PRIORITY JUNCTION CALCULATION

## 2033 Design AM

PROJECT NO.: 41000

FILENAME: J5\_KR\_OR\_xlsx

REFERENCE NO.:

INITIALS

DATE

PREPARED BY: SKL

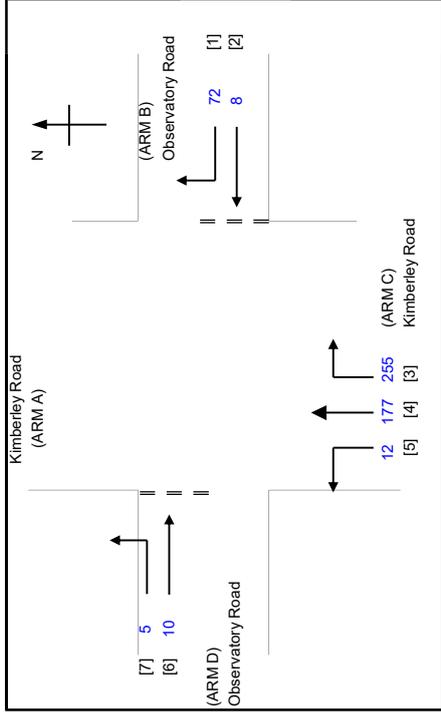
Sep-25

CHECKED BY: SLN

Sep-25

REVIEWED BY: SLN

Sep-25



NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH  
W cr = CENTRAL RESERVE WIDTH  
W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a  
W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c  
W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b  
V b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a  
V r-b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a  
V r-b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
V r-c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM c-b  
X a = STREAM-SPECIFIC (RIGHT TURN FROM A)  
X b = STREAM-SPECIFIC (RIGHT TURN FROM B)  
Z b = STREAM-SPECIFIC (LEFT TURN FROM B)  
M b = STREAM-SPECIFIC (STRAIGHT AHEAD FROM B - LEFT LANE)  
Y = (1-0.0345W)  
r b-a = RATIO OF FLOW TO CAPACITY IN STREAM b-a

### GEOMETRIC DETAILS:

|                    |   |      |          |                    |                 |
|--------------------|---|------|----------|--------------------|-----------------|
| GENERAL            |   |      |          |                    |                 |
| W                  | = | 7.4  | (metres) |                    |                 |
| W cr               | = | 0    | (metres) | Y                  | = 0.745         |
| MAJOR ROAD (ARM A) |   |      |          | MAJOR ROAD (ARM C) |                 |
| W a-d              | = | 0.00 | (metres) | W c-b              | = 3.10 (metres) |
| V r-a-d            | = | 0    | (metres) | V r-c-b            | = 22 (metres)   |
| q a-b              | = | 0    | (pcu/hr) | q c-a              | = 177 (pcu/hr)  |
| q a-c              | = | 0    | (pcu/hr) | q c-b              | = 255 (pcu/hr)  |
| q a-d              | = | 0    | (pcu/hr) | q c-d              | = 12 (pcu/hr)   |
| MINOR ROAD (ARM B) |   |      |          | MINOR ROAD (ARM D) |                 |
| W b-a              | = | 5.00 | (metres) | W d-c              | = 0.00 (metres) |
| W b-c              | = | 0.00 | (metres) | W d-a              | = 3.00 (metres) |
| V l-b-a            | = | 23   | (metres) | V l-d-c            | = 0 (metres)    |
| V r-b-a            | = | 100  | (metres) | V r-d-a            | = 0 (metres)    |
| q b-a              | = | 72   | (pcu/hr) | q d-c              | = 0 (pcu/hr)    |
| q b-c              | = | 0    | (pcu/hr) | q d-a              | = 5 (pcu/hr)    |
| q b-d              | = | 8    | (pcu/hr) | q d-b              | = 10 (pcu/hr)   |

### GEOMETRIC FACTORS :

|     |   |       |     |   |       |
|-----|---|-------|-----|---|-------|
| X b | = | 1.022 | X a | = | 0.586 |
| X c | = | 0.865 | X d | = | 0.533 |
| Z b | = | 0.586 | Z d | = | 0.857 |
| M b | = | 0.541 | M d | = | 0.780 |

### PROPORTION OF MINOR STRAIGHT AHEAD TRAFFIC :

|         |   |        |         |   |            |
|---------|---|--------|---------|---|------------|
| r b-a   | = | 0.2717 | r d-c   | = | 0.000      |
| q l b-d | = | 5.0868 | q l d-b | = | 5 (pcu/hr) |
| q r b-d | = | 2.9132 | q r d-b | = | 5 (pcu/hr) |

### CAPACITY OF MOVEMENT :

|              |   |     |          |         |   |     |          |
|--------------|---|-----|----------|---------|---|-----|----------|
| Q b-a        | = | 505 | (pcu/hr) | Q d-c   | = | 265 | (pcu/hr) |
| Q b-c        | = | 407 | (pcu/hr) | Q d-a   | = | 596 | (pcu/hr) |
| Q c-b        | = | 644 | (pcu/hr) | Q a-d   | = | 349 | (pcu/hr) |
| Q l b-d      | = | 268 | (pcu/hr) | Q l d-b | = | 397 | (pcu/hr) |
| Q r b-d      | = | 507 | (pcu/hr) | Q r d-b | = | 271 | (pcu/hr) |
| Q b-acd      | = | 505 | (pcu/hr) | Q d-abc | = | 325 | (pcu/hr) |
| TOTAL FLOW = |   | 539 |          | PCU/HR  |   |     |          |

### COMPARISON OF DESIGN FLOW TO CAPACITY:

|                         |   |        |
|-------------------------|---|--------|
| DFC b-a                 | = | 0.1426 |
| DFC b-c                 | = | 0.0000 |
| DFC c-b                 | = | 0.3960 |
| DFCI b-d                | = | 0.0190 |
| DFCr b-d                | = | 0.0057 |
| DFC d-c                 | = | 0.0000 |
| DFC d-a                 | = | 0.0084 |
| DFC a-d                 | = | 0.0000 |
| DFCI d-b                | = | 0.0126 |
| DFCr d-b                | = | 0.0185 |
| DFC b-acd (shared lane) | = | 0.1584 |
| DFC d-abc (shared lane) | = | 0.0461 |

**CRITICAL DFC = 0.40**

# LLA CONSULTANCY LIMITED

Section 16 Planning Application for Proposed Hotel at 16 Kimberley Road, Tsim Sha Tsui

J5 Kimberley Road / Observatory Road

# PRIORITY JUNCTION CALCULATION

**2033 Design PM**

PROJECT NO.: 41000

FILENAME: J5\_KR\_OR\_xlsx

REFERENCE NO.:

INITIALS

SKL

SLN

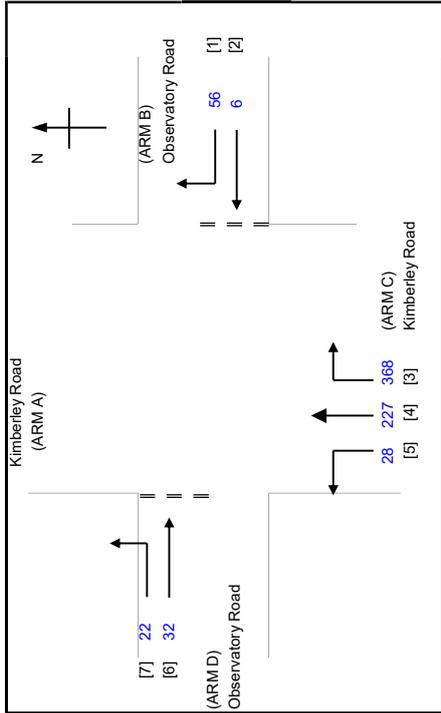
SLN

DATE

Sep-25

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NOTES : ( GEOMETRIC INPUT DATA )

