

# Appendix H

## Traffic Impact Assessment

**Application for Permission Under  
Section 16 of the Town Planning  
Ordinance (Cap. 131) for  
Proposed Comprehensive  
Development including Flats,  
Retail and Community Facilities  
and Minor Relaxation of Plot  
Ratio and Building Height  
Restriction in “Comprehensive  
Development Area” Zone at  
Various Lots in S.D.4 and  
Adjoining Government Land, Kau  
Wa Keng, Kwai Chung**

**Traffic Impact Assessment Report**

Rev. A | June 2025

This report takes into account the particular instructions and requirements of our client.

It is not intended for and should not be relied upon by any third party and no responsibility is undertaken to any third party.

Job number 299277-02

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# 1 INTRODUCTION

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## 1.1 Background

1.1.1 The Application Site falls within the "Comprehensive Development Area" zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung on the Approved Kwai Chung Outline Zoning Plan (OZP) No. S/KC/32. The location of application site is shown in **Figure 1.1**.

1.1.2 The Applicant submitted a S16 Planning Application No. A/KC/489 with a Master Layout Plan (MLP) covering the entire "CDA" zone with a pragmatic phasing strategy having due regard to the multiple land ownership pattern to increase certainty in realising the planning intention of the whole "CDA" zone. The comprehensive development proposed in the Planning Application No. A/KC/489 (hereafter referred to as the "**Approved Scheme**"), comprises 14 residential blocks with an overall PR of not more than 5 and maximum BH of not more than +120mPD.

1.1.3 The Planning Application No. A/KC/489 was deliberated in the TPB Metro Planning Committee Meeting held on 14 July 2023 (the TPB Meeting). During the TPB meeting, TPB members raised concerns on the provision of social welfare facilities and retail shops, as quoted from the meeting minutes<sup>[1]</sup>

- *"Some Members considered that retail facilities should be provided in the proposed development to cater for the daily needs of the future residents."* and *"Some Member shared the view that the provision of social welfare facilities in the proposed development was inadequate..."*.
- *"the development intensity of the proposed development could be increased for better land utilisation, e.g. provision of retail and more GIC facilities."*

After deliberation, the Planning Application No. A/KC/489 was approved with conditions.

*[1] Minutes of 722nd Meeting of the Metro Planning Committee held at 9:00 a.m. on 14.7.2023*

1.1.4 The Applicant takes the initiative to review the **Approved Scheme** and endeavours to take forward the provision of more of social welfare facilities and retail shops. The **Proposed Scheme**, keeping the phasing strategy adopted in the **Approved Scheme**, comprises 15 building blocks (including 14 building blocks with residential use) with domestic PR of not more than 6 and maximum BH of not more than +147.55mPD. Non-domestic PR of not more than 0.5 is designated for proposed retail shops, existing historical buildings, and social welfare facilities to nurture an inclusive and liveable community in the convenient location of Kwai Chung Area.

- 1.1.5 Arup Hong Kong Limited (Arup) was commissioned to carry out a Traffic Impact Assessment (TIA) report in support of the Section 16 application for the application site.

## 1.2 Objectives of this Report

- 1.2.1 The purpose of this report is to evaluate the potential traffic impact associated with the proposed residential development and community facilities, in support of the Section 16 application for the application site.

## 1.3 Scope of Study

- 1.3.1 The tasks for this TIA study are outlined as follows:
- Carry out traffic surveys at critical junctions to appreciate current traffic condition;
  - Update the inventory regarding traffic circulation patterns, traffic conditions, as well as the constraints of the existing and future committed road network in the vicinity of the application site based on the latest information available;
  - Assess the volume of traffic likely to be generated by the proposed development;
  - Set up the reference scenario with reference to the **Approved Scheme** at the site location, i.e. reference scenario with an overall PR of not more than 5;
  - Identify the likely traffic generation should the application site be developed into proposed development;
  - Compare the above two traffic scenarios for evaluation of the likely traffic impact, if any, associated with the proposed development;
  - Assess future traffic condition, taking into account any future traffic growth, as well as the traffic generated by the proposed development and other planned/committed development, if any, to be built in the vicinity;
  - Review the access arrangement for the proposed development and to make recommendation;
  - Recommend car parking provisions and goods vehicle loading/unloading arrangements;
  - Carry out pedestrian surveys at pedestrian facilities in the vicinity to appreciate current walking condition;
  - Assess pedestrian walking condition, taking into account any future population and employment growth generated by the proposed

development and other planned/committed development, if any, to be built in the vicinity

- Assess utilization of public transport services, taking into account any future population and employment growth generated by the proposed development and other planned/committed development, if any, to be built in the vicinity; and
- Review the vehicular and pedestrian impact for the Interim Scenarios of the proposed developments to be developed by phases.

## 1.4 Structure of the Report

1.4.1 The structure of this TIA report is as follows:

| <u>Chapter</u> | <u>Title</u>  | <u>Aims</u>  |
|----------------|---|--|
| 1              | Introduction  | Provide project background and scope of the Study  |
| 2              | Existing Traffic Condition                                      | Review and appreciate the existing traffic condition   |
| 3              | The Subject Development   | Provide information of the Proposed Development  |
| 4              | Traffic Impact Assessment (Full Development of Proposed Scheme) | Illustrate the results of Traffic Impact Assessment – full development of the CDA                        |
| 5              | Traffic Impact Assessment (Interim Scenario)                    | Illustrate the results of Traffic Impact Assessment – partial development of lots owned by the applicant |
| 6              | Conclusion  | Summarize the findings of this Study   |

## 2 EXISTING TRAFFIC CONDITION

### 2.1 Site Characteristics

- 2.1.1 The application site is located in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung. It is bounded by existing village houses to the north, Lai King Hill Road to the south, Castle Peak Road – Kwai Chung to the east and Princess Margaret Hospital to the west. **Figure 1.1** shows the location and the environs of the application site.

### 2.2 Existing Road Network

- 2.2.1 The application site is well-served by a comprehensive road network to and from all districts. Some major roads in the vicinity of the application site are listed as follows:

- Lai King Hill Road is district distributor, in single two-lane configuration. It connects Kwai Fuk Road to the north and Lai Wan Road to the south. Lai King Hill Road serves traffic between Kwai Chung, New Territories West and Kowloon.
- Ching Cheung Road is an urban trunk road, in dual three-lane configuration running in east-west direction. It connects Kwai Chung Road to the north and Castle Peak Road to the south. It connects Kwai Chung and Kowloon.
- Lai Wan Road is local distributor running in north-south direction. It connects Mei Lai Road to the north and a private road of Mei Foo Sun Chuen to the south.
- Mei Lai Road is a district distributor with two traffic lanes in both traffic direction connecting Mei Foo Bus Terminus and Lai King Hill Road.
- Castle Peak Road – Kwai Chung is a primary distributor, dual two-lane carriageway running north-south direction. It connects Tai Wo Interchange to the north and Ching Cheung Road to the south.

### 2.3 Existing Junction and Link Performance

- 2.3.1 To appreciate the existing traffic conditions, comprehensive classified traffic counts were conducted at the following identified key junctions in the vicinity of the application site. Locations of these surveyed junctions are listed below and shown in **Figure 2.1**.

|    |  |                       |
|----|--|-----------------------|
| J1 | - Lai King Hill Road / King Lai Path                     | (Signalized Junction) |
| J2 | - Lai King Hill Road / Chung Shan Terrance / Estate Road | (Signalized Junction) |
| J3 | - Lai King Hill Road / Kwai Chung Interchange            | (Signalized Junction) |
| J4 | - Mei Lai Road/ Lai Wan Road                             | (Signalized Junction) |
| J5 | - Mei Lai Road/ Cheung Sha Wan Road                      | (Signalized Junction) |

- 2.3.2 The counts were undertaken on 12<sup>th</sup> March 2024 during the periods of 07:00-10:00 and 17:00-20:00 hours. The morning and evening peak hours were found to be 07:45-08:45 and 17:30-18:30 respectively. The observed traffic flows during these peak hours are presented in **Figure 2.2**.

### **Junction Capacity Assessment**

- 2.3.3 Junction capacity analysis was carried out at the identified key junctions in the vicinity of the application site. Results of the capacity assessment are shown in **Table 2.3.1** below and detailed calculations are appended in **Appendix A**.

**Table 2.3.1 Year 2024 Existing Junction Performance**

| Junction |  | Type       | Performance <sup>(1)</sup> |       |
|----------|--|------------|----------------------------|-------|
|          |  |            | AM                         | PM    |
| J1       | Lai King Hill Road / King Lai Path                     | Signalized | >100%                      | >100% |
| J2       | Lai King Hill Road / Ching Shan Terrance / Estate Road | Signalized | >100%                      | >100% |
| J3       | Lai King Hill Road / Kwai Chung Interchange            | Signalized | 29%                        | 53%   |
| J4       | Mei Lai Road/ Lai Wan Road                             | Signalized | >100%                      | >100% |
| J5       | Mei Lai Road/ Cheung Sha Wan Road                      | Signalized | 64%                        | 69%   |

Notes:

(1) Figures shown represent "Reserve Capacity" (RC) in % for signalized junctions.

- 2.3.4 Results of the analysis indicate that the identified key junctions in the vicinity of the application site are currently operating satisfactorily during both morning and evening peak hours.

### **Link Capacity Assessment**

- 2.3.5 The road link capacity assessment has also been carried out to examine the volume to capacity (V/C) ratio of the identified key road links. Locations of these identified key road links are shown in **Figure 2.1**.
- 2.3.6 Results of the capacity assessment are shown in **Table 2.3.2** below. The assessment framework for the road links is based on the ratio of surveyed traffic volume over the link capacity (V/C) to measure the utilization of the road link.

**Table 2.3.2 Year 2024 Existing Link Performance <sup>(1)</sup>**

| Road Link <sup>(2)</sup> |  | Direction | Unit   | Link Capacity | Traffic Flows |       | Volume/Capacity (V/C) Ratio |      |
|--------------------------|--|-----------|--------|---------------|---------------|-------|-----------------------------|------|
|                          |  |           |        |               | AM            | PM    | AM                          | PM   |
| L1                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 1,090         | 1,085 | 0.46                        | 0.45 |
|                          |  |           | veh/hr | 2,200         | 903           | 895   | 0.41                        | 0.41 |
| L2                       | Lai King Hill Road (8m wide section)       | Two-way   | pcu/hr | 1,850         | 655           | 515   | 0.35                        | 0.28 |
|                          |  |           | veh/hr | 1,700         | 544           | 427   | 0.32                        | 0.25 |
| L3                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 550           | 545   | 0.23                        | 0.23 |
|                          |  |           | veh/hr | 2,200         | 452           | 452   | 0.21                        | 0.21 |
| L4                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 700           | 675   | 0.29                        | 0.28 |
|                          |  |           | veh/hr | 2,200         | 568           | 559   | 0.26                        | 0.25 |
| L5                       | Kwai Chung Interchange (6.8m wide section) | NB        | pcu/hr | 2,800         | 885           | 525   | 0.32                        | 0.19 |
|                          |  |           | veh/hr | 2,600         | 731           | 435   | 0.28                        | 0.17 |
| L6                       | Kwai Chung Interchange (6m wide section)   | SB        | pcu/hr | 1,400         | 425           | 575   | 0.30                        | 0.41 |
|                          |  |           | veh/hr | 1,300         | 353           | 475   | 0.27                        | 0.37 |

Notes:

- (1) Link capacity estimated according to TPDM Vol.2 Ch.2.4, for single 2-lane carriageway (for L1 to L4 with road width of 8m and 10m) or for dual 2-lane carriageway (for L5 and L6 with road width of 6m and 6.8m). Data in term of veh/hr and pcu/hr are converted according to survey pcu factor.
- (2) For conservative approach, the road links are assessed based on the greatest traffic flows at the road sections of corresponding roads within AOI.

**2.3.7 Results of the analysis indicate that the accessed road link has sufficient link capacity to cater for the existing traffic flows.**

## 2.4 Public Transport Facilities

2.4.1 The application site is served by various modes of public transport services as shown in **Figure 2.3**. The MTR Mei Foo Station is located about 500m from the application site, which is estimated to be a 8-minute walking journey. There are also a number of franchised bus and Green Minibus (GMB) service routes operating within the surrounding road network. A summary of the public transport services operating in the vicinity of the application site is provided in **Table 2.4.1**.

**Table 2.4.1 Existing Franchised Bus and GMB Services**

| Route No.             | Origin / Destination  | Peak Headway (mins)        |
|-----------------------|---|----------------------------|
| <b>Franchised Bus</b> |   |                            |
| 6                     | Star Ferry ↔ Lai Chi Kok                                    | 8-20                       |
| 30                    | Tsuen Wan (Allway Gardens) ↔ Cheung Sha Wan                 | 25-30                      |
| 32H                   | Cheung Shan ↔ Lai Chi Kok                                   | 60                         |
| 42                    | Tsing Yi (Cheung Hong Estate) ↔ Shun Lee                    | 15-20                      |
| 45                    | Kowloon City Ferry ↔ Kwai Chung (Lai Yiu Estate)            | 25-30                      |
| 46                    | Jordan (West Kowloon Station) ↔ Kwai Chung (Lai Yiu Estate) | 20-30                      |
| 46X                   | Hin Keng ↔ Mei Foo  | 5-12                       |
| 171                   | Lai Chi Kok ↔ South Horizons                                | 10-20                      |
| 171A                  | Lei Tung Estate → Lai Chi Kok                               | Weekday special departures |
| 171P                  | South Horizons → Lai Chi Kok                                | Weekday special departures |
| 904                   | Lai Chi Kok ↔ Kennedy Town (Belcher Bay)                    | 18-30                      |
| 905                   | Lai Chi Kok ↔ Exhibition Centre Station                     | 8-23                       |
| 905A                  | Exhibition Centre Station → Lai Chi Kok                     | Weekday special departures |
| 905P                  | Lai Chi Kok → Wan Chai (Harbour Road)                       | Weekday special departures |
| N171                  | Lai Chi Kok ↔ Ap Lei Chau Estate                            | Night services only        |
| N241                  | Hung Hom Station ↔ Tsing Yi (Cheung Wang Estate)            | Night services only        |
| <b>GMB</b>            |   |                            |
| 90A                   | Kwai Chung Hospital ↔ Mei Foo Station                       | Weekday special departures |
| 90M                   | Highland Park ∪ Mei Foo Station                             | 4-6 (circular)             |
| 90P                   | Princess Margaret Hospital ↔ Mei Foo Station                | 6-8                        |
| 92M                   | Wah Yuen Chuen ∪ Mei Foo Station                            | 5-10 (circular)            |

2.4.2 In summary, the subject development would have good accessibility to the public transport services via adjacent road network and the existing MTR Mei Foo Station.

## 2.5 Existing Pedestrian Condition

- 2.5.1 To appreciate the existing conditions, comprehensive pedestrian count surveys were conducted at the critical footpath in the vicinity, as shown in **Figure 2.4**. The pedestrian counts were undertaken on typical weekdays during the AM and PM peak periods on 12<sup>th</sup> March 2024.
- 2.5.2 In order to address the performance of the critical footpath, Level of Service (LOS) assessment of the critical footpath has been conducted.
- 2.5.3 LOS assessment is carried out based on the definitions presented in the Highways Capacity Manual 2000. **Table 2.5.1** shows the various LOS 'quantified' in terms of pedestrian flow rates.

**Table 2.5.1 Level of Service (LOS) for Walkway\***

| LOS | Flow rate for Walkway (ped/min/m) | Description   |
|-----|-----------------------------------|---|
| A   | ≤16                               | Pedestrians basically move in desired paths without altering their movements in response to other pedestrians. Walking speeds are freely selected, and conflicts between pedestrians are unlikely.  |
| B   | 16 – 23                           | Sufficient space is provided for pedestrians to freely select their walking speeds, to bypass other pedestrians and to avoid crossing conflicts with others. At this level, pedestrians begin to be aware of other pedestrians and to respond to their presence in the selection of walking paths.  |
| C   | 23 – 33                           | Sufficient space is available to select normal walking speeds and to bypass other pedestrians primarily in unidirectional stream. Where reverse direction or crossing movement exist, minor conflicts will occur, and speed and volume will be somewhat lower.  |
| D   | 33 – 49                           | Freedom to select individual walking speeds and bypass other pedestrians is restricted. Where crossing or reverse-flow movements exist, the probability of conflicts is high and its avoidance requires changes of speeds and position. The LOS provides reasonable fluid flow; however considerable friction and interactions between pedestrians are likely to occur.                                 |
| E   | 49 - 75                           | Virtually, all pedestrians would have their normal walking speeds restricted. At the lower range of this LOS, forward movement is possible only by shuffling. Space is insufficient to pass over slower pedestrians. Cross- and reverse-movement are possible only with extreme difficulties. Design volumes approach the limit of walking capacity with resulting stoppages and interruptions to flow. |
| F   | > 75                              | Walking speeds are severely restricted. Forward progress is made only by shuffling. There are frequent and unavoidable conflicts with other pedestrians. Cross- and reverse-movements are virtually impossible. Flow is sporadic and unstable. Space is more characteristics of queued pedestrians than of moving pedestrian streams.   |

\*Source: Extracted from Exhibit 18-3 of Highway Capacity Manual (HCM) 2000

- 2.5.4 Footpaths with LOS A to C are considered as desirable with sufficient space for pedestrian to select normal walking speeds to bypass. For footpaths with LOS D represent freedom to select individual walking speeds and bypass other pedestrian is restricted. Unless there are any site constraints, improved measures should be sought for footpath with LOS D or poorer.



2.5.5 **Table 2.5.2** summarized the observed AM and PM peak pedestrian flow and LOS in surveyed footpath and crossing.

**Table 2.5.2 Year 2024 Level of Service in AM and PM Peaks at Key Footpath**

| Footpath |  | Actual Width (m) | Effective Clear Width <sup>(1)</sup> (m) | Two-way Peak Hourly Flow (ped/hr) |     | Flow Rate <sup>(2)</sup> (ped/min/m) |     | LOS (Level) |    |
|----------|--|------------------|--|-----------------------------------|-----|--------------------------------------|-----|-------------|----|
|          |  |                  |  | AM                                | PM  | AM                                   | PM  | AM          | PM |
| F1       | Lai King Hill Road Northern Footpath               | 2.5              | 1.5                                      | 90                                | 55  | 1.2                                  | 0.7 | A           | A  |
| F1a      | Lai King Hill Road Northern Footpath (at bus stop) | 3.8              | 1.8                                      | 90                                | 55  | 1.0                                  | 0.6 | A           | A  |
| F2       | Lai King Hill Road Southern Footpath               | 2.8              | 1.8                                      | 225                               | 140 | 2.5                                  | 1.6 | A           | A  |
| F2a      | Lai King Hill Road Southern Footpath (at bus stop) | 3.5              | 1.5                                      | 225                               | 140 | 3.0                                  | 1.9 | A           | A  |
| F3       | Wah Lai Path Footpath                              | 9.5              | 8.5                                      | 220                               | 130 | 0.5                                  | 0.3 | A           | A  |

Notes:

- (1) Effective clear width = Actual width (on-site measurement) minus 0.5m dead width on both sides, and minus the width of passengers queuing at bus stops.
- (2) Pedestrian flow rates are computed based on effective clear width, with 1.2 peak factor applied for the peak minute flow rate.

2.5.6 The results presented in **Table 2.5.2** revealed that the walking condition on the critical footpath in the vicinity of the application site is satisfactory during both AM and PM peaks hours in Year 2024.

**Table 2.5.3 Year 2024 Level of Service in AM and PM Peaks at Key Pedestrian Crossing**

| Crossing Facility |   | Clear Width (m) | Cycle Time (s) |    | Green Time Proportion |     | Pedestrian Capacity (ped/hr) |       | Two-way Pedestrian Flow <sup>(1)</sup> (ped/hr) |    | Volume/ Capacity (V/C) Ratio |      |
|-------------------|---|-----------------|----------------|----|-----------------------|-----|------------------------------|-------|---|----|------------------------------|------|
|                   |   |                 | AM             | PM | AM                    | PM  | AM                           | PM    | AM  | PM | AM                           | PM   |
| C1                | Pedestrian Crossing Across Lai King Hill Road (South of the Proposed Development) | 4.2             | 60             | 60 | 28%                   | 28% | 2,230                        | 2,230 | 145   | 90 | 0.07                         | 0.04 |

Notes:

- (1) Pedestrian flow rates are computed based on effective clear width, with 1.2 peak factor applied for the peak minute flow rate.

2.5.7 The results presented in **Table 2.5.3** revealed that the concerned pedestrian crossing facility is operating satisfactorily during both AM and PM peaks in Year 2024.

## 3 THE SUBJECT DEVELOPMENT

### 3.1 Development Schedule

3.1.1 The Applicant intends to develop the application site into residential use with community facilities. The proposed development will comprise 4 phases, namely as follows:

- Phase 1A (P1A)
- Phase 1B (P1B)
- Remaining Phase A (RPA)
- Remaining Phase B (RPB)

3.1.2 The proposed development will be constructed in phases and the entire development is envisaged to be completed by Year 2032.

3.1.3 The proposed development schedule is summarized in **Table 3.1.1**, and the master layout plan is presented in **Figures 3.1**.

**Table 3.1.1 Proposed Development Parameters**

| Proposed Development | Site Area (sqm)  | Non-domestic Facilities   | Domestic   |               |  |       |
|----------------------|------------------|---|------------|---------------|--|-------|
|                      |                  |   | Plot Ratio | No. of Blocks | Flat Mix                               |       |
| Phase 1A             | About 13,577.341 | <ul style="list-style-type: none"> <li>Home Care Services (HCS) for Frail Elderly Persons (4-team size non-kitchen based)</li> <li>School Social Work Office (SSWO) (Hong Kong Family Welfare Society)</li> <li>Child Care Centre (CCC) (200 places)</li> <li>100-places Day Care Centre for the Elderly (DE)</li> <li>Retail GFA: 2,285.323 sqm</li> </ul> | 6          | 5             | FS≤40m <sup>2</sup>                    | 1,221 |
|                      |                  |   |            |               | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 651   |
|                      |                  |   |            |               | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 109   |
|                      |                  |   |            |               | Total                                  | 1,981 |
| Phase 1B             | About 10,111.772 | <ul style="list-style-type: none"> <li>Neighbourhood Elderly Centre (NEC)</li> <li>Residential Care Home for the Elderly (RCHE) (100 places)</li> <li>Retail GFA: 1,516.286 sqm</li> </ul>  | 6          | 2             | FS≤40m <sup>2</sup>                    | 910   |
|                      |                  |   |            |               | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 485   |
|                      |                  |   |            |               | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 81    |
|                      |                  |   |            |               | Total                                  | 1,476 |
| Remaining Phase A    | About 7,934.713  | <ul style="list-style-type: none"> <li>60-place Day Care Centre for the Elderly (DE)</li> <li>Office Base of On-site Pre-school Rehabilitation Services (OPRS) (Capacity: 125)</li> <li>120-place Day Care Centre for the Elderly (DE) (non-kitchen based)</li> <li>Retail GFA: 1,437.357 sqm</li> </ul>  | 6          | 2             | FS≤40m <sup>2</sup>                    | 714   |
|                      |                  |   |            |               | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 381   |
|                      |                  |   |            |               | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 63    |
|                      |                  |   |            |               | Total                                  | 1,158 |
| Remaining Phase B    | About 16,689.341 | <ul style="list-style-type: none"> <li>60-place Special Child Care Centre (SCCC)</li> <li>Residential Care Home for the Elderly (RCHE) (150 places)</li> <li>Child Care Centre (CCC) (100 places)</li> <li>Retail GFA: 832.970 sqm</li> </ul>   | 6          | 5             | FS≤40m <sup>2</sup>                    | 1,502 |
|                      |                  |   |            |               | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 801   |
|                      |                  |   |            |               | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 134   |
|                      |                  |   |            |               | Total                                  | 2,437 |
| Total                | About 48,313.167 |   | 6          | 14            | FS≤40m <sup>2</sup>                    | 4,347 |
|                      |                  |   |            |               | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 2,318 |
|                      |                  |   |            |               | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 387   |
|                      |                  |   |            |               | Total                                  | 7,052 |

## 3.2 Vehicular Access Arrangement

- 3.2.1 Two vehicular accesses are proposed for the CDA site along Lai King Hill Road, entering the site via P1A and P1B as shown in **Figure 3.2**.
- 3.2.2 The western vehicular access proposed at site P1A will have conflict with the existing pedestrian crossing and bus stop on Lai King Hill Road Eastbound. It is proposed to shift the pedestrian crossing eastwards and the bus stop to be relocated to the west, provide separation distance among the proposed pedestrian crossing, the proposed bus stop and the proposed vehicular access, as shown in **Figure 3.3\_1**. Alternative relocation option for relocating both the pedestrian crossing and bus stop towards the east have been reviewed and shown in **Figure 3.3\_2**. The implementation of the bus stop relocation scheme should be subject further review on the site constraints (DSD facilities / HyD structures etc.). On the basis that the vehicular access location of the application site to be maintained and the bus stop to be maintained on Lai King Hill Road, the relocation of bus stop will not constitute changes to the MLP.
- 3.2.3 The swept path analysis for 12m-long coach and 5m-long private car at vehicular access is shown in **Figure 3.4** and **Appendix C**.
- 3.2.4 The major ingress and egress routes for vehicular traffic approaching and leaving the application site are illustrated in **Figure 3.5** and **Figure 3.6** respectively.

## 3.3 Internal Transport Facilities Provision

- 3.3.1 The internal transport facilities provision for the proposed residential development will be provided in accordance with the high-end requirements of Hong Kong Planning Standards and Guidelines (HKPSG).
- 3.3.2 There is no standard requirement of internal transport facilities provision for the proposed GIC facilities under HKPSG, corresponding internal transport facilities provision is recommended with reference to operational need of projects with similar use.
- 3.3.3 The internal transport facilities provision for the proposed development are summarized in **Table 3.3.1** to **Table 3.3.7** below.

**Table 3.3.1 HKPSG Required Internal Transport Facilities Provision – P1A**

| Type of Development       | HKPSG Standard   |                                       |              |      | Low-end Requirement (nos.) | High-end Requirement (nos.)               |   |
|---------------------------|--|---------------------------------------|--------------|------|----------------------------|---|---|
| Private Housing           | Residential Parking Spaces   |                                       |              |      |                            |   |   |
|                           | Global Parking Standard (GPS)  | 1 car space per 4-7 flats             |              |      | Flat No.                   |   |   |
|                           | Demand Adjustment Ratio (R1)   | Flat Size (FS) (m² GFA)               | FS≤40        | 0.5  | 1,221                      | 78.49                                     | 137.36                                    |
|                           |  |                                       | 40<FS≤70     | 1.2  | 651                        | 100.44                                    | 175.77                                    |
|                           |  |                                       | 70<FS≤100    | 2.4  | 109                        | 33.63                                     | 58.86                                     |
|                           |  |                                       | 100<FS≤130   | 4.1  | -                          | -   | -   |
|                           |  |                                       | 130<FS≤160   | 5.5  | -                          | -   | -   |
|                           |  |                                       | FS>160       | 7    | -                          | -   | -   |
|                           | Total  |                                       |              |      | 1,981                      | 212.57                                    | 371.99                                    |
|                           | Accessibility Adjustment Ratio (R2)  | Within a 500m-radius of rail station  |              | 0.75 |                            | 213                                       | 372                                       |
|                           |  | Outside a 500m-radius of rail station |              | 1    |                            |   |   |
|                           | Development Intensity Adjustment Ratio (R3)  | Domestic Plot Ratio (PR)              | 0.00<PR≤1.00 | 1.3  |                            |   |   |
|                           |  |                                       | 1.00<PR≤2.00 | 1.1  |                            |   |   |
|                           |  |                                       | 2.00<PR≤5.00 | 1    |                            |   |   |
|                           |  |                                       | 5.00<PR≤8.00 | 0.9  |                            |   |   |
|                           | PR>8.00  |                                       | 0.75         |      |                            |   |   |
|                           | Parking Requirement = GPS x R1 x R2 x R3   |                                       |              |      |                            |   |   |
| Total Flat nos. 1,981     | Visitor Parking Spaces   |                                       |              |      |                            |   |   |
|                           | 5 visitor spaces per block in addition to the recommendations, or as determined by the Authority.  |                                       |              |      |                            | 25  | 25  |
|                           | Total Parking Car Parking Spaces   |                                       |              |      |                            | 238 (inclusive accessible parking spaces) | 397 (inclusive accessible parking spaces) |
|                           | Accessible Parking Spaces  |                                       |              |      |                            |   |   |
|                           | 1 space for 1-50 total number of car parking space in the lot;<br>2 spaces for 51-150 total number of car parking space in the lot;<br>3 spaces for 151-250 total number of car parking space in the lot;<br>4 spaces for 251-350 total number of car parking space in the lot;<br>5 spaces for 351-450 total number of car parking space in the lot;<br>6 spaces for above 450 total number of car parking space in the lot |                                       |              |      |                            | 3   | 5   |
| Block Nos. 5              | Motorcycle Parking Spaces  |                                       |              |      |                            |   |   |
|                           | 1 motorcycle parking space per 100-150 flats excluding non-residential elements.   |                                       |              |      |                            | 14  | 20  |
|                           | L/UL Bay   |                                       |              |      |                            |   |   |
|                           | Minimum of 1 loading / unloading bay for goods vehicles within the site for every 800 flats or part thereof, subject to a minimum of 1 bay for each housing block or as determined by the Authority.   |                                       |              |      |                            | 3   | 5   |
|                           | Private Car  |                                       |              |      |                            |   |   |
|                           | 1 car space per 150 - 300 m² GFA   |                                       |              |      |                            | 8   | 16  |
|                           | Accessible Car Parking   |                                       |              |      |                            |   |   |
|                           | 1 space for total number of car parking spaces below 50  |                                       |              |      |                            | 1   | 1   |
| Retail GFA: 2,285.323 sqm | Motorcycle   |                                       |              |      |                            |   |   |
|                           | 5 to 10% of the total provision for private cars   |                                       |              |      |                            | 1   | 2   |
|                           | Loading/ Unloading Bay   |                                       |              |      |                            |   |   |
|                           | 1 loading/ unloading bay for goods vehicles for every 800 - 1200 m² GFA  |                                       |              |      |                            | 2   | 3   |
|                           | LGV (65%)  |                                       |              |      |                            | 1   | 2   |
|                           | HGV (35%)  |                                       |              |      |                            | 1   | 1   |

**Table 3.3.2 HKPSG Required Internal Transport Facilities Provision – P1B**

| Type of Development  | HKPSG Standard  |   |              |      | Low-end Requirement (nos.) | High-end Requirement (nos.)               |   |
|--|---|---|--------------|------|----------------------------|---|---|
| Private Housing  | Residential Parking Spaces  |   |              |      |                            |   |   |
|  | Global Parking Standard (GPS)   | 1 car space per 4-7 flats   |              |      | Flat No.                   |   |   |
|  | Demand Adjustment Ratio (R1)  | Flat Size (FS) (m <sup>2</sup> GFA)   | FS≤40        | 0.5  | 910                        | 58.50                                     | 102.38                                    |
|  |   |   | 40<FS≤70     | 1.2  | 485                        | 74.83                                     | 130.95                                    |
|  |   |   | 70<FS≤100    | 2.4  | 81                         | 24.99                                     | 43.74                                     |
|  |   |   | 100<FS≤130   | 4.1  | -                          | -   | -   |
|  |   |   | 130<FS≤160   | 5.5  | -                          | -   | -   |
|  |   |   | FS>160       | 7    | -                          | -   | -   |
|  | Total   |   |              |      | 1,476                      | 158.32                                    | 277.07                                    |
|  | Accessibility Adjustment Ratio (R2)   | Within a 500m-radius of rail station  |              | 0.75 |                            | 159                                       | 278                                       |
|  |   | Outside a 500m-radius of rail station   |              | 1    |                            |   |   |
|  | Development Intensity Adjustment Ratio (R3)   | Domestic Plot Ratio (PR)  | 0.00<PR≤1.00 | 1.3  |                            |   |   |
|  |   |   | 1.00<PR≤2.00 | 1.1  |                            |   |   |
|  |   |   | 2.00<PR≤5.00 | 1    |                            |   |   |
|  |   |   | 5.00<PR≤8.00 | 0.9  |                            |   |   |
|  | PR>8.00   |   | 0.75         |      |                            |   |   |
|  | Parking Requirement = GPS x R1 x R2 x R3  |   |              |      |                            |   |   |
|  | Visitor Parking Spaces  |   |              |      |                            |   |   |
|  | Total Flat nos. 1,476   | 5 visitor spaces per block in addition to the recommendations, or as determined by the Authority. |              |      |                            | 10  | 10  |
|  | Block Nos. 2  | Total Parking Car Parking Spaces  |              |      |                            | 169 (inclusive accessible parking spaces) | 288 (inclusive accessible parking spaces) |
| Accessible Parking Spaces  |   |   |              |      |                            |   |   |
| 1 space for 1-50 total number of car parking space in the lot;<br>2 spaces for 51-150 total number of car parking space in the lot;<br>3 spaces for 151-250 total number of car parking space in the lot;<br>4 spaces for 251-350 total number of car parking space in the lot;<br>5 spaces for 351-450 total number of car parking space in the lot;<br>6 spaces for above 450 total number of car parking space in the lot |   |   |              |      | 3                          | 4   |   |
| Motorcycle Parking Spaces  |   |   |              |      |                            |   |   |
| 1 motorcycle parking space per 100-150 flats excluding non-residential elements.   |   |   |              |      | 10                         | 15  |   |
| L/UL Bay   |   |   |              |      |                            |   |   |
| Minimum of 1 loading / unloading bay for goods vehicles within the site for every 800 flats or part thereof, subject to a minimum of 1 bay for each housing block or as determined by the Authority.   |   |   |              |      | 2                          | 2   |   |
| Retail GFA: 1,516.286 sqm  | Private Car   |   |              |      |                            |   |   |
|  | 1 car space per 150 - 300 m <sup>2</sup> GFA  |   |              |      | 6                          | 11  |   |
|  | Accessible Car Parking  |   |              |      |                            |   |   |
|  | 1 space for total number of car parking spaces below 50                             |   |              |      | 1                          | 1   |   |
|  | Motorcycle  |   |              |      |                            |   |   |
|  | 5 to 10% of the total provision for private cars                                    |   |              |      | 1                          | 2   |   |
|  | Loading/ Unloading Bay  |   |              |      |                            |   |   |
|  | 1 loading/ unloading bay for goods vehicles for every 800 - 1200 m <sup>2</sup> GFA |   |              |      | 2                          | 2   |   |
|  | LGV (65%)   |   |              |      | 1                          | 1   |   |
|  | HGV (35%)   |   |              |      | 1                          | 1   |   |

**Table 3.3.3 HKPSG Required Internal Transport Facilities Provision – RPA**

| Type of Development       | HKPSG Standard  |  |              |      | Low-end Requirement (nos.) | High-end Requirement (nos.) |   |   |
|---------------------------|---|--|--------------|------|----------------------------|-----------------------------|---|---|
| Private Housing           | Residential Parking Spaces  |  |              |      |                            |                             |   |   |
|                           | Global Parking Standard (GPS)   | 1 car space per 4-7 flats  |              |      | Flat No.                   |                             |   |   |
|                           | Demand Adjustment Ratio (R1)  | Flat Size (FS) (m² GFA)  | FS≤40        | 0.5  | 714                        | 45.90                       | 80.33                                     |   |
|                           |   |  | 40<FS≤70     | 1.2  | 381                        | 58.78                       | 102.87                                    |   |
|                           |   |  | 70<FS≤100    | 2.4  | 63                         | 19.44                       | 34.02                                     |   |
|                           |   |  | 100<FS≤130   | 4.1  | -                          | -                           | -   |   |
|                           |   |  | 130<FS≤160   | 5.5  | -                          | -                           | -   |   |
|                           |   |  | FS>160       | 7    | -                          | -                           | -   |   |
|                           | Total   |  |              |      | 1,158                      | 124.12                      | 217.22                                    |   |
|                           | Accessibility Adjustment Ratio (R2)                                     | Within a 500m-radius of rail station   |              | 0.75 |                            | 125                         | 218                                       |   |
|                           |   | Outside a 500m-radius of rail station  |              | 1    |                            |                             |   |   |
|                           | Development Intensity Adjustment Ratio (R3)                             | Domestic Plot Ratio (PR)   | 0.00<PR≤1.00 |      | 1.3                        |                             |   |   |
|                           |   |  | 1.00<PR≤2.00 |      | 1.1                        |                             |   |   |
|                           |   |  | 2.00<PR≤5.00 |      | 1                          |                             |   |   |
|                           |   |  | 5.00<PR≤8.00 |      | 0.9                        |                             |   |   |
|                           |   |  | PR>8.00      |      | 0.75                       |                             |   |   |
|                           | Parking Requirement = GPS x R1 x R2 x R3                                |  |              |      |                            |                             |   |   |
|                           | Total Flat nos. 1,158   | Visitor Parking Spaces   |              |      |                            |                             |   |   |
|                           |   | 5 visitor spaces per block in addition to the recommendations, or as determined by the Authority.  |              |      |                            |                             | 10  | 10  |
|                           |   | Total Parking Car Parking Spaces   |              |      |                            |                             | 135 (inclusive accessible parking spaces) | 228 (inclusive accessible parking spaces) |
|                           |   | Accessible Parking Spaces  |              |      |                            |                             |   |   |
|                           |   | 1 space for 1-50 total number of car parking space in the lot;<br>2 spaces for 51-150 total number of car parking space in the lot;<br>3 spaces for 151-250 total number of car parking space in the lot;<br>4 spaces for 251-350 total number of car parking space in the lot;<br>5 spaces for 351-450 total number of car parking space in the lot;<br>6 spaces for above 450 total number of car parking space in the lot |              |      |                            |                             | 2   | 3   |
|                           |   | Motorcycle Parking Spaces  |              |      |                            |                             |   |   |
|                           |   | 1 motorcycle parking space per 100-150 flats excluding non-residential elements.   |              |      |                            |                             | 8   | 12  |
|                           |   | L/UL Bay   |              |      |                            |                             |   |   |
|                           |   | Minimum of 1 loading / unloading bay for goods vehicles within the site for every 800 flats or part thereof, subject to a minimum of 1 bay for each housing block or as determined by the Authority.   |              |      |                            |                             | 2   | 2   |
| Retail GFA: 1,437.357 sqm |   | Private Car  |              |      |                            |                             |   |   |
|                           | 1 car space per 150 - 300 m² GFA  |  |              |      |                            | 5                           | 10  |   |
|                           | Accessible Car Parking  |  |              |      |                            |                             |   |   |
|                           | 1 space for total number of car parking spaces below 50                 |  |              |      |                            | 1                           | 1   |   |
|                           | Motorcycle  |  |              |      |                            |                             |   |   |
|                           | 5 to 10% of the total provision for private cars                        |  |              |      |                            | 1                           | 1   |   |
|                           | Loading/ Unloading Bay  |  |              |      |                            |                             |   |   |
|                           | 1 loading/ unloading bay for goods vehicles for every 800 - 1200 m² GFA |  |              |      |                            | 2                           | 2   |   |
|                           | LGV (65%)   |  |              |      |                            | 1                           | 1   |   |
|                           | HGV (35%)   |  |              |      |                            | 1                           | 1   |   |

**Table 3.3.4 HKPSG Required Internal Transport Facilities Provision –RPB**

| Type of Development  | HKPSG Standard  |                                       |              |   | Low-end Requirement (nos.)                | High-end Requirement (nos.) |        |  |
|--|---|---------------------------------------|--------------|---|---|-----------------------------|--------|--|
| Private Housing  | Residential Parking Spaces  |                                       |              |   |   |                             |        |  |
|  | Global Parking Standard (GPS)   | 1 car space per 4-7 flats             |              |   | Flat No.                                  |                             |        |  |
|  | Demand Adjustment Ratio (R1)  | Flat Size (FS) (m² GFA)               | FS≤40        | 0.5                                       | 1,502                                     | 96.56                       | 168.98 |  |
|  |   |                                       | 40<FS≤70     | 1.2                                       | 801                                       | 123.58                      | 216.27 |  |
|  |   |                                       | 70<FS≤100    | 2.4                                       | 134                                       | 41.35                       | 72.36  |  |
|  |   |                                       | 100<FS≤130   | 4.1                                       | -   | -                           | -      |  |
|  |   |                                       | 130<FS≤160   | 5.5                                       | -   | -                           | -      |  |
|  | Total   |                                       |              | 2,437                                     | 261.49                                    | 457.61                      |        |  |
|  | Accessibility Adjustment Ratio (R2)                                     | Within a 500m-radius of rail station  |              | 0.75                                      |   | 262                         | 458    |  |
|  |   | Outside a 500m-radius of rail station |              | 1   |   |                             |        |  |
|  | Development Intensity Adjustment Ratio (R3)                             | Domestic Plot Ratio (PR)              | 0.00<PR≤1.00 | 1.3                                       |   |                             |        |  |
|  |   |                                       | 1.00<PR≤2.00 | 1.1                                       |   |                             |        |  |
|  |   |                                       | 2.00<PR≤5.00 | 1   |   |                             |        |  |
|  |   |                                       | 5.00<PR≤8.00 | 0.9                                       |   |                             |        |  |
|  | PR>8.00   |                                       | 0.75         |   |   |                             |        |  |
|  | Parking Requirement = GPS x R1 x R2 x R3                                |                                       |              |   |   |                             |        |  |
|  | Total Flat nos. 2,437   | Visitor Parking Spaces                |              |   |   |                             |        |  |
| 5 visitor spaces per block in addition to the recommendations, or as determined by the Authority.  |   |                                       |              | 25  | 25  |                             |        |  |
| Block Nos. 5   |   |                                       |              | 287 (inclusive accessible parking spaces) | 483 (inclusive accessible parking spaces) |                             |        |  |
| Total Parking Car Parking Spaces   |   |                                       |              |   |   |                             |        |  |
| Accessible Parking Spaces  |   |                                       |              |   |   |                             |        |  |
| 1 space for 1-50 total number of car parking space in the lot;<br>2 spaces for 51-150 total number of car parking space in the lot;<br>3 spaces for 151-250 total number of car parking space in the lot;<br>4 spaces for 251-350 total number of car parking space in the lot;<br>5 spaces for 351-450 total number of car parking space in the lot;<br>6 spaces for above 450 total number of car parking space in the lot |   |                                       |              |   | 4   | 6                           |        |  |
| Motorcycle Parking Spaces  |   |                                       |              |   |   |                             |        |  |
| 1 motorcycle parking space per 100-150 flats excluding non-residential elements.   |   |                                       |              |   | 17  | 25                          |        |  |
| L/UL Bay   |   |                                       |              |   |   |                             |        |  |
| Minimum of 1 loading / unloading bay for goods vehicles within the site for every 800 flats or part thereof, subject to a minimum of 1 bay for each housing block or as determined by the Authority.   |   |                                       |              |   | 4   | 5                           |        |  |
| Retail GFA: 832.970 sqm  | Private Car   |                                       |              |   |   |                             |        |  |
|  | 1 car space per 150 - 300 m² GFA  |                                       |              |   | 3   | 6                           |        |  |
|  | Accessible Car Parking  |                                       |              |   |   |                             |        |  |
|  | 1 space for total number of car parking spaces below 50                 |                                       |              |   | 1   | 1                           |        |  |
|  | Motorcycle  |                                       |              |   |   |                             |        |  |
|  | 5 to 10% of the total provision for private cars                        |                                       |              |   | 1   | 1                           |        |  |
|  | Loading/ Unloading Bay  |                                       |              |   |   |                             |        |  |
|  | 1 loading/ unloading bay for goods vehicles for every 800 - 1200 m² GFA |                                       |              |   | 1   | 2                           |        |  |
|  | LGV (65%)   |                                       |              |   | 1   | 1                           |        |  |
|  | HGV (35%)   |                                       |              |   | 0   | 1                           |        |  |

**Table 3.3.5 Recommendation for Internal Transport Facilities Provision of the Proposed GIC Facilities**

| Site | Development  | Facilities  | Recommended Provision |
|------|--|---|-----------------------|
| P1A  | Home Care Services (HCS) for Frail Elderly Persons (4-team size non-kitchen based) | Parking Space for private light bus (8m x 3m x 3.3m)                                    | 1                     |
|      |  | Shared-use loading/unloading bay for HGV and private light bus (11m x 3.5m x 4.7m)      | 1                     |
|      | Child Care Centre (CCC) (200 places)   | Ambulance Lay-by (9m x 3m x 3.8m)   | 1                     |
|      | Day Care Centre for the Elderly (DE) (100 places)                                  | Parking Space for private light bus (8m x 3m x 3.3m)                                    | 5                     |
|      |  | Shared-use loading/unloading bay for ambulance and private light bus (9m x 3m x 3.8m)   | 1                     |
|      | School Social Work Office (SSWO) (Hong Kong Family Welfare Society)                | N/A   | N/A                   |
| P1B  | Residential Care Home for the Elderly (RCHE) (100 places)                          | Accessible car parking space (5m x 3.5m x 2.4m)   | 1                     |
|      |  | Light bus parking space (8m x 3m x 3.3m)  | 1                     |
|      |  | Loading/ unloading bay for LGV (7m x 3.5m x 3.6m)                                       | 1                     |
|      |  | Private car / taxi pick-up / drop-off space (5m x 2.5m x 2.4m)                          | 1                     |
|      | Neighbourhood Elderly Centre (NEC)   | N/A   | N/A                   |
| RPA  | Day Care Centre for the Elderly (DE) (60 places)                                   | Parking Space for private light bus (8m x 3m x 3.3m)                                    | 3                     |
|      |  | Shared-use loading/ unloading area for ambulance and private light bus (9m x 3m x 3.8m) | 1                     |
|      | Office Base of On-site Pre-school Rehabilitation Services (OPRS) (125 places)      | Private car parking space (5m x 2.5m x 2.4m)  | 3                     |
|      |  | Accessible private car parking space (5m x 3.5m x 2.4m)                                 | 1                     |
|      |  | Loading/ unloading bay for LGV (7m x 3.5m x 3.6m)                                       | 1                     |
|      |  | Parking Space for private light bus (8m x 3m x 3.3m)                                    | 1                     |
|      | Day Care Centre for the Elderly (DE) (non-kitchen based) (120 places)              | Parking Space for private light bus (8m x 3m x 3.3m)                                    | 6                     |
|      |  | Shared-use loading/ unloading area for ambulance and private light bus (9m x 3m x 3.8m) | 1                     |
| RPB  | Special Child Care Centre (SCCC) (60 places)                                       | Parking Space for 48-seater coach (12m x 3.5m x 3.8m)                                   | 1                     |
|      |  | Loading / unloading bay for 48-seater coach (12m x 3.5m x 3.8m)                         | 1                     |
|      |  | Loading/ unloading bay for LGV (7m x 3.5m x 3.6m)                                       | 1                     |
|      | Residential Care Home for the Elderly (RCHE) (150 places)                          | Private car parking space (5m x 2.5m x 2.4m)  | 1                     |
|      |  | Accessible car parking space (5m x 3.5m x 2.4m)   | 1                     |
|      |  | Light bus parking space (8m x 3m x 3.3m)  | 1                     |
|      |  | L/UL for LGV (7m x 3.5m x 3.6m)   | 1                     |
|      |  | Private car / taxi pick-up / drop-off space (5m x 2.5m x 2.4m)                          | 1                     |
|      | Child Care Centre (CCC) (100 places)   | Ambulance Lay-by (9m x 3m x 3.8m)   | 1                     |



**Table 3.3.6 Transport Facilities Provision Summary Table**

| Proposed Use   | Facilities  | HKPSG Required Provision |          |          |          |                    |          |                      |          |   |   |
|----------------|---|--------------------------|----------|----------|----------|--------------------|----------|----------------------|----------|---|---|
|                |   | P1A                      |          | P1B      |          | RPA                |          | RPB                  |          | Total   |   |
|                |   | Low-end                  | High-end | Low-end  | High-end | Low-end            | High-end | Low-end              | High-end | Low-end   | High-end  |
| Residential    | Car Parking Space (5m x 2.5m x 2.4m) including residential, visitor parking | 238                      | 397      | 169      | 288      | 135                | 228      | 287                  | 483      | <u>829</u><br>(inclusive accessible parking spaces) | <u>1,396</u><br>(inclusive accessible parking spaces) |
|                | Accessible Car Parking Space (5m x 3.5m x 2.4m)                             | 3                        | 5        | 3        | 4        | 2                  | 3        | 4                    | 6        | <u>12</u>   | <u>18</u>   |
|                | Motorcycle (2.4m x 1m x 2.4m)   | 14                       | 20       | 10       | 15       | 8                  | 12       | 17                   | 25       | <u>49</u>   | <u>72</u>   |
|                | Loading/ Unloading Bay for HGV (11m x 3.5m x 4.7m)                          | 3                        | 5        | 2        | 2        | 2                  | 2        | 4                    | 5        | <u>11</u>   | <u>14</u>   |
| Retail         | Car Parking Space (5m x 2.5m x 2.4m)  | 8                        | 16       | 6        | 11       | 5                  | 10       | 3                    | 6        | <u>22</u><br>(inclusive accessible parking spaces)  | <u>43</u><br>(inclusive accessible parking spaces)    |
|                | Accessible Car Parking Space (5m x 3.5m x 2.4m)                             | 1                        | 1        | 1        | 1        | 1                  | 1        | 1                    | 1        | <u>4</u>  | <u>4</u>  |
|                | Motorcycle (2.4m x 1m x 2.4m)   | 1                        | 2        | 1        | 2        | 1                  | 1        | 1                    | 1        | <u>4</u>  | <u>6</u>  |
|                | Loading/ Unloading Bay for HGV (11m x 3.5m x 4.7m)                          | 1                        | 1        | 1        | 1        | 1                  | 1        | 0                    | 1        | <u>3</u>  | <u>4</u>  |
|                | Loading/ Unloading Bay for LGV (7m x 3.5m x 3.6m)                           | 1                        | 2        | 1        | 1        | 1                  | 1        | 1                    | 1        | <u>4</u>  | <u>5</u>  |
| GIC Facilities | Car Parking Space (5m x 2.5m x 2.4m)  | -                        | -        | -        | -        | 3 (OPRS)           |          | 1 (RCHE)             |          | <u>4</u>  |   |
|                | Accessible Parking Spaces (5m x 3.5m x 2.4m)                                | -                        | -        | 1 (RCHE) |          | 1 (OPRS)           |          | 1 (RCHE)             |          | <u>3</u>  |   |
|                | Private car / taxi pick-up / drop-off space (5m x 2.5m x 2.4m)              | -                        | -        | 1 (RCHE) |          | -                  |          | 1 (RCHE)             |          | <u>2</u>  |   |
|                | L/UL bay for LGV (7m x 3.5m x 3.6m)   | -                        | -        | 1 (RCHE) |          | 1 (OPRS)           |          | 1 (SCCC)<br>1 (RCHE) |          | <u>4</u>  |   |
|                | Parking Space for private light bus (8m x 3m x 3.3m)                        | 1 (HCS)<br>5 (DE)        | -        | 1 (RCHE) |          | 9 (DE)<br>1 (OPRS) |          | 1 (RCHE)             |          | <u>18</u>   |   |
|                | Shared-use L/UL bay for HGV and private light bus (11m x 3.5m x 4.7m)       | 1 (HCS)                  | -        | -        |          | -                  |          | -                    |          | <u>1</u>  |   |
|                | Ambulance lay-by (9m x 3m x 3.8m)   | 1 (CCC)                  | -        | -        |          | -                  |          | 1 (CCC)              |          | <u>2</u>  |   |
|                | Shared-use L/UL bay for ambulance and private light bus (9m x 3m x 3.8m)    | 1 (DE)                   | -        | -        |          | 2 (DE)             |          | -                    |          | <u>3</u>  |   |
|                | Parking Space for 48-seater coach (12m x 3.5m x 3.8m)                       | -                        | -        | -        |          | -                  |          | 1 no. (SCCC)         |          | <u>1</u>  |   |
|                | L/UL bay for 48-seater coach (12m x 3.5m x 3.8m)                            | -                        | -        | -        |          | -                  |          | 1 no. (SCCC)         |          | <u>1</u>  |   |

- 3.3.4 The proposed internal transport facilities for each phase of the proposed development will be self-contained within the respective phasing boundary. Detailed allocations of the internal transport facilities are described as follows and shown in **Figure 3.7** to **3.8**. Highlighted plans of internal transport are shown in **Appendix B** and swept path analysis at critical movement are shown in **Appendix C**.