W = MAJOR ROAD WIDTH  
W cr = CENTRAL RESERVE WIDTH  
W b-a = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-a  
W b-c = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM b-c  
W c-b = LANE WIDTH AVAILABLE TO VEHICLE WAITING IN STREAM c-b  
V b-a = VISIBILITY TO THE LEFT FOR VEHICLES WAITING IN STREAM b-a  
V r b-a = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-a  
V r b-c = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
V r c-b = VISIBILITY TO THE RIGHT FOR VEHICLES WAITING IN STREAM b-c  
X a = STREAM-SPECIFIC (RIGHT TURN FROM A)  
X b = STREAM-SPECIFIC (RIGHT TURN FROM B)  
Z b = STREAM-SPECIFIC (LEFT TURN FROM B)  
M b = STREAM-SPECIFIC (STRAIGHT AHEAD FROM B - LEFT LANE)  
Y = (1-0.0345W)  
r b-a = RATIO OF FLOW TO CAPACITY IN STREAM b-a

## GEOMETRIC DETAILS:

|                    |   |      |          |         |                 |
|--------------------|---|------|----------|---------|-----------------|
| GENERAL            |   |      |          |         |                 |
| W                  | = | 7.4  | (metres) |         |                 |
| W cr               | = | 0    | (metres) | Y       | = 0.745         |
| MAJOR ROAD (ARM A) |   |      |          |         |                 |
| W a-d              | = | 0.00 | (metres) | W c-b   | = 3.10 (metres) |
| V r a-d            | = | 0    | (metres) | V r c-b | = 22 (metres)   |
| q a-b              | = | 0    | (pcu/hr) | q c-a   | = 227 (pcu/hr)  |
| q a-c              | = | 0    | (pcu/hr) | q c-b   | = 368 (pcu/hr)  |
| q a-d              | = | 0    | (pcu/hr) | q c-d   | = 28 (pcu/hr)   |
| MINOR ROAD (ARM B) |   |      |          |         |                 |
| W b-a              | = | 5.00 | (metres) | W d-c   | = 0.00 (metres) |
| W b-c              | = | 0.00 | (metres) | W d-a   | = 3.00 (metres) |
| V l b-a            | = | 23   | (metres) | V l d-c | = 0 (metres)    |
| V r b-a            | = | 100  | (metres) | V r d-c | = 0 (metres)    |
| V r b-c            | = | 0    | (metres) | V r d-a | = 23 (metres)   |
| q b-a              | = | 56   | (pcu/hr) | q d-c   | = 0 (pcu/hr)    |
| q b-c              | = | 0    | (pcu/hr) | q d-a   | = 22 (pcu/hr)   |
| q b-d              | = | 6    | (pcu/hr) | q d-b   | = 32 (pcu/hr)   |

## GEOMETRIC FACTORS :

|  |   |        |         |              |              |
|--|---|--------|---------|--------------|--------------|
| X b  | = | 1.022  | X a     | =            | 0.586        |
| X c  | = | 0.865  | X d     | =            | 0.533        |
| Z b  | = | 0.586  | Z d     | =            | 0.857        |
| M b  | = | 0.541  | M d     | =            | 0.780        |
| PROPORTION OF MINOR STRAIGHT AHEAD TRAFFIC : |   |        |         |              |              |
| r b-a  | = | 0.2314 | r d-c   | =            | 0.000        |
| q l b-d                                      | = | 3.6942 | q l d-b | =            | 16 (pcu/hr)  |
| q r b-d                                      | = | 2.3058 | q r d-b | =            | 16 (pcu/hr)  |
| CAPACITY OF MOVEMENT :                       |   |        |         |              |              |
| Q b-a  | = | 441    | Q d-c   | =            | 242 (pcu/hr) |
| Q b-c  | = | 411    | Q d-a   | =            | 583 (pcu/hr) |
| Q c-b  | = | 644    | Q a-d   | =            | 313 (pcu/hr) |
| Q l b-d                                      | = | 239    | Q l d-b | =            | 361 (pcu/hr) |
| Q r b-d                                      | = | 451    | Q r d-b | =            | 247 (pcu/hr) |
| Q b-acd                                      | = | 441    | Q d-abc | =            | 318 (pcu/hr) |
|  |   |        |         | TOTAL FLOW = | 739 (PCU/HR) |

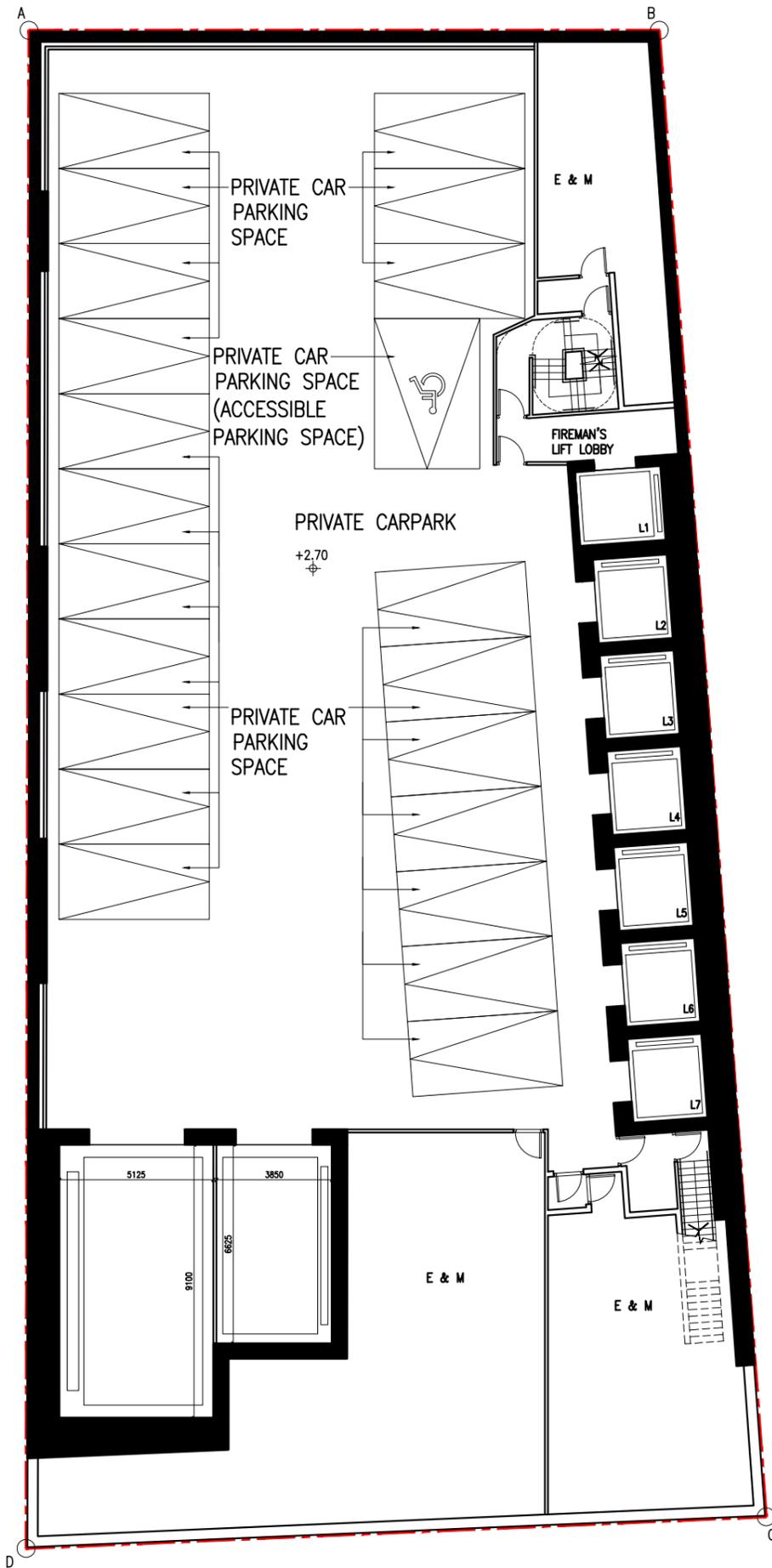
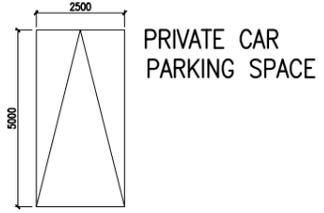
## COMPARISON OF DESIGN FLOW TO CAPACITY:

|                         |   |        |
|-------------------------|---|--------|
| DFC b-a                 | = | 0.1270 |
| DFC b-c                 | = | 0.0000 |
| DFC c-b                 | = | 0.5714 |
| DFCI b-d                | = | 0.0155 |
| DFCr b-d                | = | 0.0051 |
| DFC d-c                 | = | 0.0000 |
| DFC d-a                 | = | 0.0377 |
| DFC a-d                 | = | 0.0000 |
| DFCI d-b                | = | 0.0443 |
| DFCr d-b                | = | 0.0648 |
| DFC b-acd (shared lane) | = | 0.1406 |
| DFC d-abc (shared lane) | = | 0.1700 |

**CRITICAL DFC = 0.57**

**Appendix C**  
**Car Park Layout Plan**

**LEGEND:**



SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL WITH MINOR RELAXATION OF PLOT RATIO AND BUILDING HEIGHT RESTRICTIONS AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, KOWLOON



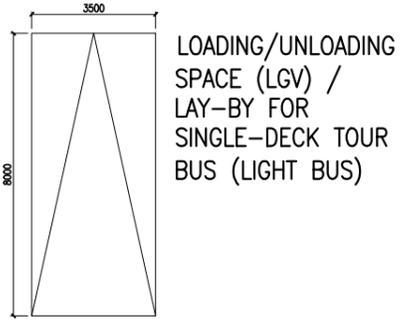
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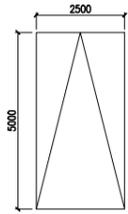
DRAWING / 圖名  
B2 FLOOR PLAN

DRAWING NUMBER / 圖號  
SK-02

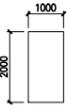
**LEGEND:**



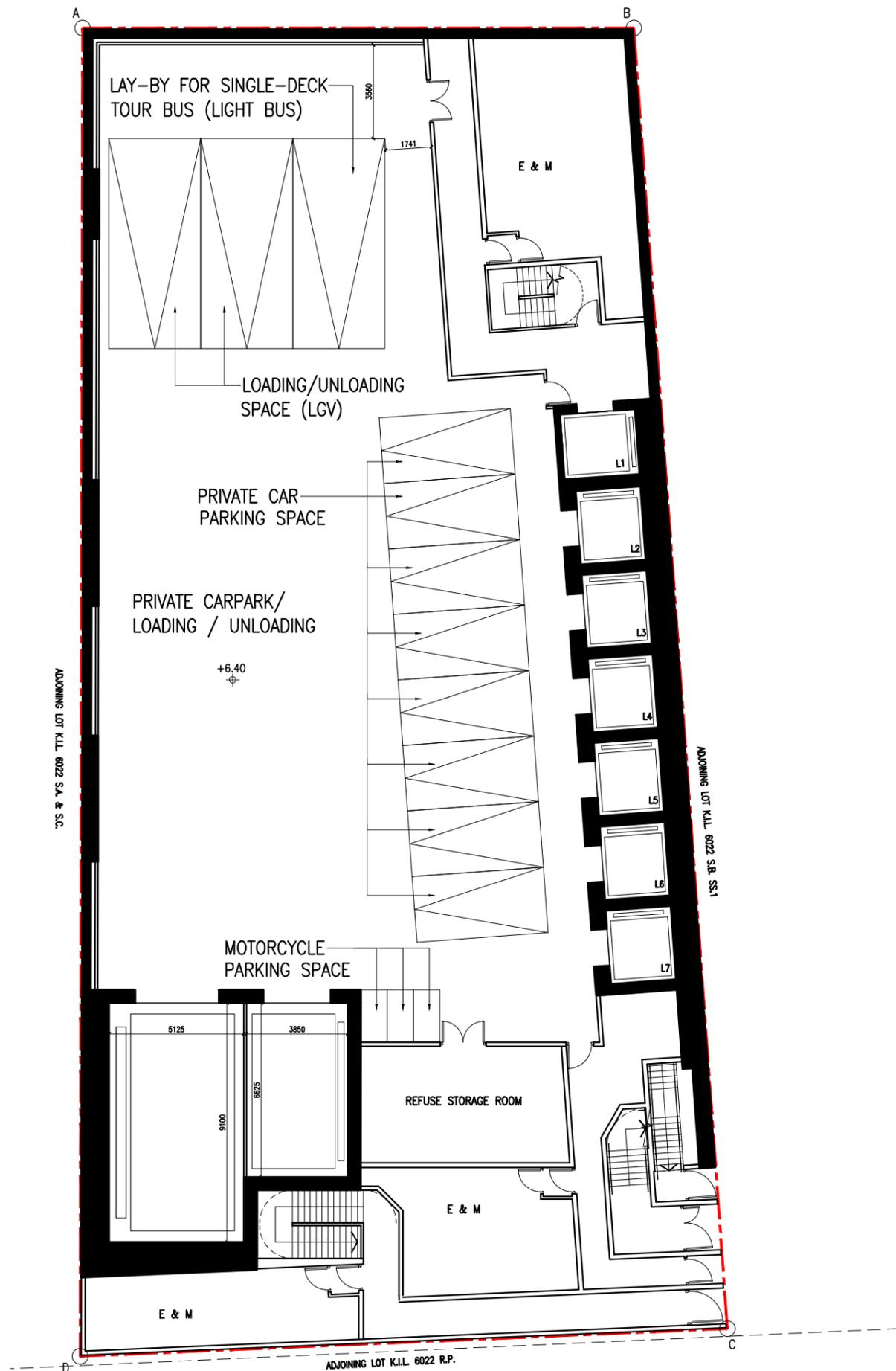
LOADING/UNLOADING SPACE (LGV) / LAY-BY FOR SINGLE-DECK TOUR BUS (LIGHT BUS)