**Car Parking Space Provision**

- 3.3.5 A total of 1,396 nos. car parking spaces (including 18 nos. accessible car parking spaces) for residential development and another 43 nos. car parking spaces (including 4 nos. accessible car parking spaces) for retail use as per HKPSG high-end requirements will be provided in the basement levels, which will be accessed via the corresponding car-ramp for each site.
- 3.3.6 A total of 7 nos. car parking spaces (including 3 nos. accessible car parking spaces) will be provided on ground floor for GIC Facilities according to the schedule of accommodation from Social Welfare Department.

**Visitor Car Parking Provision**

- 3.3.7 A total of 70 nos. visitor car parking spaces (part of total 1,396 nos. private car parking provision), as per HKPSG high-end requirements will be provided in the basement levels, which will be accessed via the corresponding car-ramp for each site.

**Motorcycle Parking Space Provision**

- 3.3.8 A total of 72 nos. motorcycle parking spaces for residential development and another 6 nos. motorcycle parking spaces for retail use as per HKPSG high-end requirements will be provided in the basement levels, which will be accessed via the corresponding car-ramp for each site.

**Private Car / Taxi Pick-up / Drop-off Provision**

- 3.3.9 A total of 2 nos. private car / taxi pick-up / drop-off spaces will be provided on ground floor for GIC Facilities according to the schedule of accommodation from Social Welfare Department.

**Loading / Unloading Bay Provision**

- 3.3.10 A total of 14 nos. HGV loading/unloading bays for residential development and another 4 nos. HGV loading/unloading bays and 5 nos. LGV loading/unloading bays for retail use as per HKPSG high-end requirement will be provided on ground floor.
- 3.3.11 A total of 4 nos. LGV loading/unloading bays will be provided on ground floor for GIC Facilities according to the schedule of accommodation from Social Welfare Department.

**Parking Space and Loading / Unloading Bay Provision for Private Light Bus**

- 3.3.12 A total of 18 nos. parking spaces, 1 no. loading / unloading bay to be shared with HGV, and 3 nos. loading / unloading bay to be shared-used with ambulance, for private light bus, will be provided on ground floor according to the schedule of accommodation from Social Welfare Department.

**Parking Space and Loading / Unloading Bay Provision for Ambulance**

- 3.3.13 A total of 2 nos. loading / unloading bay for ambulance exclusively will be provided on ground floor according to the schedule of accommodation from Social Welfare Department.

**Parking Space and Loading / Unloading Bay Provision for Coach**

- 3.3.14 1 no. parking space and 1 no. loading / unloading bay for coach will be provided on ground floor according to the schedule of accommodation from Social Welfare Department.

## 4 TRAFFIC IMPACT ASSESSMENT (FULL DEVELOPMENT OF PROPOSED SCHEME)

### 4.1 Trip Generation and Attraction of Proposed Development

4.1.1 The likely amount of traffic generated and attracted by the proposed development was calculated based on "Traffic Rates for Non-Residential Developments at 95% Confidence Level" adopted in the Transport Planning and Design Manual (TPDM) Vol.1 Table 1 of Annex D. The adopted rate and associated trip are shown in **Table 4.1.1**.

**Table 4.1.1 Adopted Trip Generation and Attraction Rates for the Proposed Development**

| Development   | AM Peak    |            | PM Peak    |            |
|---|------------|------------|------------|------------|
|   | Generation | Attraction | Generation | Attraction |
| Private Housing:<br>High-Density / R(A)<br>(pcu/hr/flat) <sup>(1)</sup> | 0.0718     | 0.0425     | 0.0286     | 0.0370     |
| Private Housing:<br>High-Density / R(A)<br>(pcu/hr/flat) <sup>(2)</sup> | 0.0888     | 0.0515     | 0.0356     | 0.0480     |
| Private Housing:<br>High-Density / R(B)<br>(pcu/hr/flat) <sup>(3)</sup> | 0.1887     | 0.0942     | 0.0862     | 0.1214     |
| Retail<br>(pcu/hr/100m <sup>2</sup> GFA) <sup>(4)</sup>                 | 0.2296     | 0.2434     | 0.3100     | 0.3563     |

Note:

- (1) Trip Rate based on "Traffic Rates for Residential Developments at 95% Confidence Level" in the Transport Planning and Design Manual (TPDM) Vol.1 Table 1, for average flat size 60m<sup>2</sup>
- (2) Trip Rate based on "Traffic Rates for Residential Developments at 95% Confidence Level" in the Transport Planning and Design Manual (TPDM) Vol.1 Table 1, for average flat size 70m<sup>2</sup>.
- (3) Trip Rate based on "Traffic Rates for Residential Developments at 95% Confidence Level" in the Transport Planning and Design Manual (TPDM) Vol.1 Table 1, for average flat size 100m<sup>2</sup>.
- (4) Trip Rate based on "Traffic Rates for Non-Residential Developments at 95% Confidence Level" in the Transport Planning and Design Manual (TPDM) Vol.1 Table 2.

4.1.2 The traffic generation and attraction trips for the design scenarios in year 2035 is estimated in **Table 4.1.2**.

**Table 4.1.2 Traffic Generation and Attraction of Proposed Development (pcu/hr)**

| Proposed Development                         | Development Parameters                 |       | AM         |            | PM         |            |
|--|--|-------|------------|------------|------------|------------|
|  |  |       | Generation | Attraction | Generation | Attraction |
| Phase 1A                                     | FS≤40m <sup>2</sup>                    | 1,221 | 88         | 52         | 35         | 45         |
|  | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 651   | 58         | 34         | 23         | 31         |
|  | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 109   | 21         | 10         | 9          | 13         |
|  | Retail: 2,285.323 sqm                  |       | 5          | 6          | 7          | 8          |
|  | <b>Sub-total</b>                       |       | <b>172</b> | <b>102</b> | <b>74</b>  | <b>97</b>  |
| Phase 1B                                     | FS≤40m <sup>2</sup>                    | 910   | 65         | 39         | 26         | 34         |
|  | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 485   | 43         | 25         | 17         | 23         |
|  | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 81    | 15         | 8          | 7          | 10         |
|  | Retail: 1,516.286 sqm                  |       | 3          | 4          | 5          | 5          |
|  | <b>Sub-total</b>                       |       | <b>126</b> | <b>76</b>  | <b>55</b>  | <b>72</b>  |
| Remaining Phase A                            | FS≤40m <sup>2</sup>                    | 714   | 51         | 30         | 20         | 26         |
|  | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 381   | 34         | 20         | 14         | 18         |
|  | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 63    | 12         | 6          | 5          | 8          |
|  | Retail: 1,437.357 sqm                  |       | 3          | 3          | 4          | 5          |
|  | <b>Sub-total</b>                       |       | <b>100</b> | <b>59</b>  | <b>43</b>  | <b>57</b>  |
| Remaining Phase B                            | FS≤40m <sup>2</sup>                    | 1,502 | 108        | 64         | 43         | 56         |
|  | 40m <sup>2</sup> <FS≤70m <sup>2</sup>  | 801   | 71         | 41         | 29         | 38         |
|  | 70m <sup>2</sup> <FS≤100m <sup>2</sup> | 134   | 25         | 13         | 12         | 16         |
|  | Retail: 832.970 sqm                    |       | 2          | 2          | 3          | 3          |
|  | <b>Sub-total</b>                       |       | <b>206</b> | <b>120</b> | <b>87</b>  | <b>113</b> |
| <b>Proposed Feeder Service<sup>(1)</sup></b> |  |       | <b>12</b>  | <b>12</b>  | <b>0</b>   | <b>0</b>   |
| <b>Total</b>                                 |  |       | <b>616</b> | <b>369</b> | <b>259</b> | <b>339</b> |

Note:

(1) Detail of proposed feeder service refer to Section 4.7.

- 4.1.3 As indicated in **Table 4.1.2**, the total trip generated by the proposed development would be around 985 pcu/hr and 598 pcu/hr (two-way) during the AM and PM peak periods respectively.

## 4.2 Adjacent Developments

- 4.2.1 In addition to the development flow, the traffic generated and attracted by adjacent major planned/committed developments in the vicinity of the proposed development, including redevelopment of Princess Margret Hospital and Kwai Chung Hospital (S16 planning application No. A/KC/451), expansion of Princess Margaret Hospital Lai King Building, redevelopment of Salvation Army Lai King Home, and private residential development at Lai Kong Street were taken into account for the traffic forecast.

### 4.3 Future Traffic Growth

4.3.1 The proposed development is targeted for completion in Year 2032. In order to assess the traffic impact of the development-related traffic on the adjacent road network, Year 2035 (i.e. 3 years after completion) is adopted as the design year of the study.

#### Annual Traffic Census

4.3.2 Reference was made to Annual Traffic Census (ATC) on annual average daily traffic (AADT) at counting stations in the vicinity of the proposed development and the corresponding traffic flows are summarized in **Table 4.3.1** below.

**Table 4.3.1 Annual Average Growth Rate by ATC**

| Station No.  | 2017 AADT      | 2018 AADT      | 2019 AADT      | 2020 AADT      | 2021 AADT      | 2022 AADT     | 2023 AADT      | Annual Average Growth Rate from 2017 to 2023 |
|--------------|----------------|----------------|----------------|----------------|----------------|---------------|----------------|--|
| 5443         | 6,720          | 6,820          | 7,590          | 7,590          | 7,880          | 7,800         | 8,060          | +3.08%                                       |
| 4623         | 10,140         | 10,260         | 10,310         | 10,160         | 10,610         | 9,070         | 9,500          | -1.08%                                       |
| 3859         | 16,090         | 16,300         | 14,920         | 14,400         | 15,860         | 13,880        | 14,920         | -1.25%                                       |
| 4628         | 3,520          | 3,680          | 3,580          | 3,500          | 4,050          | 3,720         | 3,940          | +1.90%                                       |
| 5476         | 10,890         | 11,190         | 11,430         | 12,210         | 11,870         | 11,450        | 12,930         | +2.90%                                       |
| 4003         | 56,220         | 57,820         | 57,520         | 54,350         | 56,080         | 53,180        | 56,820         | +0.18%                                       |
| <b>Total</b> | <b>103,580</b> | <b>106,070</b> | <b>105,350</b> | <b>102,210</b> | <b>106,350</b> | <b>99,100</b> | <b>106,170</b> | <b>+0.41%</b>                                |

4.3.3 The ATC historic data indicates a growth of traffic in recent years in the region with around +0.41% p.a.

#### Territorial Population and Employment Data Matrix (TPEDM)

4.3.4 Reference was also made to 2019-based TPEDM published by Planning Department. **Table 4.3.2** below summarizes the estimated and projected population and employment data as well as their respective annual average growth rate of Kwai Chung District in 2019, 2026 and 2031.

**Table 4.3.2 Annual Average Growth Rate by TPEDM**

| Year                       | 2019                                 | 2026                                 | 2031           |
|----------------------------|--------------------------------------|--------------------------------------|----------------|
| Population                 | 319,150                              | 315,800                              | 319,700        |
| Employment                 | 195,950                              | 192,350                              | 183,600        |
| <b>TOTAL</b>               | <b>515,100</b>                       | <b>508,150</b>                       | <b>503,300</b> |
| Annual Average Growth Rate | <b>-0.19%</b><br>(from 2019 to 2026) | <b>-0.19%</b><br>(from 2026 to 2031) |                |

- 4.3.5 From the table above, the annual average growth rates from 2019 to 2026 and from 2026 to 2031 are -0.19% and -0.19% respectively based on population and employment data.
- 4.3.6 For conservative purpose, growth rate of **+0.5% p.a.** is selected to produce the traffic forecasts for 2024–2035.

## 4.4 Assessment Scenarios

- 4.4.1 To evaluate the associated traffic impact likely to be induced by the proposed development, two scenarios were analysed and compared. The first scenario (i.e. Year 2035 Reference Scenario) assumed the existing land lot to be developed as the **Approved Scheme** overall PR of not more than 5, whereas the second scenario (i.e. Year 2035 Design Scenario) assumed that the **Proposed Scheme** with domestic PR of not more than 6 and non-domestic PR of not more than 0.5 is in place.

### Scenario 1

Year 2035 Reference Scenario

= Year 2024 observed traffic flows × growth factor during the period of year 2024-2035

*plus* traffic generations of adjacent major planned/committed developments in the vicinity

*plus* trips generated and attracted by the **Approved Scheme** overall PR of not more than 5 (Planning Application No. A/KC/489)

### Scenario 2

Year 2035 Design Scenario

= Year 2024 observed traffic flows × growth factor during the period of year 2024-2035

*plus* traffic generations of adjacent major planned/committed developments in the vicinity

*plus* trips generated and attracted by **Proposed Scheme** with domestic PR of not more than 6 and non-domestic PR of not more than 0.5

- 4.4.2 The forecasted traffic flows for the above two scenarios are presented in **Figures 4.1** to **4.2** respectively. The development traffic flows are also presented in **Figure 4.3**.
- 4.4.3 Additional **Baseline Scenario** at the design year 2035, with traffic generations of adjacent major planned/committed developments in the vicinity but without trips generated and attracted by the development under A/KC/489, is setup as supplementary information for comparison. The forecasted traffic flows are presented in **Figure 4.4**.

## 4.5 Junction Capacity Assessment

4.5.1 Junction capacity assessment was carried out at the identified key junctions for Year 2035 Reference and Design scenarios. Assessment results are summarized in **Table 4.5.1** below and the detailed calculations are appended in **Appendix A**.

**Table 4.5.1 Year 2035 Future Junction Performance**

| Junction |  | Type       | Performance <sup>(1)</sup> |       |                |       |             |       |
|----------|--|------------|----------------------------|-------|----------------|-------|-------------|-------|
|          |  |            | Baseline Scenario          |       | 2035 Reference |       | 2035 Design |       |
|          |  |            | AM                         | PM    | AM             | PM    | AM          | PM    |
| J1       | Lai King Hill Road / King Lai Path                         | Signalized | >100%                      | >100% | >100%          | >100% | >100%       | >100% |
| J2       | Lai King Hill Road / Ching Shan Terrace / Estate Road      | Signalized | >100%                      | >100% | >100%          | >100% | >100%       | >100% |
| J3_a     | Lai King Hill Road / Kwai Chung Interchange <sup>(2)</sup> | Signalized | 21%                        | 46%   | 3%             | 29%   | -2%         | 20%   |
| J3_b     | Lai King Hill Road / Kwai Chung Interchange <sup>(3)</sup> | Signalized | -7%                        | 7%    | -21%           | -5%   | -25%        | -11%  |
| J3_c     | Lai King Hill Road / Kwai Chung Interchange <sup>(4)</sup> | Signalized | 18%                        | 44%   | 15%            | 29%   | 15%         | 25%   |
| J4       | Mei Lai Road/ Lai Wan Road                                 | Signalized | >100%                      | >100% | >100%          | >100% | >100%       | >100% |
| J5       | Mei Lai Road/ Cheung Sha Wan Road                          | Signalized | 56%                        | 60%   | 38%            | 50%   | 34%         | 48%   |

Notes:

- (1) Figures shown represent "Reserve Capacity" (RC) in % for signalized junctions.
- (2) J3 under existing junction configuration.
- (3) J3 with TD planned improvement works.
- (4) Junction modification scheme in approved planning application (No. A/KC/489) is incorporated for assessment.

4.5.2 The above results reveal that the identified key junctions would operate within capacity with the proposed development in Year 2035, with the junction modification scheme in approved planning application (No. A/KC/489). It is anticipated that proposed development would not induce adverse traffic impact to the surrounding road network. **TD's planned improvement scheme and** the approved junction modification scheme is shown in **Appendix D** for reference.

## 4.6 Link Capacity Assessment

4.6.1 Link capacity assessment was carried out at the identified road links for Year 2035 Reference and Design scenarios. Assessment results are summarized in **Table 4.6.1** below.



**Table 4.6.1 Year 2031 Future Link Performance <sup>(1)</sup>**

| Road Link <sup>(2)</sup> |  | Direction | Unit   | Link Capacity | Traffic Flows (pcu/hr) |       |                |       |             |       | Volume/Capacity (V/C) Ratio |      |                |      |             |      |
|--------------------------|--|-----------|--------|---------------|------------------------|-------|----------------|-------|-------------|-------|-----------------------------|------|----------------|------|-------------|------|
|                          |  |           |        |               | Baseline Scenario      |       | 2035 Reference |       | 2035 Design |       | Baseline Scenario           |      | 2035 Reference |      | 2035 Design |      |
|                          |  |           |        |               | AM                     | PM    | AM             | PM    | AM          | PM    | AM                          | PM   | AM             | PM   | AM          | PM   |
| L1                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 1,160                  | 1,145 | 1,712          | 1,475 | 1,855       | 1,562 | 0.49                        | 0.48 | 0.72           | 0.62 | 0.78        | 0.65 |
|                          |  |           | veh/hr | 2,200         | 955                    | 946   | 1,419          | 1,227 | 1,529       | 1,299 | 0.43                        | 0.43 | 0.65           | 0.56 | 0.70        | 0.59 |
| L2                       | Lai King Hill Road (8m wide section)       | Two-way   | pcu/hr | 1,850         | 695                    | 540   | 1,247          | 870   | 1,390       | 957   | 0.38                        | 0.29 | 0.67           | 0.47 | 0.75        | 0.52 |
|                          |  |           | veh/hr | 1,700         | 575                    | 450   | 1,035          | 725   | 1,144       | 799   | 0.34                        | 0.26 | 0.61           | 0.43 | 0.67        | 0.47 |
| L3                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 580                    | 575   | 1,132          | 905   | 1,275       | 992   | 0.24                        | 0.24 | 0.47           | 0.38 | 0.53        | 0.42 |
|                          |  |           | veh/hr | 2,200         | 477                    | 477   | 937            | 752   | 1,046       | 826   | 0.22                        | 0.22 | 0.43           | 0.34 | 0.48        | 0.38 |
| L4                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 725                    | 710   | 960            | 853   | 1,014       | 888   | 0.30                        | 0.30 | 0.40           | 0.36 | 0.42        | 0.37 |
|                          |  |           | veh/hr | 2,200         | 601                    | 591   | 798            | 713   | 844         | 743   | 0.27                        | 0.27 | 0.36           | 0.32 | 0.38        | 0.34 |
| L5                       | Kwai Chung Interchange (6.8m wide section) | NB        | pcu/hr | 2,800         | 935                    | 555   | 1,123          | 729   | 1,165       | 773   | 0.33                        | 0.20 | 0.40           | 0.26 | 0.42        | 0.28 |
|                          |  |           | veh/hr | 2,600         | 773                    | 460   | 930            | 605   | 965         | 642   | 0.30                        | 0.18 | 0.36           | 0.23 | 0.37        | 0.25 |
| L6                       | Kwai Chung Interchange (6m wide section)   | SB        | pcu/hr | 1,400         | 450                    | 610   | 775            | 742   | 843         | 778   | 0.32                        | 0.44 | 0.55           | 0.53 | 0.60        | 0.56 |
|                          |  |           | veh/hr | 1,300         | 373                    | 501   | 643            | 613   | 699         | 642   | 0.29                        | 0.39 | 0.49           | 0.47 | 0.54        | 0.49 |

Notes:

- (1) Link capacity estimated according to TPDM Vol.2 Ch.2.4, for single 2-lane carriageway (for L1 to L4 with road width of 8m and 10m) or for dual 2-lane carriageway (for L5 and L6 with road width of 6m and 6.8m). Data in term of veh/hr and pcu/hr are converted according to survey pcu factor.
- (2) For conservative approach, the road links are assessed based on the greatest traffic flows at the road sections of corresponding roads within AOI.

4.6.2 As shown in the table above, the identified road section would continue to have sufficient link capacity to cater for the future traffic demand with the proposed development by Year 2035. The proposed development would not induce adverse traffic impact to the surrounding road network.

## 4.7 Future Occupancy of Public Transport Services

4.7.1 The Proposed Development is targeted for completion in Year 2032. In order to assess the likely impact induced by the Proposed Development on public transport connection in Year 2035 (i.e. 3 years after the target completion year of the Proposed Development) is adopted as the design year of the public transport assessment, which is in line with the design year adopted in traffic impact assessment.

4.7.2 Increase in demand on public transport service is anticipated due to the Proposed Development, the anticipated population of the Proposed Development is approximately 19,038. According to "Travel Characteristics Survey (TCS) 2011" published by Transport Department, the daily mechanised trip rate is 1.83 trips per person and the morning peak and evening peak accounted for about 12% and 10% of the daily trips. Considering this travel pattern in TCS 2011, it is estimated that the proposed development would generate a total of 4,181 pax/hr (i.e.  $19,038 \times 1.83 \times 0.12$ ) and 3,484 pax/hr (i.e.  $19,038 \times 1.83 \times 0.10$ ) during the morning peak hour and evening peak hour

respectively. The anticipated trips generated is summarized in **Table 4.7.1** below.

**Table 4.7.1 Passenger Trips Generated from Proposed Development**

| Development Parameters     |                 |                 |
|----------------------------|-----------------|-----------------|
| No. of Flats               | 7,052 flats     |                 |
| Population                 | 19,038 *        |                 |
| Peak Hours Trip Generation | AM              | PM              |
|                            | 4,181 pax/hr ** | 3,484 pax/hr ** |

\* Person Per Occupied Flat (PPOF) of 2.7 is assumed based on the 2021 census of Kwai Tsing District

\*\* According to "Travel Characteristics Survey (TCS) 2011" published by Transport Department, the daily mechanised trip rate is 1.83 trips per person and the morning peak and evening peak accounted for about 12% and 10% of the daily trips.

4.7.3 With reference to "2021 Population Census" published by Census and Statistics Department, the modal split of working population in Kwai Tsing District Council District and the corresponding passenger demand from the proposed development are estimated as summarized in **Table 4.7.2**.

**Table 4.7.2 Modal Split and Passenger Demand from The Proposed Development**

| Mode of Transport                | Proportion   | Passenger Demand from Proposed Development (pax/hr) |              |
|----------------------------------|--------------|---|--------------|
|                                  |              | AM  | PM           |
| MTR                              | 40.0%        | 1,673   | 1,394        |
| Bus                              | 30.1%        | 1,258   | 1048         |
| GMB                              | 10.0%        | 417   | 347          |
| PV & Taxi                        | 4.7%         | 198   | 165          |
| On foot                          | 10.5%        | 439   | 366          |
| Others                           | 4.7%         | 196   | 163          |
| <b>Total</b>                     | <b>100%</b>  | 4,181   | 3,484        |
| <b>Total in Public Transport</b> | <b>80.1%</b> | <b>3,348</b>  | <b>2,789</b> |

4.7.4 According to the above table, it is estimated that the total passenger demand of public transport associated with the proposed development in the morning peak hour and evening peak hour would be approx. 3,348 pax/hr and 2,789 pax/hr respectively

4.7.5 To evaluate the associated impact likely to be induced by the Proposed Development on public transport, the future occupancy of public transport services with the Proposed Development where the estimated bus passengers, GMB passenger and MTR passenger demand associated with the Proposed Development are taken into account. It is also assumed that all passenger heading to Lai King or Mei Foo MTR station will take bus/GMB for interchange, therefore inclusive as the road-based public transport demand for conservative assessment purpose.

4.7.6 Similar to the traffic forecast, a growth rate of **+0.5% p.a.** is adopted for projecting the existing bus passenger demand to Year 2035 demand.

4.7.7 Occupancy surveys for the existing public transport were carried out on 12<sup>th</sup> March 2024 at the public transport facilities in the vicinity. The survey results and the peak hour trips of franchised bus and GMB routes in the vicinity are presented in **Table 4.7.3**.

**Table 4.7.3 Peak Hour Trips of Franchised Bus and GMB routes**

| Route No.   | Origin / Destination          |                               | Observed Peak Hour Trips (trips/hr) |    | Total Observed Capacity |      | Observed Occupancy Rate (%) |     | Remaining Capacity |      |
|---|-------------------------------|-------------------------------|-------------------------------------|----|-------------------------|------|-----------------------------|-----|--------------------|------|
|   |                               |                               | AM                                  | PM | AM                      | PM   | AM                          | PM  | AM                 | PM   |
| KAU WAH KENG BUS STOP(LAI KING HILL ROAD EAST BOUND)  |                               |                               |                                     |    |                         |      |                             |     |                    |      |
| Franchised Bus  |                               |                               |                                     |    |                         |      |                             |     |                    |      |
| 30  | Allway Gardens                | Cheung Sha Wan                | 1                                   | 2  | 90                      | 180  | 11%                         | 11% | 80                 | 160  |
| 32H   | Cheung Shan                   | Lai Chi Kok                   | -                                   | 1  | -                       | 76   | -                           | 5%  | -                  | 72   |
| 42  | Tsing Yi (Cheung Hong Estate) | Shun Lee                      | 3                                   | 3  | 398                     | 383  | 17%                         | 20% | 332                | 308  |
| 45  | Lai Yiu                       | Kowloon City Ferry B/T        | 2                                   | 2  | 250                     | 250  | 28%                         | 37% | 179                | 158  |
| 46  | Lai Yiu                       | Jordan (West Kowloon Station) | 3                                   | 4  | 339                     | 501  | 36%                         | 27% | 218                | 368  |
| 46X   | Hin Keng                      | Mei Foo                       | 7                                   | 6  | 953                     | 817  | 8%                          | 11% | 881                | 726  |
| GMB   |                               |                               |                                     |    |                         |      |                             |     |                    |      |
| 90M   | Highland Park                 | Mei Foo Station               | 5                                   | 5  | 89                      | 83   | 38%                         | 46% | 55                 | 45   |
| 90P   | Princess Margaret Hospital    | Mei Foo Station               | 21                                  | 17 | 372                     | 299  | 15%                         | 82% | 317                | 53   |
| 92M   | Wah Yuen Chuen                | Mei Foo Station               | 5                                   | 4  | 80                      | 64   | 36%                         | 42% | 51                 | 37   |
| KAU WAH KENG BUS STOP (LAI KING HILL ROAD WEST BOUND) |                               |                               |                                     |    |                         |      |                             |     |                    |      |
| Franchised Bus  |                               |                               |                                     |    |                         |      |                             |     |                    |      |
| 30  | Cheung Sha Wan                | Allway Gardens                | 1                                   | 2  | 68                      | 158  | 9%                          | 6%  | 62                 | 149  |
| 32H   | Lai Chi Kok                   | Cheung Shan                   | -                                   | 1  | -                       | 76   | -                           | 11% | -                  | 68   |
| 42  | Shun Lee                      | Tsing Yi (Cheung Hong Estate) | 3                                   | 3  | 396                     | 411  | 9%                          | 7%  | 359                | 381  |
| 45  | Kowloon City Ferry B/T        | Lai Yiu                       | 2                                   | 2  | 250                     | 250  | 10%                         | 10% | 225                | 226  |
| 46  | Jordan (West Kowloon Station) | Lai Yiu                       | 3                                   | 2  | 340                     | 215  | 7%                          | 7%  | 315                | 199  |
| 46X   | Mei Foo                       | Hin Keng                      | 7                                   | 9  | 943                     | 1228 | 13%                         | 3%  | 820                | 1188 |
| GMB   |                               |                               |                                     |    |                         |      |                             |     |                    |      |
| 90M   | Mei Foo Station               | Highland Park                 | 6                                   | 4  | 99                      | 67   | 74%                         | 61% | 26                 | 26   |
| 90P   | Mei Foo Station               | Princess Margaret Hospital    | 18                                  | 13 | 309                     | 223  | 86%                         | 35% | 43                 | 144  |
| 92M   | Mei Foo Station               | Wah Yuen Chuen                | 5                                   | 3  | 80                      | 48   | 64%                         | 83% | 29                 | 8    |

| Route No.                | Origin / Destination |                            | Observed Peak Hour Trips (trips/hr) |    | Total Observed Capacity |     | Observed Occupancy Rate (%) |     | Remaining Capacity |     |
|--------------------------|----------------------|----------------------------|-------------------------------------|----|-------------------------|-----|-----------------------------|-----|--------------------|-----|
|                          |                      |                            | AM                                  | PM | AM                      | PM  | AM                          | PM  | AM                 | PM  |
| LAI CHI KOK BUS TERMINUS |                      |                            |                                     |    |                         |     |                             |     |                    |     |
| Franchised Bus           |                      |                            |                                     |    |                         |     |                             |     |                    |     |
| 6                        | Lai Chi Kok          | Star Ferry                 | 5                                   | 5  | 631                     | 676 | 19%                         | 10% | 513                | 611 |
| 171                      | Lai Chi Kok          | South Horizons             | 4                                   | 6  | 543                     | 813 | 6%                          | 1%  | 510                | 808 |
| 904                      | Lai Chi Kok          | Kennedy Town (Belcher Bay) | 2                                   | 3  | 268                     | 375 | 3%                          | 1%  | 260                | 373 |
| 905                      | Lai Chi Kok          | Exhibition Centre Station  | 6                                   | 5  | 826                     | 702 | 6%                          | 0%  | 777                | 700 |
| 905P                     | Lai Chi Kok          | Wan Chai (Harbour Road)    | 2                                   | -  | 273                     | -   | 3%                          | -   | 266                | -   |

4.7.8 The distance from the subject site to Lai Chi Kok Bus Terminus is approximate 350m which is within a reasonable walking distance. According to the interview survey conducted in July 2022, approx. 35% of residents of Kau Wah Keng Old Village and Kau Wah Keng New Village are currently using the franchise bus service at the Lai Chi Kok Bus Terminus. The composition 65% and 35% of estimated public transport demand would use the public transport services at Lai King Hill Road and Lai Chi Kok Bus Terminus respectively.

4.7.9 For conservative assessment purpose, only one traffic bound of the bus routes at the enroute stop at the Kau Wah Keng Bus Stop with Lai Chi Kok Bus Terminus are taken into account for the public transport assessment. The assessment results in AM and PM Peak are summarized in **Table 4.7.4** and **Table 4.7.5** below respectively.

**Table 4.7.4 Year 2035 Public Transport Occupancy and Public Transport Demand Associated with the Proposed Development in AM Peak**

| Public Transport Service | 2035 Design Scenario             |                      |                                  |                      |                          |                      |  |                          |
|--------------------------|----------------------------------|----------------------|----------------------------------|----------------------|--------------------------|----------------------|--|--------------------------|
|                          | On-street Facilities (Eastbound) |                      | On-street Facilities (Westbound) |                      | Lai Chi Kok Bus Terminus |                      | PT Demand Generated by Proposed Development <sup>(1)</sup> |                          |
|                          | No. of trips                     | Total Spare Capacity | No. of trips                     | Total Spare Capacity | No. of trips             | Total Spare Capacity | On-street Facilities                                       | Lai Chi Kok Bus Terminus |
| Franchised Bus           | 16                               | 1,690                | 16                               | 1,781                | 19                       | 2,326                | 2,176  | 1,172                    |
| GMB                      | 31                               | 423                  | 29                               | 98                   |                          |                      |  |                          |
| <b>Total</b>             | <b>47</b>                        | <b>2,113</b>         | <b>45</b>                        | <b>1,879</b>         |                          |                      |  |                          |

Notes:

(1) It is assumed that all passenger heading to Lai King or Mei Foo MTR station will take bus/GMB for interchange for conservative assessment of the public transport demand.

**Table 4.7.5 Year 2035 Public Transport Occupancy and Public Transport Demand Associated with the Proposed Development in PM Peak**

| Public Transport Service | 2035 Design Scenario             |                      |                                  |                      |                          |                      |  |                          |
|--------------------------|----------------------------------|----------------------|----------------------------------|----------------------|--------------------------|----------------------|--|--------------------------|
|                          | On-street Facilities (Eastbound) |                      | On-street Facilities (Westbound) |                      | Lai Chi Kok Bus Terminus |                      | PT Demand Generated by Proposed Development <sup>(1)</sup> |                          |
|                          | No. of trips                     | Total Spare Capacity | No. of trips                     | Total Spare Capacity | No. of trips             | Total Spare Capacity | On-street Facilities                                       | Lai Chi Kok Bus Terminus |
| Franchised Bus           | 18                               | 1,792                | 19                               | 2,211                | 19                       | 2,492                | 1,813  | 976                      |
| GMB                      | 26                               | 135                  | 20                               | 178                  |                          |                      |  |                          |
| <b>Total</b>             | <b>44</b>                        | <b>1,927</b>         | <b>39</b>                        | <b>2,389</b>         |                          |                      |  |                          |

Notes:

(1) It is assumed that all passenger heading to Lai King or Mei Foo MTR station will take bus/GMB for interchange for conservative assessment of the public transport demand.

- 4.7.10 Referring to **Table 4.7.4** and **Table 4.7.5** above, the results reveal that the overall spare capacity of the assessed franchised bus and GMB routes would not be adequate to cater for the public transport demand associated with Proposed Development in the AM Peak Hour.

**Proposal of Feeder Service**

- 4.7.11 According to the **Table 4.7.4** and **Table 4.7.5**, it is estimated that the passenger demand of public transport associated with the proposed development on street facilities would be approximate 2,176 pax/hr in the AM peak hour, which would overload the existing public service, with the available spare capacity of approximate 1,879 pax/hr (WB) and 2,113 pax/hr (EB) in the AM peak hour. Since there is less spare capacity on the WB traffic, WB is selected for comparison for conservative purpose.

- 4.7.12 To cater for the shortage in public transport services, the applicant proposed to provide feeder services to the nearby MTR station or bus interchange and to minimise adverse impact to the existing public transport services. Feeder service from the application site to Lai King Station is proposed. Detail of the proposed feeder service is summarised below in **Table 4.7.6**. The layby for the feeder service is shown in the MLP in drawing **Figure 3.1**.

**Table 4.7.6 Proposed Feeder Service for the Application Site**

| Item                          | AM  | PM |
|-------------------------------|---|----|
| Routing                       | To/from Application Site and nearby MTR Station / Bus Interchange |    |
| Average Handling Capacity     | 50 Passengers   |    |
| Headway                       | 10 minutes<br>(subject to road traffic condition)                 | -  |
| Level of Service in Peak Hour | 6 trips/hr  | -  |
| Hourly Capacity               | Approx. 300 pax/hr  | -  |

- 4.7.13 The proposed feeder service would provide adequate capacity (approx. 300 pax/hr in the AM peak) to cater for the exceeded peak hour passenger trip generation (approx. 297 pax/hr).
- 4.7.14 Subject to the actual demand, the proposed feeder service could be reviewed and adjusted accordingly.

## 4.8 Pedestrian Impact Assessment

### Pedestrian Generation

- 4.8.1 Similar to **Chapter 4.7 Section 4.7.2**, pedestrian generation from the Proposed Development for AM and PM Peak is estimated with reference to "Travel Characteristics Survey (TCS) 2011" published by Transport Department and "2021 Population Census" published by Census and Statistics Department. The pedestrian generation is shown in **Table 4.8.1** below.

**Table 4.8.1 Pedestrian Generation by the Proposed Development**

| Pedestrian Generation (ppl/hr) <sup>(1)</sup> |         |
|---|---------|
| AM Peak                                       | PM Peak |
| 3,787   | 3,155   |

Note: (1) Pedestrian generation by the Proposed Development is assumed to be people who will take MTR, road-based transport and walk. The pedestrian trip generation and attraction been derived based on the modal split in **Table 4.7.2**.

### Assessment Scenarios

- 4.8.2 Similar to the traffic impact assessment, year 2035 is adopted as the design year of pedestrian assessment. Annual growth rate of **+0.5% p.a.** is adopted to produce the pedestrian forecasts for 2024–2035 to derive year 2035 peak hour background pedestrian flows. Additionally, the future pedestrian volumes generated by the proposed development are taken into account for year 2035 pedestrian flows.
- 4.8.3 Similarly, to evaluate the associated pedestrian impact likely to be induced by the proposed development, two scenarios were analysed and compared.
- 4.8.4 The first scenario (i.e. Year 2035 Reference Scenario) refers to the future pedestrian flows assumed the existing land lot to be developed as the **Approved Scheme** overall PR of not more than 5, while the second scenario (i.e. Year 2035 Design Scenario) refers to the future pedestrian flow with the **Proposed Scheme** with domestic PR of not more than 6 and non-domestic PR of not more than 0.5 is in place.
- 4.8.5 As mentioned in **Chapter 3.2**, it is proposed to shift the pedestrian crossing due to conflict with proposed western vehicular access of the Proposed Development.
- 4.8.6 Having considered the location of public transport facilities, it is expected the pedestrians generated by the development would mainly pass through the pedestrian crossing at Lai King Hill Road, then access to the bus stops at Lai King Hill Road westbound or to the Mei Foo MTR Station via Lai Yan Court. The assumed route for pedestrian flow generated and the locations of assessed pedestrian facilities are shown in **Figure 4.5**.

### **Performance of Pedestrian Facilities in Year 2035**

4.8.7 In order to address the performance of the concerned pedestrian facilities, Level of Service (LOS) assessment of the critical footpaths have been conducted for Year 2035 Reference and Design Scenarios.

4.8.8 **Table 4.8.1** to **Table 4.8.4** summarized the peak pedestrian flow and the pedestrian assessment results at the critical footpaths under the Year 2035 Reference and Design Scenarios.

**Table 4.8.1 Design Year 2035 Level of Service in AM and PM Peaks along Key Footpath under Reference Scenario**

| Footpath |  | Actual Width (m) | Effective Clear Width <sup>(1)</sup> (m) | Two-way Peak Hourly Flow (ped/hr) |       | Flow Rate <sup>(2)</sup> (ped/min/m) |      | LOS (Level) |    |
|----------|--|------------------|--|-----------------------------------|-------|--------------------------------------|------|-------------|----|
|          |  |                  |  | AM                                | PM    | AM                                   | PM   | AM          | PM |
| F1(W)    | Lai King Hill Road Northern Footpath               | 2.5              | 1.5                                      | 1,115                             | 765   | 14.9                                 | 10.2 | A           | A  |
| F1(W)a   | Lai King Hill Road Northern Footpath (at bus stop) | 3.8              | 1.8                                      | 1,115                             | 765   | 12.4                                 | 8.5  | A           | A  |
| F1(E)    | Lai King Hill Road Northern Footpath               | 2.5              | 1.5                                      | 945                               | 670   | 12.6                                 | 8.9  | A           | A  |
| F2       | Lai King Hill Road Southern Footpath               | 2.8              | 1.8                                      | 1,840                             | 1,260 | 20.4                                 | 14.0 | B           | A  |
| F2a      | Lai King Hill Road Southern Footpath (at bus stop) | 3.5              | 1.5                                      | 1,840                             | 1,260 | 24.5                                 | 16.8 | C           | B  |
| F3       | Wa Lai Path Footpath                               | 9.5              | 8.5                                      | 1,515                             | 1,030 | 3.6                                  | 2.4  | A           | A  |

Notes:

- (1) Effective clear width = Actual width (on-site measurement) minus 0.5m dead width on both sides, and minus the width of passengers queuing at bus stops.
- (2) Pedestrian flow rates are computed based on effective clear width, with 1.2 peak factor applied for the peak minute flow rate.

**Table 4.8.2 Design Year 2035 Level of Service in AM and PM Peaks along Key Pedestrian Crossing under Reference Scenario**

| Crossing Facility |   | Clear Width (m) | Cycle Time (s) |    | Green Time Proportion |     | Pedestrian Capacity <sup>(1)</sup> (ped/hr) |       | Two-way Pedestrian Flow (ped/hr) |       | Volume/ Capacity (V/C) Ratio |      |
|-------------------|---|-----------------|----------------|----|-----------------------|-----|---|-------|----------------------------------|-------|------------------------------|------|
|                   |   |                 | AM             | PM | AM                    | PM  | AM  | PM    | AM                               | PM    | AM                           | PM   |
| C1                | Pedestrian Crossing Across Lai King Hill Road | 4.2             | 60             | 60 | 28%                   | 28% | 2,230                                       | 2,230 | 1,755                            | 1,430 | 0.79                         | 0.64 |

Notes:

- (1) Crossing Capacity (ped/hr) = K (1,900 ped/m/hr) x Green Time Proportion x W (width of crossing)



**Table 4.8.3 Design Year 2035 Level of Service in AM and PM Peaks along Key Footpath under Design Scenario**

| Footpath |  | Actual Width (m) | Effective Clear Width <sup>(1)</sup> (m) | Two-way Peak Hourly Flow (ped/hr) |       | Flow Rate <sup>(2)</sup> (ped/min/m) |      | LOS (Level) |    |
|----------|--|------------------|--|-----------------------------------|-------|--------------------------------------|------|-------------|----|
|          |  |                  |  | AM                                | PM    | AM                                   | PM   | AM          | PM |
| F1(W)    | Lai King Hill Road Northern Footpath               | 2.5              | 1.5                                      | 1,235                             | 1,145 | 16.5                                 | 15.3 | B           | A  |
| F1(W)a   | Lai King Hill Road Northern Footpath (at bus stop) | 3.8              | 1.8                                      | 1,235                             | 1,145 | 13.7                                 | 12.7 | A           | A  |
| F1(E)    | Lai King Hill Road Northern Footpath               | 2.5              | 1.5                                      | 1,055                             | 1,055 | 14.1                                 | 14.1 | A           | A  |
| F2       | Lai King Hill Road Southern Footpath               | 2.8              | 1.8                                      | 1,915                             | 1,235 | 21.3                                 | 13.7 | B           | A  |
| F2a      | Lai King Hill Road Southern Footpath (at bus stop) | 3.5              | 1.5                                      | 1,915                             | 1,235 | 25.5                                 | 16.5 | C           | B  |
| F3       | Wa Lai Path Footpath                               | 9.5              | 8.5                                      | 1,570                             | 975   | 3.7                                  | 2.3  | A           | A  |

Notes:

- (1) Effective clear width = Actual width (on-site measurement) minus 0.5m dead width on both sides, and minus the width of passengers queuing at bus stops.
- (2) Pedestrian flow rates are computed based on effective clear width, with 1.2 peak factor applied for the peak minute flow rate.

**Table 4.8.4 Design Year 2035 Level of Service in AM and PM Peaks along Key Pedestrian Crossing under Design Scenario**

| Crossing Facility |   | Clear Width (m) | Cycle Time (s) |    | Green Time Proportion |     | Pedestrian Capacity <sup>(1)</sup> (ped/hr) |       | Two-way Pedestrian Flow (ped/hr) |       | Volume/ Capacity (V/C) Ratio |      |
|-------------------|---|-----------------|----------------|----|-----------------------|-----|---|-------|----------------------------------|-------|------------------------------|------|
|                   |   |                 | AM             | PM | AM                    | PM  | AM  | PM    | AM                               | PM    | AM                           | PM   |
| C1                | Pedestrian Crossing Across Lai King Hill Road | 4.2             | 60             | 60 | 28%                   | 28% | 2,230                                       | 2,230 | 1,830                            | 1,180 | 0.82                         | 0.53 |

Notes:

- (1) Crossing Capacity (ped/hr) = K (1,900 ped/m/hr) x Green Time Proportion x W (width of crossing)

4.8.9 As shown in the tables above, the assessed footpaths and pedestrian crossing would be operating with desirable walking conditions at LOS "A" to "C" and V/C ratio less than 0.85 under both Reference and Design Scenario in year 2035. The pedestrian facilities would hence be adequate to cater for the additional pedestrian demand generated from the Proposed Development in design year 2035.

## 5 TRAFFIC IMPACT ASSESSMENT (INTERIM SCENARIO)

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- 5.1.1 As the applicant is currently not the only land owner of this Application Site, phased development of this Application Site is proposed with Phase 1A, Phase 1B developments to be developed by the Applicant. The implementation of the Remaining Phases A and B will be subject to actual development plan by third-parties.
- 5.1.2 Interim traffic assessment is conducted to reveal the traffic impact with only completion and population intake of the proposed Phase 1A, Phase 1B developments to be developed by the Applicant, and the development of Remaining Phase A and Remaining Phase B by third-parties.

### **Assessment Scenarios**

- 5.1.3 To evaluate the associated traffic impact likely to be induced by the partial completion of the site, interim scenarios assuming the phased development are set up as below

#### **Interim Scenario A, assuming only completion of P1A & P1B**

Year 2035 Interim Scenario A

= Year 2024 observed traffic flows × growth factor during the period of year 2024-2035

*plus* traffic generations of adjacent major planned/committed developments in the vicinity

*plus* trip generation and attraction of the proposed P1A and P1B

#### **Interim Scenario B, assuming only completion of P1A & P1B & RPA**

Year 2035 Interim Scenario B

= Year 2035 Interim Scenario A

*plus* trip generation and attraction of Remaining Phase A

#### **Interim Scenario C, assuming only completion of P1A & P1B & RPB**

Year 2035 Interim Scenario C

= Year 2035 Interim Scenario A

*plus* trip generation and attraction of Remaining Phase B

## **Trip Generation and Attraction**

5.1.4 The traffic generation and attraction trips for the interim scenarios in year 2035 is summarised in **Table 5.1.1**.

**Table 5.1.1 Traffic Generation and Attraction of Proposed Residential Development (pcu/hr)**

| Proposed Development                                  | AM         |            | PM         |            |
|---|------------|------------|------------|------------|
|   | Gen        | Att        | Gen        | Att        |
| Phase 1A  | 172        | 102        | 74         | 97         |
| Phase 1B  | 126        | 76         | 55         | 72         |
| Remaining Phase A                                     | 100        | 59         | 43         | 57         |
| Remaining Phase B                                     | 206        | 120        | 87         | 113        |
| <b>Interim Scenario A (P1A+P1B)</b>                   | <b>298</b> | <b>178</b> | <b>129</b> | <b>169</b> |
| <b>Interim Scenario B (P1A+P1B+RPA)<sup>(1)</sup></b> | <b>398</b> | <b>237</b> | <b>172</b> | <b>226</b> |
| <b>Interim Scenario C (P1A+P1B+RPB)<sup>(1)</sup></b> | <b>504</b> | <b>298</b> | <b>216</b> | <b>282</b> |

5.1.5 As indicated in **Table 5.1.1**, the total trip generated by the proposed development in the morning and evening peak would be around 476 pcu/hr and 298 pcu/hr (two-way) under Interim Scenario A, 635 pcu/hr and 398 pcu/hr (two-way) under Interim Scenario B, and 802 pcu/hr and 498 pcu/hr (two-way) under Interim Scenario C respectively.

5.1.6 The forecasted traffic flows for the above assessment scenario is presented in **Figures 5.1** to **Figure 5.3**.

## **5.2 Junction Capacity Assessment**

5.2.1 Junction capacity assessment was carried out at the identified key junctions for Year 2035 Interim Scenario A, Interim Scenario B and Interim Scenario C. Assessment results for the key junctions are summarized in **Table 5.2.1** below and the detailed calculations are appended in **Appendix A**.

**Table 5.2.1 Year 2035 Future Junction Performance**

| Junction |  | Type       | Scenario A                 |       | Scenario B                 |       | Scenario C                 |       |
|----------|--|------------|----------------------------|-------|----------------------------|-------|----------------------------|-------|
|          |  |            | Performance <sup>(1)</sup> |       | Performance <sup>(1)</sup> |       | Performance <sup>(1)</sup> |       |
|          |  |            | AM                         | PM    | AM                         | PM    | AM                         | PM    |
| J1       | Lai King Hill Road / King Lai Path                         | Signalized | >100%                      | >100% | >100%                      | >100% | >100%                      | >100% |
| J2       | Lai King Hill Road / Ching Shan Terrance / Estate Road     | Signalized | >100%                      | >100% | >100%                      | >100% | >100%                      | >100% |
| J3_a     | Lai King Hill Road / Kwai Chung Interchange <sup>(2)</sup> | Signalized | 13%                        | 42%   | 8%                         | 35%   | 2%                         | 27%   |
| J3_b     | Lai King Hill Road / Kwai Chung Interchange <sup>(3)</sup> | Signalized | -13%                       | 4%    | -17%                       | -1%   | -21%                       | -6%   |
| J3_c     | Lai King Hill Road / Kwai Chung Interchange <sup>(4)</sup> | Signalized | 16%                        | 39%   | 15%                        | 34%   | 15%                        | 30%   |
| J4       | Mei Lai Road/ Lai Wan Road                                 | Signalized | >100%                      | >100% | >100%                      | >100% | >100%                      | >100% |
| J5       | Mei Lai Road/ Cheung Sha Wan Road                          | Signalized | 45%                        | 54%   | 42%                        | 52%   | 38%                        | 50%   |

Notes:

- (1) Figures shown represent "Reserve Capacity" (RC) in % for signalized junctions.
- (2) J3 under existing junction configuration.
- (3) J3 with TD planned improvement works.
- (4) Junction modification scheme in approved planning application (No. A/KC/489) is incorporated for assessment.

**5.2.2** The above results reveal that for all Interim Scenarios, all identified key junctions would operate within capacity in Year 2035, with the junction modification scheme in approved planning application (No. A/KC/489).

## 5.3 Link Capacity Assessment

**5.3.1** Link capacity assessment was carried out at the identified road links for Year 2035 Interim Scenarios. Assessment results are summarized in **Table 5.3.1** below.

**Table 5.3.1 Year 2035 Future Link Performance <sup>(1)</sup>**

| Road Link <sup>(2)</sup> |  | Direction | Unit   | Link Capacity | Traffic Flows (pcu/hr) |       |                    |       |                    |       | Volume/Capacity (V/C) Ratio |      |                    |      |                    |      |
|--------------------------|--|-----------|--------|---------------|------------------------|-------|--------------------|-------|--------------------|-------|-----------------------------|------|--------------------|------|--------------------|------|
|                          |  |           |        |               | Interim Scenario A     |       | Interim Scenario B |       | Interim Scenario C |       | Interim Scenario A          |      | Interim Scenario B |      | Interim Scenario C |      |
|                          |  |           |        |               | AM                     | PM    | AM                 | PM    | AM                 | PM    | AM                          | PM   | AM                 | PM   | AM                 | PM   |
| L1                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 1,517                  | 1,356 | 1,628              | 1,425 | 1,744              | 1,495 | 0.63                        | 0.57 | 0.68               | 0.60 | 0.73               | 0.63 |
|                          |  |           | veh/hr | 2,200         | 1,246                  | 1,124 | 1,340              | 1,183 | 1,435              | 1,241 | 0.57                        | 0.51 | 0.61               | 0.54 | 0.65               | 0.56 |
| L2                       | Lai King Hill Road (8m wide section)       | Two-way   | pcu/hr | 1,850         | 1,052                  | 751   | 1,163              | 820   | 1,279              | 890   | 0.57                        | 0.41 | 0.63               | 0.44 | 0.69               | 0.48 |
|                          |  |           | veh/hr | 1,700         | 863                    | 627   | 955                | 685   | 1,052              | 743   | 0.51                        | 0.37 | 0.56               | 0.40 | 0.62               | 0.44 |
| L3                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 937                    | 786   | 1,048              | 855   | 1,164              | 925   | 0.39                        | 0.33 | 0.44               | 0.36 | 0.49               | 0.39 |
|                          |  |           | veh/hr | 2,200         | 765                    | 654   | 857                | 712   | 954                | 770   | 0.35                        | 0.30 | 0.39               | 0.32 | 0.43               | 0.35 |
| L4                       | Lai King Hill Road (10m wide section)      | Two-way   | pcu/hr | 2,390         | 869                    | 800   | 916                | 830   | 967                | 859   | 0.36                        | 0.33 | 0.38               | 0.35 | 0.40               | 0.36 |
|                          |  |           | veh/hr | 2,200         | 722                    | 668   | 762                | 694   | 804                | 718   | 0.33                        | 0.30 | 0.35               | 0.32 | 0.37               | 0.33 |
| L5                       | Kwai Chung Interchange (6.8m wide section) | NB        | pcu/hr | 2,800         | 1050                   | 666   | 1088               | 702   | 1127               | 738   | 0.38                        | 0.24 | 0.39               | 0.25 | 0.40               | 0.26 |
|                          |  |           | veh/hr | 2,600         | 869                    | 552   | 901                | 582   | 933                | 612   | 0.33                        | 0.21 | 0.35               | 0.22 | 0.36               | 0.24 |
| L6                       | Kwai Chung Interchange (6m wide section)   | SB        | pcu/hr | 1,400         | 644                    | 694   | 709                | 722   | 778                | 751   | 0.46                        | 0.50 | 0.51               | 0.52 | 0.56               | 0.54 |
|                          |  |           | veh/hr | 1,300         | 534                    | 571   | 588                | 595   | 645                | 619   | 0.41                        | 0.44 | 0.45               | 0.46 | 0.50               | 0.48 |

Notes:

- (1) Link capacity estimated according to TPDM Vol.2 Ch.2.4, for single 2-lane carriageway (for L1 to L4 with road width of 8m and 10m) or for dual 2-lane carriageway (for L5 and L6 with road width of 6m and 6.8m). Data in term of veh/hr and pcu/hr are converted according to survey pcu factor.
- (2) For conservative approach, the road links are assessed based on the greatest traffic flows at the road sections of corresponding roads within AOI.

**5.3.2** As shown in the table above, the identified road section would continue to have sufficient link capacity to cater for the future traffic demand with the proposed development by Year 2035. The proposed development would not induce adverse traffic impact to the surrounding road network during the interim stage.

## 5.4 Public Transport Services – Interim Scenario

5.4.1 The increase in demand on public transport service under the Interim Scenarios are estimated with the same methodology as presented in **Chapter 4.7.** and summarised in **Table 5.4.1** below.

**Table 5.4.1 Passenger Trips Generated from Proposed Development in Interim Scenario**

|  | Interim Scenario A |       | Interim Scenario B |       | Interim Scenario C |       |
|--|--------------------|-------|--------------------|-------|--------------------|-------|
| <b>No. of Flats</b>  | 3,457 flats        |       | 4,615 flats        |       | 5,894 flats        |       |
| <b>Population *</b>  | 9,333              |       | 12,459             |       | 15,912             |       |
| <b>Peak Hours Passenger Trip Generation **</b><br>(pax/hr)                             | AM                 | PM    | AM                 | PM    | AM                 | PM    |
|  | 2,050              | 1,708 | 2,736              | 2,280 | 3,495              | 2,912 |
| <b>Passenger Demand from Proposed Development for On-street Facilities</b><br>(pax/hr) | 1,067              | 889   | 1,424              | 1,187 | 1,819              | 1,516 |
| <b>Total Spare Capacity for On-Street Facilities (EB)</b>                              | 2,113              | 1,927 | 2,113              | 1,927 | 2,113              | 1,927 |
| <b>Total Spare Capacity for On-Street Facilities (WB)</b>                              | 1,879              | 2,389 | 1,879              | 2,389 | 1,879              | 2,389 |

\* Person Per Occupied Flat (PPOF) of 2.7 is assumed based on the 2021 census of Kwai Tsing District

\*\* According to "Travel Characteristics Survey (TCS) 2011" published by Transport Department, the daily mechanised trip rate is 1.83 trips per person and the morning peak and evening peak accounted for about 12% and 10% of the daily trips.

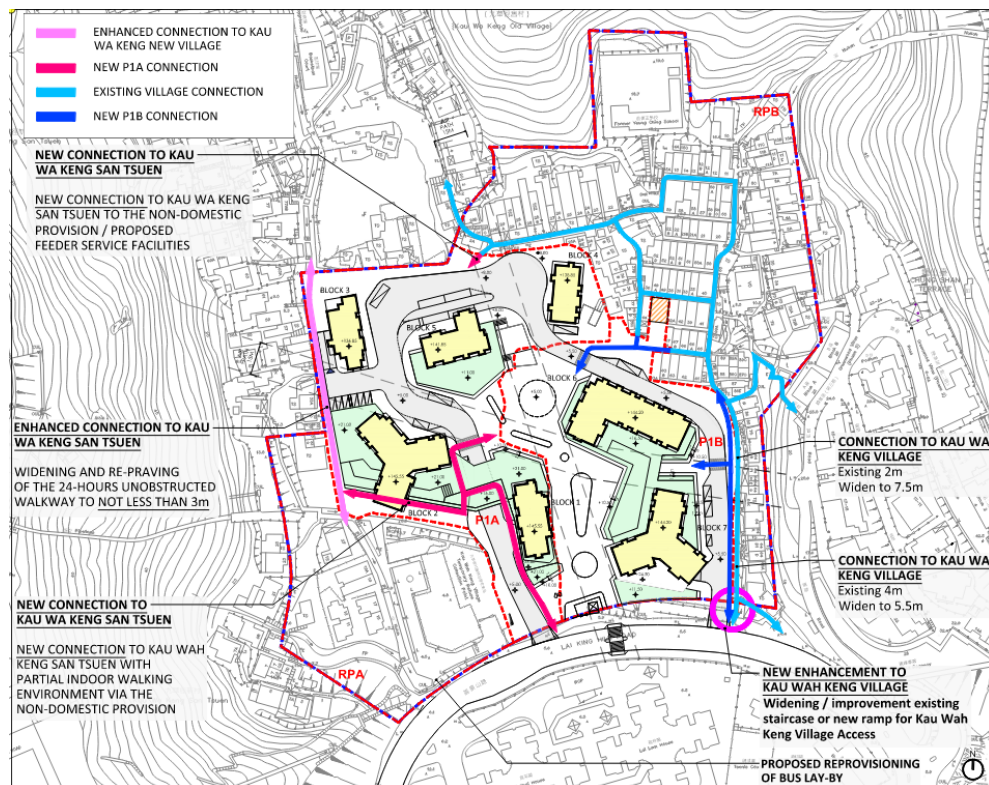
5.4.2 Referring to **Table 5.4.1** above, the results reveal that the overall spare capacity of the assessed franchised bus and GMB routes would be adequate to cater for the public transport demand associated with Proposed Development in the AM and PM peak hours under Interim Scenarios A, B, and C.

## 5.5 Pedestrian Walking Condition – Interim Scenario

5.5.1 In **Chapter 4.8**, it is revealed that under the ultimate stage, the assessed footpaths and pedestrian crossing would be operating with desirable walking conditions. The pedestrian facilities would hence be adequate to cater for the additional pedestrian demand generated from the P1A and P1B of the Proposed Development.

### Additional Pedestrian Enhancements

5.5.2 In view that the residents living in existing Kau Wa Keng San Tsuen and Kau Wah Keng Old Village will be using the existing footpaths adjacent to the boundary of P1A and P1B to/from Lai King Hill Road, the Applicant would take the opportunity of the Phase 1A, Phase 1B accessibility for these two existing villages. The widened public access will be provided at all times. **Diagram 1** below illustrated the proposed additional pedestrian enhancement.



**Diagram 1 Proposed Additional Pedestrian Enhancements**

5.5.3 Kau Wa Keng San Tsuen is currently accessible from Lai King Hill Road via the existing footpath along the nullah at the western fringe of the P1A and RPA. In the Interim Scenario, the footpath section within P1A is proposed to be widened from the existing 1.5 m width to not less than 3m wide (through zone) in accordance with the Hong Kong Planning Standards and Guidelines (HKPSG) width standard for footpaths/walkways in rural land use, and to be open for public access at all times, and connects with the existing footpath within RPA.

5.5.4 In addition, new connections to Kau Wah Keng New Village with partial indoor walking environment via the non-domestic provision and the proposed feeder service facilities will be provided within P1A.

- 5.5.5 The existing walkway to Kau Wa Keng Old Village from Lai King Hill Road falls entirely within RPB, which is currently of 2m in width at the narrowest section. In the Interim Scenario, voluntary setback will be provided along the eastern boundary of P1B such that the walkway will be widened from the current minimum of 2m to a minimum of 5.5 m. To further enhance walkability of pedestrian to/from Kau Wa Keng Old Village, widening / improvement existing staircase or new ramp at the or Kau Wah Keng Village Access will be provided. Street furniture and landscaping features such as path lighting and tree planting will be provided along the widened part of walkway within P1B.
- 5.5.6 With the above additional pedestrian enhancement, it is expected that the performance of the existing pedestrian facilities would be maintained if not improved.



## 6 CONCLUSION

### 6.1 Summary

6.1.1 The Application Site falls within the "Comprehensive Development Area" zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung on the Approved Kwai Chung Outline Zoning Plan (OZP) No. S/KC/32.

6.1.2 The Applicant submitted a S16 Planning Application No. A/KC/489. The comprehensive development proposed in the Planning Application No. A/KC/489 ("**Approved Scheme**"), comprises 14 residential blocks with an overall PR of not more than 5 and maximum BH of not more than +120mPD.

6.1.3 The Planning Application No. A/KC/489 was deliberated in the TPB Metro Planning Committee Meeting held on 14 July 2023 (the TPB Meeting). During the TPB meeting, TPB members raised concerns on the provision of social welfare facilities and retail shops, as quoted from the meeting minutes<sup>[1]</sup>

- *"Some Members considered that retail facilities should be provided in the proposed development to cater for the daily needs of the future residents."* and *"Some Member shared the view that the provision of social welfare facilities in the proposed development was inadequate..."*.
- *"the development intensity of the proposed development could be increased for better land utilisation, e.g. provision of retail and more GIC facilities."*

After deliberation, the Planning Application No. A/KC/489 was approved with conditions.

*[1] Minutes of 722nd Meeting of the Metro Planning Committee held at 9:00 a.m. on 14.7.2023*

6.1.4 The Applicant takes the initiative to review the **Approved Scheme** and endeavours to take forward the provision of more of social welfare facilities and retail shops. The **Proposed Scheme**, keeping the phasing strategy adopted in the **Approved Scheme**, comprises 15 building blocks (including 14 building blocks with residential use) with domestic PR of not more than 6 and maximum BH of not more than +147.55mPD. Non-domestic PR of not more than 0.5 is designated for proposed retail shops, existing historical buildings, and social welfare facilities to nurture an inclusive and liveable community in the convenient location of Kwai Chung Area.

6.1.5 A Traffic Impact Assessment (TIA) study was carried out to evaluate the likely traffic impact associated with the proposed development, in support of the Section 16 application for the application site.

6.1.6 The proposed provision of internal parking and servicing facilities for each site of the subject development is in full compliance with the HKPSG requirements and will be self-contained within the respective site boundary. Vehicles will access to/from each site of the subject



development through the respective vehicular access at Lai King Hill Road.

- 6.1.7 The identified key junctions in the vicinity were assessed with respect to traffic generation of the proposed development upon Year 2035 (3 years after the target Completion Year 2032), taking into account the traffic generation by the major planned/recently constructed developments in the vicinity.
- 6.1.8 Traffic impact assessment scenarios were set up for the proposed development, namely Year 2035 Reference scenario (the existing land lot to be developed as the **Approved Scheme** overall PR of not more than 5) and Year 2035 Design scenario (the existing land lot to be developed as the **Proposed Scheme** with domestic PR of not more than 6 and non-domestic PR of not more than 0.5 is in place).
- 6.1.9 The junction assessment results revealed that the identified key junctions would operate within capacity with the proposed development in Year 2035, with the junction modification scheme in approved planning application (No. A/KC/489). It is anticipated that the implication to the road network with the proposed development would be minimal.
- 6.1.10 Assessment results also revealed that the identified key road links would continue to operate within capacity under both Reference and Design scenarios with the proposed development by Year 2035.
- 6.1.11 Based on the public transport utilization assessment, the results reveal that the overall spare capacity of the assessed franchised bus and GMB routes would not be adequate to cater for the public transport demand associated with Proposed Development.
- 6.1.12 To cater for the shortage in public transport services, the applicant proposed to provide feeder services to the nearby MTR station or bus interchange to minimise adverse impact to the existing public transport services. Feeder service from the application site to Lai King Station is proposed. Detail of the proposed feeder service is discussed in **Chapter 4.7**.
- 6.1.13 Pedestrian impact assessment has been conducted and the walking condition on the critical footpath in vicinity of the application site is desirable during both AM and PM peaks in Year 2035. No adverse pedestrian impact will be generated by the proposed development.
- 6.1.14 Interim traffic assessment is conducted to reveal the traffic impact with only completion and population intake of the proposed Phase 1A, Phase 1B developments to be developed by the Applicant, and the development of Remaining Phase A and Remaining Phase B by third-parties
- 6.1.15 The interim junction assessment results revealed that all identified key junctions would operate within capacity with the completion and population intake of Remaining Phase A and Remaining Phase B, with the implementation of the junction modification scheme in approved planning application (No. A/KC/489).

- 6.1.16 The interim link capacity assessment results revealed that the identified key road links would continue to operate within capacity under interim scenarios with the proposed development by Year 2035.
- 6.1.17 It is viewed that both the public transport services and the pedestrian facilities would be sufficient to cater for the pedestrian demand in the interim scenarios given that it had be assessed that there is no capacity issue in the ultimate stage.
- 6.1.18 Additional pedestrian enhancement schemes have been proposed to improve the accessibility and walking condition for the residents living in existing Kau Wa Keng San Tsuen and Kau Wah Keng Old Village. With the additionally proposed pedestrian enhancements, it is expected that the performance of the existing pedestrian facilities would be maintained if not improved.

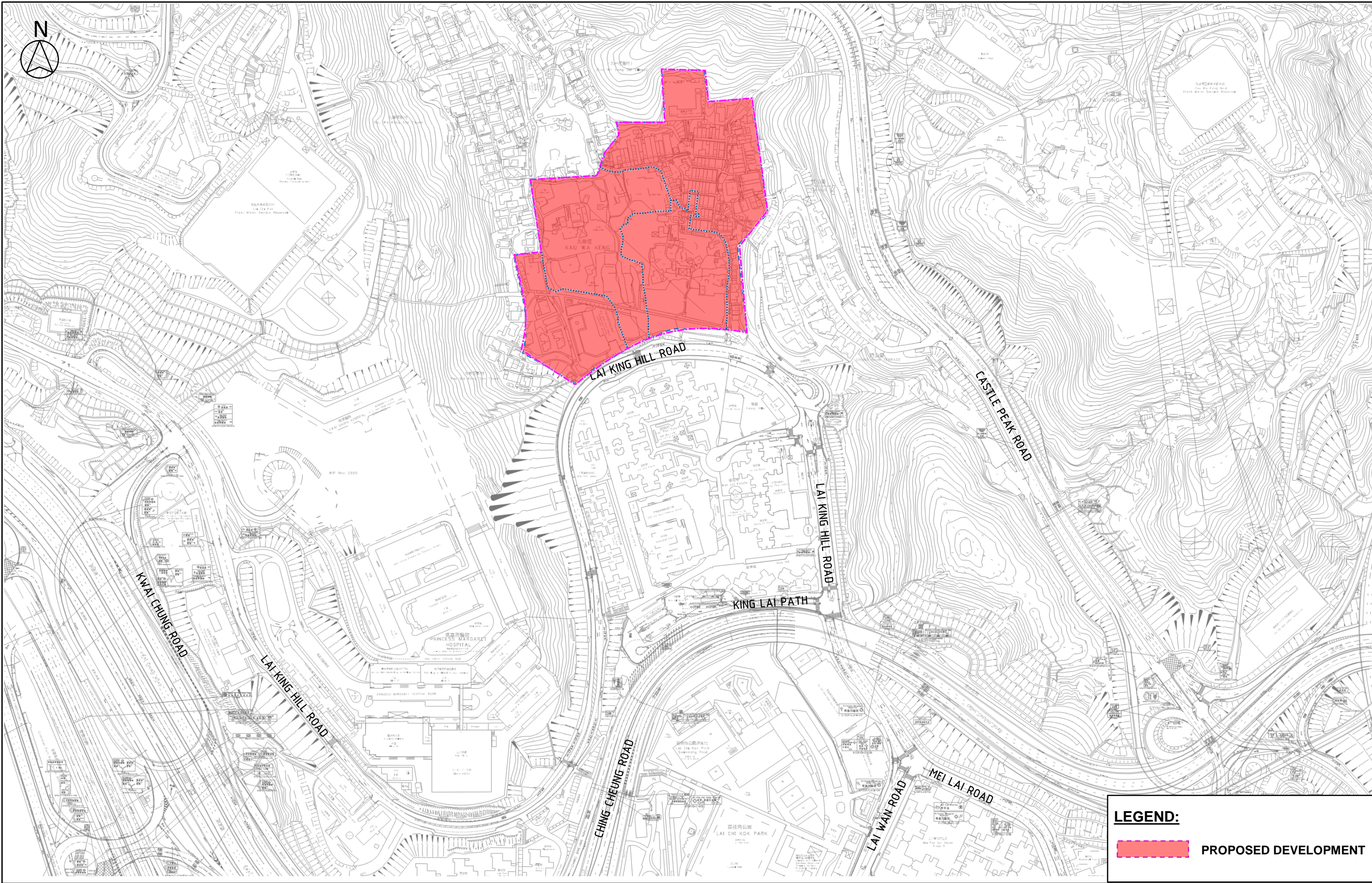
## 6.2 Conclusion

- 6.2.1 It could be concluded that the proposed development will not induce insurmountable traffic impact on the surrounding road network and thus is feasible from the traffic engineering point of view.

# Figures

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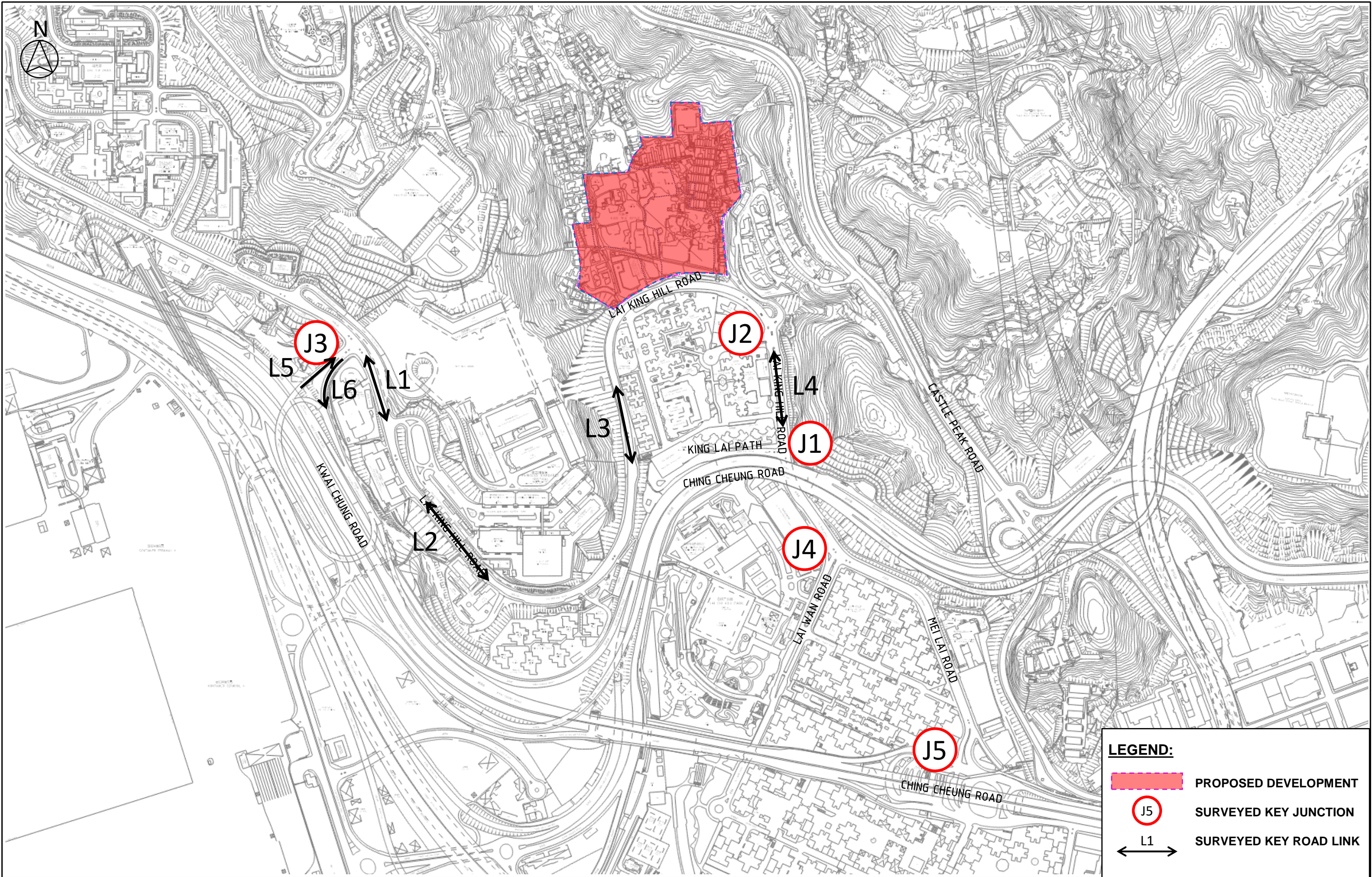


|           |           |                              |   |
|-----------|-----------|------------------------------|---|
| Job Title |           |                              | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in “Comprehensive Development Area” Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |
| Date      | Scale     | Drawing Title                |   |
| JUN 24    | NTS       |                              |   |
| Drawn     | Job No.   | LOCATION OF APPLICATION SITE |   |
| YNNC      | 299277-02 |                              |   |

FIGURE 1.1

ARUP



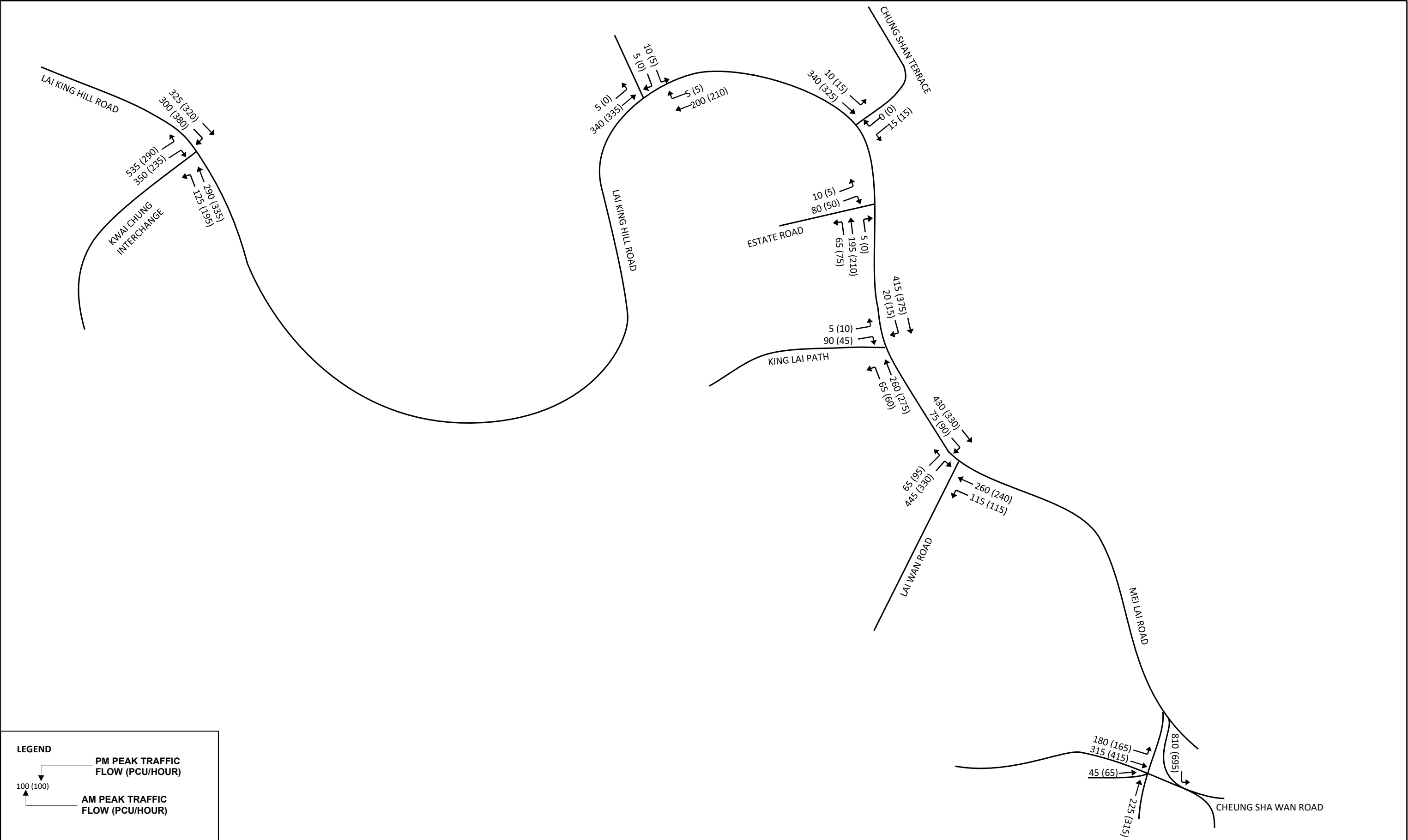


**LEGEND:**

- PROPOSED DEVELOPMENT
- J5 SURVEYED KEY JUNCTION
- L1 SURVEYED KEY ROAD LINK

|           |           |  |   |  |  |            |
|-----------|-----------|--|---|--|--|------------|
| Job Title |           |  | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |  | FIGURE 2.1 |
| Date      | Scale     | Drawing Title  |   |  |  | ARUP       |
| JUN 24    | NTS       | LOCATION OF SURVEYED JUNCTIONS IN THE VICINITY OF PROPOSED DEVELOPMENT |   |  |  |            |
| Drawn     | Job No.   |  |   |  |  |            |
| YNNC      | 299277-02 |  |   |  |  |            |



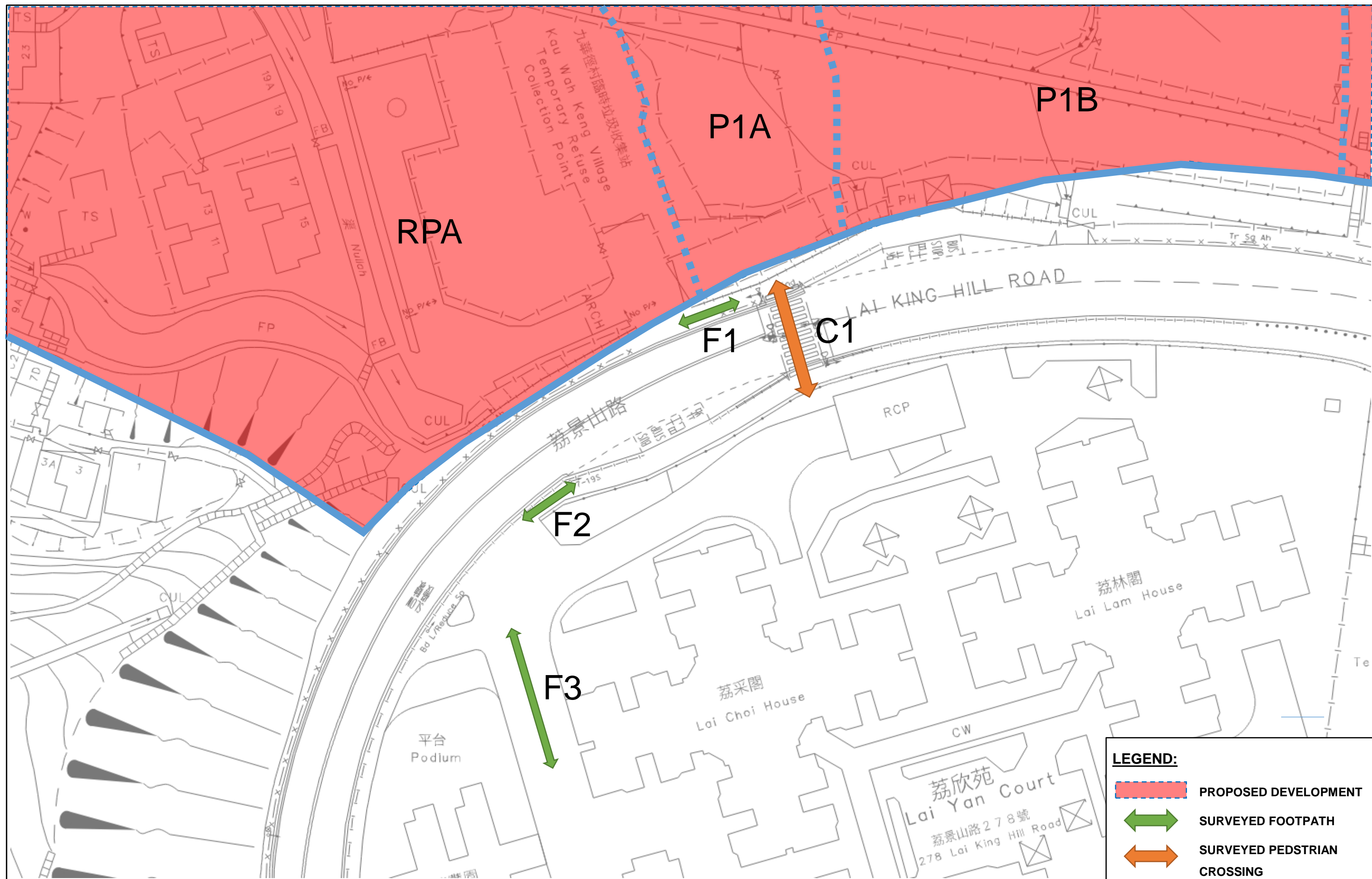


|           |           |               |   |                                 |            |
|-----------|-----------|---------------|---|---------------------------------|------------|
| Job Title |           |               | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |                                 | FIGURE 2.2 |
| Date      | Scale     | Drawing Title |   | YEAR 2024 EXISTING TRAFFIC FLOW | ARUP       |
| JUN24     | NTS       |               |   |                                 |            |
| Drawn     | Job No.   |               |   |                                 |            |
| YNNC      | 299277-02 |               |   |                                 |            |









**LEGEND:**

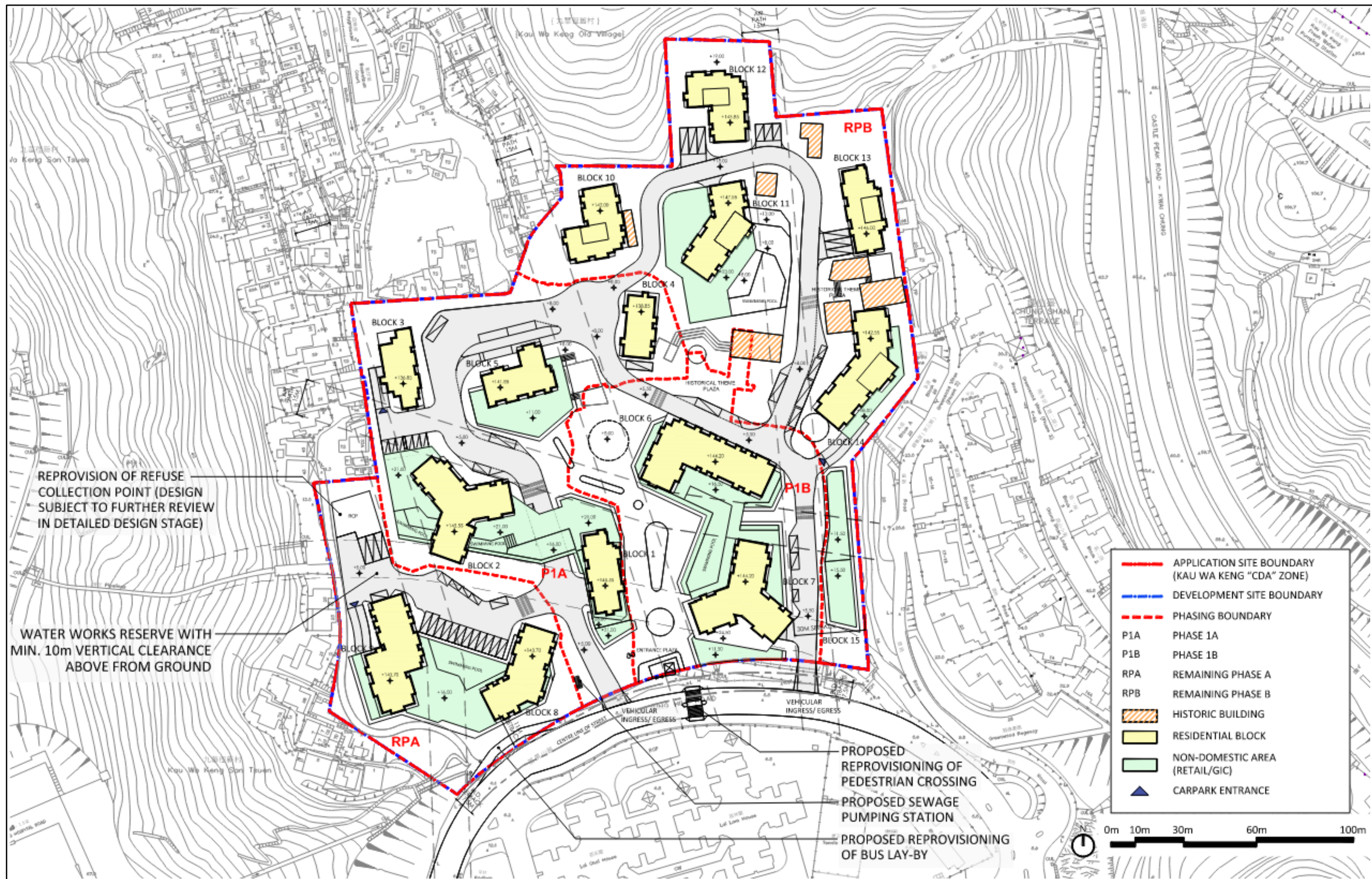
- PROPOSED DEVELOPMENT
- ↔ SURVEYED FOOTPATH
- ↔ SURVEYED PEDSTRIAN CROSSING

|           |           |   |  |
|-----------|-----------|---|--|
| Job Title |           | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in “Comprehensive Development Area” Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |
| Date      | Scale     | Drawing Title   |  |
| JUN 24    | NTS       | PEDESTRIAN FACILITIES ALONG MAJOR PEDESTRIAN ROUTES JUNCTIONS IN THE VICINITY OF PROPOSED DEVELOPMENT   |  |
| Drawn     | Job No.   |   |  |
| YNNC      | 299277-02 |   |  |

**FIGURE 2.4**

**ARUP**





Job Title: Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung

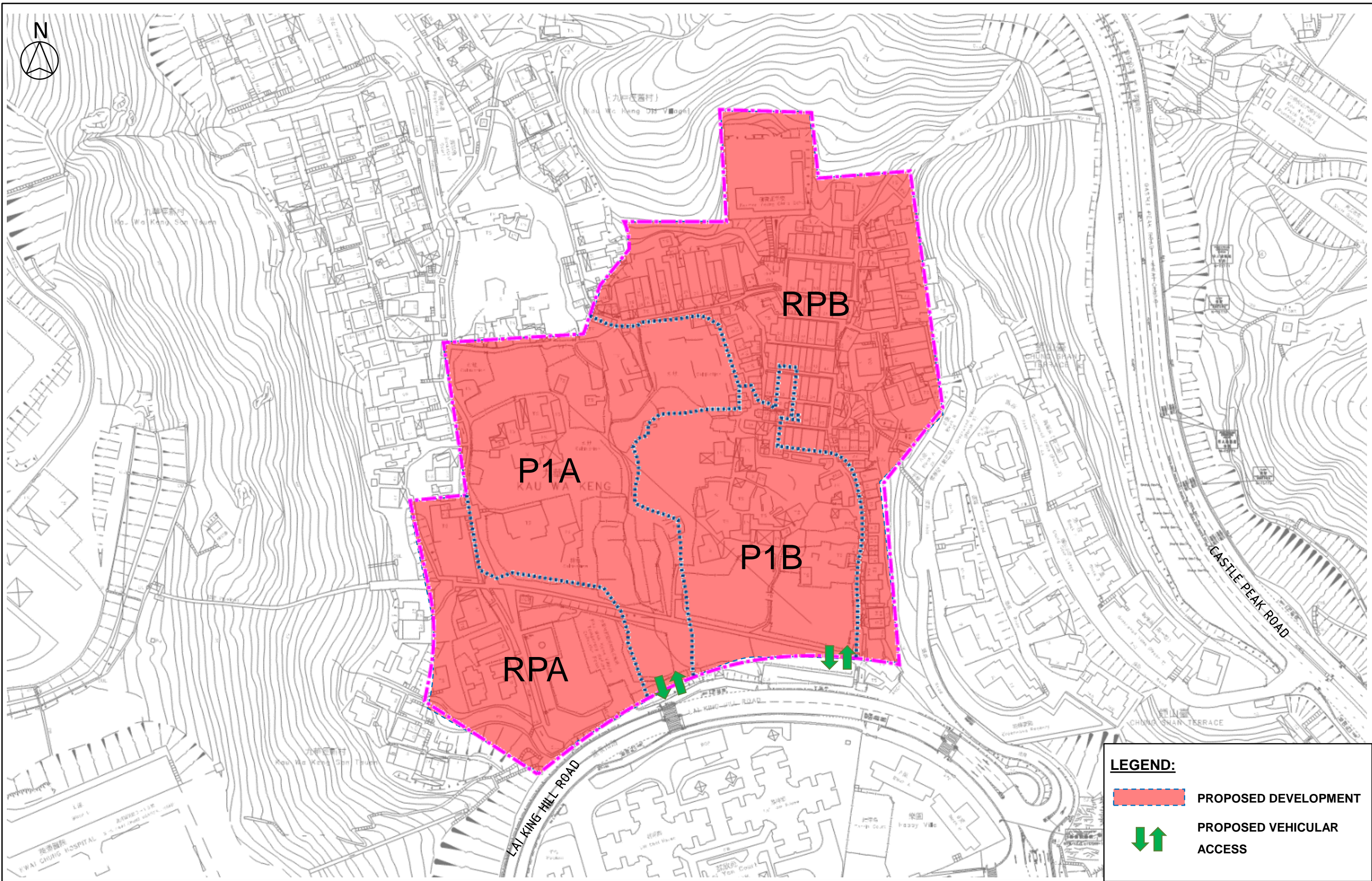
FIGURE 3.1

|        |           |               |
|--------|-----------|---------------|
| Date   | Scale     | Drawing Title |
| JUN 24 | NTS       |               |
| Drawn  | Job No.   |               |
| YNNC   | 299277-02 |               |

## MASTER LAYOUT PLAN OF PROPOSED DEVELOPMENT

ARUP





Job Title **Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in “Comprehensive Development Area” Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung**

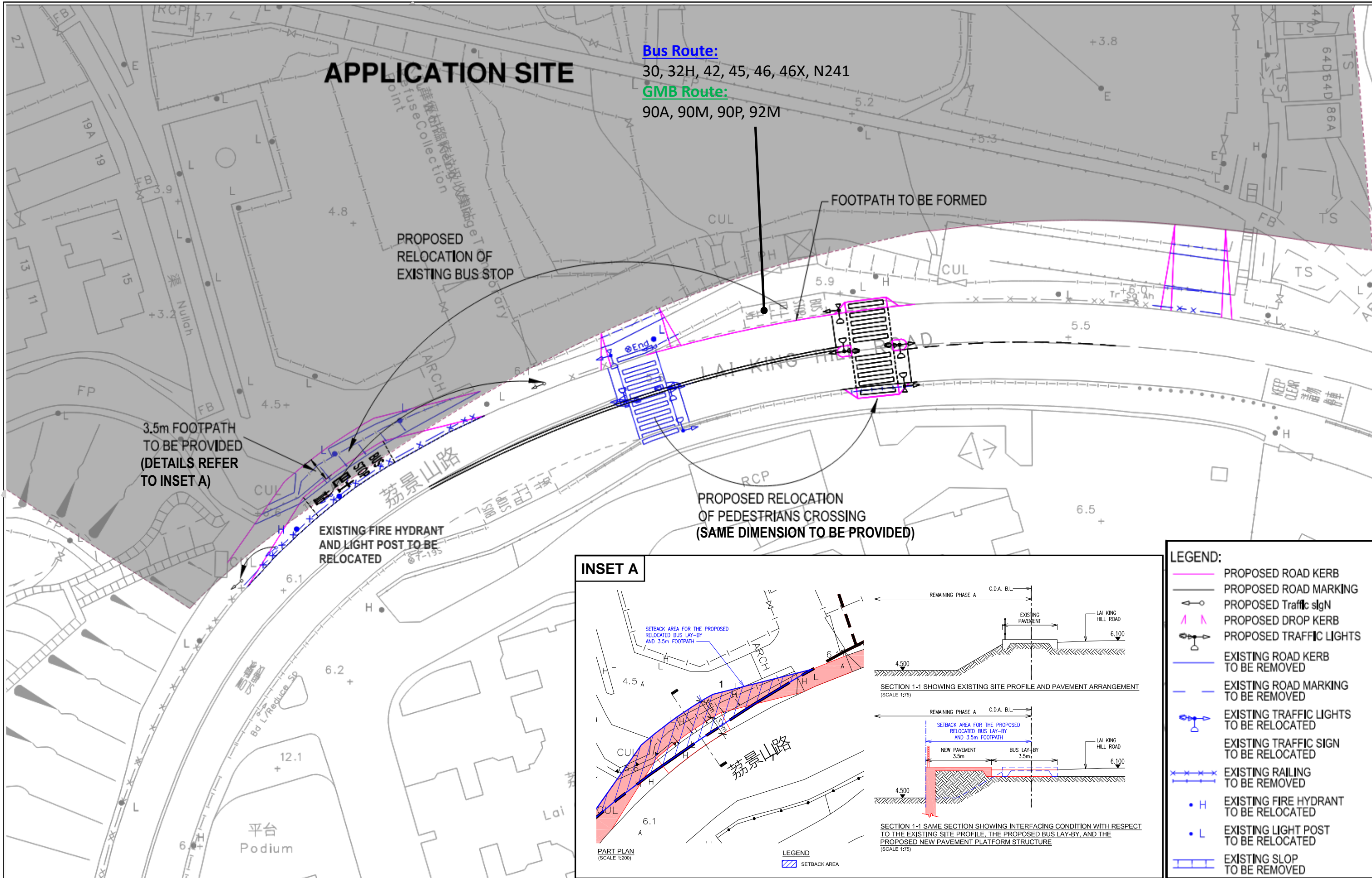
|        |           |
|--------|-----------|
| Date   | Scale     |
| JUN 24 | NTS       |
| Drawn  | Job No.   |
| YNNC   | 299277-02 |

|  |
|--|
| Drawing Title  |
| <b>PROPOSED VEHICULAR ACCESSES OF PROPOSED DEVELOPMENT</b> |