PRIVATE CAR PARKING SPACE



MOTORCYCLE PARKING SPACE



SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL WITH MINOR RELAXATION OF PLOT RATIO AND BUILDING HEIGHT RESTRICTIONS AT 16 KIMBERLEY ROAD, TSIM SHA TSUI, KOWLOON



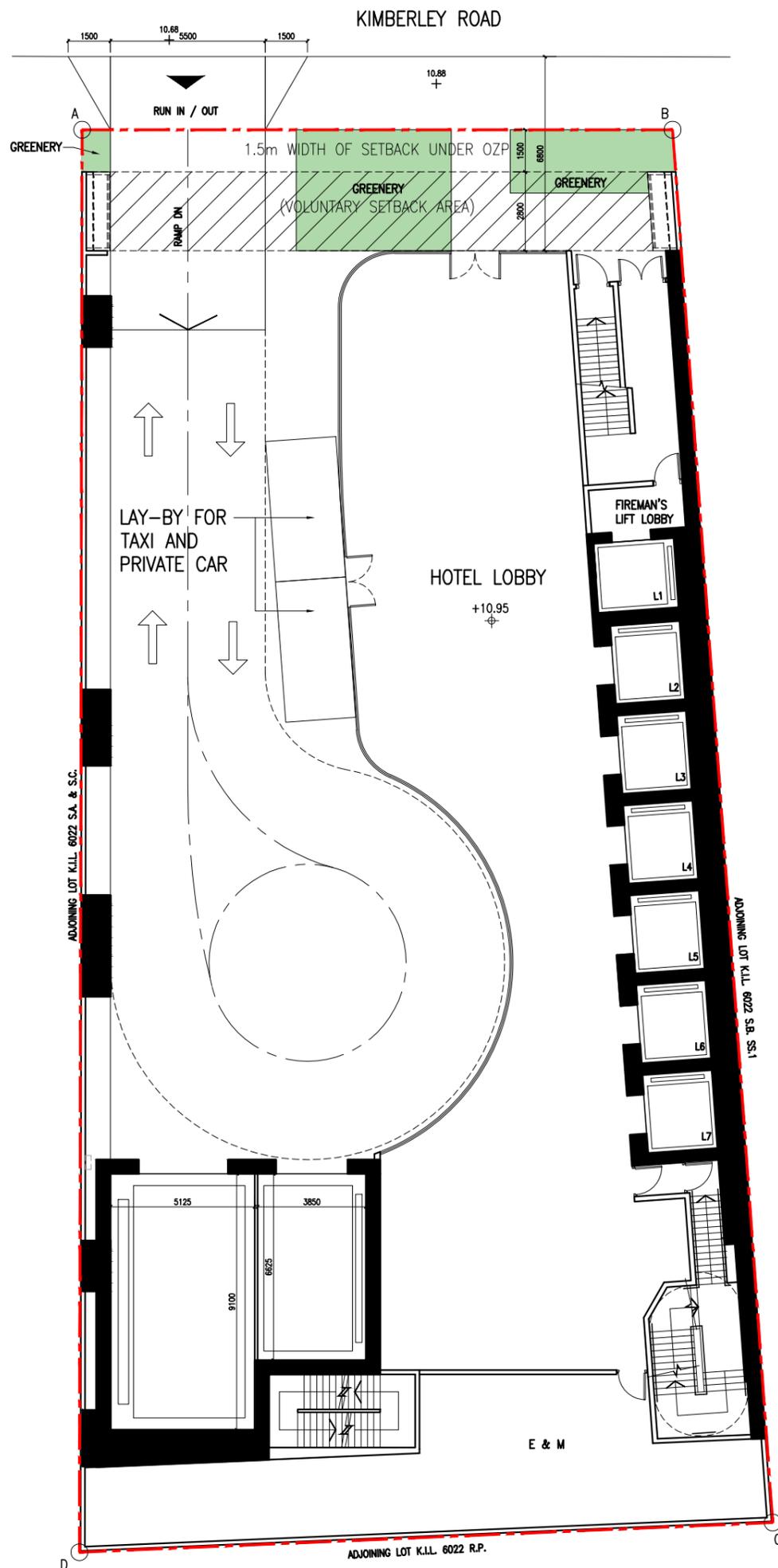
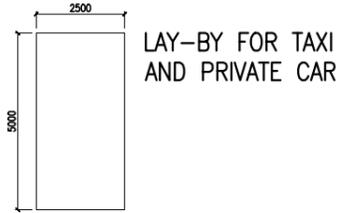
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DRAWING / 圖名  
B1 FLOOR PLAN

DRAWING NUMBER / 圖號  
SK-03

**LEGEND:**



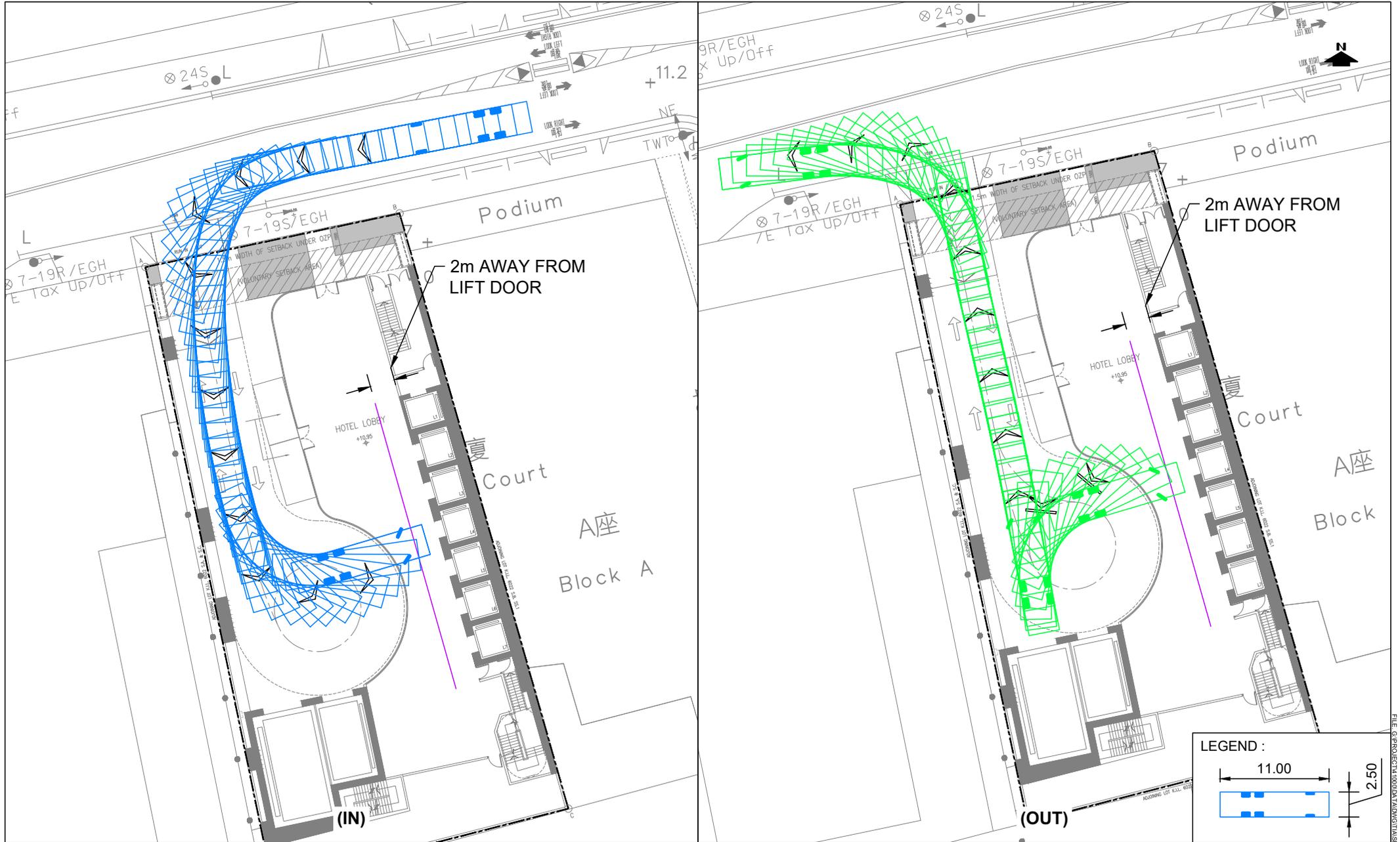
SECTION 16 PLANNING APPLICATION FOR PROPOSED HOTEL WITH MINOR RELAXATION OF PLOT RATIO AND BUILDING HEIGHT RESTRICTIONS AT 16 KIMBERLEY ROAD, TSM SHA TSUI, KOWLOON



## **Appendix D**

### **Swept Path Analysis**

**– To Demonstrate HGV Cannot Make a 3-point Turn Within the Site**



**SWEPT PATH ANALYSIS - HGV (G/F)**

(SCALE 1:400 @ A4)

**Appendix E**  
**Car Lift Assessment**

## APPENDIX E - CAR LIFT ANALYSIS

### Proposed New Non-domestic Building at 16 Kimberley Road, Tsim Sha Tsui

#### 1. Carpark Spaces Arrangement

|   |          |                     |                             |
|---|----------|---------------------|-----------------------------|
| No. of Carlift                              | [n]      | =                   | 2                           |
| No. of Parking Space(s) & Waiting Spaces(s) |          |                     |                             |
| G/F (+10.845m)                              | =        | 0 waiting spaces(s) |                             |
| B1/F (+6.295m)                              | =        | 0 waiting spaces(s) | + 14 parking space(s)       |
| B2/F (+2.595m)                              | =        | 0 waiting spaces(s) | + 22 parking space(s)       |
| <b>Total</b>                                | <b>=</b> |                     | <b>36 parking spaces(s)</b> |

#### 2. Arrival Rate Estimate

|   |     |                     |
|---|-----|---------------------|
| Peak Hour Arrival Rate  | =   | 25 veh/hr           |
| Peak Hour Arrival Rate - Car Park Oriented<br>(40% of the Peak Hour Arrival Rate)                                 | =   | 10 veh/hr           |
| <b>Peak 15-minute Arrival Rate - Car Park Oriented</b><br>(50% of the Peak Hour Arrival Rate - Car Park Oriented) | [λ] | <b>5 veh/15-min</b> |

#### 3. Estimate of Round Trip Time of Car Lift

|   |       |                |
|---|-------|----------------|
| Level Difference between G/F and parking floor (Weighted Average) | =     | 6.8 m          |
| Travelling Speed of the Car Lift                                  | =     | 0.5 m/s        |
| Weighted Average Travelling Time from G/F                         | =     | 13.6 s         |
| Door Open   | =     | 8.0 s          |
| Vehicle Out   | =     | 8.0 s          |
| Vehicle Enters  | =     | 8.0 s          |
| Safety Buffer   | =     | 5.0 s          |
| Door Close  | =     | 8.0 s          |
| Weighted Average Travelling Time from G/F                         | =     | 13.6 s         |
| Door Open   | =     | 8.0 s          |
| Vehicle Out   | =     | 8.0 s          |
| Vehicle Enters  | =     | 8.0 s          |
| Safety Buffer   | =     | 5.0 s          |
| Door Close  | =     | 8.0 s          |
| Weight Average Travelling Time to G/F                             | =     | 13.6 s         |
| Round Trip Time   | =     | 101.2 s        |
| <b>Total Round Trip Time</b>                                      | [1/μ] | <b>102.0 s</b> |

#### 4. Estimated Average Servicing Rate

|   |           |   |                 |
|---|-----------|---|-----------------|
| <b>Average Servicing Rate per Carlift</b>                 | [μ]       | = | 900s / 102      |
|   |           | = | 8.82 veh/15-min |
| <b>With 2 car lifts available, (M/M/N) model is used.</b> |           |   |                 |
| Peak 15-minute Arrival Rate - Car Park Oriented           | [λ]       | = | 5.00 veh/15-min |
| Traffic Intensity   | [ρ = λ/μ] | = | 5.00 / 8.82     |
|   |           | = | 0.5667          |

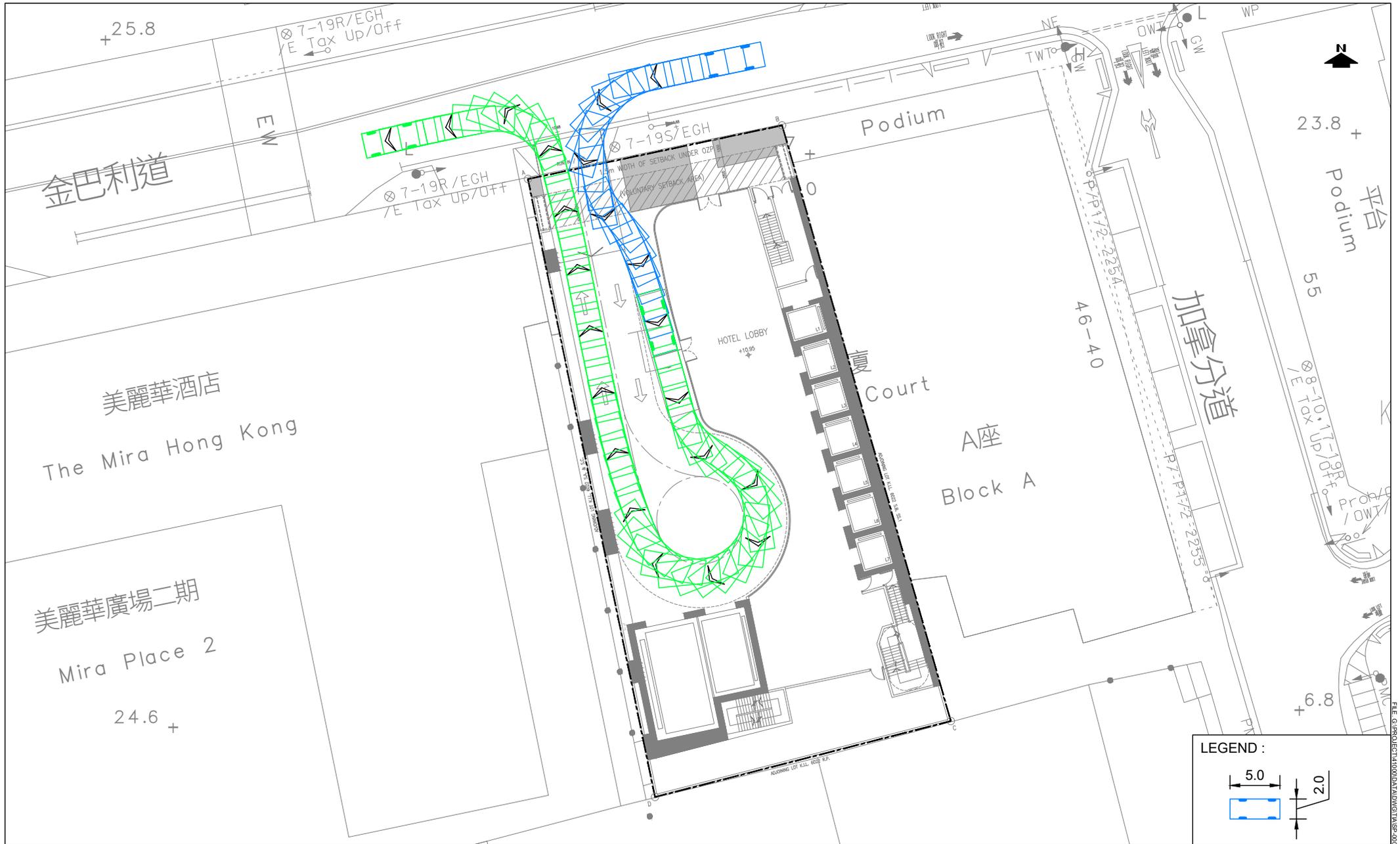
#### 5. Estimated Average Servicing Rate