**FIGURE 3.2**

**ARUP**



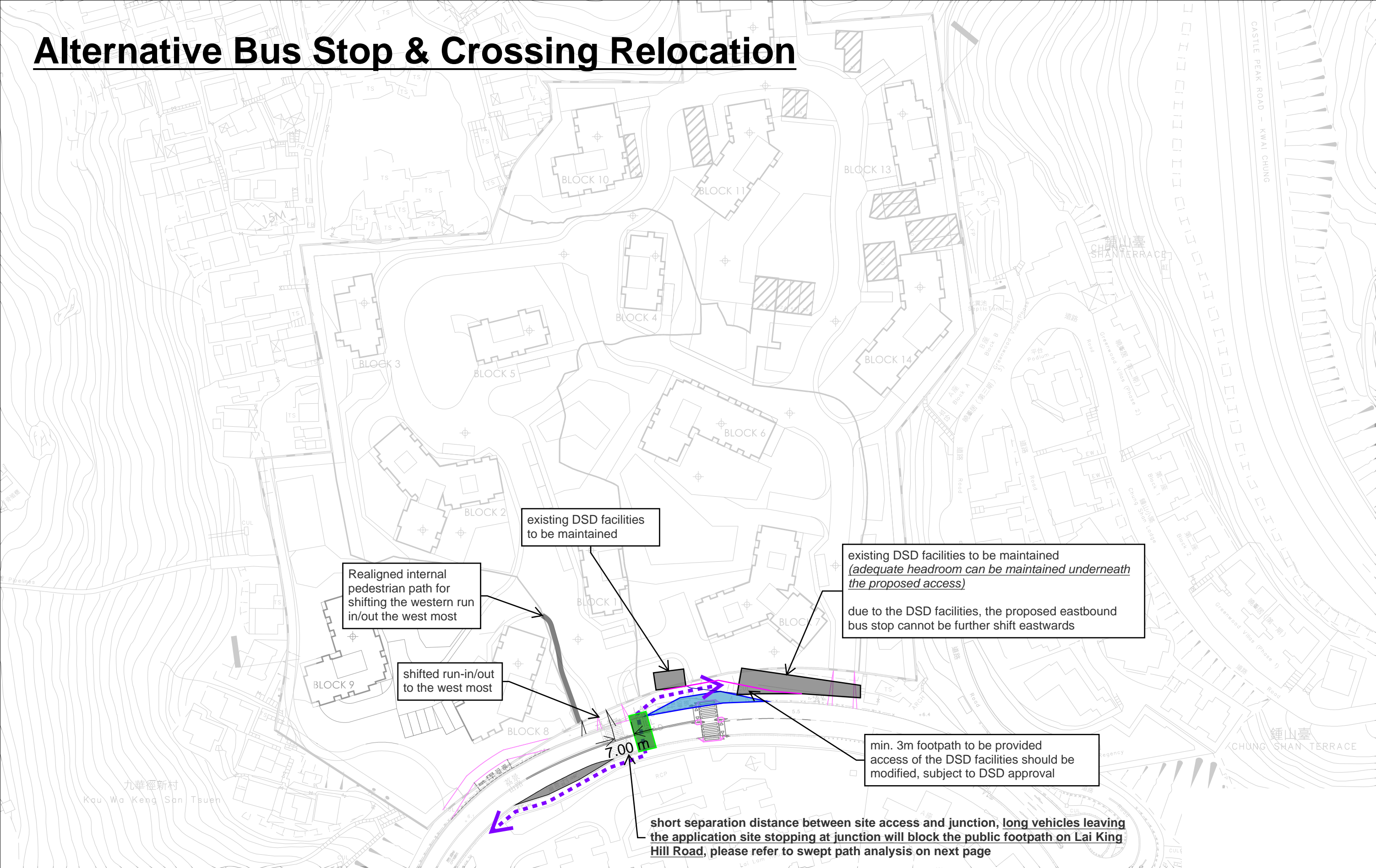


Job Title: Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung

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| Date   | Scale     |
| JUN 24 | NTS       |
| Drawn  | Job No.   |
| YNNC   | 299277-02 |

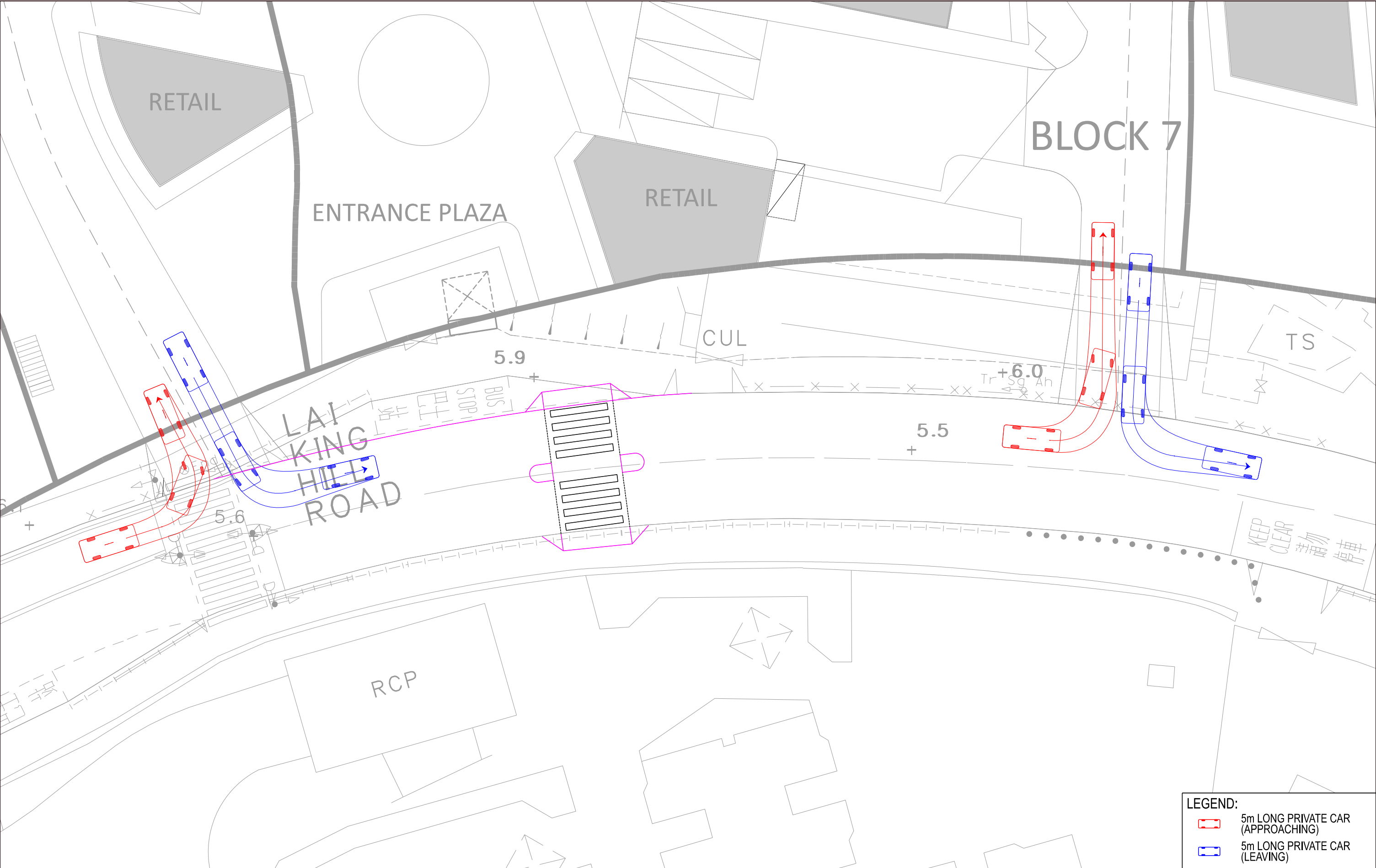
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|--|
| Drawing Title  |
| PROPOSED PEDESTRIAN CROSSING AND BUS STOP RELOCATION |

# Alternative Bus Stop & Crossing Relocation



|   |                     |  |              |
|---|---------------------|--|--------------|
| Job Title : Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |                     |  | FIGURE 3.3_2 |
| Date : JUN 24   | Scale : NTS         | INDICATIVE POSSIBLE ALTERNATIVE LAI KING HILL ROAD TRAFFIC ARRANGEMENT - CROSSING FACILITY BETWEEN BUS STOPS | ARUP         |
| Drawn : YNNC  | Job No. : 299277-02 |  |              |





- LEGEND:
- 5m LONG PRIVATE CAR (APPROACHING)
  - 5m LONG PRIVATE CAR (LEAVING)

Job Title Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung

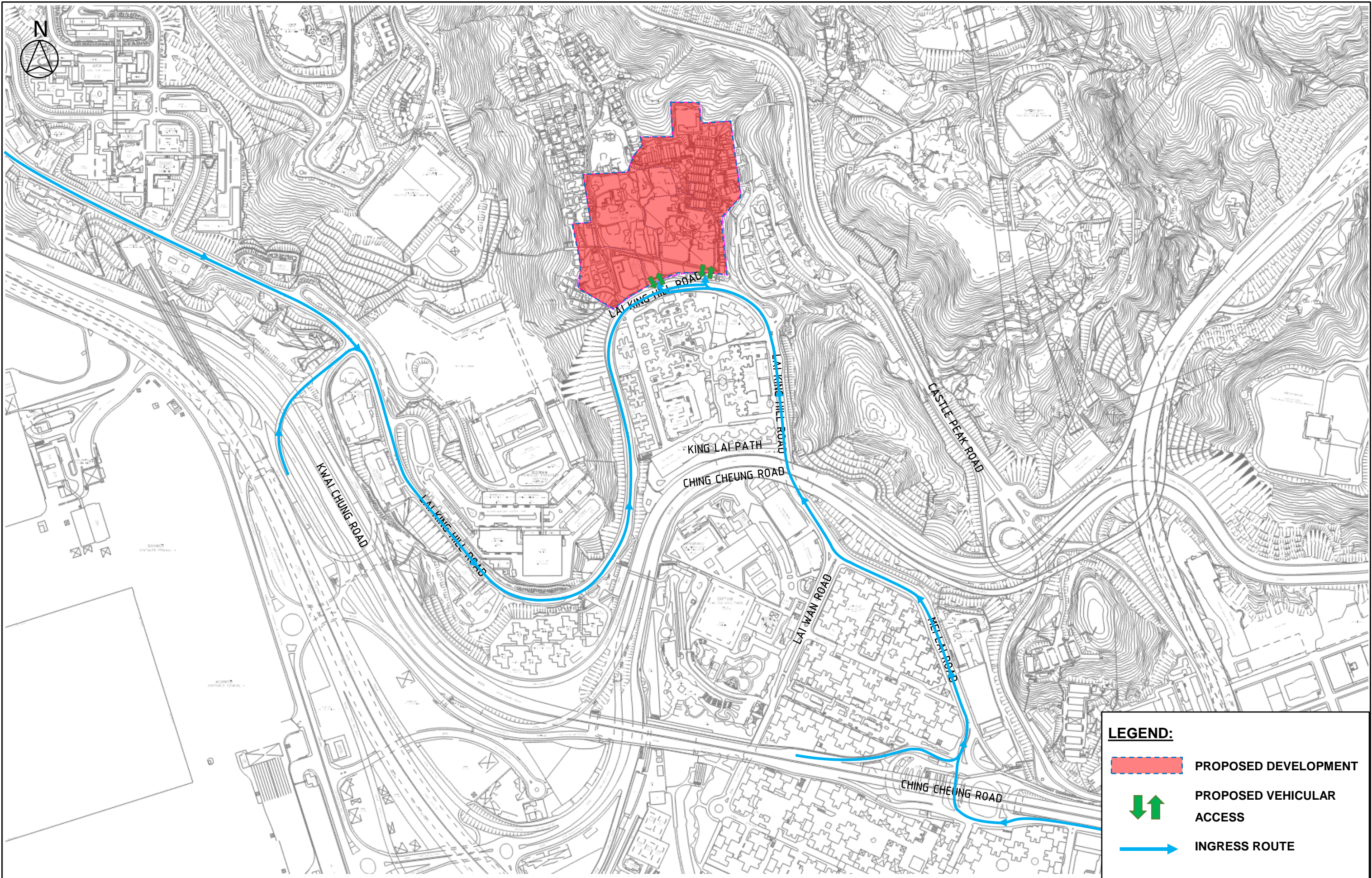
FIGURE 3.4

|         |           |
|---------|-----------|
| Date    | Scale     |
| 15JAN25 | 1:500@A3  |
| Drawn   | Job No.   |
| YNNC    | 299277-02 |

SWEPT PATH ANALYSIS AT VEHICULAR ACCESS

ARUP





**LEGEND:**

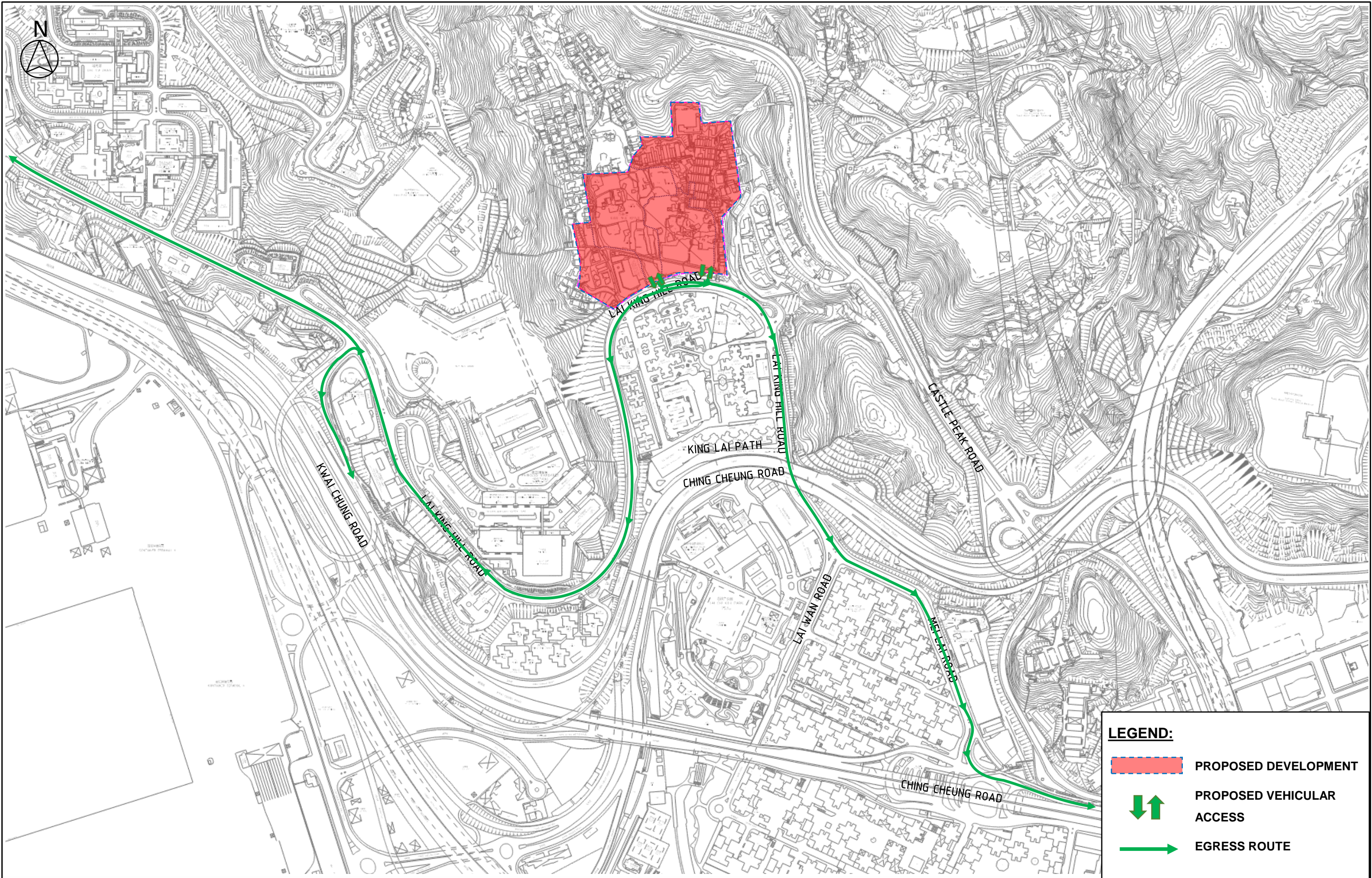
- PROPOSED DEVELOPMENT
- PROPOSED VEHICULAR ACCESS
- INGRESS ROUTE

|           |           |   |  |  |  |  |  |  |  |  |  |
|-----------|-----------|---|--|--|--|--|--|--|--|--|--|
| Job Title |           | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |  |  |  |  |  |  |  |  |
| Date      | Scale     | Drawing Title   |  |  |  |  |  |  |  |  |  |
| JUN 24    | NTS       | INGRESS VEHICULAR ROUTES OF PROPOSED DEVELOPMENT  |  |  |  |  |  |  |  |  |  |
| Drawn     | Job No.   |   |  |  |  |  |  |  |  |  |  |
| YNNC      | 299277-02 |   |  |  |  |  |  |  |  |  |  |

**FIGURE 3.5**

**ARUP**





Job Title: Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung

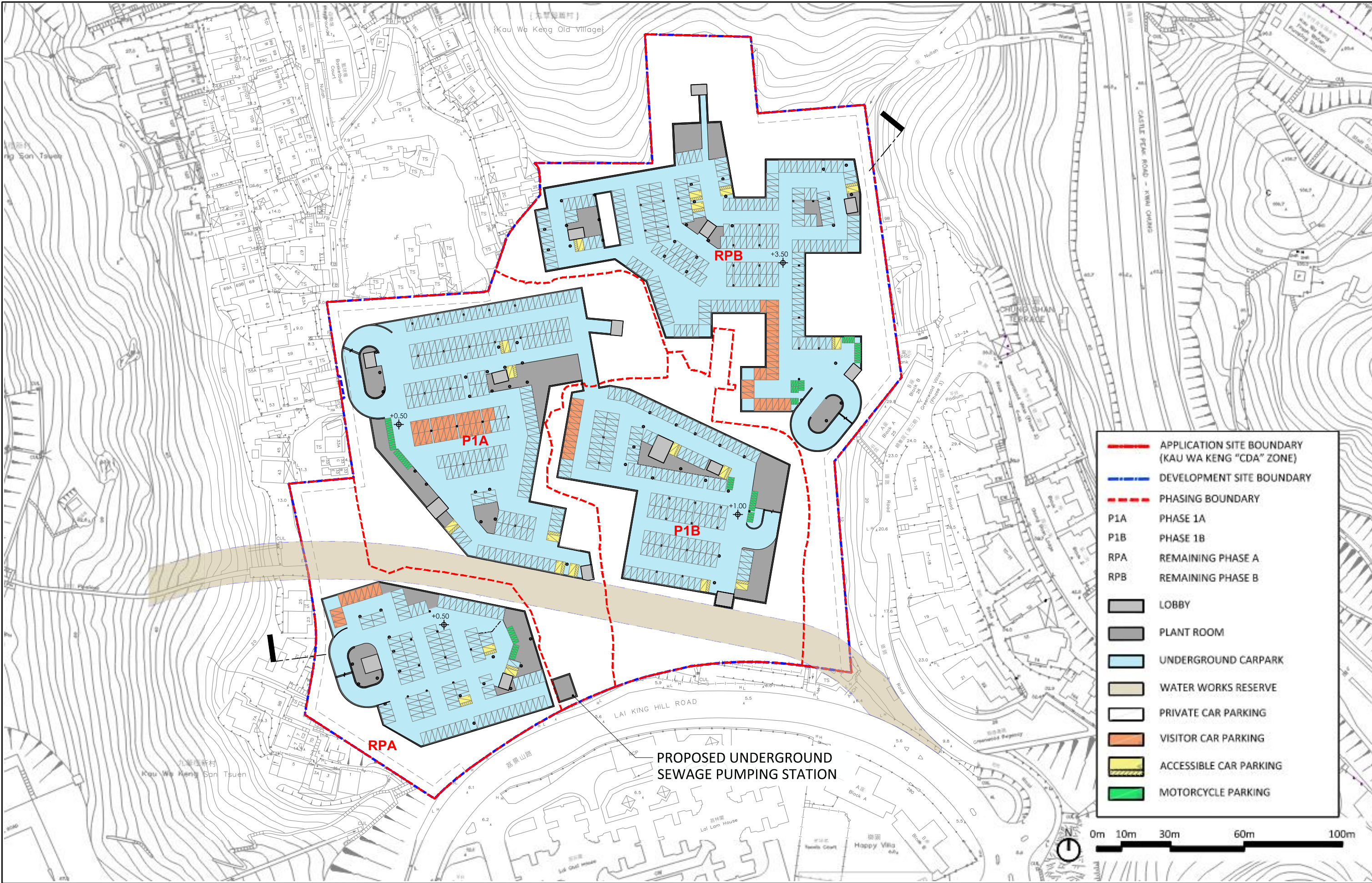
FIGURE 3.6

|        |           |
|--------|-----------|
| Date   | Scale     |
| JUN 24 | NTS       |
| Drawn  | Job No.   |
| YNNC   | 299277-02 |

**EGRESS VEHICULAR ROUTES OF PROPOSED DEVELOPMENT**

**ARUP**





Job Title Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung

FIGURE 3.7

|        |           |
|--------|-----------|
| Date   | Scale     |
| JUN 24 | NTS       |
| Drawn  | Job No.   |
| YNNC   | 299277-02 |

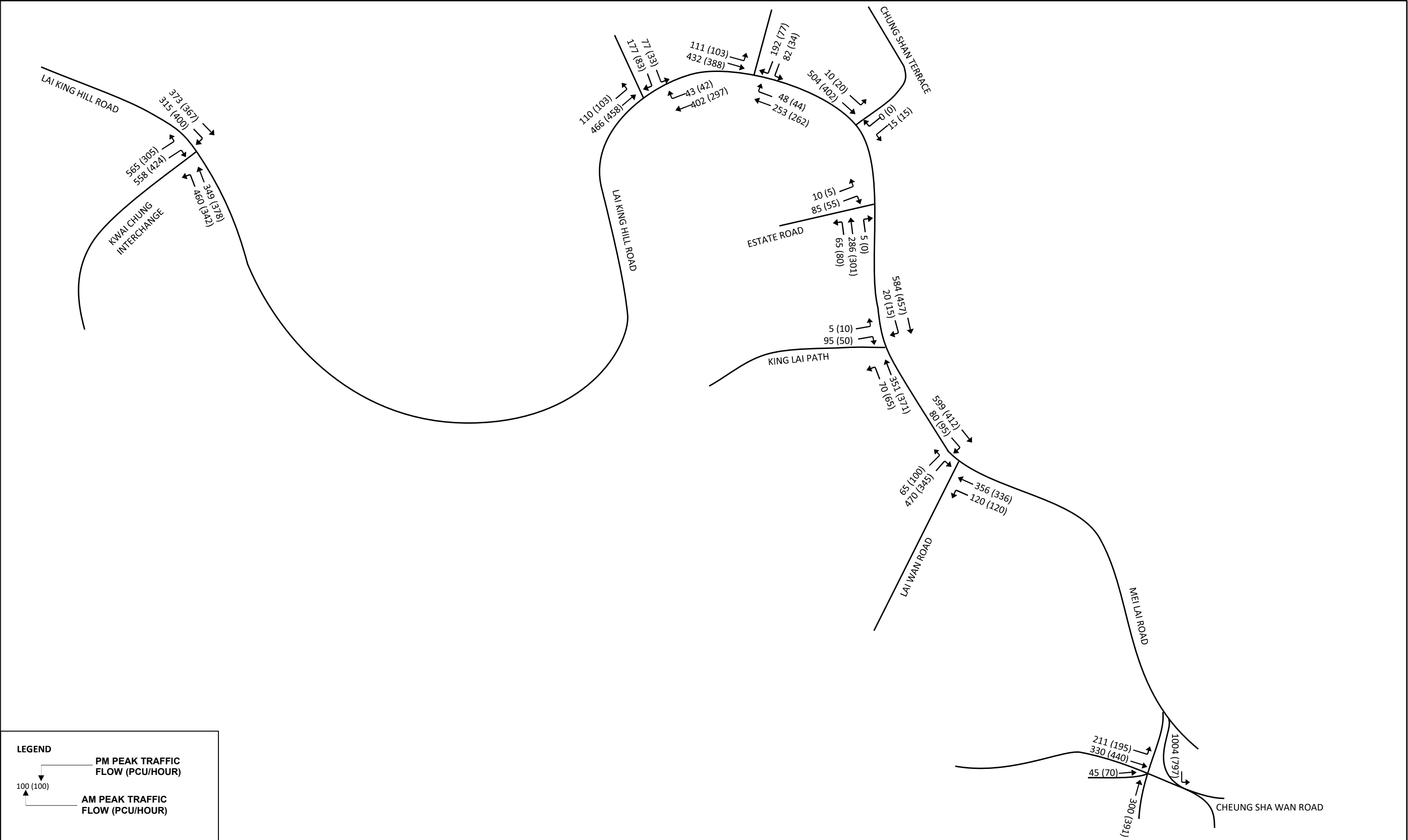
Drawing Title

PROPOSED BASEMENT 1/F LAYOUT PLAN

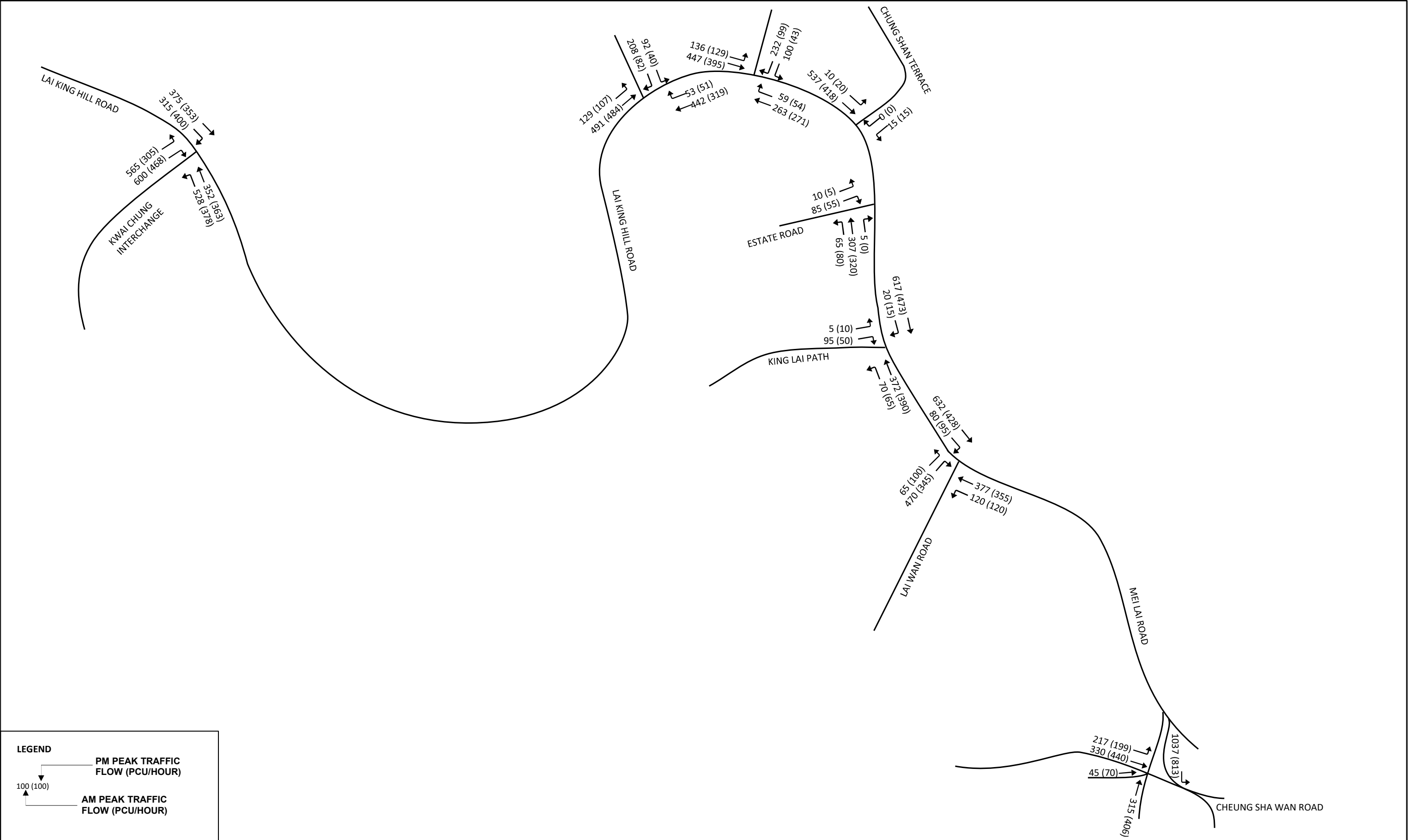
ARUP







|   |           |                                  |            |
|---|-----------|----------------------------------|------------|
| Job Title   |           |                                  | FIGURE 4.1 |
| Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |           |                                  |            |
| Date  | Scale     | Drawing Title                    | ARUP       |
| JUN24   | NTS       |                                  |            |
| Drawn   | Job No.   |                                  |            |
| YNNC  | 299277-02 | YEAR 2035 REFERENCE TRAFFIC FLOW |            |



LEGEND

PM PEAK TRAFFIC FLOW (PCU/HOUR)

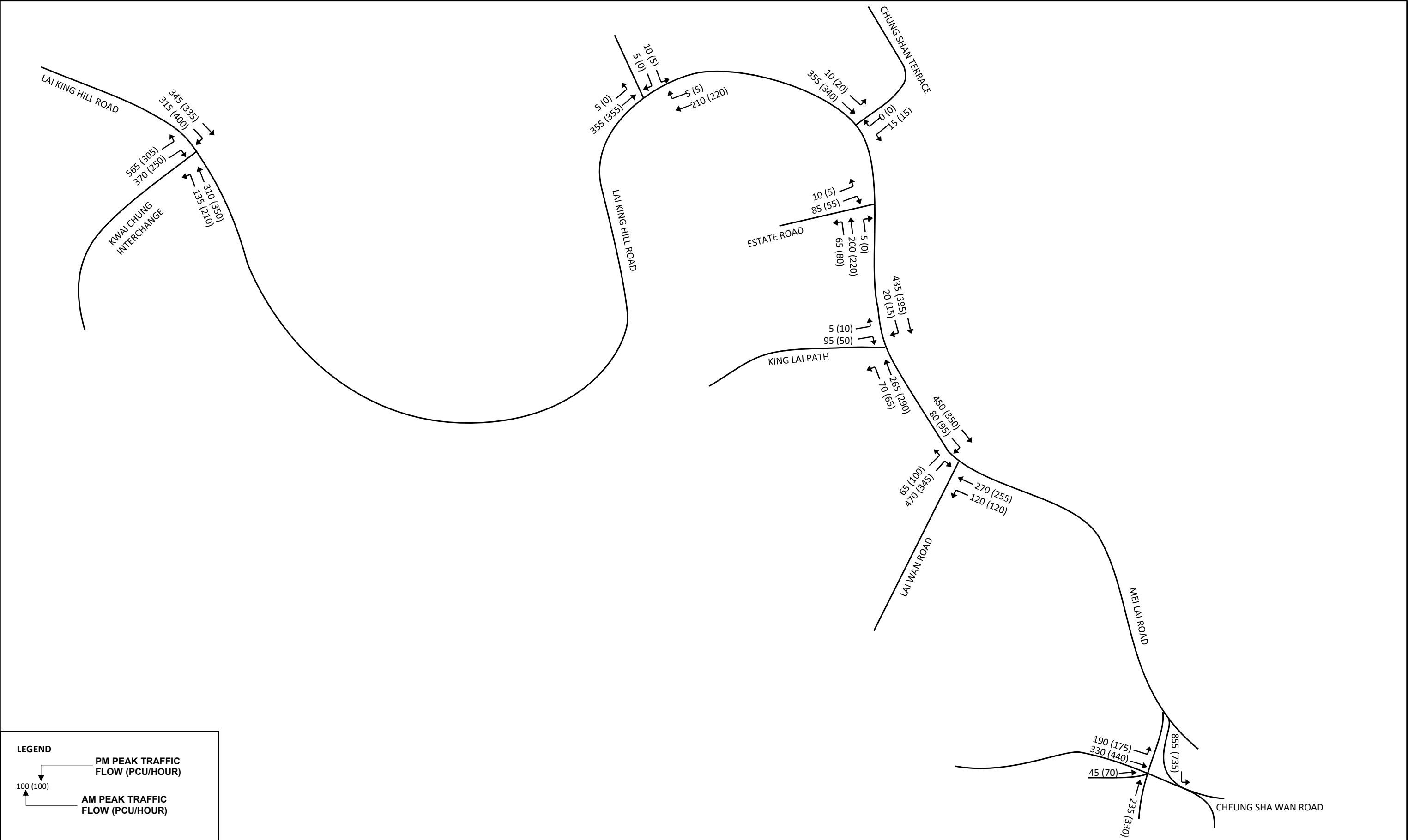
AM PEAK TRAFFIC FLOW (PCU/HOUR)

100 (100)

|  |                      |  |            |  |
|--|----------------------|--|------------|--|
| Job Title<br>Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |                      |  | FIGURE 4.2 |  |
| Date<br>JUN24  | Scale<br>NTS         | Drawing Title<br>YEAR 2035 DESIGN TRAFFIC FLOW | ARUP       |  |
| Drawn<br>YNNC  | Job No.<br>299277-02 |  |            |  |







LEGEND

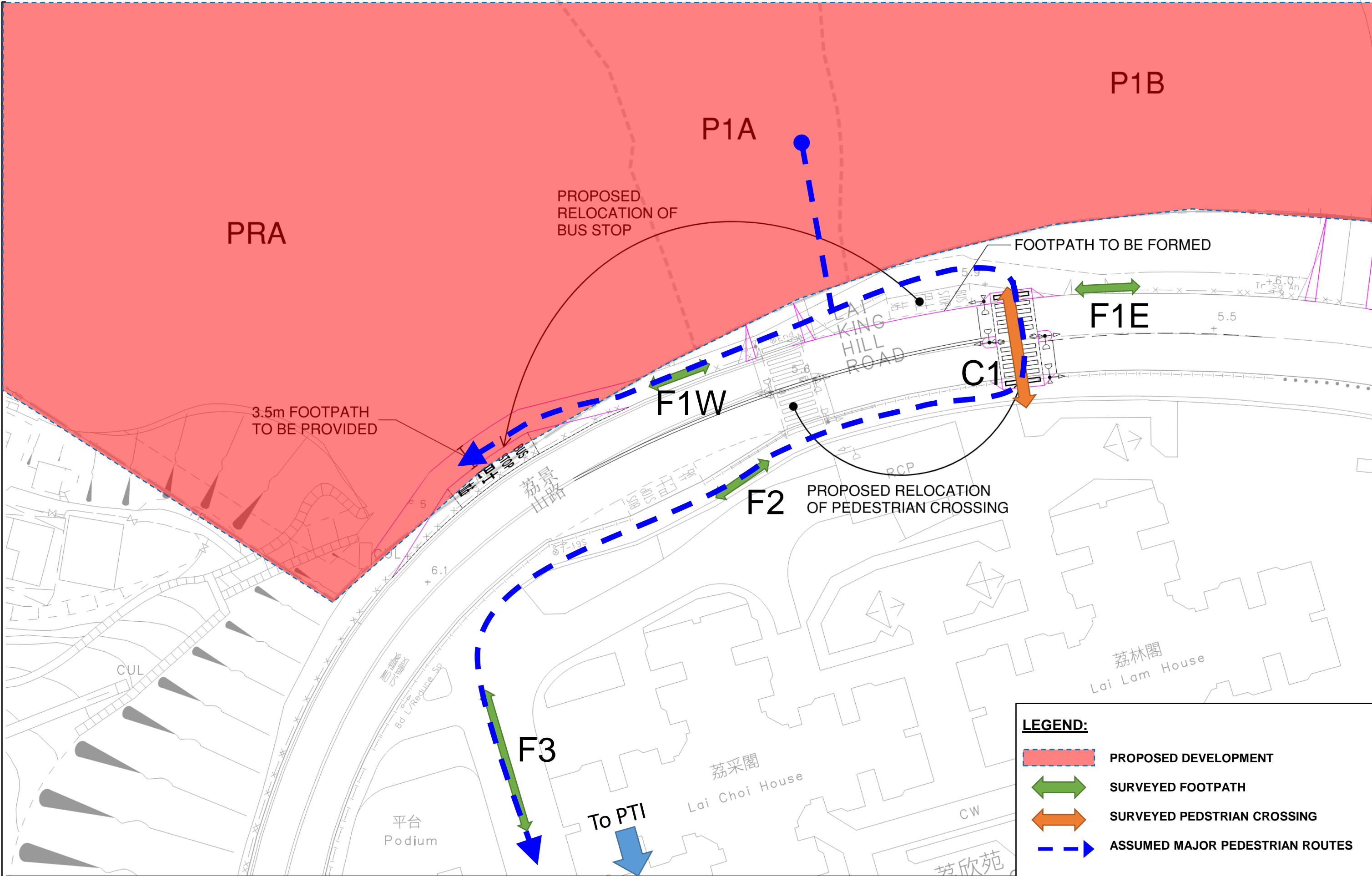
PM PEAK TRAFFIC FLOW (PCU/HOUR)

AM PEAK TRAFFIC FLOW (PCU/HOUR)

100 (100)

|           |           |                                 |   |  |            |      |
|-----------|-----------|---------------------------------|---|--|------------|------|
| Job Title |           |                                 | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  | FIGURE 4.4 |      |
| Date      | Scale     | Drawing Title                   |   |  |            |      |
| JUN24     | NTS       | YEAR 2035 BASELINE TRAFFIC FLOW |   |  |            | ARUP |
| Drawn     | Job No.   |                                 |   |  |            |      |
| YNNC      | 299277-02 |                                 |   |  |            |      |

ARUP



**LEGEND:**

- PROPOSED DEVELOPMENT
- SURVEYED FOOTPATH
- SURVEYED PEDESTRIAN CROSSING
- ASSUMED MAJOR PEDESTRIAN ROUTES

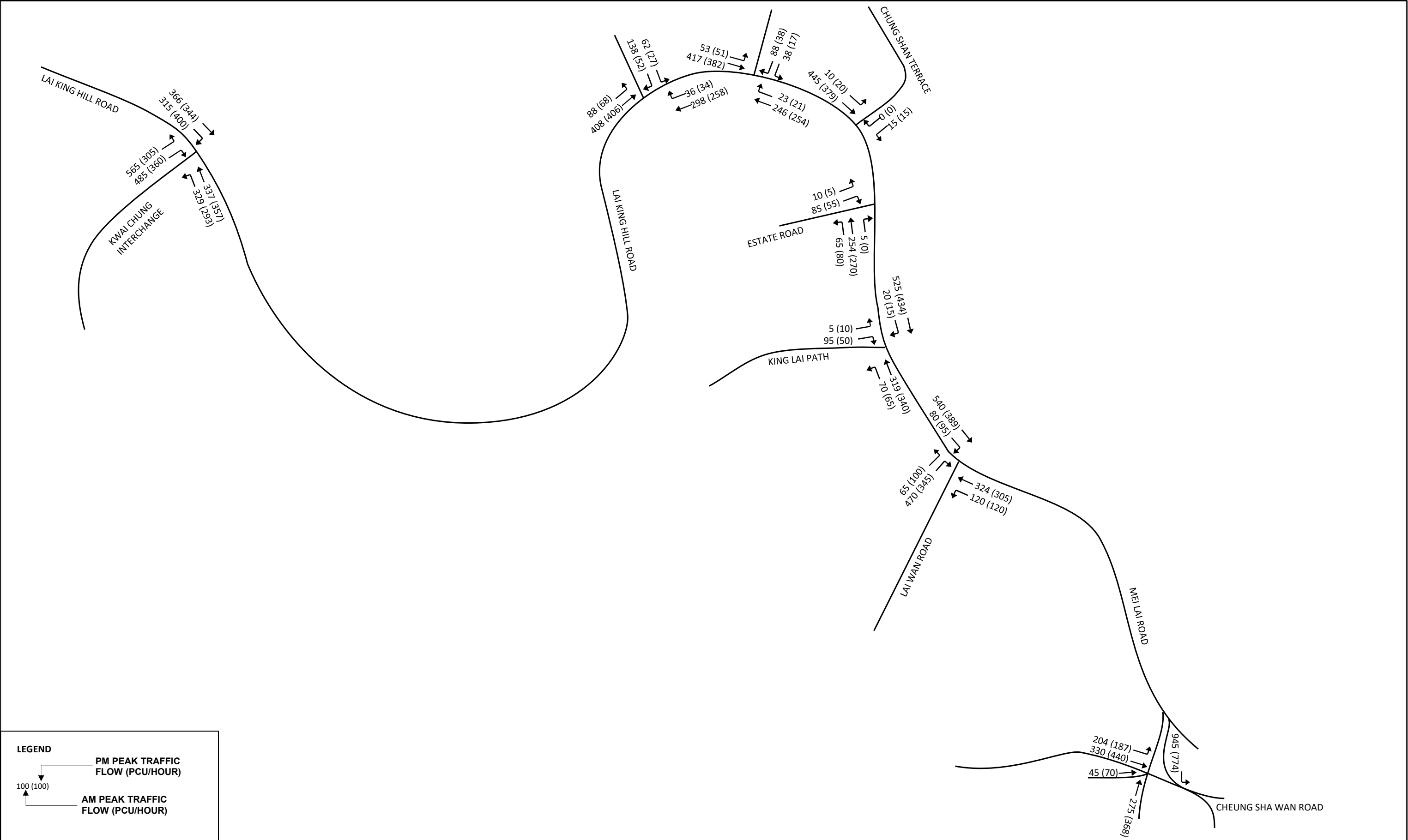
Job Title: Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung

|        |           |
|--------|-----------|
| Date   | Scale     |
| JUN 24 | NTS       |
| Drawn  | Job No.   |
| YNNC   | 299277-02 |

|   |  |
|---|--|
| Drawing Title   |  |
| LOCATION OF PEDESTRIAN FACILITIES ALONG MAJOR PEDESTRIAN ROUTES IN THE VICINITY OF PROPOSED DEVELOPMENT |  |

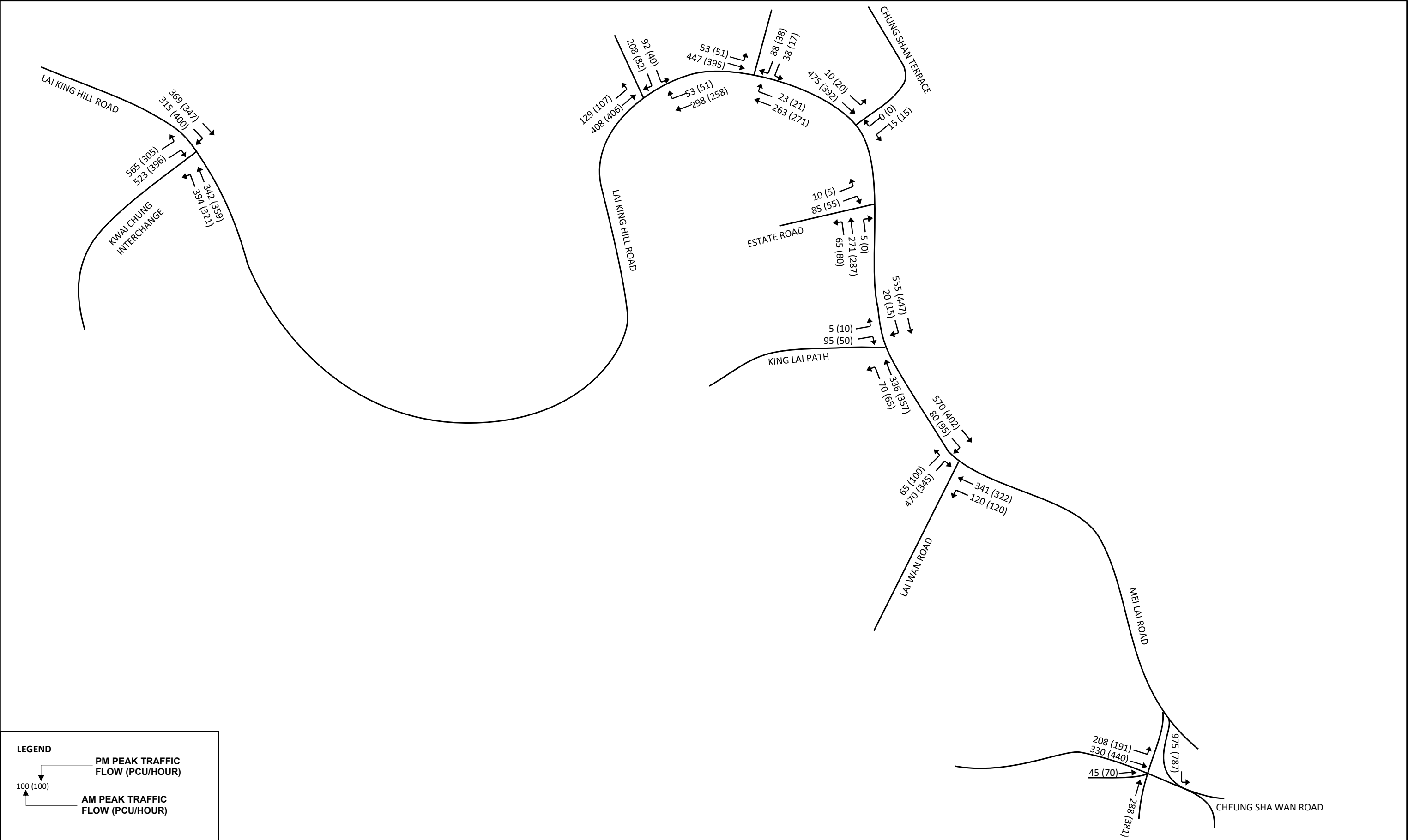
FIGURE 4.5

ARUP



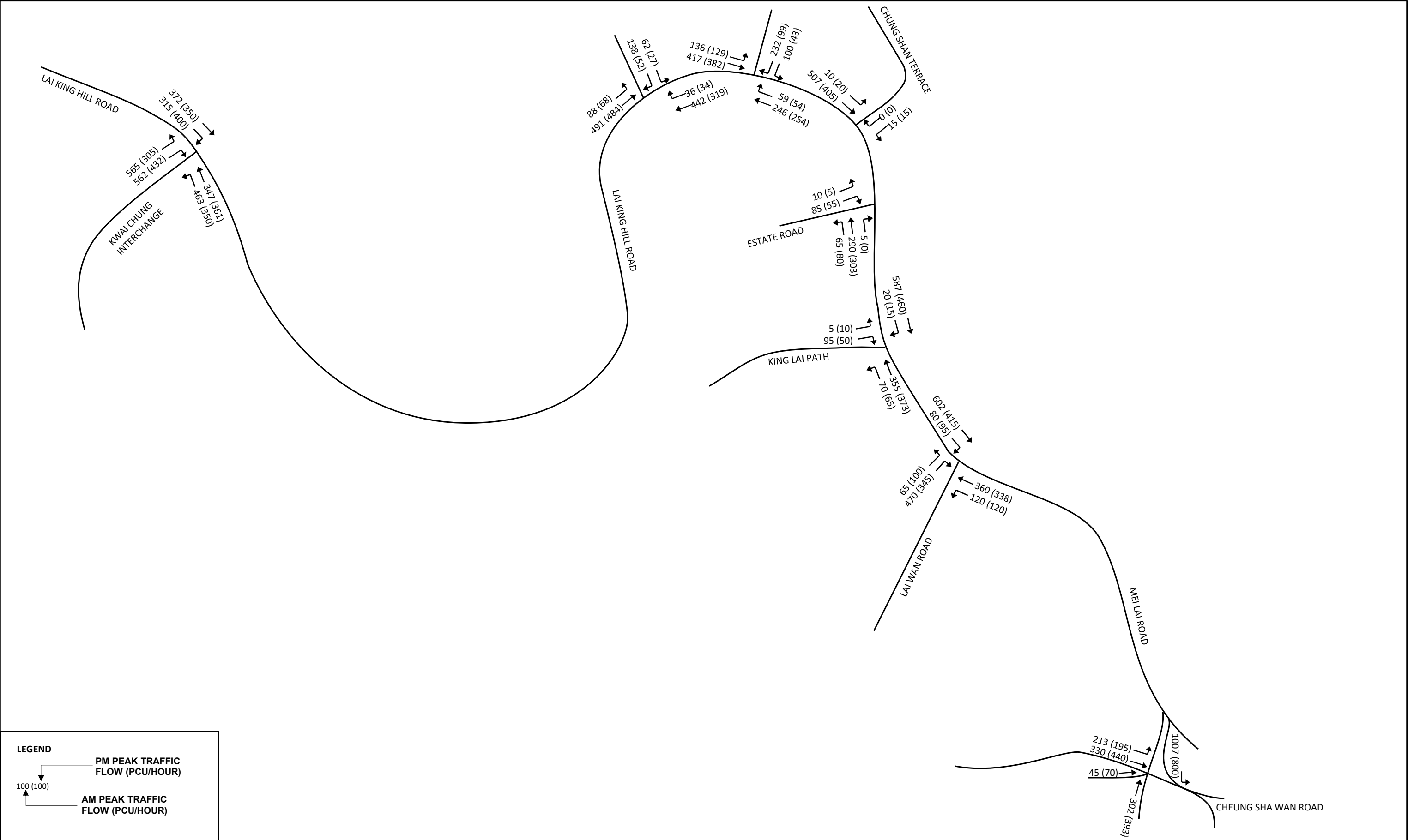
|   |                      |  |            |      |
|---|----------------------|--|------------|------|
| Job Title<br>Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in<br>"Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |                      |  | FIGURE 5.1 |      |
| Date<br>JUN24   | Scale<br>NTS         | Drawing Title<br><br>YEAR 2035 INTERIM SCENARIO A TRAFFIC FLOW |            | ARUP |
| Drawn<br>YNNC   | Job No.<br>299277-02 |  |            |      |

ARUP



|   |           |   |            |
|---|-----------|---|------------|
| Job Title   |           |   | FIGURE 5.2 |
| Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |           |   |            |
| Date  | Scale     | Drawing Title                             | ARUP       |
| JUN24   | NTS       |   |            |
| Drawn   | Job No.   | YEAR 2035 INTERIM SCENARIO B TRAFFIC FLOW |            |
| YNNC  | 299277-02 |   |            |





|  |                      |  |            |  |
|--|----------------------|--|------------|--|
| Job Title<br>Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |                      |  | FIGURE 5.3 |  |
| Date<br>JUN24  | Scale<br>NTS         | Drawing Title<br>YEAR 2035 INTERIM SCENARIO C TRAFFIC FLOW | ARUP       |  |
| Drawn<br>YNNC  | Job No.<br>299277-02 |  |            |  |

# Appendix A

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## Junction Calculation Sheets

## J1 YEAR 2024 AM TRAFFIC FLOW

[illegible]

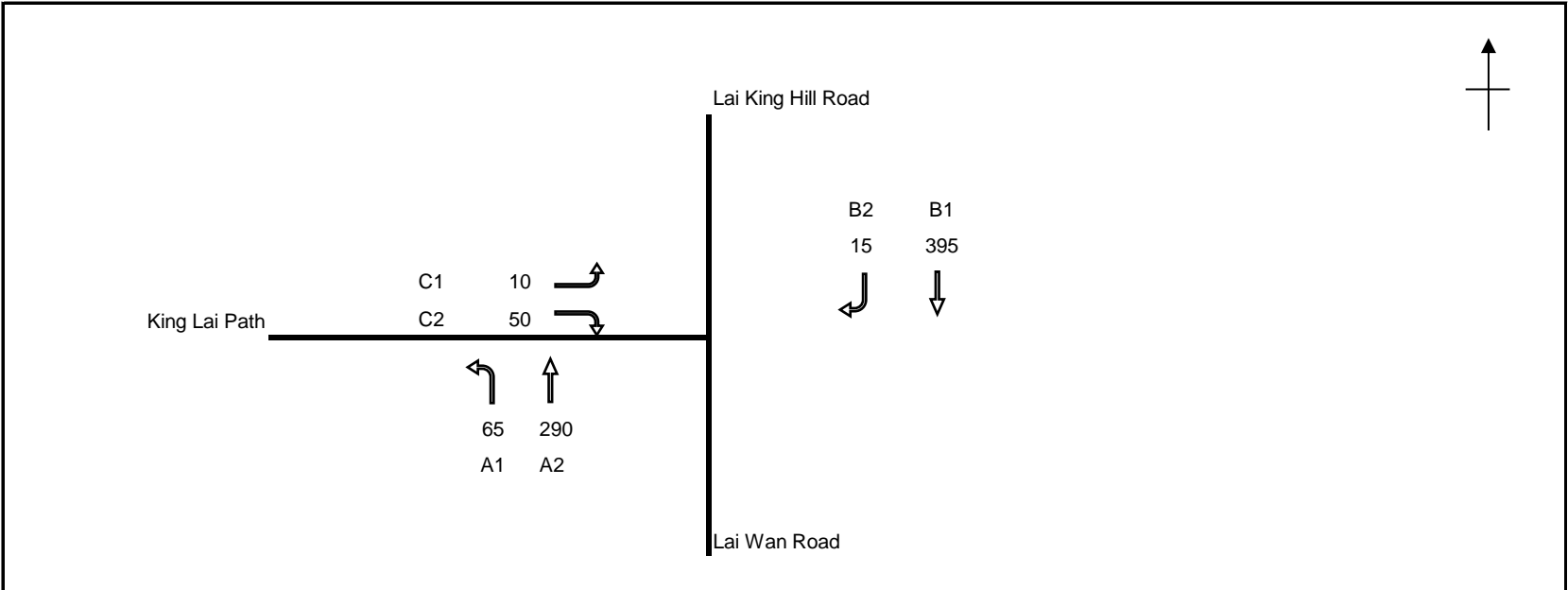
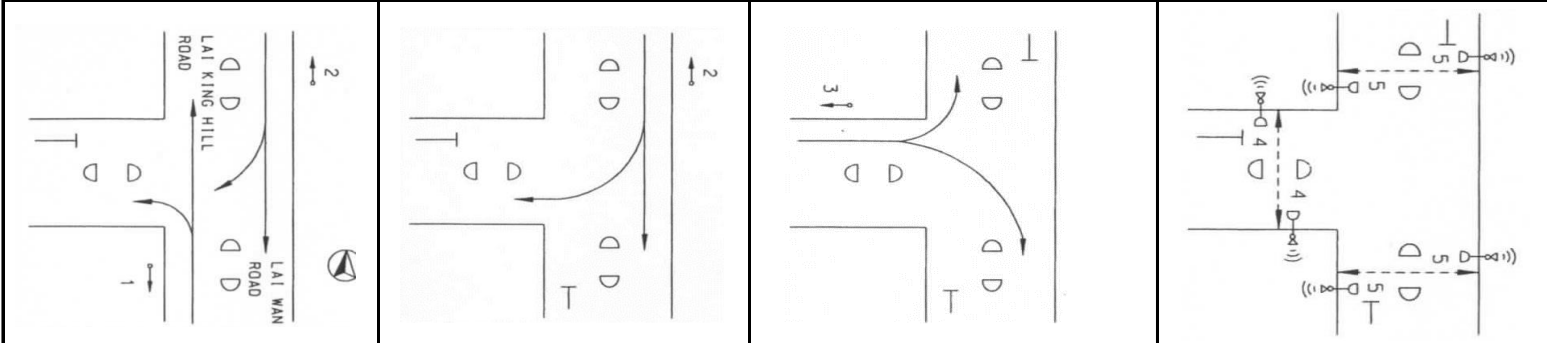
## J1 YEAR 2024 PM TRAFFIC FLOW

[illegible]

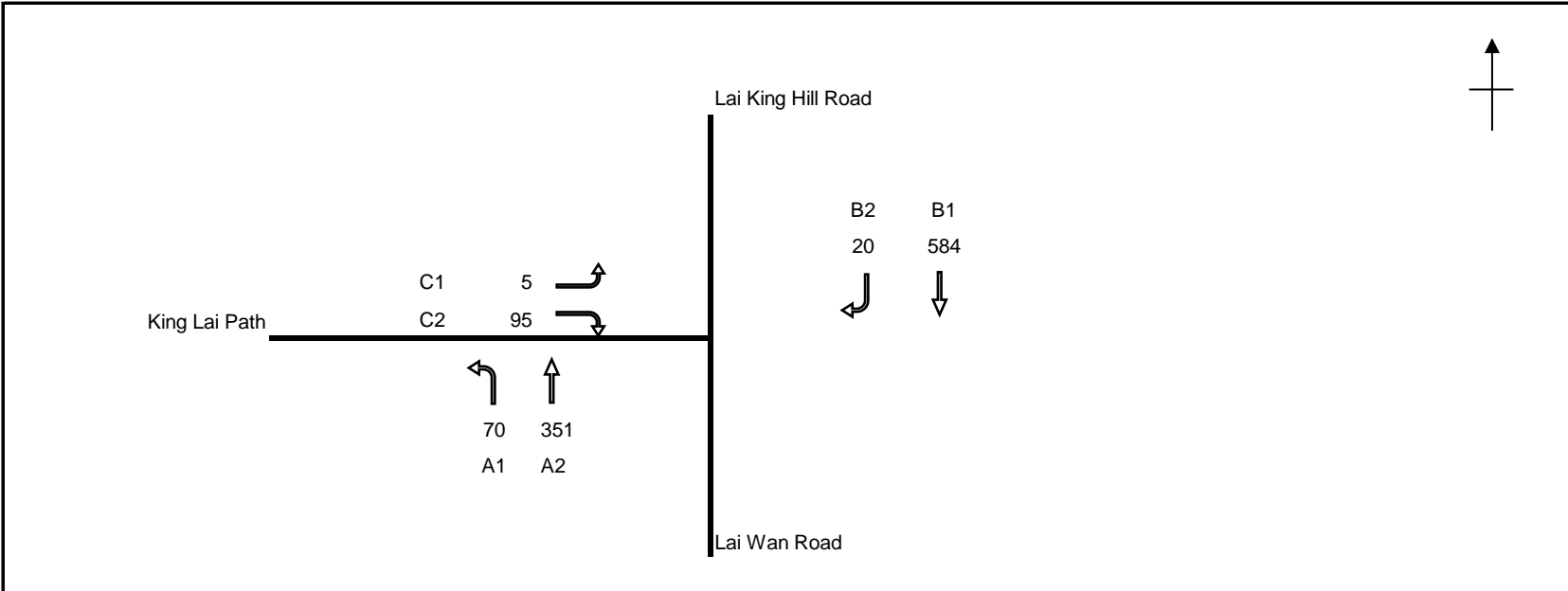
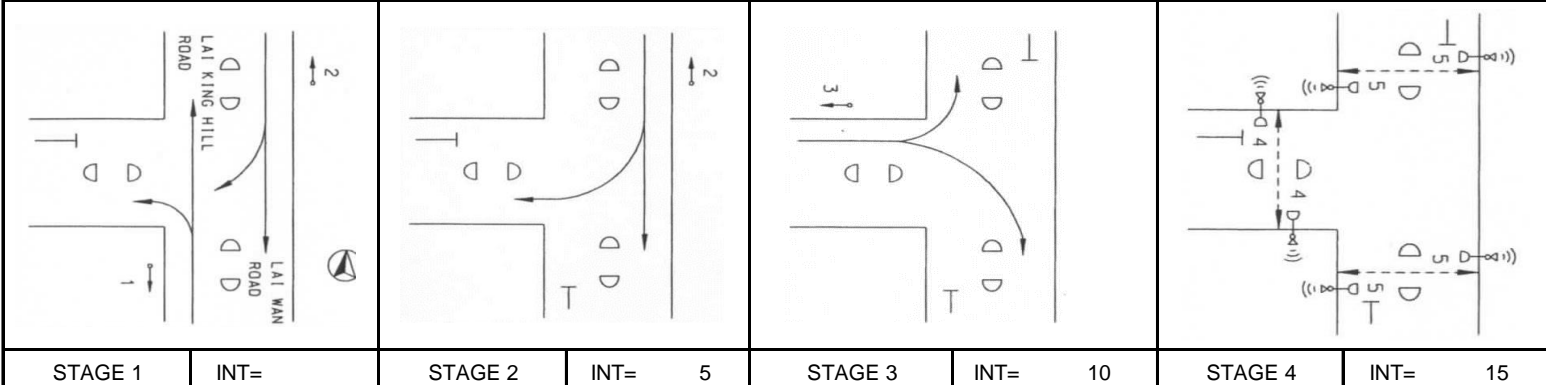
## J1 YEAR 2035 AM TRAFFIC FLOW BASELINE SCENARIO

| OVE ARUP & PARTNERS   |                       |                         |       |             |                         |        |    | TRAFFIC SIGNAL CALCULATION |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|--------|----|----------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|---|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-------|-------|-----------|-------|--------|------------|----|---------|----|-------------------|------------|----|-----------|------------|------|------|---------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng   |                       |                         |       |             |                         |        |    | PROJECT NO: 299277-02      |            |                |             |                  |                                |                 |                   | Junction No. J1   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Lai King Hill Road / King Lai Path  |                       |                         |       | J1_BASE_AM  |                         |        |    | DATE : 21-Jan-25           |            |                |             | FILENAME :       |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.176</td></tr> <tr> <td>Loss time</td><td>L =</td><td>35 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>890 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 69.8 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 42.5 sec</td></tr> <tr> <td>Yult</td><td></td><td>= 0.638</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 261.5 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 43.5 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.708</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 261 %</td></tr> </table> |                         |       |           |       |                  |               |                        | No. of stages per cycle | N =       | 4                       | No. of stage using for calculation | N = | 2                       | Cycle time | C = | 120 sec | Sum(y) | Y =   | 0.176 | Loss time | L =   | 35 sec | Total Flow | =  | 890 pcu | Co | = (1.5*L+5)/(1-Y) | = 69.8 sec | Cm | = L/(1-Y) | = 42.5 sec | Yult |      | = 0.638 | R.C.ult | = (Yult-Y)/Y*100% | = 261.5 % | Cp | = 0.9*L/(0.9-Y) | = 43.5 sec | Ymax | = 1-L/C | = 0.708 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 261 % |
| No. of stages per cycle   | N =                   | 4                       |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| No. of stage using for calculation  | N =                   | 2                       |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Sum(y)  | Y =                   | 0.176                   |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Loss time   | L =                   | 35 sec                  |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Total Flow  | =                     | 890 pcu                 |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Co  | = (1.5*L+5)/(1-Y)     | = 69.8 sec              |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cm  | = L/(1-Y)             | = 42.5 sec              |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Yult  |                       | = 0.638                 |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 261.5 %               |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cp  | = 0.9*L/(0.9-Y)       | = 43.5 sec              |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ymax  | = 1-L/C               | = 0.708                 |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 261 %                 |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Dp</td><td>10</td><td>8</td><td>2</td><td>11</td><td>8</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>Ep</td><td>10.5</td><td>7</td><td>8</td><td>12</td><td>7</td><td>8</td><td>12</td><td>OK</td></tr> </table>   |                         |       |           |       |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   | SG     | Delay | FG    | SG        | Delay | FG     | Dp         | 10 | 8       | 2  | 11                | 8          | 2  | 11        | OK         | Ep   | 10.5 | 7       | 8       | 12                | 7         | 8  | 12              | OK         |      |         |         |         |                       |         |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |        |    | Check                      |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       | SG                      | Delay | FG          | SG                      | Delay  | FG |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Dp  | 10                    | 8                       | 2     | 11          | 8                       | 2      | 11 | OK                         |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  | 10.5                  | 7                       | 8     | 12          | 7                       | 8      | 12 | OK                         |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| STAGE 1   |                       | INT=                    |       | STAGE 2     |                         | INT= 5 |    | STAGE 3                    |            | INT= 10        |             | STAGE 4          |                                | INT= 15         |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O      | N  | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h   | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.       |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| A1,A2   | 1                     | 3.75                    | A     | 1           | 15                      |        | N  | 1990                       | 70         | 89             |             | 159              | 0.44                           | 1906            |                   |   | 1906                    | 0.083 |           | 28    | 40               | 40            | 0.250                  | 21                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| A2  | 1                     | 3.75                    | A     | 1           |                         |        |    | 2130                       |            | 176            |             | 176              | 0.00                           | 2130            |                   |   | 2130                    | 0.083 |           |       | 40               | 40            | 0.248                  | 23                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| B1  | 1,2                   | 3.40                    | B     | 1           |                         |        | N  | 1955                       |            | 233            |             | 233              | 0.00                           | 1955            |                   |   | 1955                    | 0.119 | 0.120     |       | 57               | 57            | 0.251                  | 24                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| B1,B2   | 1,2                   | 3.40                    | B     | 1           | 20                      | O      |    | 2095                       |            | 202            | 20          | 222              | 0.09                           | 1852            |                   |   | 1852                    | 0.120 |           |       | 58               | 57            | 0.252                  | 23                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| C1,C2   | 3                     | 4.20                    | C     | 1           | 10                      |        | N  | 2035                       | 5          |                | 95          | 100              | 1.00                           | 1770            |                   |   | 1770                    | 0.057 | 0.057     |       | 27               | 27            | 0.251                  | 16                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  |                       |                         |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           | 7     |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| NOTE : 'O' - OPPOSING TRAFFIC      N - NEAR SIDE LANE      SG - STEADY GREEN      FG - FLASHING GREEN      PEDESTRIAN WALKING SPEED = 0.9m/s      QUEUING LENGTH = AVERAGE QUEUE * 6m |                       |                         |       |             |                         |        |    |                            |            |                |             |                  |                                |                 |                   |   |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |    |         |    |                   |            |    |           |            |      |      |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |

## **J1 YEAR 2035 PM TRAFFIC FLOW**

| OVE ARUP & PARTNERS   |                       |                         |       |             |                         |        |    | TRAFFIC SIGNAL CALCULATION |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|--------|----|----------------------------|---|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|-------------------------|-------------------|---|------------------------------------|-----|---|------------|-------|-------------------------|--------|-----|-------------------------|-----------|-----|--------|------------|-----|---------|-------|-------------------|------------|-------|-----------|------------|------|---|---------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng   |                       |                         |       |             |                         |        |    |                            | PROJECT NO: 299277-02   |                |             |                  |                                | Junction No. J1 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Lai King Hill Road / King Lai Path  |                       |                         |       | J1_BASE_PM  |                         |        |    |                            | DATE : 21-Jan-25  |                |             |                  | FILENAME :                     |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|                     |                       |                         |       |             |                         |        |    |                            | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.142</td></tr> <tr> <td>Loss time</td><td>L =</td><td>35 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>825 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 67.0 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 40.8 sec</td></tr> <tr> <td>Yult</td><td></td><td>= 0.638</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 349.7 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 41.5 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.708</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 350 %</td></tr> </table> |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               | No. of stages per cycle | N =               | 4 | No. of stage using for calculation | N = | 2 | Cycle time | C =   | 120 sec                 | Sum(y) | Y = | 0.142                   | Loss time | L = | 35 sec | Total Flow | =   | 825 pcu | Co    | = (1.5*L+5)/(1-Y) | = 67.0 sec | Cm    | = L/(1-Y) | = 40.8 sec | Yult |   | = 0.638 | R.C.ult | = (Yult-Y)/Y*100% | = 349.7 % | Cp | = 0.9*L/(0.9-Y) | = 41.5 sec | Ymax | = 1-L/C | = 0.708 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 350 % |
| No. of stages per cycle   | N =                   | 4                       |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| No. of stage using for calculation  | N =                   | 2                       |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Sum(y)  | Y =                   | 0.142                   |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Loss time   | L =                   | 35 sec                  |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Total Flow  | =                     | 825 pcu                 |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Co  | = (1.5*L+5)/(1-Y)     | = 67.0 sec              |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cm  | = L/(1-Y)             | = 40.8 sec              |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Yult  |                       | = 0.638                 |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 349.7 %               |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cp  | = 0.9*L/(0.9-Y)       | = 41.5 sec              |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ymax  | = 1-L/C               | = 0.708                 |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 350 %                 |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|                    |                       |                         |       |             |                         |        |    |                            | <table> <tr> <td>Pedestrian</td><td>Width</td><td colspan="3">Green Time Required (s)</td><td colspan="3">Green Time Provided (s)</td><td rowspan="4">Check</td></tr> <tr> <td>Phase</td><td>(m)</td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td></tr> <tr> <td>Dp</td><td>10</td><td>8</td><td>2</td><td>11</td><td>8</td><td>2</td><td>11</td></tr> <tr> <td>Ep</td><td>10.5</td><td>7</td><td>8</td><td>12</td><td>7</td><td>8</td><td>12</td></tr> </table>   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   | Pedestrian | Width | Green Time Required (s) |        |     | Green Time Provided (s) |           |     | Check  | Phase      | (m) | SG      | Delay | FG                | SG         | Delay | FG        | Dp         | 10   | 8 | 2       | 11      | 8                 | 2         | 11 | Ep              | 10.5       | 7    | 8       | 12      | 7       | 8                     | 12      |
| Pedestrian  | Width                 | Green Time Required (s) |       |             | Green Time Provided (s) |        |    | Check                      |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Phase   | (m)                   | SG                      | Delay | FG          | SG                      | Delay  | FG |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Dp  | 10                    | 8                       | 2     | 11          | 8                       | 2      | 11 |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  | 10.5                  | 7                       | 8     | 12          | 7                       | 8      | 12 |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| STAGE 1   |                       | INT=                    |       | STAGE 2     |                         | INT= 5 |    | STAGE 3                    |   | INT= 10        |             | STAGE 4          |                                | INT= 15         |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O      | N  | Straight-Ahead Sat. Flow   | Flow  |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            | Left pcu/h  | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| A1,A2   | 1                     | 3.75                    | A     | 1           | 15                      |        | N  | 1990                       | 65  | 103            |             | 168              | 0.39                           | 1916            |                   |                         | 1916                    | 0.088 |           | 28    | 53               | 53            | 0.199                   | 19                |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| A2  | 1                     | 3.75                    | A     | 1           |                         |        | N  | 2130                       |   | 187            |             | 187              | 0.00                           | 2130            |                   |                         | 2130                    | 0.088 |           |       | 53               | 53            | 0.199                   | 21                |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| B1  | 1,2                   | 3.40                    | B     | 1           |                         |        | N  | 1955                       |   | 210            |             | 210              | 0.00                           | 1955            |                   |                         | 1955                    | 0.107 | 0.108     |       | 64               | 64            | 0.201                   | 20                |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| B1,B2   | 1,2                   | 3.40                    | B     | 1           | 20                      | O      | N  | 2095                       |   | 185            | 15          | 200              | 0.08                           | 1855            |                   |                         | 1855                    | 0.108 |           |       | 65               | 64            | 0.202                   | 19                |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| C1,C2   | 3                     | 4.20                    | C     | 1           | 10                      |        | N  | 2035                       | 10  |                | 50          | 60               | 1.00                           | 1770            |                   |                         | 1770                    | 0.034 | 0.034     |       | 20               | 20            | 0.203                   | 10                |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  |                       |                         |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           | 7     |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| NOTE : 'O' - OPPOSING TRAFFIC      N - NEAR SIDE LANE      SG - STEADY GREEN      FG - FLASHING GREEN |                       |                         |       |             |                         |        |    |                            |   |                |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |   |                                    |     |   |            |       |                         |        |     |                         |           |     |        |            |     |         |       |                   |            |       |           |            |      |   |         |         |                   |           |    |                 |            |      |         |         |         |                       |         |

## J1 YEAR 2035 AM TRAFFIC FLOW REFERENCE SCENARIO

| OVE ARUP & PARTNERS   |                       |                         |       |             |                         |        |    | TRAFFIC SIGNAL CALCULATION |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|--------|----|----------------------------|------------------|---|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|-------------------------|-------------------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|----|----------|----|-------------------|------------|----|-----------|------------|------|----|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng   |                       |                         |       |             |                         |        |    |                            |                  |   |             |                  | PROJECT NO: 299277-02          |                 |                   | Junction No. J1         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Lai King Hill Road / King Lai Path  |                       |                         |       | J1_REF_AM   |                         |        |    |                            | DATE : 21-Jan-25 |   |             | FILENAME :       |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            |                  | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.215</td></tr> <tr> <td>Loss time</td><td>L =</td><td>35 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1125 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 73.3 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 44.6 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.638</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 196.4 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 46.0 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.708</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 196 %</td></tr> </table> |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               | No. of stages per cycle | N =               | 4                       | No. of stage using for calculation | N = | 2                       | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.215 | Loss time | L = | 35 sec | Total Flow | =  | 1125 pcu | Co | = (1.5*L+5)/(1-Y) | = 73.3 sec | Cm | = L/(1-Y) | = 44.6 sec | Yult | =  | 0.638 | R.C.ult | = (Yult-Y)/Y*100% | = 196.4 % | Cp | = 0.9*L/(0.9-Y) | = 46.0 sec | Ymax | = 1-L/C | = 0.708 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 196 % |
| No. of stages per cycle   | N =                   | 4                       |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| No. of stage using for calculation  | N =                   | 2                       |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Sum(y)  | Y =                   | 0.215                   |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Loss time   | L =                   | 35 sec                  |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Total Flow  | =                     | 1125 pcu                |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Co  | = (1.5*L+5)/(1-Y)     | = 73.3 sec              |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cm  | = L/(1-Y)             | = 44.6 sec              |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Yult  | =                     | 0.638                   |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 196.4 %               |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cp  | = 0.9*L/(0.9-Y)       | = 46.0 sec              |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ymax  | = 1-L/C               | = 0.708                 |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 196 %                 |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|    |                       |                         |       |             |                         |        |    |                            |                  | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <td></td><td></td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td><td></td></tr> <tr> <td>Dp</td><td>10</td><td>8</td><td>2</td><td>11</td><td>8</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>Ep</td><td>10.5</td><td>7</td><td>8</td><td>12</td><td>7</td><td>8</td><td>12</td><td>OK</td></tr> </table>  |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               | Pedestrian Phase        | Width (m)         | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   |        |     | SG    | Delay     | FG  | SG     | Delay      | FG |          | Dp | 10                | 8          | 2  | 11        | 8          | 2    | 11 | OK    | Ep      | 10.5              | 7         | 8  | 12              | 7          | 8    | 12      | OK      |         |                       |         |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |        |    | Check                      |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       | SG                      | Delay | FG          | SG                      | Delay  | FG |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Dp  | 10                    | 8                       | 2     | 11          | 8                       | 2      | 11 | OK                         |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  | 10.5                  | 7                       | 8     | 12          | 7                       | 8      | 12 | OK                         |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| STAGE 1   |                       | INT=                    |       | STAGE 2     |                         | INT= 5 |    | STAGE 3                    |                  | INT= 10   |             | STAGE 4          |                                | INT= 15         |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O      | N  | Straight-Ahead Sat. Flow   | Flow             |   |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            | Left pcu/h       | Straight pcu/h  | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| A1,A2   | 1                     | 3.75                    | A     | 1           | 15                      |        | N  | 1990                       | 70               | 130   |             | 200              | 0.35                           | 1923            |                   |                         | 1923                    | 0.104 |           | 28    | 41               | 41            | 0.304                   | 26                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| A2  | 1                     | 3.75                    | A     | 1           |                         |        | N  | 2130                       |                  | 221   |             | 221              | 0.00                           | 2130            |                   |                         | 2130                    | 0.104 |           |       | 41               | 41            | 0.304                   | 29                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| B1  | 1,2                   | 3.40                    | B     | 1           |                         |        | N  | 1955                       |                  | 310   |             | 310              | 0.00                           | 1955            |                   |                         | 1955                    | 0.159 | 0.159     |       | 63               | 63            | 0.302                   | 29                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| B1,B2   | 1,2                   | 3.40                    | B     | 1           | 20                      | O      | N  | 2095                       |                  | 274   | 20          | 294              | 0.07                           | 1856            |                   |                         | 1856                    | 0.158 |           |       | 63               | 63            | 0.302                   | 28                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| C1,C2   | 3                     | 4.20                    | C     | 1           | 10                      |        | N  | 2035                       | 5                |   | 95          | 100              | 1.00                           | 1770            |                   |                         | 1770                    | 0.057 | 0.057     |       | 22               | 22            | 0.308                   | 16                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  |                       |                         |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           | 7     |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| NOTE : 'O' - OPPOSING TRAFFIC    N - NEAR SIDE LANE    SG - STEADY GREEN    FG - FLASHING GREEN    PEDESTRIAN WALKING SPEED = 0.9m/s    QUEUING LENGTH = AVERAGE QUEUE * 6m |                       |                         |       |             |                         |        |    |                            |                  |   |             |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |

## J1 YEAR 2035 PM TRAFFIC FLOW REFERENCE SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |       |             |                         |        |    | TRAFFIC SIGNAL CALCULATION |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|--------|----|----------------------------|------------------|----------------|-------------|------------------|--------------------------------|-----------------|--|-------------------------|-------------------------|-------|-----------|---|------------------|---------------|-------------------------|-------------------|------------|------------------------------------|-------------------------|---|------------|-------------------------|---------|--------|-------|-------|-----------|-----|--------|------------|----|---------|----|-------------------|------------|----|-----------|------------|------|---|-------|---------|-------------------|-----------|------|-----------------|------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |       |             |                         |        |    |                            |                  |                |             |                  | PROJECT NO: 299277-02          |                 |  | Junction No. J1         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Lai King Hill Road / King Lai Path                      |                       |                         |       | J1_REF_PM   |                         |        |    |                            | DATE : 21-Jan-25 |                |             | FILENAME :       |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.158</td></tr> <tr> <td>Loss time</td><td>L =</td><td>35 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>968 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 68.3 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 41.6 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.638</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 303.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 42.4 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.708</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 304 %</td></tr> </table> |                         |                         |       |           |   |                  |               | No. of stages per cycle | N =               | 4          | No. of stage using for calculation | N =                     | 2 | Cycle time | C =                     | 120 sec | Sum(y) | Y =   | 0.158 | Loss time | L = | 35 sec | Total Flow | =  | 968 pcu | Co | = (1.5*L+5)/(1-Y) | = 68.3 sec | Cm | = L/(1-Y) | = 41.6 sec | Yult | = | 0.638 | R.C.ult | = (Yult-Y)/Y*100% | = 303.9 % | Cp   | = 0.9*L/(0.9-Y) | = 42.4 sec | Ymax | = 1-L/C | = 0.708 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 304 % |
| No. of stages per cycle                                 | N =                   | 4                       |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| No. of stage using for calculation                      | N =                   | 2                       |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Sum(y)  | Y =                   | 0.158                   |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Loss time   | L =                   | 35 sec                  |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Total Flow  | =                     | 968 pcu                 |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Co  | = (1.5*L+5)/(1-Y)     | = 68.3 sec              |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Cm  | = L/(1-Y)             | = 41.6 sec              |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Yult  | =                     | 0.638                   |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 303.9 %               |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Cp  | = 0.9*L/(0.9-Y)       | = 42.4 sec              |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Ymax  | = 1-L/C               | = 0.708                 |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 304 %                 |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           | <table> <tr> <th>Pedestrian</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <th>Phase</th><th></th><th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th><th></th></tr> <tr> <td>Dp</td><td>10</td><td>8</td><td>2</td><td>11</td><td>8</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>Ep</td><td>10.5</td><td>7</td><td>8</td><td>12</td><td>7</td><td>8</td><td>12</td><td>OK</td></tr> </table> |                  |               |                         |                   | Pedestrian | Width (m)                          | Green Time Required (s) |   |            | Green Time Provided (s) |         |        | Check | Phase |           | SG  | Delay  | FG         | SG | Delay   | FG |                   | Dp         | 10 | 8         | 2          | 11   | 8 | 2     | 11      | OK                | Ep        | 10.5 | 7               | 8          | 12   | 7       | 8       | 12      | OK                    |         |
| Pedestrian  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |        |    | Check                      |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Phase   |                       | SG                      | Delay | FG          | SG                      | Delay  | FG |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Dp  | 10                    | 8                       | 2     | 11          | 8                       | 2      | 11 | OK                         |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Ep  | 10.5                  | 7                       | 8     | 12          | 7                       | 8      | 12 | OK                         |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| STAGE 1   |                       | INT=                    |       | STAGE 2     |                         | INT= 5 |    | STAGE 3                    |                  | INT= 10        |             | STAGE 4          |                                | INT= 15         |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O      | N  | Straight-Ahead Sat. Flow   | Flow             |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient %  | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec   | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |             |                         |        |    |                            | Left pcu/h       | Straight pcu/h | Right pcu/h |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| A1,A2   | 1                     | 3.75                    | A     | 1           | 15                      |        | N  | 1990                       | 65               | 142            |             | 207              | 0.31                           | 1929            |  |                         | 1929                    | 0.107 |           | 28  | 58               | 58            | 0.222                   | 21                |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| A2  | 1                     | 3.75                    | A     | 1           |                         |        | N  | 2130                       |                  | 229            |             | 229              | 0.00                           | 2130            |  |                         | 2130                    | 0.108 |           |   | 58               | 58            | 0.222                   | 24                |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| B1  | 1,2                   | 3.40                    | B     | 1           |                         |        | N  | 1955                       |                  | 242            |             | 242              | 0.00                           | 1955            |  |                         | 1955                    | 0.124 | 0.124     |   | 67               | 67            | 0.222                   | 21                |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| B1,B2   | 1,2                   | 3.40                    | B     | 1           | 20                      | O      |    | 2095                       |                  | 215            | 15          | 230              | 0.07                           | 1856            |  |                         | 1856                    | 0.124 |           |   | 67               | 67            | 0.222                   | 20                |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| C1,C2   | 3                     | 4.20                    | C     | 1           | 10                      |        | N  | 2035                       | 10               |                | 50          | 60               | 1.00                           | 1770            |  |                         | 1770                    | 0.034 | 0.034     |   | 18               | 18            | 0.226                   | 10                |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| Ep  |                       |                         |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           | 7   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |
| NOTE : 'O' - OPPOSING TRAFFIC    N - NEAR SIDE LANE     |                       |                         |       |             |                         |        |    |                            |                  |                |             |                  |                                |                 |  |                         |                         |       |           |   |                  |               |                         |                   |            |                                    |                         |   |            |                         |         |        |       |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |      |                 |            |      |         |         |         |                       |         |



## J1 YEAR 2035 AM TRAFFIC FLOW DESIGN SCENARIO

[illegible]

## J1 YEAR 2035 PM TRAFFIC FLOW

OVE ARUP & PARTNERS

TRAFFIC SIGNAL CALCULATION

S16 Application for Proposed Development at Kau Wa Keng

PROJECT NO: 299277-02Junction No. J1

Lai King Hill Road / King Lai Path

J1\_DES\_PM

DATE : 21-Jan-25FILENAME :

The site plan shows an intersection between Lai King Hill Road (vertical) and King Lai Path (horizontal). Traffic flows are as follows:  
Lai King Hill Road Northbound: B2 (left turn, 15 vehicles), B1 (through/right turn, 473 vehicles).  
King Lai Path Southbound: C1 (left turn, 10 vehicles), C2 (through/right turn, 50 vehicles).  
King Lai Path Northbound: A1 (left turn, 65 vehicles), A2 (through/right turn, 390 vehicles).

|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 4          |
| No. of stage using for calculation | N =                   | 2          |
| Cycle time                         | C =                   | 120 sec    |
| Sum(y)                             | Y =                   | 0.162      |
| Loss time                          | L =                   | 35 sec     |
| Total Flow                         | =                     | 1003 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 68.6 sec |
| Cm                                 | = L/(1-Y)             | = 41.8 sec |
| Yult                               | =                     | 0.638      |
| R.C. ult                           | = (Yult-Y)/Y*100%     | = 292.8 %  |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 42.7 sec |
| Ymax                               | = 1-L/C               | = 0.708    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 293 %    |

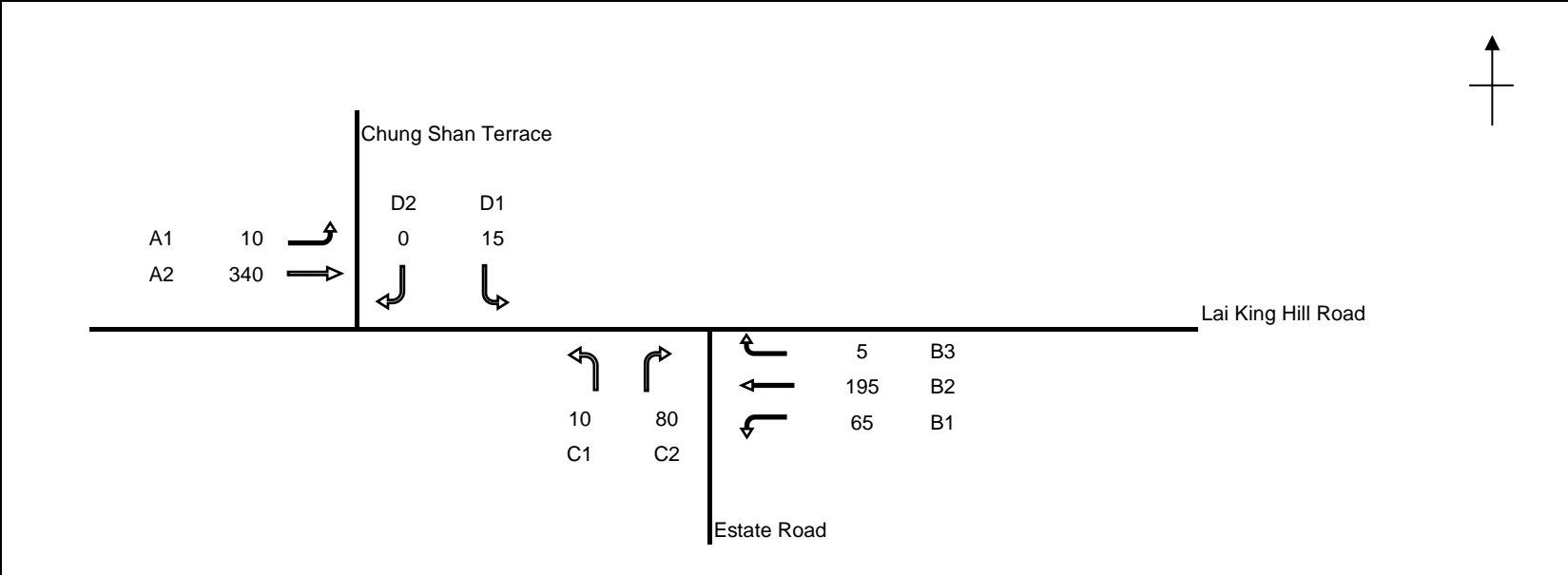
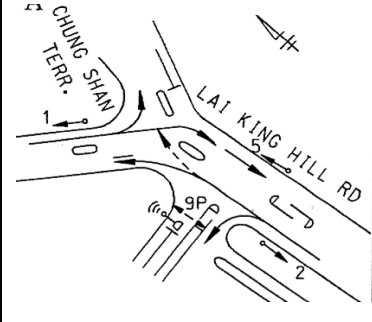
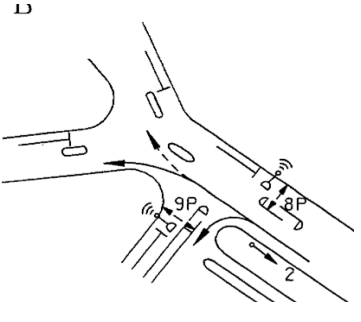
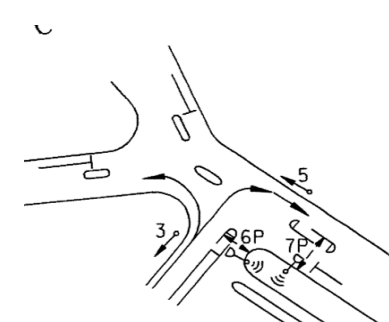
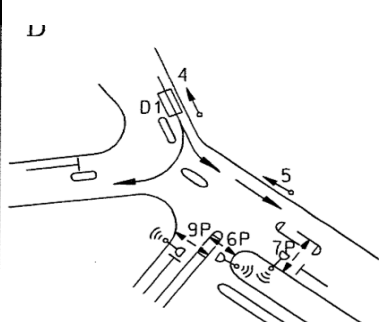
Detailed descriptions of the four stages:  
STAGE 1: Shows left-turning traffic from King Lai Path (A1) and right-turning traffic from Lai King Hill Road (B1).  
STAGE 2: Shows left-turning traffic from Lai King Hill Road (B2) and right-turning traffic from King Lai Path (C2).  
STAGE 3: Shows left-turning traffic from Lai King Hill Road (B2) and right-turning traffic from King Lai Path (C1).  
STAGE 4: Shows left-turning traffic from King Lai Path (A1) and right-turning traffic from Lai King Hill Road (B1).

| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |
| Dp               | 10        | 8                       | 2     | 11 | 8                       | 2     | 11 | OK    |
| Ep               | 10.5      | 7                       | 8     | 12 | 7                       | 8     | 12 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|          |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| A1,A2    | 1     | 3.75          | A     | 1           | 15        |   | N | 1990                     | 65         | 152            |             | 217              | 0.30                           | 1932            |                   |                         | 1932                    | 0.112 |           | 28    | 59               | 59            | 0.228                  | 22                |
| A2       | 1     | 3.75          | A     | 1           |           |   |   | 2130                     |            | 238            |             | 238              | 0.00                           | 2130            |                   |                         | 2130                    | 0.112 |           |       | 59               | 59            | 0.227                  | 24                |
| B1       | 1,2   | 3.40          | B     | 1           |           |   | N | 1955                     |            | 251            |             | 251              | 0.00                           | 1955            |                   |                         | 1955                    | 0.128 | 0.128     |       | 67               | 67            | 0.230                  | 22                |
| B1,B2    | 1,2   | 3.40          | B     | 1           | 20        | O |   | 2095                     |            | 222            | 15          | 237              | 0.06                           | 1856            |                   |                         | 1856                    | 0.128 |           |       | 67               | 67            | 0.229                  | 21                |
| C1,C2    | 3     | 4.20          | C     | 1           | 10        |   | N | 2035                     | 10         |                | 50          | 60               | 1.00                           | 1770            |                   |                         | 1770                    | 0.034 | 0.034     |       | 18               | 18            | 0.226                  | 10                |
| Ep       |       |               |       |             |           |   |   |                          |            |                |             |                  |                                |                 |                   |                         |                         |       |           | 7     |                  |               |                        |                   |

NOTE : 'O' - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

## J2 YEAR 2024 AM TRAFFIC FLOW

| OVE ARUP & PARTNERS  |                       |                         |         |   |                         |           |      | TRAFFIC SIGNAL CALCULATION   |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|--|-----------------------|-------------------------|---------|---|-------------------------|-----------|------|--|------------|----------------|-------------|--|--------------------------------|--|-------------------|--|-------------------------|-----------------|-----------|-------|------------------|---------------|------------------------|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|----|---------|-----|-------------------|------------|----|-----------|------------|------|----|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|---|---|---|---|----|----|-----|---|---|---|----|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng                            |                       |                         |         |   |                         |           |      |  |            |                |             |  |                                | PROJECT NO: 299277-02  |                   |  |                         | Junction No. J2 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Lai King Hill Road / Chung Shan Terrace  |                       |                         |         |   |                         | J2_OBS_AM |      |  |            |                |             |  |                                | DATE : 21-Jan-25   |                   |  |                         | FILENAME :      |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       |                         |         |   |                         |           |      |  |            |                |             |  |                                | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.119</td></tr> <tr> <td>Loss time</td><td>L =</td><td>37 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>720 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 68.7 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 42.0 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.623</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 422.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 42.6 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.692</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 423 %</td></tr> </table> |                   |  |                         |                 |           |       |                  |               |                        | No. of stages per cycle | N =       | 4                       | No. of stage using for calculation | N = | 3                       | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.119 | Loss time | L = | 37 sec | Total Flow | =  | 720 pcu | Co  | = (1.5*L+5)/(1-Y) | = 68.7 sec | Cm | = L/(1-Y) | = 42.0 sec | Yult | =  | 0.623 | R.C.ult | = (Yult-Y)/Y*100% | = 422.9 % | Cp | = 0.9*L/(0.9-Y) | = 42.6 sec | Ymax | = 1-L/C | = 0.692 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 423 % |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stages per cycle  | N =                   | 4                       |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stage using for calculation   | N =                   | 3                       |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cycle time   | C =                   | 120 sec                 |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Sum(y)   | Y =                   | 0.119                   |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Loss time  | L =                   | 37 sec                  |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Total Flow   | =                     | 720 pcu                 |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 68.7 sec              |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cm   | = L/(1-Y)             | = 42.0 sec              |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Yult   | =                     | 0.623                   |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 422.9 %               |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 42.6 sec              |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Ymax   | = 1-L/C               | = 0.692                 |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 423 %                 |         |   |                         |           |      |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       |                         |         |  |                         |           |      |  |            |                |             |  |                                |  |                   | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th></th><th></th><th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>6.8</td><td>5</td><td>3</td><td>6</td><td>24</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Fp</td><td>6.8</td><td>5</td><td>1</td><td>6</td><td>26</td><td>1</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>7</td><td>6</td><td>3</td><td>6</td><td>6</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Hp</td><td>7.3</td><td>7</td><td>1</td><td>7</td><td>89</td><td>1</td><td>7</td><td>OK</td></tr> </table> |                         |                 |           |       |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   |        |     | SG    | Delay     | FG  | SG     | Delay      | FG | Ep      | 6.8 | 5                 | 3          | 6  | 24        | 3          | 6    | OK | Fp    | 6.8     | 5                 | 1         | 6  | 26              | 1          | 6    | OK      | Gp      | 7       | 6                     | 3       | 6 | 6 | 3 | 6 | OK | Hp | 7.3 | 7 | 1 | 7 | 89 | 1 | 7 | OK |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |         |   | Green Time Provided (s) |           |      | Check  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       | SG                      | Delay   | FG  | SG                      | Delay     | FG   |  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Ep   | 6.8                   | 5                       | 3       | 6   | 24                      | 3         | 6    | OK   |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Fp   | 6.8                   | 5                       | 1       | 6   | 26                      | 1         | 6    | OK   |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Gp   | 7                     | 6                       | 3       | 6   | 6                       | 3         | 6    | OK   |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Hp   | 7.3                   | 7                       | 1       | 7   | 89                      | 1         | 7    | OK   |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| STAGE 1  | INT=                  | 12                      | STAGE 2 | INT=  | 10                      | STAGE 3   | INT= | 7  | STAGE 4    | INT=           | 5           |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Move-ment  | Stage                 | Lane Width m.           | Phase   | No. of lane   | Radius m.               | O         | N    | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h   | Proportion of Turning Vehicles | Sat. Flow pcu/h  | Uphill Gradient % | Short lane Effect pcu/h  | Revised Sat. Flow pcu/h | y               | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.       |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       |                         |         |   |                         |           |      |  | Left pcu/h | Straight pcu/h | Right pcu/h |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| A1, A2   | 1                     | 3.40                    | A       | 1   | 10                      |           | N    | 1955   | 10         | 158            |             | 168  | 0.06                           | 1938   |                   |  | 1938                    | 0.087           | 0.087     | 31    | 60               | 60            | 0.173                  | 17                      |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| A2   | 1                     | 3.40                    | A       | 1   |                         |           | N    | 2095   |            | 182            |             | 182  | 0.00                           | 2095   |                   |  | 2095                    | 0.087           |           |       | 61               | 60            | 0.174                  | 18                      |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| B1   | 1,2                   | 3.40                    | B       | 1   | 15                      |           | N    | 1955   | 65         |                |             | 65   | 1.00                           | 1777   |                   |  | 1777                    | 0.037           |           |       | 25               | 77            | 0.057                  | 5                       |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| B2,B3  | 1,2                   | 3.40                    | B       | 1   | 15                      | O         | N    | 2095   |            | 195            | 5           | 200  | 0.03                           | 1860   |                   |  | 1860                    | 0.108           |           |       | 75               | 77            | 0.168                  | 14                      |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| C1,C2  | 3                     | 3.40                    | C       | 1   | 15                      |           | N    | 1955   | 10         |                | 33          | 43   | 1.00                           | 1777   |                   |  | 1777                    | 0.024           | 0.024     |       | 17               | 17            | 0.171                  | 7                       |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| C2   | 3                     | 3.40                    | C       | 1   | 25                      |           | N    | 209  |            |                |             |  |                                |  |                   |  |                         |                 |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |    |    |     |   |   |   |    |   |   |    |

## J2 YEAR 2024 PM TRAFFIC FLOW

[illegible]