|  |        |   |        |
|--|--------|---|--------|
| Probability of no vehicle in the system,                       | P(x=n) | = | 0.5584 |
| Probability of one car lift in use,                            |        | = | 0.3165 |
| Probability of two car lifts in use,                           |        | = | 0.0897 |
| Probability of two car lifts in use & waiting space is in use, |        | = | 0.0254 |

**Sum of P(x<=n) =** 0.5584 + 0.3165 + 0.0897 + 0.0254 = = 0.9900

**The chances that car park traffic will queue up on public road is less than =** 1 - 0.9900 = 1.0%

**Appendix F**  
**Swept Path Analysis**  
**– To Demonstrate the Feasibility of Vehicles Manoeuvring Within the Site**



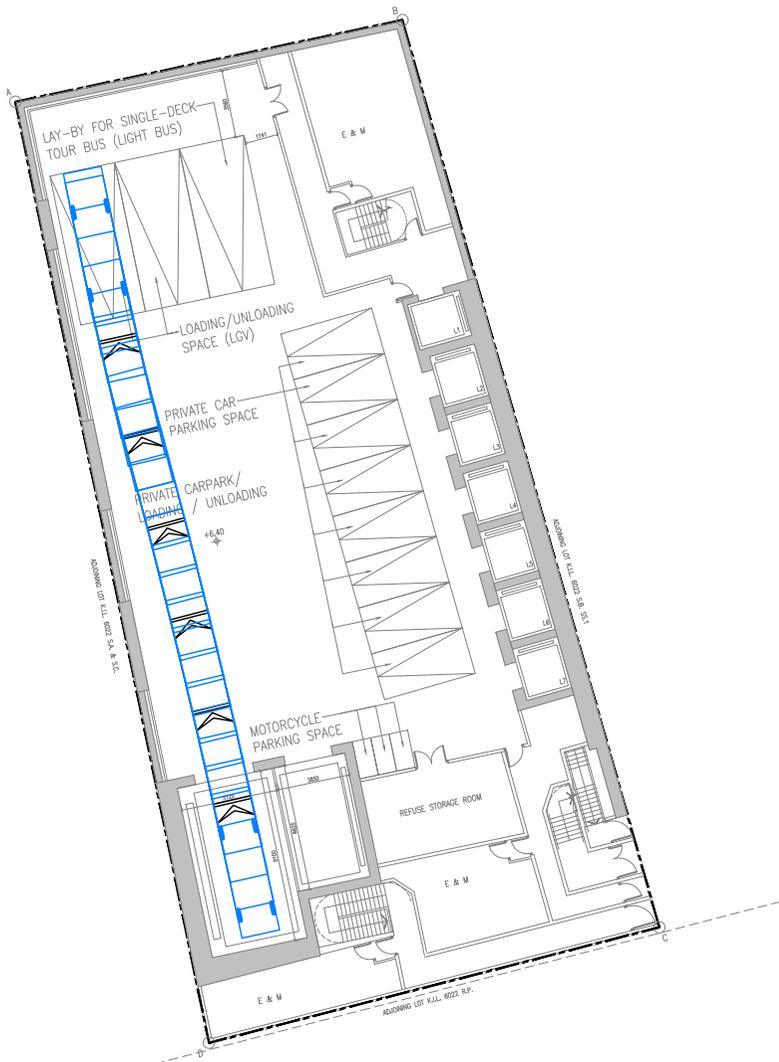
**SWEPT PATH ANALYSIS - PC (G/F) (1 OF 2)**

(SCALE 1:400 @ A4)