## J2 YEAR 2035 AM TRAFFIC FLOW BASELINE SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |         |             |                         |         |      | TRAFFIC SIGNAL CALCULATION |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
|---|-----------------------|-------------------------|---------|-------------|-------------------------|---------|------|----------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|--|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|--|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|----|---------|-----|-------------------|------------|----|-----------|------------|------|----|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|---|---|----|-----|---|---|---|----|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |         |             |                         |         |      | PROJECT NO: 299277-02      |            |                |             |                  |                                |                 |                   | Junction No. J2  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Lai King Hill Road / Chung Shan Terrace                 |                       |                         |         | J2_BASE_AM  |                         |         |      | DATE : 21-Jan-25           |            |                |             | FILENAME :       |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
|   |                       |                         |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.124</td></tr> <tr> <td>Loss time</td><td>L =</td><td>37 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>745 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 69.1 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 42.2 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.623</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 402.1 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 42.9 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.692</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 402 %</td></tr> </table> |                         |       |           |       |                  |               |                        |                   |  | No. of stages per cycle | N =       | 4                       | No. of stage using for calculation | N = | 3                       | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.124 | Loss time | L = | 37 sec | Total Flow | =  | 745 pcu | Co  | = (1.5*L+5)/(1-Y) | = 69.1 sec | Cm | = L/(1-Y) | = 42.2 sec | Yult | =  | 0.623 | R.C.ult | = (Yult-Y)/Y*100% | = 402.1 % | Cp | = 0.9*L/(0.9-Y) | = 42.9 sec | Ymax | = 1-L/C | = 0.692 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 402 % |   |   |    |     |   |   |   |    |   |   |    |
| No. of stages per cycle                                 | N =                   | 4                       |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| No. of stage using for calculation                      | N =                   | 3                       |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Cycle time  | C =                   | 120 sec                 |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Sum(y)  | Y =                   | 0.124                   |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Loss time   | L =                   | 37 sec                  |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Total Flow  | =                     | 745 pcu                 |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 69.1 sec              |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Cm  | = L/(1-Y)             | = 42.2 sec              |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Yult  | =                     | 0.623                   |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 402.1 %               |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 42.9 sec              |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Ymax  | = 1-L/C               | = 0.692                 |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 402 %                 |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
|   |                       |                         |         |             |                         |         |      |                            |            |                |             |                  |                                |                 |                   | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="5">Check</th></tr> <tr> <td></td><td></td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td></tr> <tr> <td>Ep</td><td>6.8</td><td>5</td><td>3</td><td>6</td><td>23</td><td>3</td><td>6</td></tr> <tr> <td>Fp</td><td>6.8</td><td>5</td><td>1</td><td>6</td><td>25</td><td>1</td><td>6</td></tr> <tr> <td>Gp</td><td>7</td><td>6</td><td>3</td><td>6</td><td>6</td><td>3</td><td>6</td></tr> <tr> <td>Hp</td><td>7.3</td><td>7</td><td>1</td><td>7</td><td>88</td><td>1</td><td>7</td><td>OK</td></tr> </table>  |                         |       |           |       |                  |               |                        |                   |  | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   |        |     | SG    | Delay     | FG  | SG     | Delay      | FG | Ep      | 6.8 | 5                 | 3          | 6  | 23        | 3          | 6    | Fp | 6.8   | 5       | 1                 | 6         | 25 | 1               | 6          | Gp   | 7       | 6       | 3       | 6                     | 6       | 3 | 6 | Hp | 7.3 | 7 | 1 | 7 | 88 | 1 | 7 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |         |             | Green Time Provided (s) |         |      | Check                      |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
|   |                       | SG                      | Delay   | FG          | SG                      | Delay   | FG   |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Ep  | 6.8                   | 5                       | 3       | 6           | 23                      | 3       | 6    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Fp  | 6.8                   | 5                       | 1       | 6           | 25                      | 1       | 6    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Gp  | 7                     | 6                       | 3       | 6           | 6                       | 3       | 6    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Hp  | 7.3                   | 7                       | 1       | 7           | 88                      | 1       | 7    | OK                         |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| STAGE 1   | INT=                  | 12                      | STAGE 2 | INT=        | 10                      | STAGE 3 | INT= | 7                          | STAGE 4    | INT=           | 5           |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| Move-ment   | Stage                 | Lane Width m.           | Phase   | No. of lane | Radius m.               | O       | N    | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h  | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
|   |                       |                         |         |             |                         |         |      |                            | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| A1, A2  | 1                     | 3.40                    | A       | 1           | 10                      |         | N    | 1955                       | 10         | 165            |             | 175              | 0.06                           | 1938            |                   |  | 1938                    | 0.090 | 0.091     | 31    | 60               | 60            | 0.181                  | 18                |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| A2  | 1                     | 3.40                    | A       | 1           |                         |         | N    | 2095                       |            | 190            |             | 190              | 0.00                           | 2095            |                   |  | 2095                    | 0.091 |           |       | 61               | 60            | 0.181                  | 19                |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| B1  | 1,2                   | 3.40                    | B       | 1           | 15                      |         | N    | 1955                       | 65         |                |             | 65               | 1.00                           | 1777            |                   |  | 1777                    | 0.037 |           |       | 24               | 77            | 0.057                  | 5                 |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| B2,B3   | 1,2                   | 3.40                    | B       | 1           | 15                      | O       | N    | 2095                       |            | 200            | 5           | 205              | 0.02                           | 1860            |                   |  | 1860                    | 0.110 |           |       | 74               | 77            | 0.172                  | 15                |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |
| C1,C2   | 3                     | 3.40                    | C       | 1           | 15                      |         | N    | 1955                       | 10         |                | 35          | 45               | 1.00                           | 1777            |                   |  | 1777                    | 0.025 | 0.025     |       | 17               | 17            | 0.179                  | 8                 |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |    |

## J2 YEAR 2035 PM TRAFFIC FLOW BASELINE SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |       |             |                         |       |    | TRAFFIC SIGNAL CALCULATION |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|-------|----|----------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|--|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|--|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|----|---------|-----|-------------------|------------|----|-----------|------------|------|----|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|---|---|----|-----|---|---|---|----|---|---|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |       |             |                         |       |    | PROJECT NO: 299277-02      |            |                |             |                  |                                |                 |                   | Junction No. J2  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Lai King Hill Road / Chung Shan Terrace                 |                       |                         |       | J2_BASE_PM  |                         |       |    | DATE : 21-Jan-25           |            |                |             | FILENAME :       |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
|   |                       |                         |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.142</td></tr> <tr> <td>Loss time</td><td>L =</td><td>16 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>735 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 33.8 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 18.7 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.780</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 448.3 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 19.0 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.867</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 448 %</td></tr> </table> |                         |       |           |       |                  |               |                        |                   |  | No. of stages per cycle | N =       | 4                       | No. of stage using for calculation | N = | 3                       | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.142 | Loss time | L = | 16 sec | Total Flow | =  | 735 pcu | Co  | = (1.5*L+5)/(1-Y) | = 33.8 sec | Cm | = L/(1-Y) | = 18.7 sec | Yult | =  | 0.780 | R.C.ult | = (Yult-Y)/Y*100% | = 448.3 % | Cp | = 0.9*L/(0.9-Y) | = 19.0 sec | Ymax | = 1-L/C | = 0.867 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 448 % |   |   |    |     |   |   |   |    |   |   |
| No. of stages per cycle                                 | N =                   | 4                       |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| No. of stage using for calculation                      | N =                   | 3                       |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Sum(y)  | Y =                   | 0.142                   |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Loss time   | L =                   | 16 sec                  |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Total Flow  | =                     | 735 pcu                 |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Co  | = (1.5*L+5)/(1-Y)     | = 33.8 sec              |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Cm  | = L/(1-Y)             | = 18.7 sec              |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Yult  | =                     | 0.780                   |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 448.3 %               |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Cp  | = 0.9*L/(0.9-Y)       | = 19.0 sec              |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Ymax  | = 1-L/C               | = 0.867                 |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 448 %                 |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
|   |                       |                         |       |             |                         |       |    |                            |            |                |             |                  |                                |                 |                   | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="6">Check</th></tr> <tr> <th></th><th></th><th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>6.8</td><td>5</td><td>3</td><td>6</td><td>19</td><td>3</td><td>6</td></tr> <tr> <td>Fp</td><td>6.8</td><td>5</td><td>1</td><td>6</td><td>21</td><td>1</td><td>6</td></tr> <tr> <td>Gp</td><td>7</td><td>6</td><td>3</td><td>6</td><td>6</td><td>3</td><td>6</td></tr> <tr> <td>Hp</td><td>7.3</td><td>7</td><td>1</td><td>7</td><td>94</td><td>1</td><td>7</td></tr> </table>   |                         |       |           |       |                  |               |                        |                   |  | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   |        |     | SG    | Delay     | FG  | SG     | Delay      | FG | Ep      | 6.8 | 5                 | 3          | 6  | 19        | 3          | 6    | Fp | 6.8   | 5       | 1                 | 6         | 21 | 1               | 6          | Gp   | 7       | 6       | 3       | 6                     | 6       | 3 | 6 | Hp | 7.3 | 7 | 1 | 7 | 94 | 1 | 7 |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |       |    | Check                      |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
|   |                       | SG                      | Delay | FG          | SG                      | Delay | FG |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Ep  | 6.8                   | 5                       | 3     | 6           | 19                      | 3     | 6  |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Fp  | 6.8                   | 5                       | 1     | 6           | 21                      | 1     | 6  |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Gp  | 7                     | 6                       | 3     | 6           | 6                       | 3     | 6  |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Hp  | 7.3                   | 7                       | 1     | 7           | 94                      | 1     | 7  |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| STAGE 1   | INT=                  | STAGE 2                 | INT=  | 7           | STAGE 3                 | INT=  | 7  | STAGE 4                    | INT=       | 5              |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O     | N  | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h  | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
|   |                       |                         |       |             |                         |       |    |                            | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| A1, A2  | 1                     | 3.40                    | A     | 1           | 10                      |       | N  | 1955                       | 20         | 152            |             | 172              | 0.12                           | 1921            |                   |  | 1921                    | 0.090 |           | 16    | 65               | 65            | 0.165                  | 16                |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| A2  | 1                     | 3.40                    | A     | 1           |                         |       | N  | 2095                       |            | 188            |             | 188              | 0.00                           | 2095            |                   |  | 2095                    | 0.090 |           |       | 66               | 66            | 0.163                  | 17                |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| B1  | 1,2                   | 3.40                    | B     | 1           | 15                      |       | N  | 1955                       | 80         |                |             | 80               | 1.00                           | 1777            |                   |  | 1777                    | 0.045 | 0.118     |       | 33               | 86            | 0.063                  | 5                 |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| B2,B3   | 1,2                   | 3.40                    | B     | 1           | 15                      | O     | N  | 2095                       |            | 220            | 0           | 220              | 0.00                           | 1865            |                   |  | 1865                    | 0.118 |           |       | 86               | 86            | 0.165                  | 12                |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |
| C1,C2   | 3                     | 3.40                    | C     | 1           | 15                      | </    |    |                            |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |                   |  |                         |           |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |     |                   |            |    |           |            |      |    |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |     |   |   |   |    |   |   |



## J2 YEAR 2035 AM TRAFFIC FLOW REFERENCE SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |       |             |                         |         |    |                          |            | TRAFFIC SIGNAL CALCULATION |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|---------|----|--------------------------|------------|----------------------------|-------------|------------------|--------------------------------|--|-------------------|-------------------------|-------------------------|-------|-----------|-----------------|------------------|---------------|-------------------------|-------------------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|----|---------|----|-------------------|------------|----|-----------|------------|------|---|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|---|---|---|---|---|----|----|-----|---|---|---|----|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |       |             |                         |         |    |                          |            | PROJECT NO: 299277-02      |             |                  |                                |  |                   |                         |                         |       |           | Junction No. J2 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Lai King Hill Road / Chung Shan Terrace                 |                       |                         |       |             | J2_REF_AM               |         |    |                          |            | DATE : 21-Jan-25           |             |                  |                                |  | FILENAME :        |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       |                         |       |             |                         |         |    |                          |            |                            |             |                  |                                | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.161</td></tr> <tr> <td>Loss time</td><td>L =</td><td>39 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>980 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 75.7 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 46.5 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.608</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 277.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 47.5 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.675</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 278 %</td></tr> </table> |                   |                         |                         |       |           |                 |                  |               | No. of stages per cycle | N =               | 4                       | No. of stage using for calculation | N = | 3                       | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.161 | Loss time | L = | 39 sec | Total Flow | =  | 980 pcu | Co | = (1.5*L+5)/(1-Y) | = 75.7 sec | Cm | = L/(1-Y) | = 46.5 sec | Yult | = | 0.608 | R.C.ult | = (Yult-Y)/Y*100% | = 277.9 % | Cp | = 0.9*L/(0.9-Y) | = 47.5 sec | Ymax | = 1-L/C | = 0.675 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 278 % |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stages per cycle                                 | N =                   | 4                       |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stage using for calculation                      | N =                   | 3                       |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Sum(y)  | Y =                   | 0.161                   |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Loss time   | L =                   | 39 sec                  |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Total Flow  | =                     | 980 pcu                 |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 75.7 sec              |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cm  | = L/(1-Y)             | = 46.5 sec              |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Yult  | =                     | 0.608                   |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 277.9 %               |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 47.5 sec              |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Ymax  | = 1-L/C               | = 0.675                 |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 278 %                 |       |             |                         |         |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       |                         |       |             |                         |         |    |                          |            |                            |             |                  |                                | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <td></td><td></td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td><td></td></tr> <tr> <td>Ep</td><td>6.8</td><td>5</td><td>3</td><td>6</td><td>20</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Fp</td><td>6.8</td><td>5</td><td>1</td><td>6</td><td>22</td><td>1</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>7</td><td>6</td><td>3</td><td>6</td><td>6</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Hp</td><td>7.3</td><td>7</td><td>1</td><td>7</td><td>93</td><td>1</td><td>7</td><td>OK</td></tr> </table>  |                   |                         |                         |       |           |                 |                  |               | Pedestrian Phase        | Width (m)         | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   |        |     | SG    | Delay     | FG  | SG     | Delay      | FG |         | Ep | 6.8               | 5          | 3  | 6         | 20         | 3    | 6 | OK    | Fp      | 6.8               | 5         | 1  | 6               | 22         | 1    | 6       | OK      | Gp      | 7                     | 6       | 3 | 6 | 6 | 3 | 6 | OK | Hp | 7.3 | 7 | 1 | 7 | 93 | 1 | 7 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |         |    | Check                    |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       | SG                      | Delay | FG          | SG                      | Delay   | FG |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Ep  | 6.8                   | 5                       | 3     | 6           | 20                      | 3       | 6  | OK                       |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Fp  | 6.8                   | 5                       | 1     | 6           | 22                      | 1       | 6  | OK                       |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Gp  | 7                     | 6                       | 3     | 6           | 6                       | 3       | 6  | OK                       |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Hp  | 7.3                   | 7                       | 1     | 7           | 93                      | 1       | 7  | OK                       |            |                            |             |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| STAGE 1   |                       | INT= 12                 |       | STAGE 2     |                         | INT= 10 |    | STAGE 3                  |            | INT= 7                     |             | STAGE 4          |                                | INT= 5   |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O       | N  | Straight-Ahead Sat. Flow | Flow       |                            |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h  | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec           | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       |                         |       |             |                         |         |    |                          | Left pcu/h | Straight pcu/h             | Right pcu/h |                  |                                |  |                   |                         |                         |       |           |                 |                  |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| A1, A2  | 1                     | 3.40                    | A     | 1           | 10                      |         | N  | 1955                     | 10         | 237                        |             | 247              | 0.04                           | 1943   |                   |                         | 1943                    | 0.127 | 0.127     | 31              | 64               | 64            | 0.238                   | 23                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| A2  | 1                     | 3.40                    | A     | 1           |                         |         |    | 2095                     |            | 267                        |             | 267              | 0.00                           | 2095   |                   |                         | 2095                    | 0.127 |           |                 | 64               | 64            | 0.239                   | 25                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| B1  | 1,2                   | 3.40                    | B     | 1           | 15                      |         | N  | 1955                     | 65         |                            |             | 65               | 1.00                           | 1777   |                   |                         | 1777                    | 0.037 |           |                 | 18               | 81            | 0.054                   | 4                 |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| B2,B3   | 1,2                   | 3.40                    | B     | 1           | 15                      | O       |    | 2095                     |            | 286                        | 5           | 291              | 0.02                           | 1862   |                   |                         | 1862                    | 0.156 |           |                 | 79               | 81            | 0.232                   | 19                |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| C1,C2   | 3                     | 3.40                    | C     | 1           | 15                      |         | N  | 1955                     | 10         |                            | 35          | 45               | 1.00                           | 1777   |                   |                         | 1777                    | 0.025 | 0.025     |                 | 13               | 13            | 0.234                   | 8                 |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| C2  | 3                     | 3.40                    | C     | 1           | 25                      |         |    | 2095                     |            |                            | 50          | 50               | 1.00                           | 1976   |                   |                         | 1976                    | 0.025 |           |                 | 13               |               |                         |                   |                         |                                    |     |                         |            |     |         |        |     |       |           |     |        |            |    |         |    |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |

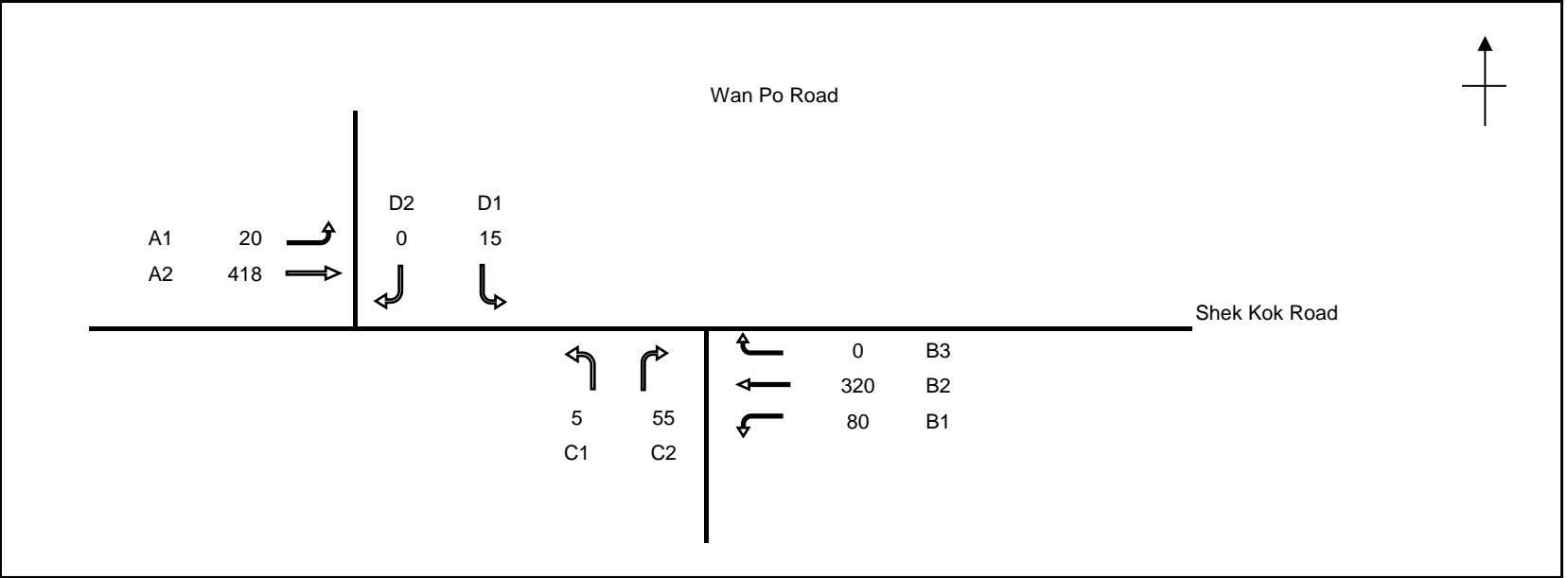
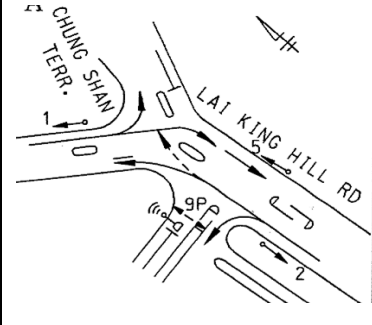
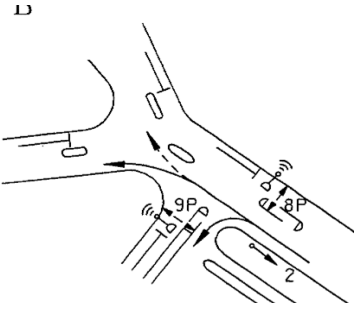
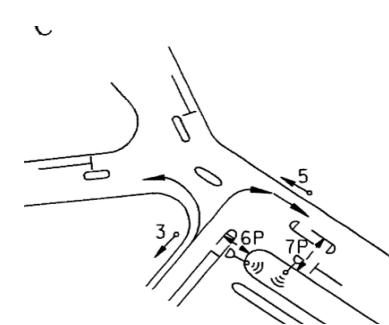
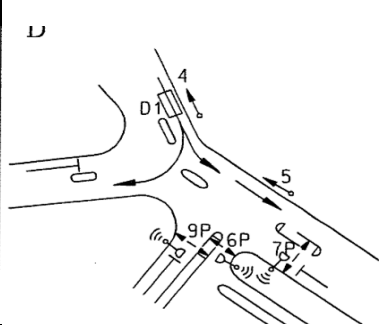
## J2 YEAR 2035 PM TRAFFIC FLOW REFERENCE SCENARIO

[illegible]

## J2 YEAR 2035 AM TRAFFIC FLOW DESIGN SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |       |             |                         |         |    |                          |            | TRAFFIC SIGNAL CALCULATION  |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|---------|----|--------------------------|------------|---|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-----------------|------------------|---------------|------------------------|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-------|-------|-----------|-------|--------|------------|-----|----------|----|-------------------|------------|----|-----------|------------|------|-----|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|---|---|----|----|-----|---|---|---|----|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |       |             |                         |         |    |                          |            | PROJECT NO: 299277-02   |             |                  |                                |                 |                   |                         |                         |       |           | Junction No. J2 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Lai King Hill Road / Chung Shan Terrace                 |                       |                         |       |             | J2_DES_AM               |         |    |                          |            | DATE : 21-Jan-25  |             |                  |                                |                 | FILENAME :        |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       |                         |       |             |                         |         |    |                          |            | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.169</td></tr> <tr> <td>Loss time</td><td>L =</td><td>39 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1034 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 76.4 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 46.9 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.608</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 259.8 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 48.0 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.675</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 260 %</td></tr> </table> |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        | No. of stages per cycle | N =       | 4                       | No. of stage using for calculation | N = | 3                       | Cycle time | C = | 120 sec | Sum(y) | Y =   | 0.169 | Loss time | L =   | 39 sec | Total Flow | =   | 1034 pcu | Co | = (1.5*L+5)/(1-Y) | = 76.4 sec | Cm | = L/(1-Y) | = 46.9 sec | Yult | =   | 0.608 | R.C.ult | = (Yult-Y)/Y*100% | = 259.8 % | Cp | = 0.9*L/(0.9-Y) | = 48.0 sec | Ymax | = 1-L/C | = 0.675 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 260 % |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stages per cycle                                 | N =                   | 4                       |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stage using for calculation                      | N =                   | 3                       |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Sum(y)  | Y =                   | 0.169                   |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Loss time   | L =                   | 39 sec                  |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Total Flow  | =                     | 1034 pcu                |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 76.4 sec              |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Cm  | = L/(1-Y)             | = 46.9 sec              |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Yult  | =                     | 0.608                   |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 259.8 %               |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 48.0 sec              |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Ymax  | = 1-L/C               | = 0.675                 |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 260 %                 |       |             |                         |         |    |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       |                         |       |             |                         |         |    |                          |            | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>6.8</td><td>5</td><td>3</td><td>6</td><td>19</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Fp</td><td>6.8</td><td>5</td><td>1</td><td>6</td><td>21</td><td>1</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>7</td><td>6</td><td>3</td><td>6</td><td>6</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Hp</td><td>7.3</td><td>7</td><td>1</td><td>7</td><td>94</td><td>1</td><td>7</td><td>OK</td></tr> </table>  |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   | SG     | Delay | FG    | SG        | Delay | FG     | Ep         | 6.8 | 5        | 3  | 6                 | 19         | 3  | 6         | OK         | Fp   | 6.8 | 5     | 1       | 6                 | 21        | 1  | 6               | OK         | Gp   | 7       | 6       | 3       | 6                     | 6       | 3 | 6 | OK | Hp | 7.3 | 7 | 1 | 7 | 94 | 1 | 7 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |         |    | Check                    |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       | SG                      | Delay | FG          | SG                      | Delay   | FG |                          |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Ep  | 6.8                   | 5                       | 3     | 6           | 19                      | 3       | 6  | OK                       |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Fp  | 6.8                   | 5                       | 1     | 6           | 21                      | 1       | 6  | OK                       |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Gp  | 7                     | 6                       | 3     | 6           | 6                       | 3       | 6  | OK                       |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Hp  | 7.3                   | 7                       | 1     | 7           | 94                      | 1       | 7  | OK                       |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| STAGE 1   |                       | INT= 12                 |       | STAGE 2     |                         | INT= 10 |    | STAGE 3                  |            | INT= 7  |             | STAGE 4          |                                | INT= 5          |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O       | N  | Straight-Ahead Sat. Flow | Flow       |   |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec           | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.       |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
|   |                       |                         |       |             |                         |         |    |                          | Left pcu/h | Straight pcu/h  | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| A1, A2  | 1                     | 3.40                    | A     | 1           | 10                      |         | N  | 1955                     | 10         | 253   |             | 263              | 0.04                           | 1944            |                   |                         | 1944                    | 0.135 | 0.136     | 31              | 65               | 65            | 0.250                  | 24                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| A2  | 1                     | 3.40                    | A     | 1           |                         |         |    | 2095                     |            | 284   |             | 284              | 0.00                           | 2095            |                   |                         | 2095                    | 0.136 |           |                 | 65               | 65            | 0.250                  | 26                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| B1  | 1,2                   | 3.40                    | B     | 1           | 15                      |         | N  | 1955                     | 65         |   |             | 65               | 1.00                           | 1777            |                   |                         | 1777                    | 0.037 |           |                 | 18               | 82            | 0.054                  | 4                       |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| B2,B3   | 1,2                   | 3.40                    | B     | 1           | 15                      | O       |    | 2095                     |            | 307   | 5           | 312              | 0.02                           | 1862            |                   |                         | 1862                    | 0.168 |           |                 | 80               | 82            | 0.245                  | 20                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| C1,C2   | 3                     | 3.40                    | C     | 1           | 15                      |         | N  | 1955                     | 10         |   | 35          | 45               | 1.00                           | 1777            |                   |                         | 1777                    | 0.025 | 0.025     |                 | 12               | 12            | 0.253                  | 8                       |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |
| C2  | 3                     | 3.40                    | C     | 1           | 25                      |         |    | 2095                     |            |   |             |                  |                                |                 |                   |                         |                         |       |           |                 |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |    |     |   |   |   |    |   |   |    |

## J2 YEAR 2035 PM TRAFFIC FLOW DESIGN SCENARIO

| OVE ARUP & PARTNERS  |                       |                         |       |             |   |       |    | TRAFFIC SIGNAL CALCULATION |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|--|-----------------------|-------------------------|-------|-------------|---|-------|----|----------------------------|------------|--|-------------|------------------|--------------------------------|-----------------|--|-------------------------|-------------------------|-------|-----------|---|------------------|-------------------------|------------------------|-------------------|------------------------------------|-----------|-------------------------|------------|-----|-------------------------|--------|-----|-------|-----------|-----|--------|------------|----|---------|-------|-------------------|------------|----|-----------|------------|------|---|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|----|---|---|---|---|---|---|---|----|----|-----|---|---|---|----|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng                            |                       |                         |       |             |   |       |    | PROJECT NO: 299277-02      |            |  |             |                  |                                |                 |  | Junction No. J2         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Lai King Hill Road / Chung Shan Terrace  |                       |                         |       | J2_DES_PM   |   |       |    | DATE : 21-Jan-25           |            |  |             | FILENAME :       |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       |                         |       |             |   |       |    |                            |            |  |             |                  |                                |                 | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.196</td></tr> <tr> <td>Loss time</td><td>L =</td><td>18 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>913 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 39.8 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 22.4 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.765</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 290.5 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 23.0 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.850</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 291 %</td></tr> </table> |                         |                         |       |           |   |                  | No. of stages per cycle | N =                    | 4                 | No. of stage using for calculation | N =       | 3                       | Cycle time | C = | 120 sec                 | Sum(y) | Y = | 0.196 | Loss time | L = | 18 sec | Total Flow | =  | 913 pcu | Co    | = (1.5*L+5)/(1-Y) | = 39.8 sec | Cm | = L/(1-Y) | = 22.4 sec | Yult | = | 0.765 | R.C.ult | = (Yult-Y)/Y*100% | = 290.5 % | Cp | = 0.9*L/(0.9-Y) | = 23.0 sec | Ymax | = 1-L/C | = 0.850 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 291 % |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stages per cycle  | N =                   | 4                       |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| No. of stage using for calculation   | N =                   | 3                       |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cycle time   | C =                   | 120 sec                 |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Sum(y)   | Y =                   | 0.196                   |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Loss time  | L =                   | 18 sec                  |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Total Flow   | =                     | 913 pcu                 |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 39.8 sec              |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cm   | = L/(1-Y)             | = 22.4 sec              |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Yult   | =                     | 0.765                   |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 290.5 %               |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 23.0 sec              |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Ymax   | = 1-L/C               | = 0.850                 |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 291 %                 |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       |                         |       |             |  |       |    |                            |            |  |             |                  |                                |                 |    |                         |                         |       |           | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <td></td><td></td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td><td></td></tr> <tr> <td>Ep</td><td>6.8</td><td>5</td><td>3</td><td>6</td><td>15</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Fp</td><td>6.8</td><td>5</td><td>1</td><td>6</td><td>17</td><td>1</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>7</td><td>6</td><td>3</td><td>6</td><td>6</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Hp</td><td>7.3</td><td>7</td><td>1</td><td>7</td><td>97</td><td>1</td><td>7</td><td>OK</td></tr> </table> |                  |                         |                        |                   | Pedestrian Phase                   | Width (m) | Green Time Required (s) |            |     | Green Time Provided (s) |        |     | Check |           |     | SG     | Delay      | FG | SG      | Delay | FG                |            | Ep | 6.8       | 5          | 3    | 6 | 15    | 3       | 6                 | OK        | Fp | 6.8             | 5          | 1    | 6       | 17      | 1       | 6                     | OK      | Gp | 7 | 6 | 3 | 6 | 6 | 3 | 6 | OK | Hp | 7.3 | 7 | 1 | 7 | 97 | 1 | 7 | OK |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s)   |       |    | Check                      |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       | SG                      | Delay | FG          | SG  | Delay | FG |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Ep   | 6.8                   | 5                       | 3     | 6           | 15  | 3     | 6  | OK                         |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Fp   | 6.8                   | 5                       | 1     | 6           | 17  | 1     | 6  | OK                         |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Gp   | 7                     | 6                       | 3     | 6           | 6   | 3     | 6  | OK                         |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Hp   | 7.3                   | 7                       | 1     | 7           | 97  | 1     | 7  | OK                         |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| STAGE 1  | INT=                  | STAGE 2                 | INT=  | 7           | STAGE 3   | INT=  | 7  | STAGE 4                    | INT=       | 5  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| Move-ment  | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.   | O     | N  | Straight-Ahead Sat. Flow   | Flow       |  |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient %  | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec   | g (required) sec | g (input) sec           | Degree of Saturation X | Queuing Length m. |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
|  |                       |                         |       |             |   |       |    |                            | Left pcu/h | Straight pcu/h   | Right pcu/h |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| A1, A2   | 1                     | 3.40                    | A     | 1           | 10  |       | N  | 1955                       | 20         | 191  |             | 211              | 0.09                           | 1928            |  |                         | 1928                    | 0.109 |           | 16  | 57               | 57                      | 0.230                  | 22                |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| A2   | 1                     | 3.40                    | A     | 1           |   |       | N  | 2095                       |            | 227  |             | 227              | 0.00                           | 2095            |  |                         | 2095                    | 0.108 |           |   | 56               | 56                      | 0.232                  | 24                |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| B1   | 1,2                   | 3.40                    | B     | 1           | 15  |       | N  | 1955                       | 80         |  |             | 80               | 1.00                           | 1777            |  |                         | 1777                    | 0.045 | 0.172     |   | 23               | 89                      | 0.061                  | 4                 |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| B2,B3  | 1,2                   | 3.40                    | B     | 1           | 15  | O     | N  | 2095                       |            | 320  | 0           | 320              | 0.00                           | 1865            |  |                         | 1865                    | 0.172 |           |   | 89               | 89                      | 0.231                  | 17                |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| C1,C2  | 3                     | 3.40                    | C     | 1           | 15  |       | N  | 1955                       | 5          |  | 24          | 29               | 1.00                           | 1777            |  |                         | 1777                    | 0.016 | 0.016     |   | 8                | 8                       | 0.245                  | 5                 |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| C2   | 3                     | 3.40                    | C     | 1           | 25  |       | N  | 2095                       |            |  | 31          | 31               | 1.00                           | 1976            |  |                         | 1976                    | 0.016 |           |   | 8                | 8                       | 0.235                  | 6                 |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |
| D1,D2  | 4                     |                         |       |             |   |       |    |                            |            |  |             |                  |                                |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |           |                         |            |     |                         |        |     |       |           |     |        |            |    |         |       |                   |            |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |    |   |   |   |   |   |   |   |    |    |     |   |   |   |    |   |   |    |

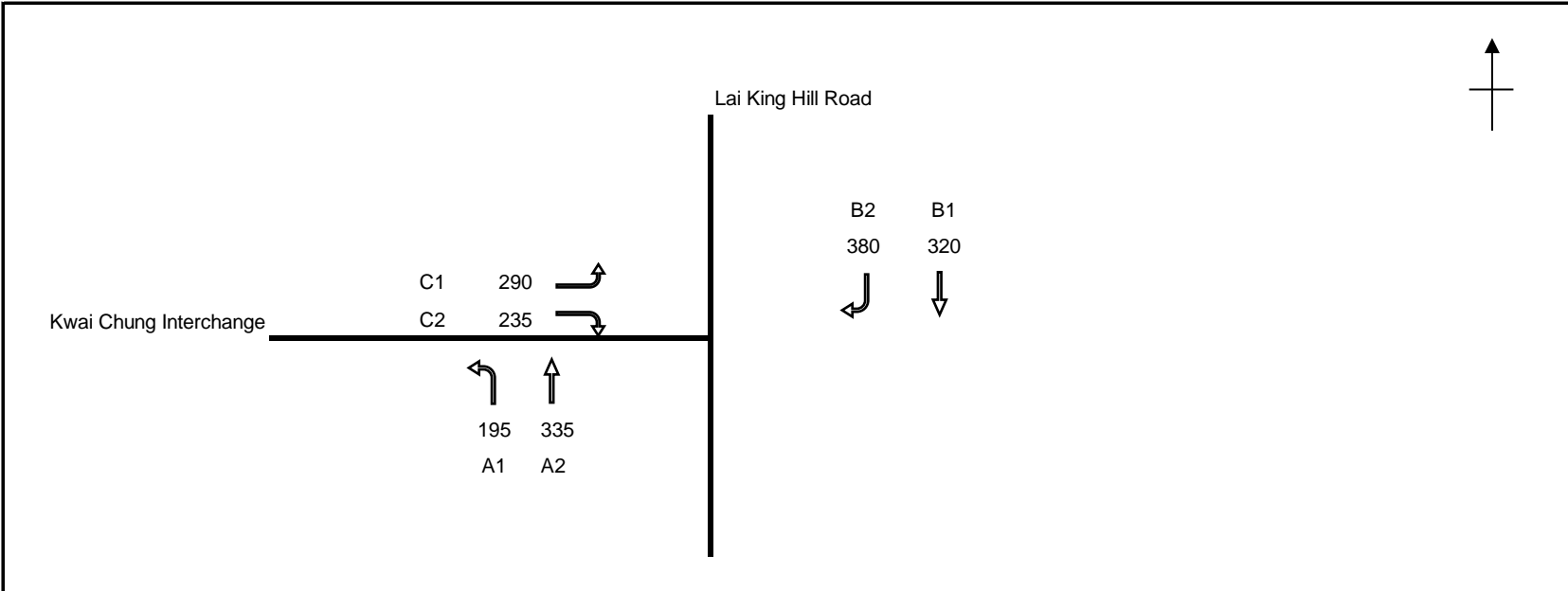

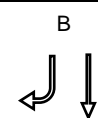
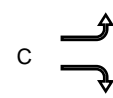

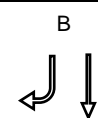
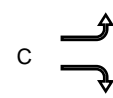

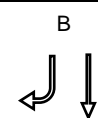
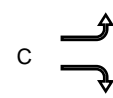
### J3 YEAR 2024 AM TRAFFIC FLOW

#### EXISTING LAYOUT

| OVE ARUP & PARTNERS   |       |               |       |              |           |        | TRAFFIC SIGNAL CALCULATION |                          |   |           |     |  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |  |
|---|-------|---------------|-------|--------------|-----------|--------|----------------------------|--------------------------|---|-----------|-----|--|--------------------------------|--|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|--|
| S16 Application for Proposed Development at Kau Wa Keng   |       |               |       |              |           |        |                            |                          |   |           |     | PROJECT NO:                            |                                | 299277-02                              |                   | Junction No.            |                         | J3    |           |       |                  |               |                        |                   |  |
| Lai King Hill Road / Kwai Chung Interchange   |       |               |       |              |           |        |                            | J3_OBS_AM                |   |           |     | DATE :                                 |                                | 21-Jan-25                              |                   | FILENAME :              |                         |       |           |       |                  |               |                        |                   |  |
| <div><div>No. of stages per cycle<br/>No. of stage using for calculation<br/><br/>Cycle time<br/>Sum(y)<br/>Loss time<br/>Total Flow<br/><br/>Co = (1.5*L+5)/(1-Y)<br/>Cm = L/(1-Y)<br/>Yult =<br/>R.C.ult = (Yult-Y)/Y*100%<br/>Cp = 0.9*L/(0.9-Y)<br/>Ymax = 1-L/C<br/>R.C.(C) = (0.9*Ymax-Y)/Y*100%</div><div>N = 3<br/>N = 3<br/><br/>C = 120 sec<br/>Y = 0.629<br/>L = 12 sec<br/>= 1925 pcu<br/><br/>= 62.0 sec<br/>= 32.4 sec<br/>= 0.810<br/>= 28.8 %<br/>= 39.9 sec<br/>= 0.900<br/>= 29 %</div></div> |       |               |       |              |           |        |                            |                          |   |           |     |  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |  |
| <div>A</div>  |       | <div>B</div>  |       | <div>C</div> |           |        |                            | Pedestrian Phase         |   | Width (m) |     | Green Time Required (s)<br>SG Delay FG |                                | Green Time Provided (s)<br>SG Delay FG |                   | Check                   |                         |       |           |       |                  |               |                        |                   |  |
| STAGE 1   |       | INT= 5        |       | STAGE 2      |           | INT= 5 |                            | STAGE 3                  |   | INT= 5    |     |  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |  |
| Movement  | Stage | Lane Width m. | Phase | No. of lane  | Radius m. | O      | N                          | Straight-Ahead Sat. Flow | Flow<br>Left pcu/h Straight pcu/h Right pcu/h |           |     | Total Flow pcu/h                       | Proportion of Turning Vehicles | Sat. Flow pcu/h                        | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |  |
| A1,A2   | 1     | 3.75          | A     | 1            | 15        |        | N                          | 1990                     | 125   |           |     | 125                                    | 1.00                           | 1809                                   |                   |                         | 1809                    | 0.069 | 0.136     | 12    | 12               | 23            | 0.360                  | 20                |  |
| A2  | 1     | 3.75          | A     | 1            |           |        |                            | 2130                     |   | 290       |     | 290                                    | 0.00                           | 2130                                   |                   |                         | 2130                    | 0.136 |           |       | 23               | 23            | 0.710                  | 47                |  |
| B1  | 2     | 3.30          | B     | 1            |           |        | N                          | 1945                     |   | 325       |     | 325                                    | 0.00                           | 1945                                   |                   |                         | 1945                    | 0.167 | 0.167     |       | 29               | 29            | 0.691                  | 49                |  |
| B2  | 2     | 3.30          | B     | 1            | 20        |        |                            | 2085                     |   |           | 300 | 300                                    | 1.00                           | 1940                                   |                   |                         | 1940                    | 0.155 |           |       | 27               | 29            | 0.640                  | 46                |  |
| C1  | 3     | 3.50          | C     | 1            | 18        |        | N                          | 1965                     | 535   |           |     | 535                                    | 1.00                           | 1814                                   | 4.10%             | -172                    | 1642                    | 0.326 | 0.326     |       | 56               | 56            | 0.698                  | 57                |  |
| C2  | 3     | 3.50          | C     | 1            | 25        |        |                            | 2105                     |   |           | 350 | 350                                    | 1.00                           | 1986                                   | 4.10%             | -172                    | 1814                    | 0.193 |           |       | 33               | 56            | 0.413                  | 37                |  |
| NOTE : 'O' - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE * 6m  |       |               |       |              |           |        |                            |                          |   |           |     |  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |  |

### J3 YEAR 2024 PM TRAFFIC FLOW

#### EXISTING LAYOUT

| OVE ARUP & PARTNERS  |                       |                         |   |             |  |         |        | TRAFFIC SIGNAL CALCULATION |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|--|-----------------------|-------------------------|---|-------------|--|---------|--------|----------------------------|------|--|---------|------------------|---|-----------------|--|-------------------------|-------------------------|-------|-----------|---|------------------|-------------------------|------------------------|-------------------|------------------------------------|-----|---|------------|-----|------------------|-----------|-------------------------|-------|-----------|-------------------------|--------|------------|-------|----------|-------|-------------------|------------|-------|-----------|------------|------|--|---------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |   |             |  |         |        |                            |      | PROJECT NO: 299277-02  |         |                  |   |                 | Junction No. J3  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                         |   |             | J3_OBS_PM  |         |        |                            |      | DATE : 21-Jan-25   |         |                  |   |                 | FILENAME :   |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|    |                       |                         |   |             |  |         |        |                            |      | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.530</td></tr> <tr> <td>Loss time</td><td>L =</td><td>12 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1755 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 48.9 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 25.5 sec</td></tr> <tr> <td>Yult</td><td></td><td>= 0.810</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 52.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 29.2 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.900</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 53 %</td></tr> </table> |         |                  |   |                 |  |                         |                         |       |           |   |                  | No. of stages per cycle | N =                    | 3                 | No. of stage using for calculation | N = | 3 | Cycle time | C = | 120 sec          | Sum(y)    | Y =                     | 0.530 | Loss time | L =                     | 12 sec | Total Flow | =     | 1755 pcu | Co    | = (1.5*L+5)/(1-Y) | = 48.9 sec | Cm    | = L/(1-Y) | = 25.5 sec | Yult |  | = 0.810 | R.C.ult | = (Yult-Y)/Y*100% | = 52.9 % | Cp | = 0.9*L/(0.9-Y) | = 29.2 sec | Ymax | = 1-L/C | = 0.900 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 53 % |
| No. of stages per cycle  | N =                   | 3                       |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| No. of stage using for calculation   | N =                   | 3                       |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Cycle time   | C =                   | 120 sec                 |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Sum(y)   | Y =                   | 0.530                   |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Loss time  | L =                   | 12 sec                  |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Total Flow   | =                     | 1755 pcu                |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Co   | = (1.5*L+5)/(1-Y)     | = 48.9 sec              |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Cm   | = L/(1-Y)             | = 25.5 sec              |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Yult   |                       | = 0.810                 |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 52.9 %                |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Cp   | = 0.9*L/(0.9-Y)       | = 29.2 sec              |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Ymax   | = 1-L/C               | = 0.900                 |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 53 %                  |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| <table> <tr> <td rowspan="2">  </td><td rowspan="2">STAGE 1</td><td rowspan="2">INT= 5</td><td rowspan="3">  </td><td rowspan="3">INT= 5</td><td rowspan="2">  </td><td rowspan="3">STAGE 3</td><td rowspan="3">INT= 5</td><td rowspan="2"></td><td rowspan="2"></td></tr> <tr> </tr> </table> |                       |                         |   |             |  |         |        |                            |      |   | STAGE 1 | INT= 5           |  | INT= 5          |  | STAGE 3                 | INT= 5                  |       |           | <table> <tr> <td rowspan="2">Pedestrian Phase</td><td rowspan="2">Width (m)</td><td colspan="3">Green Time Required (s)</td><td colspan="3">Green Time Provided (s)</td><td rowspan="2">Check</td></tr> <tr> <td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td></tr> </table> |                  |                         |                        |                   |                                    |     |   |            |     | Pedestrian Phase | Width (m) | Green Time Required (s) |       |           | Green Time Provided (s) |        |            | Check | SG       | Delay | FG                | SG         | Delay | FG        |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|   | STAGE 1               | INT= 5                  |  | INT= 5      |  | STAGE 3 | INT= 5 |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|  |                       |                         |   |             |  |         |        |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |   |             | Green Time Provided (s)  |         |        | Check                      |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|  |                       | SG                      | Delay   | FG          | SG   | Delay   | FG     |                            |      |  |         |                  |   |                 |  |                         |                         |       |           |   |                  |                         |                        |                   |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Move-ment  | Stage                 | Lane Width m.           | Phase   | No. of lane | Radius m.  | O       | N      | Straight-Ahead Sat. Flow   | Flow |  |         | Total Flow pcu/h | Proportion of Turning Vehicles  | Sat. Flow pcu/h | Uphill Gradient %  | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec   | g (required) sec | g (input) sec           | Degree of Saturation X | Queuing Length m. |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| A1,A2  | 1                     | 3.75                    | A   | 1           | 15   |         | N      | 1990                       | 195  |  |         | 195              | 1.00  | 1809            |  |                         | 1809                    | 0.108 | 0.157     | 12  | 22               | 32                      | 0.404                  | 29                |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| A2   | 1                     | 3.75                    | A   | 1           |  |         |        | 2130                       |      | 335  |         | 335              | 0.00  | 2130            |  |                         | 2130                    | 0.157 |           |   | 32               | 32                      | 0.590                  | 49                |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| B1   | 2                     | 3.30                    | B   | 1           |  |         | N      | 1945                       |      | 320  |         | 320              | 0.00  | 1945            |  |                         | 1945                    | 0.165 | 0.196     |   | 34               | 40                      | 0.494                  | 43                |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| B2   | 2                     | 3.30                    | B   | 1           | 20   |         |        | 2085                       |      |  | 380     | 380              | 1.00  | 1940            |  |                         | 1940                    | 0.196 |           |   | 40               | 40                      | 0.588                  | 51                |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| C1   | 3                     | 3.50                    | C   | 1           | 18   |         | N      | 1965                       | 290  |  |         | 290              | 1.00  | 1814            | 4.10%  | -172                    | 1642                    | 0.177 | 0.177     |   | 36               | 36                      | 0.589                  | 41                |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| C2   | 3                     | 3.50                    | C   | 1           | 25   |         |        | 2105                       |      |  | 235     | 235              | 1.00  | 1986            | 4.10%  | -172                    | 1814                    | 0.130 |           |   | 26               | 36                      | 0.432                  | 33                |                                    |     |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |       |                   |            |       |           |            |      |  |         |         |                   |          |    |                 |            |      |         |         |         |                       |        |

NOTE : 'O' - OPPOSING TRAFFIC    N - NEAR SIDE LANE    SG - STEADY GREEN    FG - FLASHING GREEN

PEDESTRIAN WALKING SPEED = 0.9m/s    QUEUING LENGTH = AVERAGE QUEUE \* 6m



### J3 YEAR 2035 AM TRAFFIC FLOW BASELINE SCENARIO EXISTING LAYOUT

### J3 YEAR 2035 PM TRAFFIC FLOW

#### BASELINE SCENARIO

#### EXISTING LAYOUT

| OVE ARUP & PARTNERS  |  |             |               |             |             |           |   | TRAFFIC SIGNAL CALCULATION |                          |   |  |   |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |
|--|--|-------------|---------------|-------------|-------------|-----------|---|----------------------------|--------------------------|---|--|---|------------------|--------------------------------|--|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| S16 Application for Proposed Development at Kau Wa Keng  |  |             |               |             |             |           |   |                            |                          |   |  | PROJECT NO: 299277-02   |                  |                                |  | Junction No. J3   |                         |                         |       |           |       |                  |               |                        |                   |
| Lai King Hill Road / Kwai Chung Interchange  |  |             |               |             |             |           |   | J3_BASE_PM                 |                          |   |  | DATE : 21-Jan-25  |                  |                                |  | FILENAME :        |                         |                         |       |           |       |                  |               |                        |                   |
| <div></div>  |  |             |               |             |             |           |   |                            |                          |   |  | <div><div>No. of stages per cycleN = 3</div><div>No. of stage using for calculationN = 3</div><div>Cycle timeC = 120 sec</div><div>Sum(y)Y = 0.556</div><div>Loss timeL = 12 sec</div><div>Total Flow= 1850 pcu</div><div>Co = (1.5*L+5)/(1-Y) = 51.8 sec</div><div>Cm = L/(1-Y) = 27.0 sec</div><div>Yult = 0.810</div><div>R.C.ult = (Yult-Y)/Y*100% = 45.6 %</div><div>Cp = 0.9*L/(0.9-Y) = 31.4 sec</div><div>Ymax = 1-L/C = 0.900</div><div>R.C.(C) = (0.9*Ymax-Y)/Y*100% = 46 %</div></div> |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |
| <div></div>  |  | <div></div> |               | <div></div> |             |           |   | Pedestrian Phase           |                          | Width (m)                                   |  | Green Time Required (s)<br>SG Delay FG  |                  |                                | Green Time Provided (s)<br>SG Delay FG |                   |                         | Check                   |       |           |       |                  |               |                        |                   |
| STAGE 1  |  | INT= 5      |               | STAGE 2     |             | INT= 5    |   | STAGE 3                    |                          | INT= 5                                      |  |   |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |
| Move-ment  |  | Stage       | Lane Width m. | Phase       | No. of lane | Radius m. | O | N                          | Straight-Ahead Sat. Flow | Flow<br>Left pcu/hStraight pcu/hRight pcu/h |  |   | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h                        | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
| A1,A2  |  | 1           | 3.75          | A           | 1           | 15        |   | N                          | 1990                     | 210   |  |   | 210              | 1.00                           | 1809                                   |                   |                         | 1809                    | 0.116 | 0.164     | 12    | 23               | 32            | 0.435                  | 31                |
| A2   |  | 1           | 3.75          | A           | 1           |           |   |                            | 2130                     | 350   |  |   | 350              | 0.00                           | 2130                                   |                   |                         | 2130                    | 0.164 |           |       | 32               | 32            | 0.616                  | 51                |
| B1   |  | 2           | 3.30          | B           | 1           |           |   | N                          | 1945                     | 335   |  |   | 335              | 0.00                           | 1945                                   |                   |                         | 1945                    | 0.172 | 0.206     |       | 33               | 40            | 0.517                  | 45                |
| B2   |  | 2           | 3.30          | B           | 1           | 20        |   |                            | 2085                     |   |  |   | 400              | 400                            | 1.00                                   | 1940              |                         | 1940                    | 0.206 |           |       | 40               | 40            | 0.619                  | 53                |
| C1   |  | 3           | 3.50          | C           | 1           | 18        |   | N                          | 1965                     | 305   |  |   | 305              | 1.00                           | 1814                                   | 4.10%             | -172                    | 1642                    | 0.186 | 0.186     |       | 36               | 36            | 0.619                  | 43                |
| C2   |  | 3           | 3.50          | C           | 1           | 25        |   |                            | 2105                     |   |  |   | 250              | 250                            | 1.00                                   | 1986              | 4.10%                   | -172                    | 1814  | 0.138     |       | 27               | 36            | 0.459                  | 35                |
| NOTE : 'O' - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE * 6m |  |             |               |             |             |           |   |                            |                          |   |  |   |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                   |

### J3 YEAR 2035 AM TRAFFIC FLOW

#### REFERENCE SCENARIO

#### EXISTING LAYOUT

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_REF\_AM

PROJECT NO: 299277-02  
Junction No. J3  
DATE : 21-Jan-25  
FILENAME :

The diagram illustrates the intersection of Lai King Hill Road and Kwai Chung Interchange. Traffic flows from the interchange towards the hill road. Lane configurations include left-turn lanes (A1, C1), through/right-turn lanes (A2, C2), and dedicated right-turn lanes (B1, B2) on the hill road approach. Vehicle counts are provided for each movement.

|                                    |                       |             |
|------------------------------------|-----------------------|-------------|
| No. of stages per cycle            | N =                   | 3           |
| No. of stage using for calculation | N =                   | 3           |
| Cycle time                         | C =                   | 120 sec     |
| Sum(y)                             | Y =                   | 0.790       |
| Loss time                          | L =                   | 12 sec      |
| Total Flow                         | =                     | 2620 pcu    |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 109.6 sec |
| Cm                                 | = L/(1-Y)             | = 57.2 sec  |
| Yult                               |                       | = 0.810     |
| R.C. ult                           | = (Yult-Y)/Y*100%     | = 2.5 %     |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 98.3 sec  |
| Ymax                               | = 1-L/C               | = 0.900     |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 3 %       |

A

B

C

|         |        |         |        |         |        |  |  |
|---------|--------|---------|--------|---------|--------|--|--|
| STAGE 1 | INT= 5 | STAGE 2 | INT= 5 | STAGE 3 | INT= 5 |  |  |
|---------|--------|---------|--------|---------|--------|--|--|

| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow |     |     | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------|-----|-----|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| A1,A2    | 1     | 3.75          | A     | 1           | 15        |   | N | 1990                     | 460  |     |     | 460              | 1.00                           | 1809            |                   |                         | 1809                    | 0.254 | 0.254     | 12    | 35               | 35            | 0.872                  | 65                |
| A2       | 1     | 3.75          | A     | 1           |           |   |   | 2130                     |      | 349 |     | 349              | 0.00                           | 2130            |                   |                         | 2130                    | 0.164 |           |       | 22               | 35            | 0.562                  | 49                |
| B1       | 2     | 3.30          | B     | 1           |           |   | N | 1945                     |      | 373 |     | 373              | 0.00                           | 1945            |                   |                         | 1945                    | 0.192 | 0.192     |       | 26               | 26            | 0.885                  | 58                |
| B2       | 2     | 3.30          | B     | 1           | 20        |   |   | 2085                     |      |     | 315 | 315              | 1.00                           | 1940            |                   |                         | 1940                    | 0.162 |           |       | 22               | 26            | 0.750                  | 49                |
| C1       | 3     | 3.50          | C     | 1           | 18        |   | N | 1965                     | 565  |     |     | 565              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344 | 0.344     |       | 47               | 47            | 0.879                  | 69                |
| C2       | 3     | 3.50          | C     | 1           | 25        |   |   | 2105                     |      |     | 558 | 558              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.308 |           |       | 42               | 47            | 0.785                  | 68                |

NOTE : 'O' - OPPOSING TRAFFIC      N - NEAR SIDE LANE      SG - STEADY GREEN      FG - FLASHING GREEN      PEDESTRIAN WALKING SPEED = 0.9m/s      QUEUING LENGTH = AVERAGE QUEUE \* 6m

### J3 YEAR 2035 PM TRAFFIC FLOW

#### REFERENCE SCENARIO

#### EXISTING LAYOUT

| OVE ARUP & PARTNERS  |  |             |               |             |             |           |   |         |                          | TRAFFIC SIGNAL CALCULATION                  |  |                  |   |                                |  |  |                   |                         |  |       |           |       |                  |               |                        |                   |
|--|--|-------------|---------------|-------------|-------------|-----------|---|---------|--------------------------|---|--|------------------|---|--------------------------------|--|--|-------------------|-------------------------|--|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| S16 Application for Proposed Development at Kau Wa Keng  |  |             |               |             |             |           |   |         |                          |   |  |                  | PROJECT NO: 299277-02   |                                |  |  | Junction No. J3   |                         |  |       |           |       |                  |               |                        |                   |
| Lai King Hill Road / Kwai Chung Interchange  |  |             |               |             | J3_REF_PM   |           |   |         |                          | DATE : 21-Jan-25                            |  |                  |   | FILENAME :                     |  |  |                   |                         |  |       |           |       |                  |               |                        |                   |
| <div></div>  |  |             |               |             |             |           |   |         |                          |   |  |                  | <div><div>No. of stages per cycleN = 3</div><div>No. of stage using for calculationN = 3</div><div>Cycle timeC = 120 sec</div><div>Sum(y)Y = 0.629</div><div>Loss timeL = 12 sec</div><div>Total Flow= 2216 pcu</div><div>Co = (1.5*L+5)/(1-Y) = 62.0 sec</div><div>Cm = L/(1-Y) = 32.3 sec</div><div>Yult = 0.810</div><div>R.C.ult = (Yult-Y)/Y*100% = 28.8 %</div><div>Cp = 0.9*L/(0.9-Y) = 39.9 sec</div><div>Ymax = 1-L/C = 0.900</div><div>R.C.(C) = (0.9*Ymax-Y)/Y*100% = 29 %</div></div> |                                |  |  |                   |                         |  |       |           |       |                  |               |                        |                   |
| <div></div>  |  | <div></div> |               | <div></div> |             |           |   |         |                          |   |  | Pedestrian Phase |   | Width (m)                      |  | Green Time Required (s)<br>SG Delay FG |                   |                         | Green Time Provided (s)<br>SG Delay FG |       |           | Check |                  |               |                        |                   |
| STAGE 1  |  | INT= 5      |               | STAGE 2     |             | INT= 5    |   | STAGE 3 |                          | INT= 5                                      |  |                  |   |                                |  |  |                   |                         |  |       |           |       |                  |               |                        |                   |
| Move-ment  |  | Stage       | Lane Width m. | Phase       | No. of lane | Radius m. | O | N       | Straight-Ahead Sat. Flow | Flow<br>Left pcu/hStraight pcu/hRight pcu/h |  |                  | Total Flow pcu/h  | Proportion of Turning Vehicles |  | Sat. Flow pcu/h                        | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h                | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
| A1,A2  |  | 1           | 3.75          | A           | 1           | 15        |   | N       | 1990                     | 342   |  |                  | 342   | 1.00                           |  | 1809                                   |                   |                         | 1809                                   | 0.189 | 0.189     | 12    | 32               | 32            | 0.709                  | 50                |
| A2   |  | 1           | 3.75          | A           | 1           |           |   |         | 2130                     | 378   |  |                  | 378   | 0.00                           |  | 2130                                   |                   |                         | 2130                                   | 0.177 |           |       | 30               | 32            | 0.665                  | 55                |
| B1   |  | 2           | 3.30          | B           | 1           |           |   | N       | 1945                     | 367   |  |                  | 367   | 0.00                           |  | 1945                                   |                   |                         | 1945                                   | 0.189 | 0.206     |       | 32               | 35            | 0.647                  | 52                |
| B2   |  | 2           | 3.30          | B           | 1           | 20        |   |         | 2085                     | 400   |  |                  | 400   | 1.00                           |  | 1940                                   |                   |                         | 1940                                   | 0.206 |           |       | 35               | 35            | 0.707                  | 57                |
| C1   |  | 3           | 3.50          | C           | 1           | 18        |   | N       | 1965                     | 305   |  |                  | 305   | 1.00                           |  | 1814                                   | 4.10%             | -172                    | 1642                                   | 0.186 | 0.234     |       | 32               | 40            | 0.557                  | 41                |
| C2   |  | 3           | 3.50          | C           | 1           | 25        |   |         | 2105                     | 424   |  |                  | 424   | 1.00                           |  | 1986                                   | 4.10%             | -172                    | 1814                                   | 0.234 |           |       | 40               | 40            | 0.701                  | 57                |
| NOTE : 'O' - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE * 6m |  |             |               |             |             |           |   |         |                          |   |  |                  |   |                                |  |  |                   |                         |  |       |           |       |                  |               |                        |                   |

## EXISTING LAYOUT



## EXISTING LAYOUT

Ove Arup & Partners

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_DES\_PM

PROJECT NO:

299277-02

Junction No.

J3

DATE :

21-Jan-25

FILENAME :

Kwai Chung Interchange

C1     305  
C2     468

A1    378    A2    363

B2     400  
B1     353

Lai King Hill Road

No. of stages per cycle

N =

3

No. of stage using for calculation

N =

3

Cycle time

C =

120 sec

Sum(y)

Y =

0.673

Loss time

L =

12 sec

Total Flow

=

2267 pcu

Co

= (1.5\*L+5)/(1-Y)

=

70.4 sec

Cm

= L/(1-Y)

=

36.7 sec

Yult

=

0.810

R.C. ult

= (Yult-Y)/Y\*100%

=

20.3 %

Cp

= 0.9\*L/(0.9-Y)

=

47.6 sec

Ymax

= 1-L/C

=

0.900

R.C.(C)

= (0.9\*Ymax-Y)/Y\*100%

=

20 %

A

B

C

STAGE 1

INT=

5

STAGE 2

INT=

5

STAGE 3

INT=

5

Pedestrian Phase

Width (m)

Green Time Required (s)

SG Delay FG

Green Time Provided (s)

SG Delay FG

Check

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | <div>FlowLeft pcu/hStraight pcu/hRight pcu/h</div> | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|--|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| A1,A2    | 1     | 3.75          | A     | 1           | 15        |   | N | 1990                     | 378  |                  |                                | 378             |                   | 1.00                    | 1809                    |       |           | 12    | 34               | 34            | 0.737                  | 54                |
| A2       | 1     | 3.75          | A     | 1           |           |   |   | 2130                     |  | 363              | 0.00                           | 2130            |                   |                         | 2130                    | 0.170 |           |       | 27               | 34            | 0.601                  | 52                |
| B1       | 2     | 3.30          | B     | 1           |           |   | N | 1945                     |  | 353              | 0.00                           | 1945            |                   |                         | 1945                    | 0.181 | 0.206     |       | 29               | 33            | 0.660                  | 51                |
| B2       | 2     | 3.30          | B     | 1           | 20        |   |   | 2085                     |  |                  | 1.00                           | 1940            |                   |                         | 1940                    | 0.206 |           |       | 33               | 33            | 0.750                  | 58                |
| C1       | 3     | 3.50          | C     | 1           | 18        |   | N | 1965                     | 305  |                  | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.186 | 0.258     |       | 30               | 41            | 0.544                  | 40                |
| C2       | 3     | 3.50          | C     | 1           | 25        |   |   | 2105                     |  | 468              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.258 |           |       | 41               | 41            | 0.755                  | 62                |

NOTE : 'O' - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m

### J3 YEAR 2035 AM TRAFFIC FLOW INTERIM SCENARIO A EXISTING LAYOUT

|   |  |  |  |  |  |  |  |             |  |                            |  |                  |  |                       |  |  |  |                 |  |
|---|--|--|--|--|--|--|--|-------------|--|----------------------------|--|------------------|--|-----------------------|--|--|--|-----------------|--|
| OVE ARUP & PARTNERS   |  |  |  |  |  |  |  |             |  | TRAFFIC SIGNAL CALCULATION |  |                  |  |                       |  |  |  |                 |  |
| S16 Application for Proposed Development at Kau Wa Keng   |  |  |  |  |  |  |  |             |  |                            |  |                  |  | PROJECT NO: 299277-02 |  |  |  | Junction No. J3 |  |
| Lai King Hill Road / Kwai Chung Interchange   |  |  |  |  |  |  |  | J3_INT_A_AM |  |                            |  | DATE : 21-Jan-25 |  | FILENAME :            |  |  |  |                 |  |
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### J3 YEAR 2035 AM TRAFFIC FLOW

#### INTERIM SCENARIO B

#### EXISTING LAYOUT

[illegible]

### J3 YEAR 2035 PM TRAFFIC FLOW

#### INTERIM SCENARIO B

#### EXISTING LAYOUT

| OVE ARUP & PARTNERS  |                       |                         |       |             |                         |        |    |                          |            | TRAFFIC SIGNAL CALCULATION |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
|--|-----------------------|-------------------------|-------|-------------|-------------------------|--------|----|--------------------------|------------|----------------------------|-------------|------------------|--------------------------------|--|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-----------|-------------------------|------------------------------------|-------------|-------------------------|------------|-----|--------------------------|-------------------|-------|-------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|----|-------------------|------------|------------------|---------------|------------------------|-------------------|------------|----------------|-------------|-------------------|----------|------|-----------------|------------|------|---------|---------|---------|-----------------------|--------|--|-----|------|------|--|--|------|-------|-------|----|----|----|-------|----|----|---|------|---|---|--|--|--|------|--|-----|--|-----|------|------|--|--|------|-------|--|--|----|----|-------|----|----|---|------|---|---|--|--|---|------|--|-----|--|-----|------|------|--|--|------|-------|-------|--|----|----|-------|----|----|---|------|---|---|----|--|--|------|--|--|-----|-----|------|------|--|--|------|-------|--|--|----|----|-------|----|----|---|------|---|---|----|--|---|------|-----|--|--|-----|------|------|-------|------|------|-------|-------|--|----|----|-------|----|----|---|------|---|---|----|--|--|------|--|--|-----|-----|------|------|-------|------|------|-------|--|--|----|----|-------|----|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |       |             |                         |        |    |                          |            | PROJECT NO: 299277-02      |             |                  |                                | Junction No. J3  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                         |       |             | J3_INT_B_PM             |        |    |                          |            | DATE : 21-Jan-25           |             |                  |                                | FILENAME :   |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
|  |                       |                         |       |             |                         |        |    |                          |            |                            |             |                  |                                | <table><tr><td>No. of stages per cycle</td><td>N =</td><td>3</td></tr><tr><td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr><tr><td>Cycle time</td><td>C =</td><td>120 sec</td></tr><tr><td>Sum(y)</td><td>Y =</td><td>0.602</td></tr><tr><td>Loss time</td><td>L =</td><td>12 sec</td></tr><tr><td>Total Flow</td><td>=</td><td>2128 pcu</td></tr><tr><td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 57.8 sec</td></tr><tr><td>Cm</td><td>= L/(1-Y)</td><td>= 30.2 sec</td></tr><tr><td>Yult</td><td>=</td><td>0.810</td></tr><tr><td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 34.6 %</td></tr><tr><td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 36.2 sec</td></tr><tr><td>Ymax</td><td>= 1-L/C</td><td>= 0.900</td></tr><tr><td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 35 %</td></tr></table> |                   |                         |                         |       |           |       |                  |               |                        | No. of stages per cycle | N =       | 3                       | No. of stage using for calculation | N =         | 3                       | Cycle time | C = | 120 sec                  | Sum(y)            | Y =   | 0.602 | Loss time        | L =                            | 12 sec          | Total Flow        | =                       | 2128 pcu                | Co | = (1.5*L+5)/(1-Y) | = 57.8 sec | Cm               | = L/(1-Y)     | = 30.2 sec             | Yult              | =          | 0.810          | R.C.ult     | = (Yult-Y)/Y*100% | = 34.6 % | Cp   | = 0.9*L/(0.9-Y) | = 36.2 sec | Ymax | = 1-L/C | = 0.900 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 35 % |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| No. of stages per cycle  | N =                   | 3                       |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| No. of stage using for calculation   | N =                   | 3                       |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Cycle time   | C =                   | 120 sec                 |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Sum(y)   | Y =                   | 0.602                   |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Loss time  | L =                   | 12 sec                  |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Total Flow   | =                     | 2128 pcu                |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 57.8 sec              |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Cm   | = L/(1-Y)             | = 30.2 sec              |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Yult   | =                     | 0.810                   |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 34.6 %                |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 36.2 sec              |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Ymax   | = 1-L/C               | = 0.900                 |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 35 %                  |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
|  |                       |                         |       |             |                         |        |    |                          |            |                            |             |                  |                                | <table><tr><td rowspan="2">Pedestrian Phase</td><td rowspan="2">Width (m)</td><td colspan="3">Green Time Required (s)</td><td colspan="3">Green Time Provided (s)</td><td rowspan="2">Check</td></tr><tr><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td></tr></table>   |                   |                         |                         |       |           |       |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |             | Green Time Provided (s) |            |     | Check                    | SG                | Delay | FG    | SG               | Delay                          | FG              |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |        |    | Check                    |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
|  |                       | SG                      | Delay | FG          | SG                      | Delay  | FG |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| STAGE 1  |                       | INT= 5                  |       | STAGE 2     |                         | INT= 5 |    | STAGE 3                  |            | INT= 5                     |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| <table><thead><tr><th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr><tr><th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr></thead><tbody><tr><td>A1,A2</td><td>1</td><td>3.75</td><td>A</td><td>1</td><td>15</td><td></td><td>N</td><td>1990</td><td>321</td><td></td><td></td><td>321</td><td>1.00</td><td>1809</td><td></td><td></td><td>1809</td><td>0.177</td><td>0.177</td><td>12</td><td>32</td><td>32</td><td>0.665</td><td>47</td></tr><tr><td>A2</td><td>1</td><td>3.75</td><td>A</td><td>1</td><td></td><td></td><td></td><td>2130</td><td></td><td>359</td><td></td><td>359</td><td>0.00</td><td>2130</td><td></td><td></td><td>2130</td><td>0.169</td><td></td><td></td><td>30</td><td>32</td><td>0.632</td><td>53</td></tr><tr><td>B1</td><td>2</td><td>3.30</td><td>B</td><td>1</td><td></td><td></td><td>N</td><td>1945</td><td></td><td>347</td><td></td><td>347</td><td>0.00</td><td>1945</td><td></td><td></td><td>1945</td><td>0.178</td><td>0.206</td><td></td><td>32</td><td>37</td><td>0.579</td><td>48</td></tr><tr><td>B2</td><td>2</td><td>3.30</td><td>B</td><td>1</td><td>20</td><td></td><td></td><td>2085</td><td></td><td></td><td>400</td><td>400</td><td>1.00</td><td>1940</td><td></td><td></td><td>1940</td><td>0.206</td><td></td><td></td><td>37</td><td>37</td><td>0.669</td><td>55</td></tr><tr><td>C1</td><td>3</td><td>3.50</td><td>C</td><td>1</td><td>18</td><td></td><td>N</td><td>1965</td><td>305</td><td></td><td></td><td>305</td><td>1.00</td><td>1814</td><td>4.10%</td><td>-172</td><td>1642</td><td>0.186</td><td>0.218</td><td></td><td>33</td><td>39</td><td>0.572</td><td>41</td></tr><tr><td>C2</td><td>3</td><td>3.50</td><td>C</td><td>1</td><td>25</td><td></td><td></td><td>2105</td><td></td><td></td><td>396</td><td>396</td><td>1.00</td><td>1986</td><td>4.10%</td><td>-172</td><td>1814</td><td>0.218</td><td></td><td></td><td>39</td><td>39</td><td>0.672</td><td>53</td></tr></tbody></table> |                       |                         |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        | Move-ment               | Stage     | Lane Width m.           | Phase                              | No. of lane | Radius m.               | O          | N   | Straight-Ahead Sat. Flow | Flow              |       |       | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y  | Greater y         | L sec      | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. | Left pcu/h | Straight pcu/h | Right pcu/h | A1,A2             | 1        | 3.75 | A               | 1          | 15   |         | N       | 1990    | 321                   |        |  | 321 | 1.00 | 1809 |  |  | 1809 | 0.177 | 0.177 | 12 | 32 | 32 | 0.665 | 47 | A2 | 1 | 3.75 | A | 1 |  |  |  | 2130 |  | 359 |  | 359 | 0.00 | 2130 |  |  | 2130 | 0.169 |  |  | 30 | 32 | 0.632 | 53 | B1 | 2 | 3.30 | B | 1 |  |  | N | 1945 |  | 347 |  | 347 | 0.00 | 1945 |  |  | 1945 | 0.178 | 0.206 |  | 32 | 37 | 0.579 | 48 | B2 | 2 | 3.30 | B | 1 | 20 |  |  | 2085 |  |  | 400 | 400 | 1.00 | 1940 |  |  | 1940 | 0.206 |  |  | 37 | 37 | 0.669 | 55 | C1 | 3 | 3.50 | C | 1 | 18 |  | N | 1965 | 305 |  |  | 305 | 1.00 | 1814 | 4.10% | -172 | 1642 | 0.186 | 0.218 |  | 33 | 39 | 0.572 | 41 | C2 | 3 | 3.50 | C | 1 | 25 |  |  | 2105 |  |  | 396 | 396 | 1.00 | 1986 | 4.10% | -172 | 1814 | 0.218 |  |  | 39 | 39 | 0.672 | 53 |
| Move-ment  | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O      | N  | Straight-Ahead Sat. Flow | Flow       |                            |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h  | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X |                         |           |                         |                                    |             |                         |            |     |                          | Queuing Length m. |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
|  |                       |                         |       |             |                         |        |    |                          | Left pcu/h | Straight pcu/h             | Right pcu/h |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| A1,A2  | 1                     | 3.75                    | A     | 1           | 15                      |        | N  | 1990                     | 321        |                            |             | 321              | 1.00                           | 1809   |                   |                         | 1809                    | 0.177 | 0.177     | 12    | 32               | 32            | 0.665                  | 47                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| A2   | 1                     | 3.75                    | A     | 1           |                         |        |    | 2130                     |            | 359                        |             | 359              | 0.00                           | 2130   |                   |                         | 2130                    | 0.169 |           |       | 30               | 32            | 0.632                  | 53                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| B1   | 2                     | 3.30                    | B     | 1           |                         |        | N  | 1945                     |            | 347                        |             | 347              | 0.00                           | 1945   |                   |                         | 1945                    | 0.178 | 0.206     |       | 32               | 37            | 0.579                  | 48                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| B2   | 2                     | 3.30                    | B     | 1           | 20                      |        |    | 2085                     |            |                            | 400         | 400              | 1.00                           | 1940   |                   |                         | 1940                    | 0.206 |           |       | 37               | 37            | 0.669                  | 55                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| C1   | 3                     | 3.50                    | C     | 1           | 18                      |        | N  | 1965                     | 305        |                            |             | 305              | 1.00                           | 1814   | 4.10%             | -172                    | 1642                    | 0.186 | 0.218     |       | 33               | 39            | 0.572                  | 41                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| C2   | 3                     | 3.50                    | C     | 1           | 25                      |        |    | 2105                     |            |                            | 396         | 396              | 1.00                           | 1986   | 4.10%             | -172                    | 1814                    | 0.218 |           |       | 39               | 39            | 0.672                  | 53                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |
| NOTE : 'O' - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE * 6m   |                       |                         |       |             |                         |        |    |                          |            |                            |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |  |     |      |      |  |  |      |       |       |    |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |

### J3 YEAR 2035 AM TRAFFIC FLOW

#### INTERIM SCENARIO C

#### EXISTING LAYOUT

| OVE ARUP & PARTNERS  |  |  |  |  |  |  |  | TRAFFIC SIGNAL CALCULATION |  |  |  |                  |                       |  |            |                 |  |  |
|--|--|--|--|--|--|--|--|----------------------------|--|--|--|------------------|-----------------------|--|------------|-----------------|--|--|
| S16 Application for Proposed Development at Kau Wa Keng  |  |  |  |  |  |  |  |                            |  |  |  |                  | PROJECT NO: 299277-02 |  |            | Junction No. J3 |  |  |
| Lai King Hill Road / Kwai Chung Interchange  |  |  |  |  |  |  |  | J3_INT_C_AM                |  |  |  | DATE : 21-Jan-25 |                       |  | FILENAME : |                 |  |  |
| <div><div><div><div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div><div><div></div><div></div></div></div> <div><div></div><div></div></div> <div><div></div><div></div></div> <div><div></div><div></div></div> <div><div></div><div></div></div> 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|  |  |  |  |  |  |                            |  |  |  |                  |                       |  |            |                 |  |  |



### J3 YEAR 2035 PM TRAFFIC FLOW

#### INTERIM SCENARIO C

#### EXISTING LAYOUT

Ove Arup & Partners

Traffic Signal Calculation

|   |  |  |  |  |  |  |  |             |  |                       |  |  |                  |  |                 |  |  |  |  |
|---|--|--|--|--|--|--|--|-------------|--|-----------------------|--|--|------------------|--|-----------------|--|--|--|--|
| S16 Application for Proposed Development at Kau Wa Keng |  |  |  |  |  |  |  |             |  | Project No: 299277-02 |  |  |                  |  | Junction No. J3 |  |  |  |  |
| Lai King Hill Road / Kwai Chung Interchange             |  |  |  |  |  |  |  | J3_INT_C_PM |  |                       |  |  | Date : 21-Jan-25 |  | Filename :      |  |  |  |  |

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|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 3          |
| No. of stage using for calculation | N =                   | 3          |
| Cycle time                         | C =                   | 120 sec    |
| Sum(y)                             | Y =                   | 0.638      |
| Loss time                          | L =                   | 12 sec     |
| Total Flow                         | =                     | 2198 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 63.5 sec |
| Cm                                 | = L/(1-Y)             | = 33.1 sec |
| Yult                               | =                     | 0.810      |
| R.C.ult                            | = (Yult-Y)/Y*100%     | = 27.0 %   |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 41.2 sec |
| Ymax                               | = 1-L/C               | = 0.900    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 27 %     |

|         |        |         |        |                  |           |  |  |  |  |  |  |       |
|---------|--------|---------|--------|------------------|-----------|--|--|--|--|--|--|-------|
|         |        |         |        | Pedestrian Phase | Width (m) | Green Time Required (s)<br>SG Delay FG |  |  | Green Time Provided (s)<br>SG Delay FG |  |  | Check |
|         |        |         |        |                  |           |  |  |  |  |  |  |       |
| STAGE 1 | INT= 5 | STAGE 2 | INT= 5 | STAGE 3          | INT= 5    |  |  |  |  |  |  |       |

| Move-ment | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|-----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|           |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| A1,A2     | 1     | 3.75          | A     | 1           | 15        |   | N | 1990                     | 350        |                |             | 350              | 1.00                           | 1809            |                   |                         | 1809                    | 0.193 | 0.193     | 12    | 33               | 33            | 0.704                  | 51                |
| A2        | 1     | 3.75          | A     | 1           |           |   |   | 2130                     |            | 361            |             | 361              | 0.00                           | 2130            |                   |                         | 2130                    | 0.169 |           |       | 29               | 33            | 0.616                  | 52                |
| B1        | 2     | 3.30          | B     | 1           |           |   | N | 1945                     |            | 350            |             | 350              | 0.00                           | 1945            |                   |                         | 1945                    | 0.180 | 0.206     |       | 30               | 35            | 0.617                  | 50                |
| B2        | 2     | 3.30          | B     | 1           | 20        |   |   | 2085                     |            |                | 400         | 400              | 1.00                           | 1940            |                   |                         | 1940                    | 0.206 |           |       | 35               | 35            | 0.707                  | 57                |
| C1        | 3     | 3.50          | C     | 1           | 18        |   | N | 1965                     | 305        |                |             | 305              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.186 | 0.238     |       | 31               | 40            | 0.557                  | 41                |
| C2        | 3     | 3.50          | C     | 1           | 25        |   |   | 2105                     |            |                | 432         | 432              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.238 |           |       | 40               | 40            | 0.715                  | 58                |

NOTE :    'O' - OPPOSING TRAFFIC       N - NEAR SIDE LANE       SG - STEADY GREEN       FG - FLASHING GREEN       PEDESTRIAN WALKING SPEED = 0.9m/s       QUEUING LENGTH = AVERAGE QUEUE \* 6m



## TD PLANNED JUNCTION ARRANGEMENT

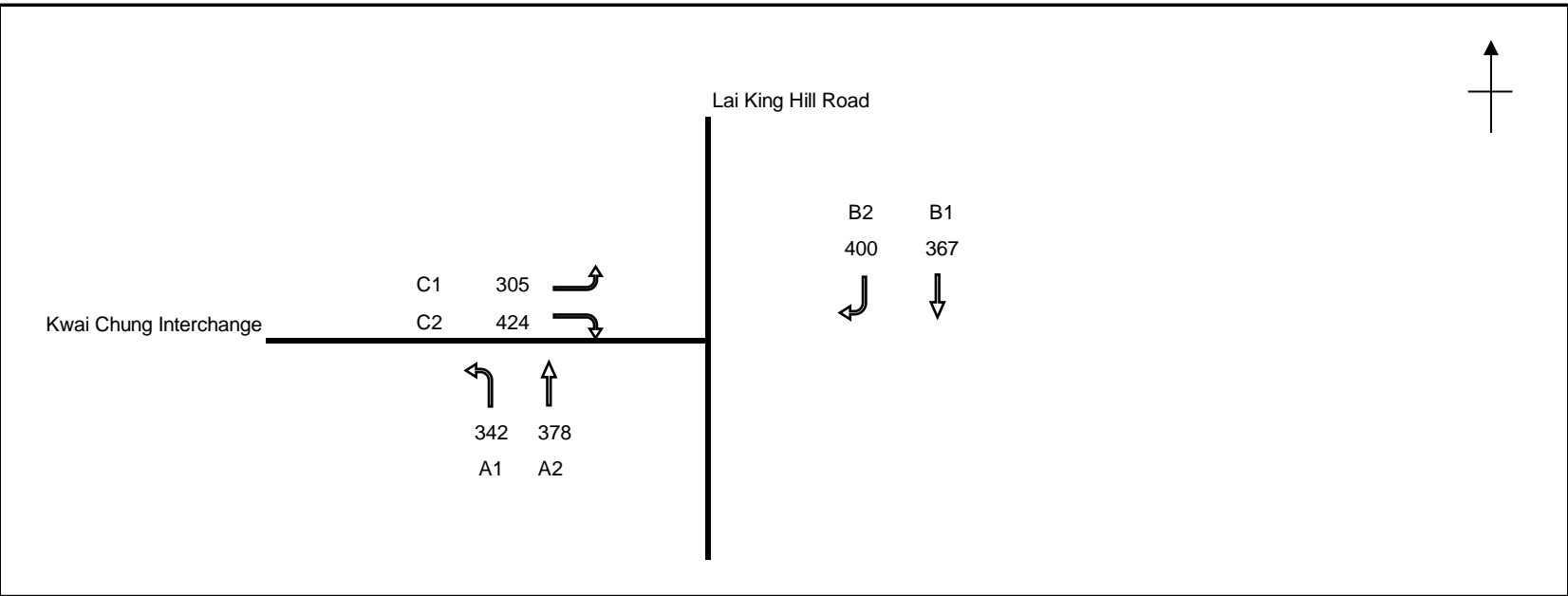
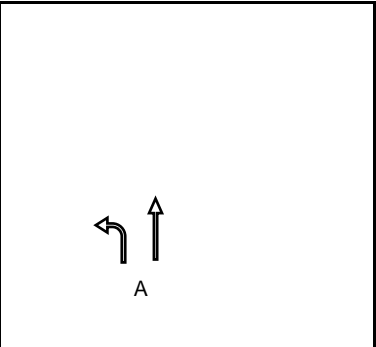
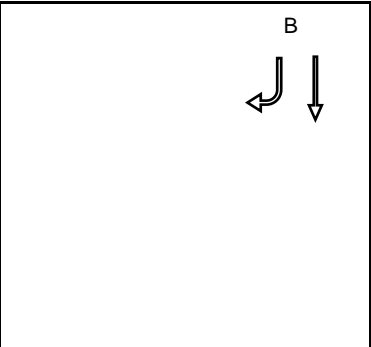
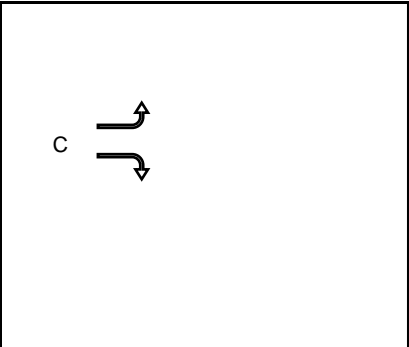
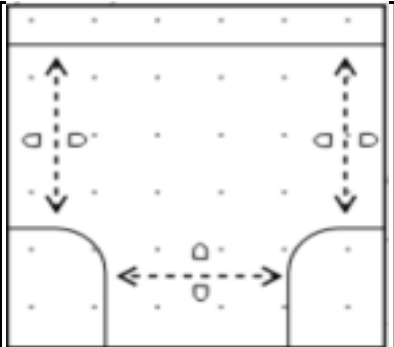
[illegible]

## TD PLANNED JUNCTION ARRANGEMENT

[illegible]

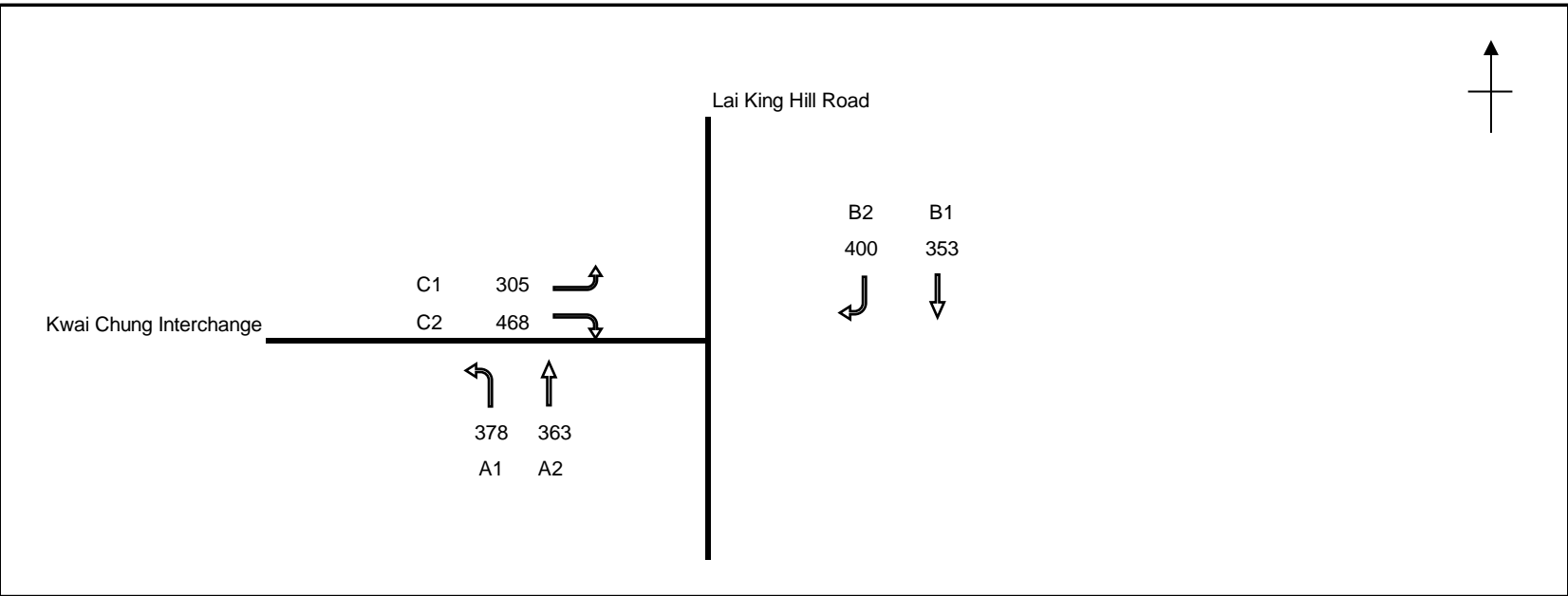
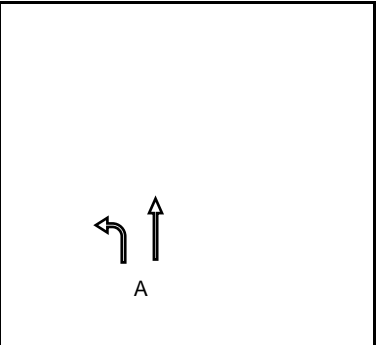
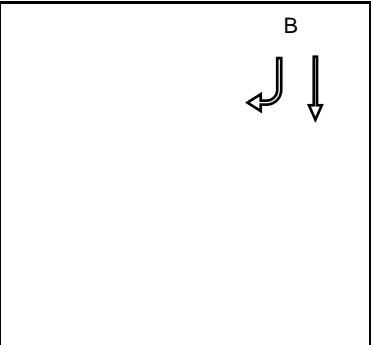
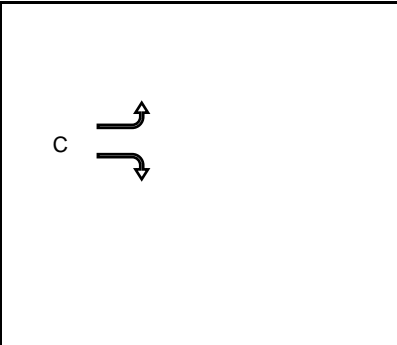
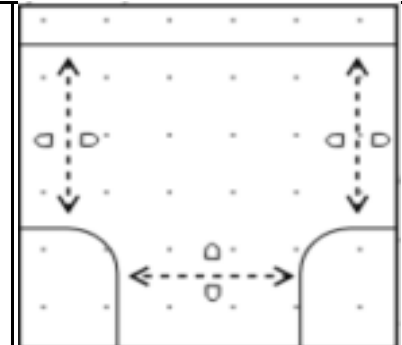


## TD PLANNED JUNCTION ARRANGEMENT

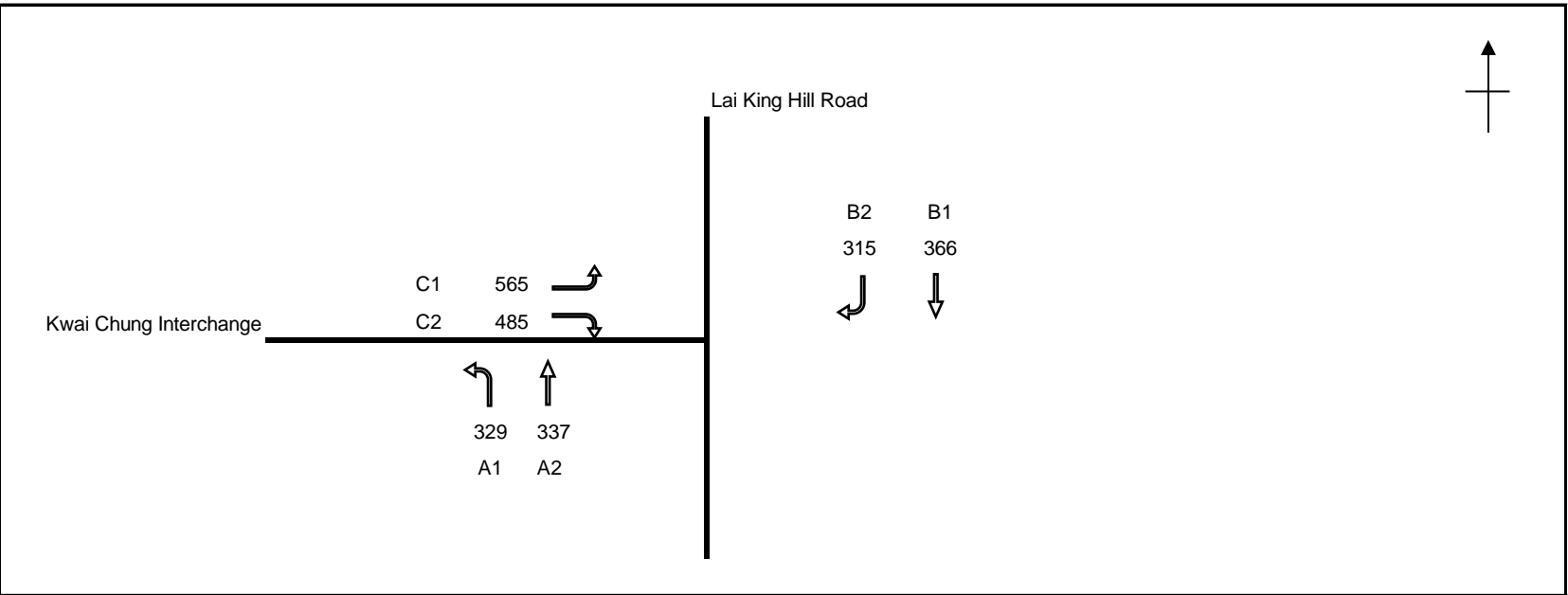
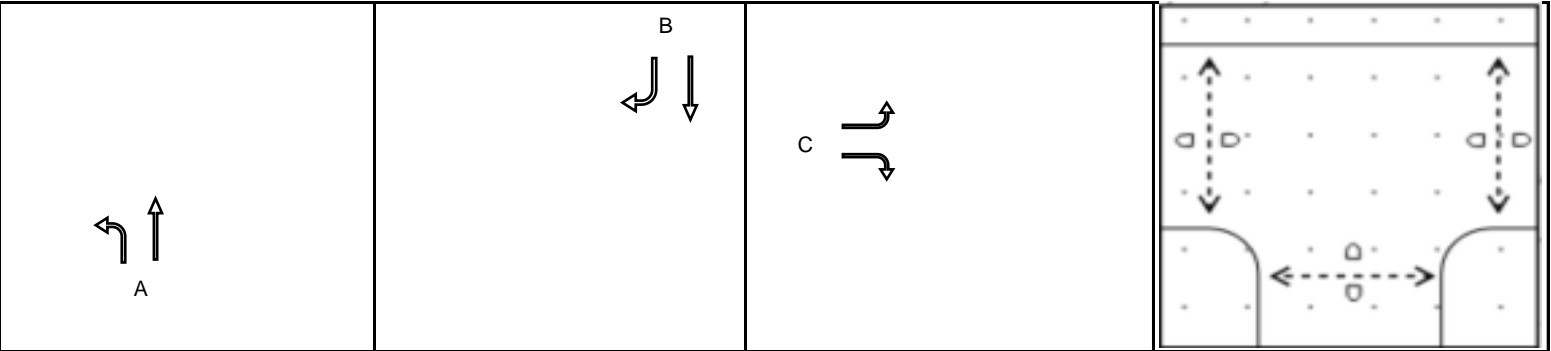
| OVE ARUP & PARTNERS  |                       |   |        |  |                         |  |      | TRAFFIC SIGNAL CALCULATION  |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
|--|-----------------------|---|--------|--|-------------------------|--|------|---|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|--|-------------------------|-------------------------|-----------|-------|-------------------------|---------------|------------------------|-------------------------|-----|------|------------------------------------|-------|----|------------|-------|---------|--------|-----|-------|-----------|-----|--------|------------|---|----------|----|-------------------|-------------|----|-----------|-------------|------|---|-------|---------|-------------------|----------|----|-----------------|-------------|------|---------|---------|---------|-----------------------|--------|
| S16 Application for Proposed Development at Kau Wa Keng                            |                       |   |        |  |                         |  |      | PROJECT NO: 299277-02   |            |                |             |                  |                                |                 |                   | Junction No. J3  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Lai King Hill Road / Kwai Chung Interchange  |                       |   |        | J3_REF_PM_(TD)   |                         |  |      | DATE : 21-Jan-25  |            |                |             | FILENAME :       |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
|  |                       |   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.655</td></tr> <tr> <td>Loss time</td><td>L =</td><td>37 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2216 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 175.2 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 107.1 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.623</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= -4.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 135.7 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.692</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= -5 %</td></tr> </table> |                         |                         |           |       |                         |               |                        | No. of stages per cycle | N = | 3    | No. of stage using for calculation | N =   | 3  | Cycle time | C =   | 120 sec | Sum(y) | Y = | 0.655 | Loss time | L = | 37 sec | Total Flow | = | 2216 pcu | Co | = (1.5*L+5)/(1-Y) | = 175.2 sec | Cm | = L/(1-Y) | = 107.1 sec | Yult | = | 0.623 | R.C.ult | = (Yult-Y)/Y*100% | = -4.9 % | Cp | = 0.9*L/(0.9-Y) | = 135.7 sec | Ymax | = 1-L/C | = 0.692 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = -5 % |
| No. of stages per cycle  | N =                   | 3   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| No. of stage using for calculation   | N =                   | 3   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Cycle time   | C =                   | 120 sec   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Sum(y)   | Y =                   | 0.655   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Loss time  | L =                   | 37 sec  |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Total Flow   | =                     | 2216 pcu  |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Co   | = (1.5*L+5)/(1-Y)     | = 175.2 sec   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Cm   | = L/(1-Y)             | = 107.1 sec   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Yult   | =                     | 0.623   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| R.C.ult  | = (Yult-Y)/Y*100%     | = -4.9 %  |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Cp   | = 0.9*L/(0.9-Y)       | = 135.7 sec   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Ymax   | = 1-L/C               | = 0.692   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = -5 %  |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
|  |                       |  |        |  |                         |  |      | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <td>D</td><td>10.6</td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td><td>OK</td></tr> <tr> <td>F</td><td>11.4</td><td>10</td><td>7</td><td>8</td><td>10</td><td>7</td><td>8</td><td>OK</td></tr> <tr> <td>G</td><td>9.3</td><td>8</td><td>7</td><td>7</td><td>11</td><td>7</td><td>7</td><td>OK</td></tr> </table> |            |                |             |                  |                                |                 |                   | Pedestrian Phase   | Width (m)               | Green Time Required (s) |           |       | Green Time Provided (s) |               |                        | Check                   | D   | 10.6 | SG                                 | Delay | FG | SG         | Delay | FG      | OK     | F   | 11.4  | 10        | 7   | 8      | 10         | 7 | 8        | OK | G                 | 9.3         | 8  | 7         | 7           | 11   | 7 | 7     | OK      |                   |          |    |                 |             |      |         |         |         |                       |        |
| Pedestrian Phase   | Width (m)             | Green Time Required (s)   |        |  | Green Time Provided (s) |  |      | Check   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| D  | 10.6                  | SG  | Delay  | FG   | SG                      | Delay  | FG   | OK  |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| F  | 11.4                  | 10  | 7      | 8  | 10                      | 7  | 8    | OK  |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| G  | 9.3                   | 8   | 7      | 7  | 11                      | 7  | 7    | OK  |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| STAGE 1  | INT= 5                | STAGE 2   | INT= 5 | STAGE 3  | INT= 5                  | STAGE 4  | INT= |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| Move-ment  | Stage                 | Lane Width m.   | Phase  | No. of lane  | Radius m.               | O  | N    | Straight-Ahead Sat. Flow  | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h  | Revised Sat. Flow pcu/h | y                       | Greater y | L sec | g (required) sec        | g (input) sec | Degree of Saturation X | Queuing Length m.       |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
|  |                       |   |        |  |                         |  |      |   | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| A1,A2  | 1                     | 3.75  | A      | 1  | 15                      |  | N    | 1990  | 342        |                |             | 342              | 1.00                           | 1809            |                   |  | 1809                    | 0.189                   | 0.189     | 12    | 24                      | 24            | 0.945                  | 77                      |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| A2   | 1                     | 3.75  | A      | 1  |                         |  | N    | 2130  |            | 378            |             | 378              | 0.00                           | 2130            |                   |  | 2130                    | 0.177                   |           |       | 23                      | 24            | 0.887                  | 60                      |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| B1   | 2                     | 3.30  | B      | 1  |                         |  | N    | 1945  |            | 367            |             | 367              | 0.00                           | 1945            |                   |  | 1945                    | 0.189                   | 0.232     |       | 24                      | 29            | 0.781                  | 56                      |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| B2   | 2                     | 3.30  | B      | 1  | 20                      | O  | N    | 2085  |            |                | 400         | 400              | 1.00                           | 1726            |                   |  | 1726                    | 0.232                   |           |       | 29                      | 29            | 0.959                  | 98                      |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| C1   | 3                     | 3.50  | C      | 1  | 18                      |  | N    | 1965  | 305        |                |             | 305              | 1.00                           | 1814            | 4.10%             | -172   | 1642                    | 0.186                   | 0.234     |       | 24                      | 30            | 0.743                  | 46                      |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
| C2   | 3                     | 3.50  | C      | 1  | 25                      |  | N    | 2105  |            |                | 424         | 424              | 1.00                           | 1986            | 4.10%             | -172   | 1814                    | 0.234                   |           |       | 30                      | 30            | 0.935                  | 73                      |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |
|  |                       |   |        |  |                         |  |      |   |            |                |             |                  |                                |                 |                   |  |                         |                         |           |       |                         |               |                        |                         |     |      |                                    |       |    |            |       |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |          |    |                 |             |      |         |         |         |                       |        |