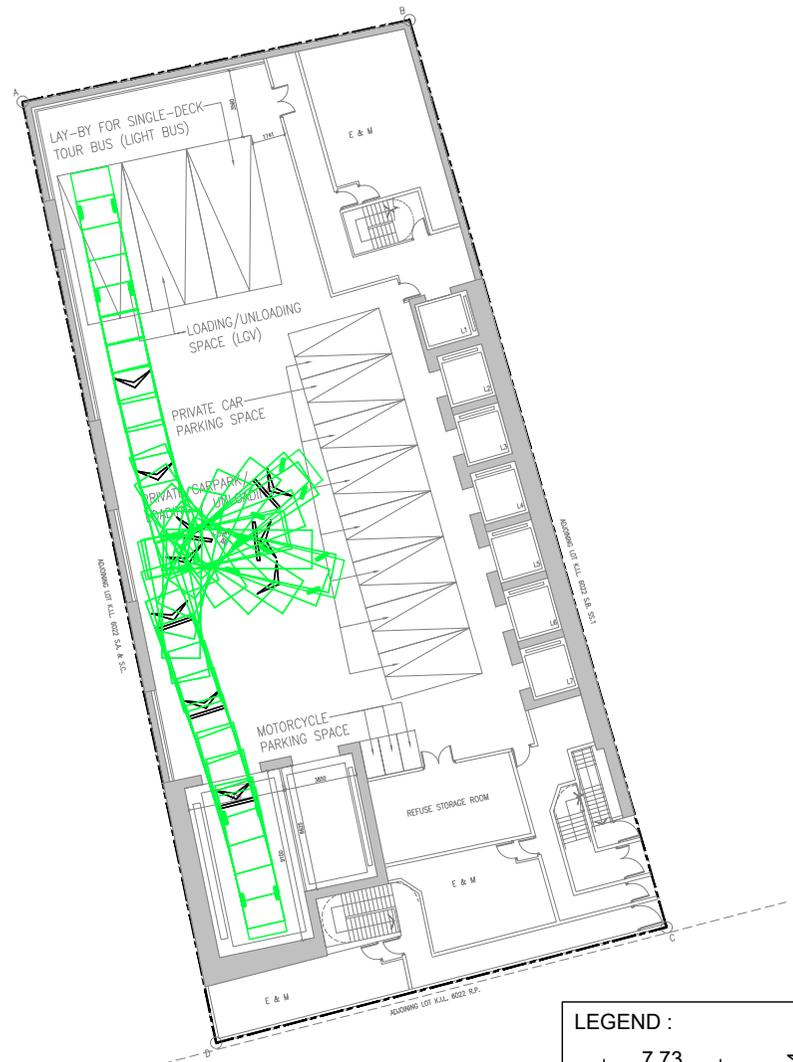


**SWEPT PATH ANALYSIS - 28 SEATERS (G/F) (2 OF 2)**

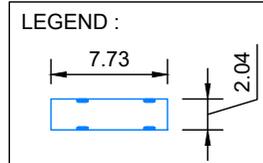
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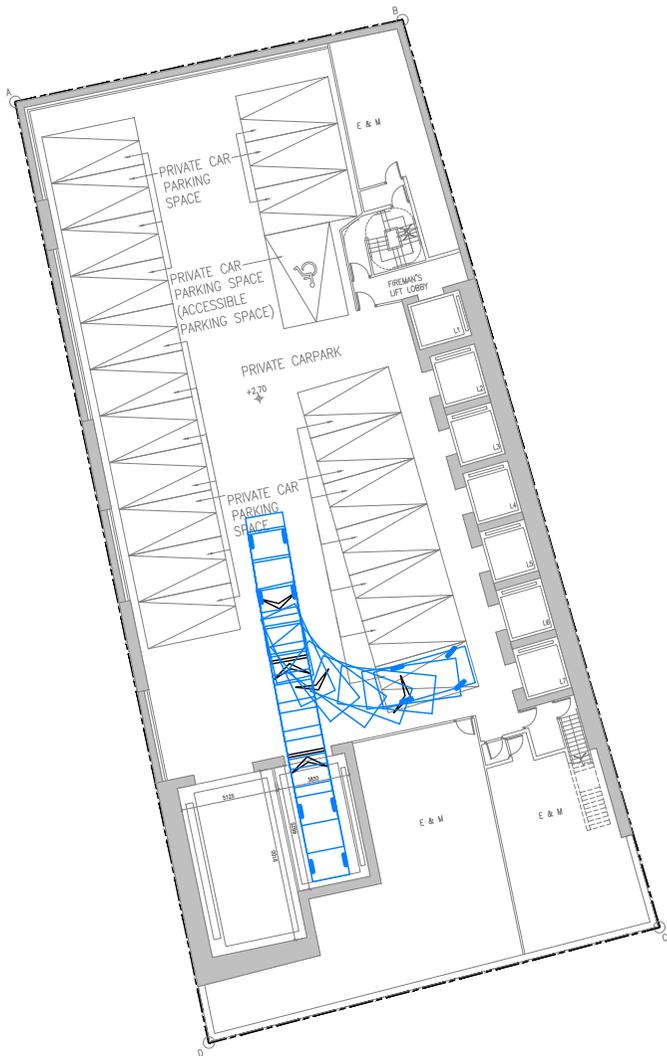


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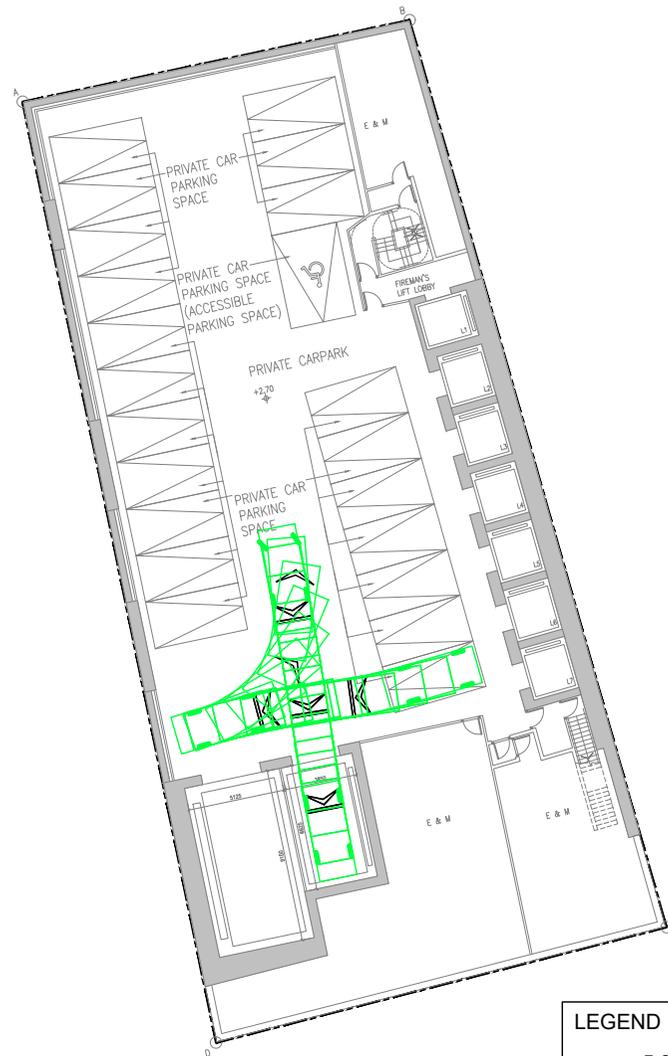


**SWEPT PATH ANALYSIS - 28 SEATERS (B1/F)**

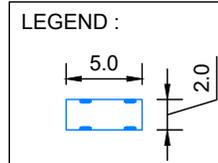
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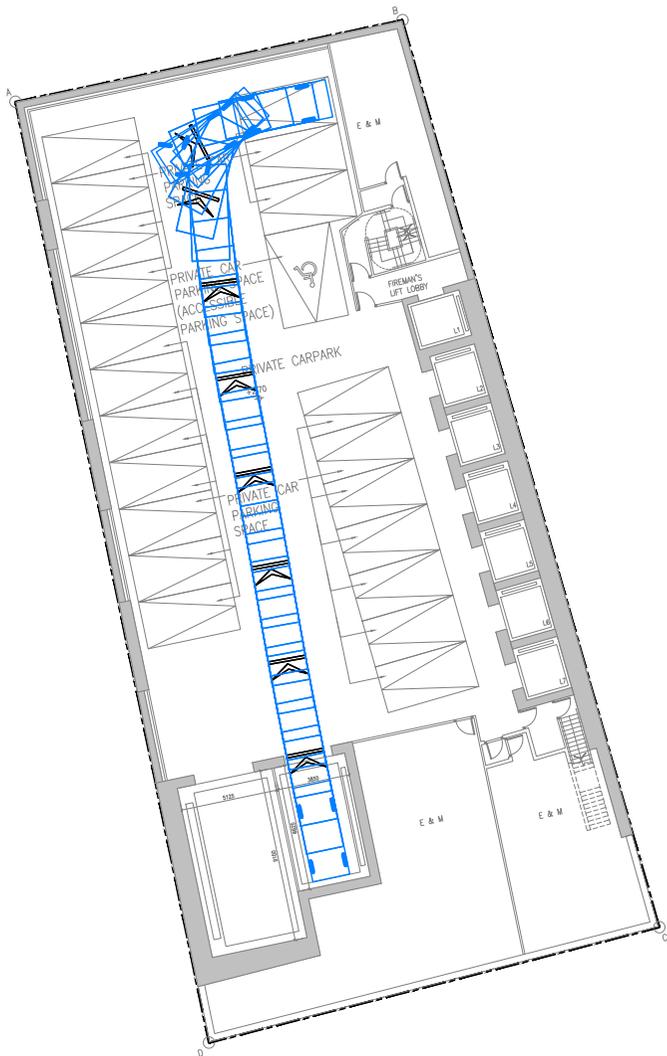
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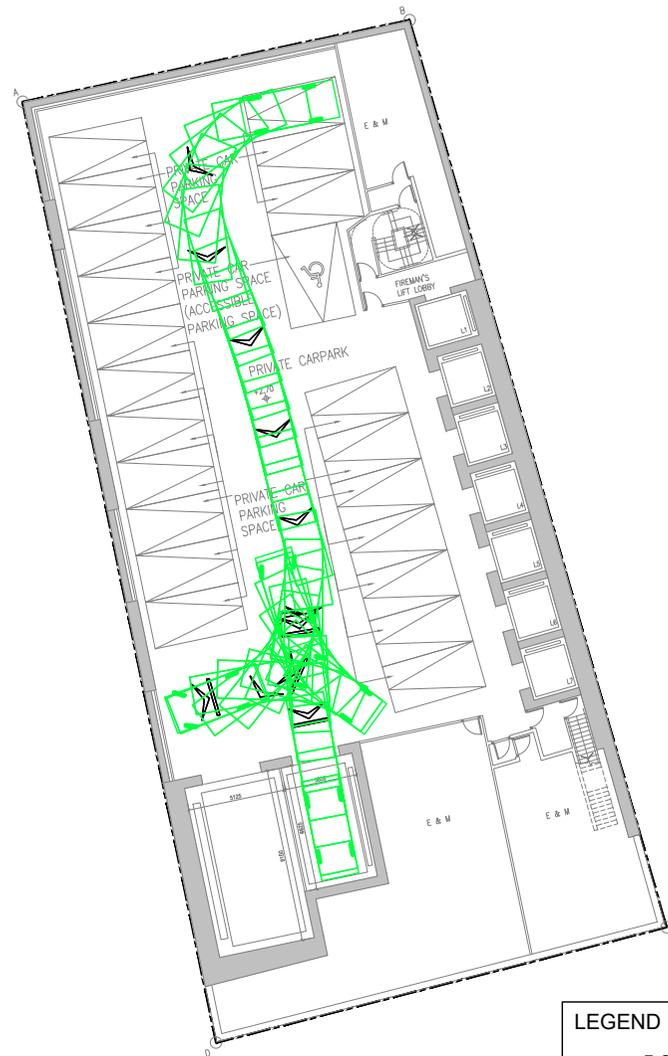
**SWEPT PATH ANALYSIS - PC (B2/F) (1 OF 3)**

(SCALE 1:400 @ A4)

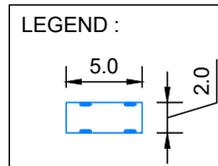




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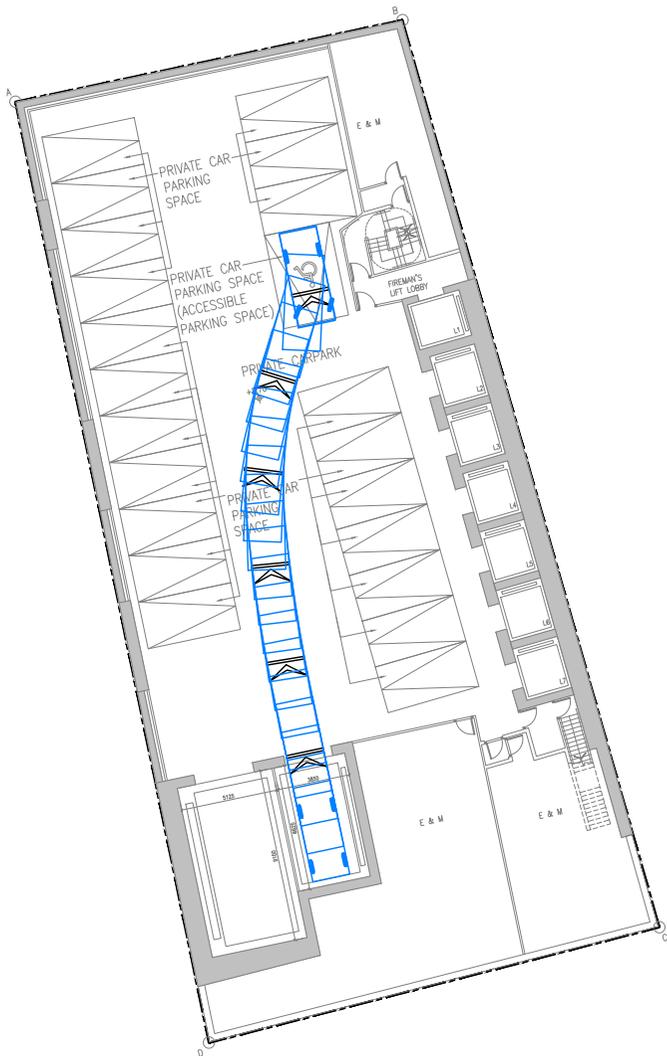


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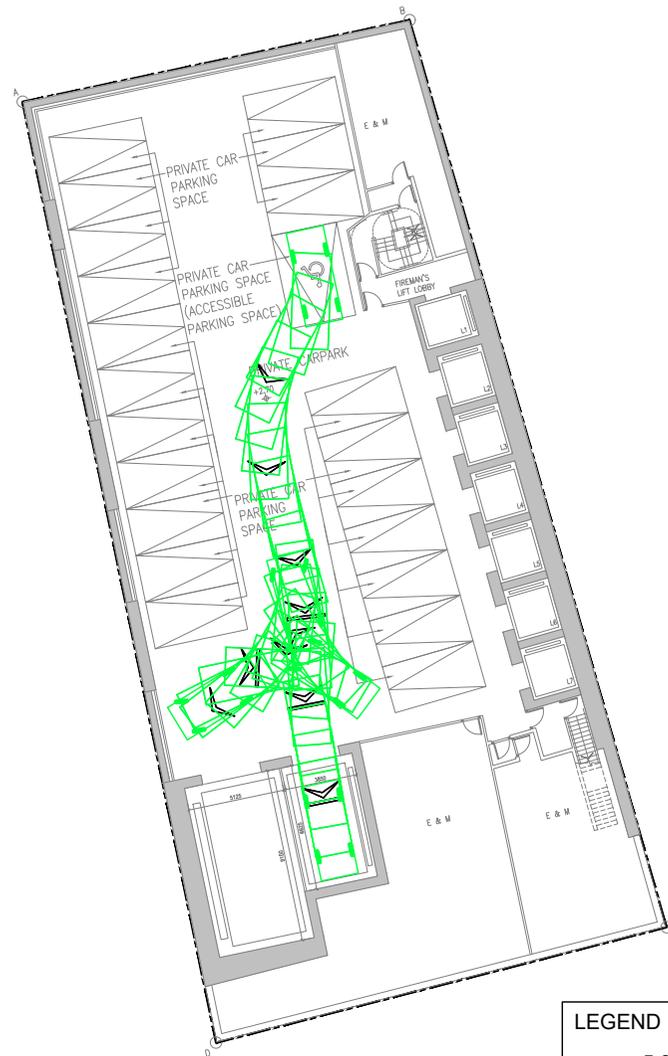


SWEPT PATH ANALYSIS - PC (B2/F) (2 OF 3)

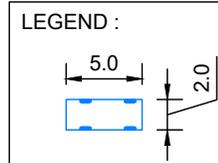
(SCALE 1:400 @ A4)



(IN)



(OUT)



**SWEPT PATH ANALYSIS - PC (B2/F) (3 OF 3)**

(SCALE 1:400 @ A4)