## TD PLANNED JUNCTION ARRANGEMENT

| OVE ARUP & PARTNERS  |                       |                         |         |                |                         |         |      | TRAFFIC SIGNAL CALCULATION   |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
|--|-----------------------|-------------------------|---------|----------------|-------------------------|---------|------|--|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|--|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|--|-----|---|------------------------------------|---|---|------------|-----|------------------|-----------|-------------------------|-------|-----------|-------------------------|--------|------------|-------|----------|------|-------------------|-------------|----|-----------|-------------|------|----|-------|---------|-------------------|-----------|----|-----------------|-------------|------|---------|---------|---------|-----------------------|---------|---|----|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng                            |                       |                         |         |                |                         |         |      | PROJECT NO: 299277-02  |            |                |             |                  |                                |                 |                   | Junction No. J3  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                         |         | J3_DES_PM_(TD) |                         |         |      | DATE : 21-Jan-25   |            |                |             | FILENAME :       |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
|  |                       |                         |         |                |                         |         |      | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.699</td></tr> <tr> <td>Loss time</td><td>L =</td><td>37 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2267 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 200.8 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 122.8 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.623</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= -10.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 165.5 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.692</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= -11 %</td></tr> </table> |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        | No. of stages per cycle  | N = | 3 | No. of stage using for calculation | N =   | 3 | Cycle time | C = | 120 sec          | Sum(y)    | Y =                     | 0.699 | Loss time | L =                     | 37 sec | Total Flow | =     | 2267 pcu | Co   | = (1.5*L+5)/(1-Y) | = 200.8 sec | Cm | = L/(1-Y) | = 122.8 sec | Yult | =  | 0.623 | R.C.ult | = (Yult-Y)/Y*100% | = -10.9 % | Cp | = 0.9*L/(0.9-Y) | = 165.5 sec | Ymax | = 1-L/C | = 0.692 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = -11 % |   |    |   |   |    |
| No. of stages per cycle  | N =                   | 3                       |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| No. of stage using for calculation   | N =                   | 3                       |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Cycle time   | C =                   | 120 sec                 |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Sum(y)   | Y =                   | 0.699                   |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Loss time  | L =                   | 37 sec                  |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Total Flow   | =                     | 2267 pcu                |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 200.8 sec             |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Cm   | = L/(1-Y)             | = 122.8 sec             |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Yult   | =                     | 0.623                   |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = -10.9 %               |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 165.5 sec             |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Ymax   | = 1-L/C               | = 0.692                 |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = -11 %                 |         |                |                         |         |      |  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
|  |                       |                         |         |                |                         |         |      |   |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <td>D</td><td>10.6</td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td><td>OK</td></tr> <tr> <td>F</td><td>11.4</td><td>10</td><td>7</td><td>8</td><td>10</td><td>7</td><td>8</td><td>OK</td></tr> <tr> <td>G</td><td>9.3</td><td>8</td><td>7</td><td>7</td><td>11</td><td>7</td><td>7</td><td>OK</td></tr> </table> |   |            |     | Pedestrian Phase | Width (m) | Green Time Required (s) |       |           | Green Time Provided (s) |        |            | Check | D        | 10.6 | SG                | Delay       | FG | SG        | Delay       | FG   | OK | F     | 11.4    | 10                | 7         | 8  | 10              | 7           | 8    | OK      | G       | 9.3     | 8                     | 7       | 7 | 11 | 7 | 7 | OK |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |         |                | Green Time Provided (s) |         |      | Check  |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| D  | 10.6                  | SG                      | Delay   | FG             | SG                      | Delay   | FG   | OK   |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| F  | 11.4                  | 10                      | 7       | 8              | 10                      | 7       | 8    | OK   |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| G  | 9.3                   | 8                       | 7       | 7              | 11                      | 7       | 7    | OK   |            |                |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| STAGE 1  | INT=                  | 5                       | STAGE 2 | INT=           | 5                       | STAGE 3 | INT= | 5  | STAGE 4    | INT=           |             |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| Move-ment  | Stage                 | Lane Width m.           | Phase   | No. of lane    | Radius m.               | O       | N    | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h  | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
|  |                       |                         |         |                |                         |         |      |  | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |  |                         |       |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| A1,A2  | 1                     | 3.75                    | A       | 1              | 15                      |         | N    | 1990   | 378        |                |             | 378              | 1.00                           | 1809            |                   |  | 1809                    | 0.209 | 0.209     | 12    | 25               | 25            | 1.003                  | 60   |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| A2   | 1                     | 3.75                    | A       | 1              |                         |         |      | 2130   |            | 363            |             | 363              | 0.00                           | 2130            |                   |  | 2130                    | 0.170 |           |       | 20               | 25            | 0.818                  | 57   |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| B1   | 2                     | 3.30                    | B       | 1              |                         |         | N    | 1945   |            | 353            |             | 353              | 0.00                           | 1945            |                   |  | 1945                    | 0.181 | 0.232     |       | 22               | 28            | 0.778                  | 54   |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| B2   | 2                     | 3.30                    | B       | 1              | 20                      | O       |      | 2085   |            |                | 400         | 400              | 1.00                           | 1726            |                   |  | 1726                    | 0.232 |           |       | 28               | 28            | 0.993                  | 484  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| C1   | 3                     | 3.50                    | C       | 1              | 18                      |         | N    | 1965   | 305        |                |             | 305              | 1.00                           | 1814            | 4.10%             | -172   | 1642                    | 0.186 | 0.258     |       | 22               | 31            | 0.719                  | 45   |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |
| C2   | 3                     | 3.50                    | C       | 1              | 25                      |         |      | 2105   |            |                | 468         | 468              | 1.00                           | 1986            | 4.10%             | -172   | 1814                    | 0.258 |           |       |                  |               |                        |  |     |   |                                    |   |   |            |     |                  |           |                         |       |           |                         |        |            |       |          |      |                   |             |    |           |             |      |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |   |    |   |   |    |

## TD PLANNED JUNCTION ARRANGEMENT

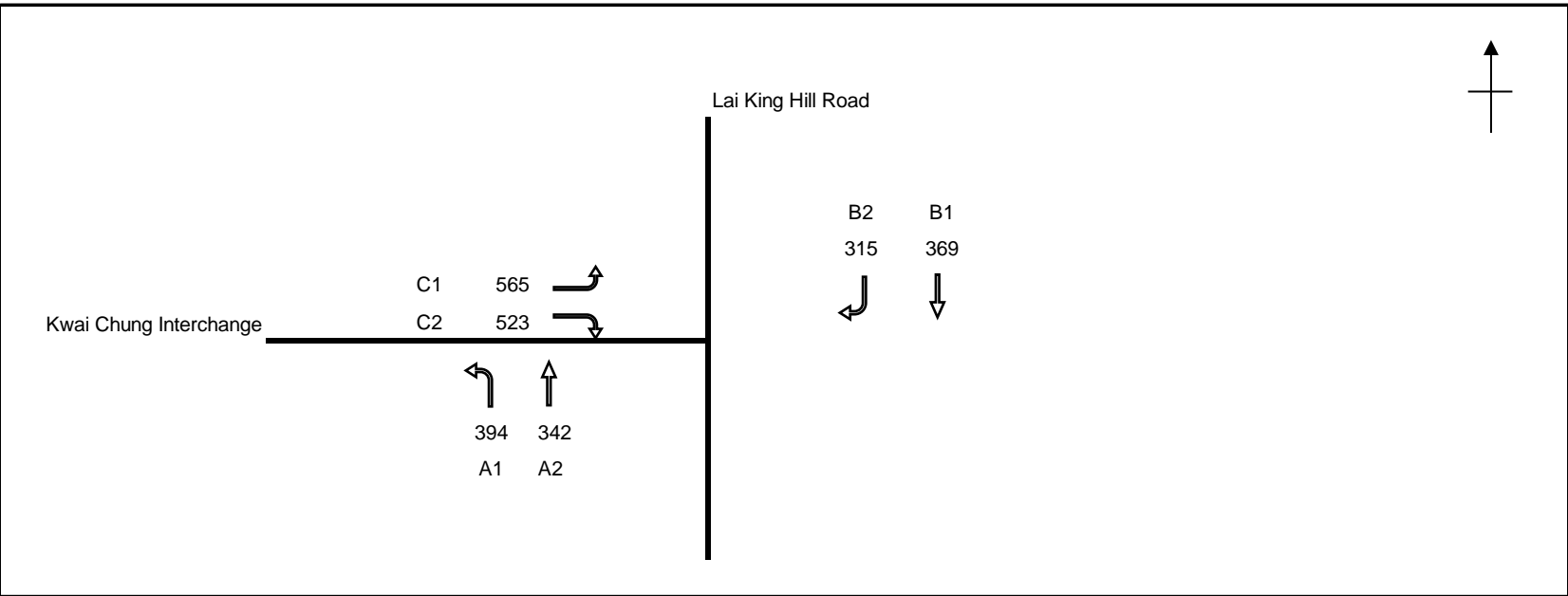
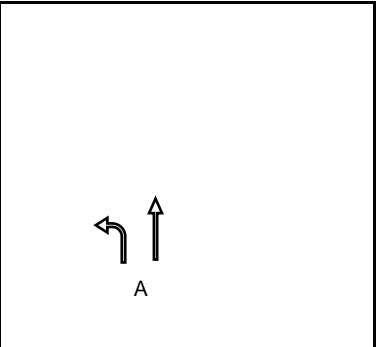
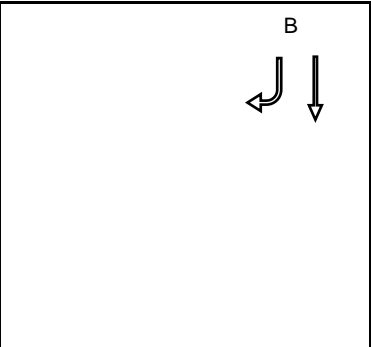
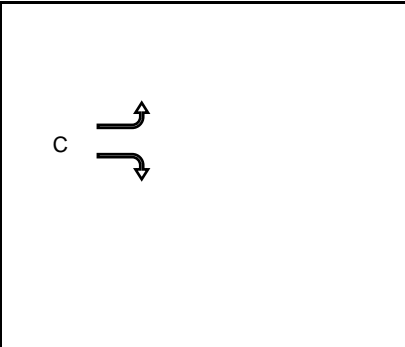
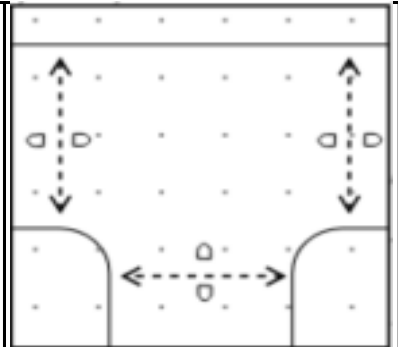
| OVE ARUP & PARTNERS  |                       |                         |         |                  |                         |         |      | TRAFFIC SIGNAL CALCULATION   |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|--|-----------------------|-------------------------|---------|------------------|-------------------------|---------|------|--|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------------------------|-----------|-------|-------------------------|---------------|------------------------|-------------------------|-----|-------|------------------------------------|-----|-------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|---|----------|----|-------------------|-------------|----|-----------|-------------|------|---|-------|---------|-------------------|-----------|----|-----------------|-------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |         |                  |                         |         |      | PROJECT NO: 299277-02  |            |                |             |                  |                                |                 |                   | Junction No. J3         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                         |         | J3_INT_A_AM_(TD) |                         |         |      | DATE : 21-Jan-25   |            |                |             | FILENAME :       |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|    |                       |                         |         |                  |                         |         |      | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.714</td></tr> <tr> <td>Loss time</td><td>L =</td><td>37 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2397 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 211.7 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 129.4 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.623</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= -12.8 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 179.2 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.692</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= -13 %</td></tr> </table> |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        | No. of stages per cycle | N = | 3     | No. of stage using for calculation | N = | 3     | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.714 | Loss time | L = | 37 sec | Total Flow | = | 2397 pcu | Co | = (1.5*L+5)/(1-Y) | = 211.7 sec | Cm | = L/(1-Y) | = 129.4 sec | Yult | = | 0.623 | R.C.ult | = (Yult-Y)/Y*100% | = -12.8 % | Cp | = 0.9*L/(0.9-Y) | = 179.2 sec | Ymax | = 1-L/C | = 0.692 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = -13 % |
| No. of stages per cycle  | N =                   | 3                       |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| No. of stage using for calculation   | N =                   | 3                       |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Cycle time   | C =                   | 120 sec                 |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Sum(y)   | Y =                   | 0.714                   |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Loss time  | L =                   | 37 sec                  |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Total Flow   | =                     | 2397 pcu                |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Co   | = (1.5*L+5)/(1-Y)     | = 211.7 sec             |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Cm   | = L/(1-Y)             | = 129.4 sec             |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Yult   | =                     | 0.623                   |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| R.C.ult  | = (Yult-Y)/Y*100%     | = -12.8 %               |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Cp   | = 0.9*L/(0.9-Y)       | = 179.2 sec             |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Ymax   | = 1-L/C               | = 0.692                 |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = -13 %                 |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|   |                       |                         |         |                  |                         |         |      | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>D</td><td>10.6</td><td>9</td><td>2</td><td>8</td><td>15</td><td>2</td><td>8</td><td>OK</td></tr> <tr> <td>F</td><td>11.4</td><td>10</td><td>7</td><td>8</td><td>10</td><td>7</td><td>8</td><td>OK</td></tr> <tr> <td>G</td><td>9.3</td><td>8</td><td>7</td><td>7</td><td>11</td><td>7</td><td>7</td><td>OK</td></tr> </table>  |            |                |             |                  |                                |                 |                   | Pedestrian Phase        | Width (m)               | Green Time Required (s) |           |       | Green Time Provided (s) |               |                        | Check                   | SG  | Delay | FG                                 | SG  | Delay | FG         | D   | 10.6    | 9      | 2   | 8     | 15        | 2   | 8      | OK         | F | 11.4     | 10 | 7                 | 8           | 10 | 7         | 8           | OK   | G | 9.3   | 8       | 7                 | 7         | 11 | 7               | 7           | OK   |         |         |         |                       |         |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |         |                  | Green Time Provided (s) |         |      | Check  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|  |                       | SG                      | Delay   | FG               | SG                      | Delay   | FG   |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| D  | 10.6                  | 9                       | 2       | 8                | 15                      | 2       | 8    | OK   |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| F  | 11.4                  | 10                      | 7       | 8                | 10                      | 7       | 8    | OK   |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| G  | 9.3                   | 8                       | 7       | 7                | 11                      | 7       | 7    | OK   |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| STAGE 1  | INT=                  | 5                       | STAGE 2 | INT=             | 5                       | STAGE 3 | INT= | 5  | STAGE 4    | INT=           |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Move-ment  | Stage                 | Lane Width m.           | Phase   | No. of lane      | Radius m.               | O       | N    | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y                       | Greater y | L sec | g (required) sec        | g (input) sec | Degree of Saturation X | Queuing Length m.       |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|  |                       |                         |         |                  |                         |         |      |  | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| A1,A2  | 1                     | 3.75                    | A       | 1                | 15                      |         | N    | 1990   | 329        |                |             | 329              | 1.00                           | 1809            |                   |                         | 1809                    | 0.182                   | 0.182     | 12    | 21                      | 21            | 1.039                  | 54                      |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| A2   | 1                     | 3.75                    | A       | 1                |                         |         |      | 2130   |            | 337            |             | 337              | 0.00                           | 2130            |                   |                         | 2130                    | 0.158                   |           |       | 18                      | 21            | 0.904                  | 56                      |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| B1   | 2                     | 3.30                    | B       | 1                |                         |         | N    | 1945   |            | 366            |             | 366              | 0.00                           | 1945            |                   |                         | 1945                    | 0.188                   | 0.188     |       | 22                      | 22            | 1.026                  | 60                      |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| B2   | 2                     | 3.30                    | B       | 1                | 20                      | O       |      | 2085   |            |                | 315         | 315              | 1.00                           | 1726            |                   |                         | 1726                    | 0.183                   |           |       | 21                      | 22            | 0.996                  | 720                     |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| C1   | 3                     | 3.50                    | C       | 1                | 18                      |         | N    | 1965   | 565        |                |             | 565              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344                   | 0.344     |       | 40                      | 40            | 1.032                  | 75                      |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| C2   | 3                     | 3.50                    | C       | 1                | 25                      |         |      | 2105   |            |                | 485         | 485              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.267                   |           |       | 31                      | 40            | 0.802                  | 65                      |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| <div>NOTE : 'O' - OPPOSING TRAFFIC      'N' - NEAR SIDE LANE      SG - STEADY GREEN      FG - FLASHING GREEN      PEDESTRIAN WALKING SPEED = 0.9m/s      QUEUING LENGTH = AVERAGE QUEUE * 6m</div> |                       |                         |         |                  |                         |         |      |  |            |                |             |                  |                                |                 |                   |                         |                         |                         |           |       |                         |               |                        |                         |     |       |                                    |     |       |            |     |         |        |     |       |           |     |        |            |   |          |    |                   |             |    |           |             |      |   |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |

## TD PLANNED JUNCTION ARRANGEMENT

[illegible]



## TD PLANNED JUNCTION ARRANGEMENT

| OVE ARUP & PARTNERS  |                       |   |        |  |                         |  |      | TRAFFIC SIGNAL CALCULATION   |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|--|-----------------------|---|--------|--|-------------------------|--|------|--|------------|------------------|-------------|-------------------------|--------------------------------|-----------------|-------------------------|--|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-----|---|------------------------------------|-----|------|------------|-----|---------|--------|-----|-------|-----------|-----|--------|------------|----|----------|----|-------------------|-------------|----|-----------|-------------|-------|----|-------|---------|-------------------|-----------|----|-----------------|-------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng                            |                       |   |        |  |                         |  |      | PROJECT NO: 299277-02  |            |                  |             |                         |                                |                 |                         | Junction No. J3  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Lai King Hill Road / Kwai Chung Interchange  |                       |   |        | J3_INT_B_AM_(TD)   |                         |  |      | DATE : 21-Jan-25   |            |                  |             | FILENAME :              |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|  |                       |   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.752</td></tr> <tr> <td>Loss time</td><td>L =</td><td>37 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2508 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 243.6 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 149.0 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.623</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= -17.2 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 224.4 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.692</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= -17 %</td></tr> </table> |                         |       |           |       |                  |               |                        | No. of stages per cycle | N = | 3 | No. of stage using for calculation | N = | 3    | Cycle time | C = | 120 sec | Sum(y) | Y = | 0.752 | Loss time | L = | 37 sec | Total Flow | =  | 2508 pcu | Co | = (1.5*L+5)/(1-Y) | = 243.6 sec | Cm | = L/(1-Y) | = 149.0 sec | Yult  | =  | 0.623 | R.C.ult | = (Yult-Y)/Y*100% | = -17.2 % | Cp | = 0.9*L/(0.9-Y) | = 224.4 sec | Ymax | = 1-L/C | = 0.692 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = -17 % |
| No. of stages per cycle  | N =                   | 3   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| No. of stage using for calculation   | N =                   | 3   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Cycle time   | C =                   | 120 sec   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Sum(y)   | Y =                   | 0.752   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Loss time  | L =                   | 37 sec  |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Total Flow   | =                     | 2508 pcu  |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Co   | = (1.5*L+5)/(1-Y)     | = 243.6 sec   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Cm   | = L/(1-Y)             | = 149.0 sec   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Yult   | =                     | 0.623   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| R.C.ult  | = (Yult-Y)/Y*100%     | = -17.2 %   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Cp   | = 0.9*L/(0.9-Y)       | = 224.4 sec   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Ymax   | = 1-L/C               | = 0.692   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = -17 %   |        |  |                         |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|  |                       |  |        |  |                         |  |      | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th><th colspan="3"></th></tr> <tr> <td>D</td><td>10.6</td><td>9 2 8</td><td>15</td><td>2</td><td>8</td><td colspan="3">OK</td></tr> <tr> <td>F</td><td>11.4</td><td>10 7 8</td><td>10</td><td>7</td><td>8</td><td colspan="3">OK</td></tr> <tr> <td>G</td><td>9.3</td><td>8 7 7</td><td>11</td><td>7</td><td>7</td><td colspan="3">OK</td></tr> </table> |            | Pedestrian Phase | Width (m)   | Green Time Required (s) |                                |                 | Green Time Provided (s) |  |                         | Check | SG        | Delay | FG               | SG            | Delay                  | FG                      |     |   |                                    | D   | 10.6 | 9 2 8      | 15  | 2       | 8      | OK  |       |           | F   | 11.4   | 10 7 8     | 10 | 7        | 8  | OK                |             |    | G         | 9.3         | 8 7 7 | 11 | 7     | 7       | OK                |           |    |                 |             |      |         |         |         |                       |         |
| Pedestrian Phase   | Width (m)             | Green Time Required (s)   |        |  | Green Time Provided (s) |  |      | Check  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| SG   | Delay                 | FG  | SG     | Delay  | FG                      |  |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| D  | 10.6                  | 9 2 8   | 15     | 2  | 8                       | OK   |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| F  | 11.4                  | 10 7 8  | 10     | 7  | 8                       | OK   |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| G  | 9.3                   | 8 7 7   | 11     | 7  | 7                       | OK   |      |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| STAGE 1  | INT= 5                | STAGE 2   | INT= 5 | STAGE 3  | INT= 5                  | STAGE 4  | INT= |  |            |                  |             |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| Move-ment  | Stage                 | Lane Width m.   | Phase  | No. of lane  | Radius m.               | O  | N    | Straight-Ahead Sat. Flow   | Flow       |                  |             | Total Flow pcu/h        | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient %       | Short lane Effect pcu/h  | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.       |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
|  |                       |   |        |  |                         |  |      |  | Left pcu/h | Straight pcu/h   | Right pcu/h |                         |                                |                 |                         |  |                         |       |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| A1,A2  | 1                     | 3.75  | A      | 1  | 15                      |  | N    | 1990   | 394        |                  |             | 394                     | 1.00                           | 1809            |                         |  | 1809                    | 0.218 | 0.218     | 12    | 24               | 24            | 1.089                  | 63                      |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| A2   | 1                     | 3.75  | A      | 1  |                         |  |      | 2130   |            | 342              |             | 342                     | 0.00                           | 2130            |                         |  | 2130                    | 0.161 |           |       | 18               | 24            | 0.803                  | 55                      |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| B1   | 2                     | 3.30  | B      | 1  |                         |  | N    | 1945   |            | 369              |             | 369                     | 0.00                           | 1945            |                         |  | 1945                    | 0.190 | 0.190     |       | 21               | 21            | 1.084                  | 61                      |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| B2   | 2                     | 3.30  | B      | 1  | 20                      | O  |      | 2085   |            |                  | 315         | 315                     | 1.00                           | 1726            |                         |  | 1726                    | 0.183 |           |       | 20               | 21            | 1.043                  | 52                      |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| C1   | 3                     | 3.50  | C      | 1  | 18                      |  | N    | 1965   | 565        |                  |             | 565                     | 1.00                           | 1814            | 4.10%                   | -172   | 1642                    | 0.344 | 0.344     |       | 38               | 38            | 1.087                  | 77                      |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |
| C2   | 3                     | 3.50  | C      | 1  | 25                      |  |      | 2105   |            |                  | 523         | 523                     | 1.00                           | 1986            | 4.10%                   | -172   | 1814                    | 0.2   |           |       |                  |               |                        |                         |     |   |                                    |     |      |            |     |         |        |     |       |           |     |        |            |    |          |    |                   |             |    |           |             |       |    |       |         |                   |           |    |                 |             |      |         |         |         |                       |         |

## TD PLANNED JUNCTION ARRANGEMENT

[illegible]



## TD PLANNED JUNCTION ARRANGEMENT

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_INT\_C\_PM\_(TD)

PROJECT NO:  
DATE :

299277-02  
21-Jan-25

Junction No.  
FILENAME :

J3

No. of stages per cycle  
No. of stage using for calculation

N =  
N =

3  
3

Cycle time  
Sum(y)  
Loss time  
Total Flow

C =  
Y =  
L =  
=

120 sec  
0.663  
37 sec  
2198 pcu

Co      = (1.5\*L+5)/(1-Y)                 =  
Cm      = L/(1-Y)                          =  
Yult   =  
R.C. ult   = (Yult-Y)/Y\*100%                =  
Cp      = 0.9\*L/(0.9-Y)                    =  
Ymax      = 1-L/C                             =  
  
R.C.(C)   = (0.9\*Ymax-Y)/Y\*100%          =

=  
=  
=  
=  
=  
=  
=-6 %

A

B

C

D

E

F

G

H

I

J

K

L

M

N

O

P

Q

R

S

T

U

V

W

X

Y

Z

[Diagram showing traffic flow directions and lane configurations]

| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |
| D                | 10.6      | 9                       | 2     | 8  | 15                      | 2     | 8  | OK    |
| F                | 11.4      | 10                      | 7     | 8  | 10                      | 7     | 8  | OK    |
| G                | 9.3       | 8                       | 7     | 7  | 11                      | 7     | 7  | OK    |

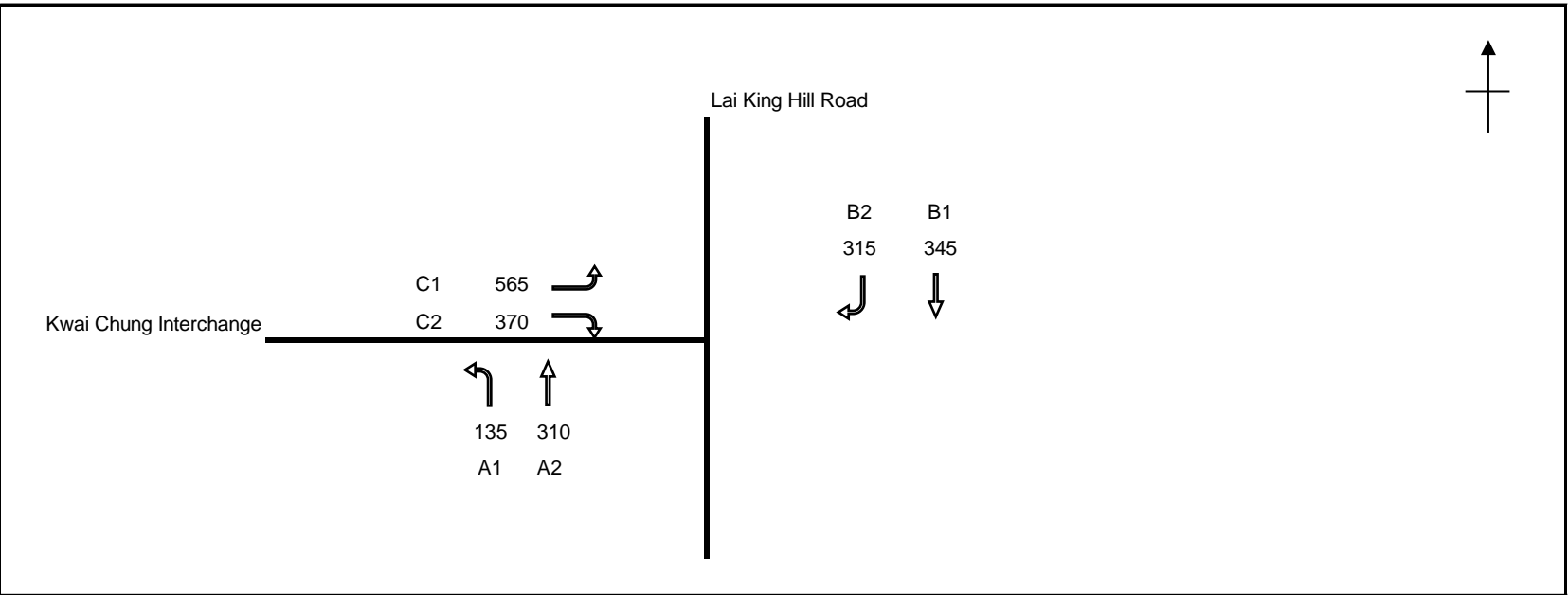
| Move-ment | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|-----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|           |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| A1,A2     | 1     | 3.75          | A     | 1           | 15        |   | N | 1990                     | 350        |                |             | 350              | 1.00                           | 1809            |                   |                         | 1809                    | 0.193 | 0.193     | 12    | 24               | 24            | 0.967                  | 115               |
| A2        | 1     | 3.75          | A     | 1           |           |   | N | 2130                     |            | 361            |             | 361              | 0.00                           | 2130            |                   |                         | 2130                    | 0.169 |           |       | 21               | 24            | 0.847                  | 58                |
| B1        | 2     | 3.30          | B     | 1           |           |   | N | 1945                     |            | 350            |             | 350              | 0.00                           | 1945            |                   |                         | 1945                    | 0.180 | 0.232     |       | 23               | 29            | 0.745                  | 53                |
| B2        | 2     | 3.30          | B     | 1           | 20        | O | N | 2085                     |            |                | 400         | 400              | 1.00                           | 1726            |                   |                         | 1726                    | 0.232 |           |       | 29               | 29            | 0.959                  | 98                |
| C1        | 3     | 3.50          | C     | 1           | 18        |   | N | 1965                     | 305        |                |             | 305              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.186 | 0.238     |       | 23               | 30            | 0.743                  | 46                |
| C2        | 3     | 3.50          | C     | 1           | 25        |   |   | 2105                     |            |                | 432         | 432              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.238 |           | 25    | 30               | 30            | 0.953                  | 91                |

NOTE :   'O - OPPOSING TRAFFIC       N - NEAR SIDE LANE       SG - STEADY GREEN       FG - FLASHING GREEN

PEDESTRIAN WALKING SPEED = 0.9m/s

QUEUING LENGTH = AVERAGE QUEUE \* 6m

## PROPOSED JUNCTION IMPROVEMENT

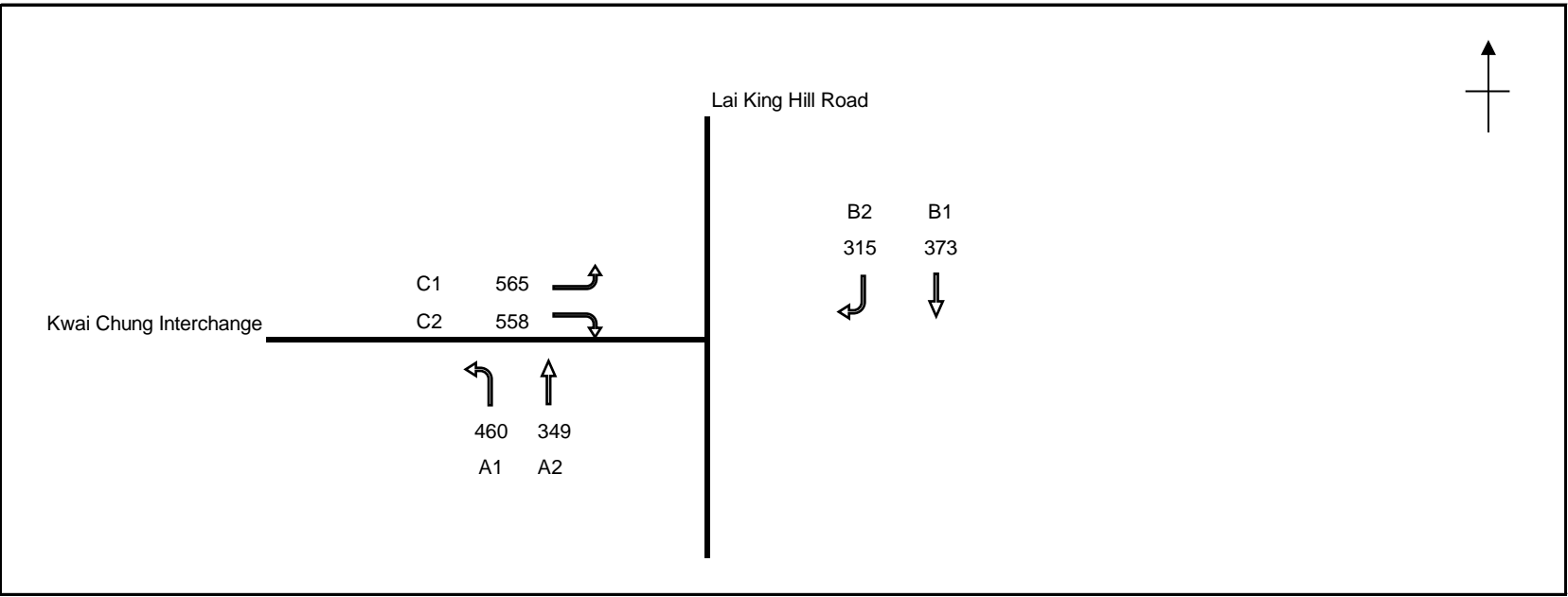
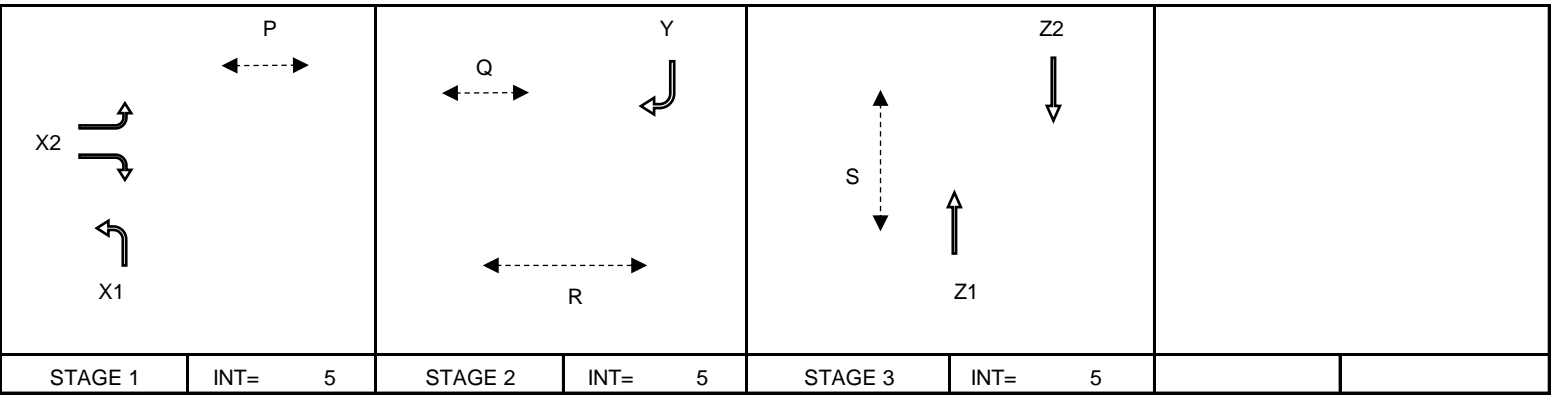
| OVE ARUP & PARTNERS  |                       |            |    |                |    |        |   | TRAFFIC SIGNAL CALCULATION |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|--|-----------------------|------------|----|----------------|----|--------|---|----------------------------|----|-----------|---|------------|---|----|---|---|----|------|----|------------------|---|--------------------------------|----|-------------------------|-----|-------------------|------------------------------------|-------------------------|----|-------------------------|-----|---------|--------|-----------|-------|-----------|-----|------------------|------------|---------------|----------|------------------------|-------------------|-------------------|----|-----------|------------|------|---|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |            |    |                |    |        |   | PROJECT NO: 299277-02      |    |           |   |            |   |    |   | Junction No. J3   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Lai King Hill Road / Kwai Chung Interchange  |                       |            |    | J3_BASE_IMP_AM |    |        |   | DATE : 21-Jan-25           |    |           |   | FILENAME : |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|    |                       |            |    |                |    |        |   |                            |    |           |   |            |   |    |   | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.684</td></tr> <tr> <td>Loss time</td><td>L =</td><td>12 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2040 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 72.8 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 38.0 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.810</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 18.4 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 50.0 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.900</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 18 %</td></tr> </table> |    |      |    |                  |   |                                |    | No. of stages per cycle | N = | 3                 | No. of stage using for calculation | N =                     | 3  | Cycle time              | C = | 120 sec | Sum(y) | Y =       | 0.684 | Loss time | L = | 12 sec           | Total Flow | =             | 2040 pcu | Co                     | = (1.5*L+5)/(1-Y) | = 72.8 sec        | Cm | = L/(1-Y) | = 38.0 sec | Yult | = | 0.810 | R.C.ult | = (Yult-Y)/Y*100% | = 18.4 % | Cp | = 0.9*L/(0.9-Y) | = 50.0 sec | Ymax | = 1-L/C | = 0.900 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 18 % |
| No. of stages per cycle  | N =                   | 3          |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| No. of stage using for calculation   | N =                   | 3          |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Cycle time   | C =                   | 120 sec    |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Sum(y)   | Y =                   | 0.684      |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Loss time  | L =                   | 12 sec     |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Total Flow   | =                     | 2040 pcu   |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Co   | = (1.5*L+5)/(1-Y)     | = 72.8 sec |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Cm   | = L/(1-Y)             | = 38.0 sec |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Yult   | =                     | 0.810      |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 18.4 %   |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Cp   | = 0.9*L/(0.9-Y)       | = 50.0 sec |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Ymax   | = 1-L/C               | = 0.900    |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 18 %     |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| <table> <tr> <td rowspan="5">Pedestrian Phase</td><td>P</td><td>5</td><td>6</td><td>1</td><td>5</td><td>52</td><td>1</td><td>5</td><td>OK</td></tr> <tr> <td>Q</td><td>10</td><td>6</td><td>2</td><td>11</td><td>17</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>R</td><td>12</td><td>13</td><td>5</td><td>12</td><td>13</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>S</td><td>11</td><td>12</td><td>5</td><td>11</td><td>16</td><td>5</td><td>11</td><td>OK</td></tr> <tr> <td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr> </table> |                       |            |    |                |    |        |   | Pedestrian Phase           | P  | 5         | 6 | 1          | 5 | 52 | 1 | 5   | OK | Q    | 10 | 6                | 2 | 11                             | 17 | 2                       | 11  | OK                | R                                  | 12                      | 13 | 5                       | 12  | 13      | 5      | 12        | OK    | S         | 11  | 12               | 5          | 11            | 16       | 5                      | 11                | OK                |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Pedestrian Phase   | P                     | 5          | 6  | 1              | 5  | 52     | 1 |                            | 5  | OK        |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|  | Q                     | 10         | 6  | 2              | 11 | 17     | 2 |                            | 11 | OK        |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|  | R                     | 12         | 13 | 5              | 12 | 13     | 5 |                            | 12 | OK        |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|  | S                     | 11         | 12 | 5              | 11 | 16     | 5 |                            | 11 | OK        |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
|  |                       |            |    |                |    |        |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| STAGE 1  |                       | INT= 5     |    | STAGE 2        |    | INT= 5 |   | STAGE 3                    |    | INT= 5    |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| Move-ment  |                       | Stage      |    | Lane Width m.  |    | Phase  |   | No. of lane                |    | Radius m. |   | O          |   | N  |   | Straight-Ahead Sat. Flow  |    | Flow |    | Total Flow pcu/h |   | Proportion of Turning Vehicles |    | Sat. Flow pcu/h         |     | Uphill Gradient % |                                    | Short lane Effect pcu/h |    | Revised Sat. Flow pcu/h |     | y       |        | Greater y |       | L sec     |     | g (required) sec |            | g (input) sec |          | Degree of Saturation X |                   | Queuing Length m. |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| A1   |                       | 1          |    | 3.75           |    | X1     |   | 1                          |    | 15        |   |            |   | N  |   | 1990  |    | 135  |    | 135              |   | 1.00                           |    | 1809                    |     |                   |                                    | 1809                    |    | 0.075                   |     |         |        | 12        |       | 12        |     | 54               |            | 0.166         |          | 15                     |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| C1   |                       | 1          |    | 3.50           |    | X2     |   | 1                          |    | 18        |   |            |   | N  |   | 1965  |    | 565  |    | 565              |   | 1.00                           |    | 1814                    |     | 4.10%             |                                    | -172                    |    | 1642                    |     | 0.344   |        | 0.344     |       | 54        |     | 54               |            | 0.765         |          | 62                     |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |
| C2   |                       | 1          |    | 3.50           |    | X2     |   |                            |    |           |   |            |   |    |   |   |    |      |    |                  |   |                                |    |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |



## PROPOSED JUNCTION IMPROVEMENT

[illegible]

## PROPOSED JUNCTION IMPROVEMENT

| OVE ARUP & PARTNERS  |                       |                         |       |               |                         |       |    | TRAFFIC SIGNAL CALCULATION |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
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| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |       |               |                         |       |    |                            |            |                |             | PROJECT NO: 299277-02   |                                |                 |                   | Junction No. J3         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                         |       | J3_REF_IMP_AM |                         |       |    | DATE : 21-Jan-25           |            |                |             | FILENAME :  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
|    |                       |                         |       |               |                         |       |    |                            |            |                |             | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.698</td></tr> <tr> <td>Loss time</td><td>L =</td><td>13 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2620 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 81.2 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 43.1 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.803</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 14.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 58.0 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.892</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 15 %</td></tr> </table> |                                |                 |                   |                         |                         |       |           |       |                  |               |                        | No. of stages per cycle | N =       | 3                       | No. of stage using for calculation | N =         | 3                       | Cycle time | C = | 120 sec                  | Sum(y)            | Y =   | 0.698 | Loss time        | L =                            | 13 sec          | Total Flow        | =                       | 2620 pcu                | Co | = (1.5*L+5)/(1-Y) | = 81.2 sec | Cm               | = L/(1-Y)     | = 43.1 sec             | Yult              | =          | 0.803          | R.C.ult     | = (Yult-Y)/Y*100% | = 14.9 % | Cp   | = 0.9*L/(0.9-Y) | = 58.0 sec | Ymax | = 1-L/C | = 0.892 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 15 % |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| No. of stages per cycle  | N =                   | 3                       |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| No. of stage using for calculation   | N =                   | 3                       |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Cycle time   | C =                   | 120 sec                 |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Sum(y)   | Y =                   | 0.698                   |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Loss time  | L =                   | 13 sec                  |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Total Flow   | =                     | 2620 pcu                |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 81.2 sec              |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Cm   | = L/(1-Y)             | = 43.1 sec              |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Yult   | =                     | 0.803                   |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 14.9 %                |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 58.0 sec              |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Ymax   | = 1-L/C               | = 0.892                 |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 15 %                  |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
|   |                       |                         |       |               |                         |       |    |                            |            |                |             | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>P</td><td>5</td><td>6</td><td>1</td><td>5</td><td>51</td><td>1</td><td>5</td><td>OK</td></tr> <tr> <td>Q</td><td>10</td><td>6</td><td>2</td><td>11</td><td>17</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>R</td><td>12</td><td>13</td><td>5</td><td>12</td><td>13</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>S</td><td>11</td><td>12</td><td>5</td><td>11</td><td>17</td><td>5</td><td>11</td><td>OK</td></tr> </table>  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |             | Green Time Provided (s) |            |     | Check                    | SG                | Delay | FG    | SG               | Delay                          | FG              | P                 | 5                       | 6                       | 1  | 5                 | 51         | 1                | 5             | OK                     | Q                 | 10         | 6              | 2           | 11                | 17       | 2    | 11              | OK         | R    | 12      | 13      | 5       | 12                    | 13     | 5 | 12  | OK   | S    | 11 | 12 | 5    | 11    | 17 | 5  | 11 | OK |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |       |               | Green Time Provided (s) |       |    | Check                      |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
|  |                       | SG                      | Delay | FG            | SG                      | Delay | FG |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| P  | 5                     | 6                       | 1     | 5             | 51                      | 1     | 5  | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| Q  | 10                    | 6                       | 2     | 11            | 17                      | 2     | 11 | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| R  | 12                    | 13                      | 5     | 12            | 13                      | 5     | 12 | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| S  | 11                    | 12                      | 5     | 11            | 17                      | 5     | 11 | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| <table> <tr> <th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr> <tr> <th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr> <tr> <td>A1</td><td>1</td><td>3.75</td><td>X1</td><td>1</td><td>15</td><td></td><td>N</td><td>1990</td><td>460</td><td></td><td></td><td>460</td><td>1.00</td><td>1809</td><td></td><td></td><td>1809</td><td>0.254</td><td></td><td>12</td><td>39</td><td>53</td><td>0.576</td><td>51</td></tr> <tr> <td>C1</td><td>1</td><td>3.50</td><td>X2</td><td>1</td><td>18</td><td></td><td>N</td><td>1965</td><td>565</td><td></td><td></td><td>565</td><td>1.00</td><td>1814</td><td>4.10%</td><td>-172</td><td>1642</td><td>0.344</td><td>0.344</td><td></td><td>53</td><td>53</td><td>0.779</td><td>63</td></tr> <tr> <td>C2</td><td>1</td><td>3.50</td><td>X2</td><td>1</td><td>25</td><td></td><td></td><td>2105</td><td></td><td></td><td>558</td><td>558</td><td>1.00</td><td>1986</td><td>4.10%</td><td>-172</td><td>1814</td><td>0.308</td><td></td><td></td><td>47</td><td>53</td><td>0.697</td><td>62</td></tr> <tr> <td>A2</td><td>3</td><td>3.75</td><td>Z1</td><td>1</td><td></td><td></td><td></td><td>2130</td><td></td><td>349</td><td></td><td>349</td><td>0.00</td><td>2130</td><td></td><td></td><td>2130</td><td>0.164</td><td></td><td></td><td>25</td><td>29</td><td>0.678</td><td>53</td></tr> <tr> <td>B1</td><td>3</td><td>3.30</td><td>Z2</td><td>1</td><td></td><td></td><td>N</td><td>1945</td><td></td><td>373</td><td></td><td>373</td><td>0.00</td><td>1945</td><td></td><td></td><td>1945</td><td>0.192</td><td>0.192</td><td></td><td>29</td><td>29</td><td>0.794</td><td>57</td></tr> <tr> <td>B2</td><td>2</td><td>3.30</td><td>Y</td><td>1</td><td>20</td><td></td><td></td><td>2085</td><td></td><td></td><td>315</td><td>315</td><td>1.00</td><td>1940</td><td></td><td></td><td>1940</td><td>0.162</td><td>0.162</td><td>1</td><td>25</td><td>26</td><td>0.750</td><td>49</td></tr> </table> |                       |                         |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        | Move-ment               | Stage     | Lane Width m.           | Phase                              | No. of lane | Radius m.               | O          | N   | Straight-Ahead Sat. Flow | Flow              |       |       | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y  | Greater y         | L sec      | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. | Left pcu/h | Straight pcu/h | Right pcu/h | A1                | 1        | 3.75 | X1              | 1          | 15   |         | N       | 1990    | 460                   |        |   | 460 | 1.00 | 1809 |    |    | 1809 | 0.254 |    | 12 | 39 | 53 | 0.576 | 51 | C1 | 1 | 3.50 | X2 | 1 | 18 |  | N | 1965 | 565 |  |  | 565 | 1.00 | 1814 | 4.10% | -172 | 1642 | 0.344 | 0.344 |  | 53 | 53 | 0.779 | 63 | C2 | 1 | 3.50 | X2 | 1 | 25 |  |  | 2105 |  |  | 558 | 558 | 1.00 | 1986 | 4.10% | -172 | 1814 | 0.308 |  |  | 47 | 53 | 0.697 | 62 | A2 | 3 | 3.75 | Z1 | 1 |  |  |  | 2130 |  | 349 |  | 349 | 0.00 | 2130 |  |  | 2130 | 0.164 |  |  | 25 | 29 | 0.678 | 53 | B1 | 3 | 3.30 | Z2 | 1 |  |  | N | 1945 |  | 373 |  | 373 | 0.00 | 1945 |  |  | 1945 | 0.192 | 0.192 |  | 29 | 29 | 0.794 | 57 | B2 | 2 | 3.30 | Y | 1 | 20 |  |  | 2085 |  |  | 315 | 315 | 1.00 | 1940 |  |  | 1940 | 0.162 | 0.162 | 1 | 25 | 26 | 0.750 | 49 |
| Move-ment  | Stage                 | Lane Width m.           | Phase | No. of lane   | Radius m.               | O     | N  | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h  | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X |                         |           |                         |                                    |             |                         |            |     |                          | Queuing Length m. |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
|  |                       |                         |       |               |                         |       |    |                            | Left pcu/h | Straight pcu/h | Right pcu/h |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| A1   | 1                     | 3.75                    | X1    | 1             | 15                      |       | N  | 1990                       | 460        |                |             | 460   | 1.00                           | 1809            |                   |                         | 1809                    | 0.254 |           | 12    | 39               | 53            | 0.576                  | 51                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| C1   | 1                     | 3.50                    | X2    | 1             | 18                      |       | N  | 1965                       | 565        |                |             | 565   | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344 | 0.344     |       | 53               | 53            | 0.779                  | 63                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| C2   | 1                     | 3.50                    | X2    | 1             | 25                      |       |    | 2105                       |            |                | 558         | 558   | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.308 |           |       | 47               | 53            | 0.697                  | 62                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| A2   | 3                     | 3.75                    | Z1    | 1             |                         |       |    | 2130                       |            | 349            |             | 349   | 0.00                           | 2130            |                   |                         | 2130                    | 0.164 |           |       | 25               | 29            | 0.678                  | 53                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| B1   | 3                     | 3.30                    | Z2    | 1             |                         |       | N  | 1945                       |            | 373            |             | 373   | 0.00                           | 1945            |                   |                         | 1945                    | 0.192 | 0.192     |       | 29               | 29            | 0.794                  | 57                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| B2   | 2                     | 3.30                    | Y     | 1             | 20                      |       |    | 2085                       |            |                | 315         | 315   | 1.00                           | 1940            |                   |                         | 1940                    | 0.162 | 0.162     | 1     | 25               | 26            | 0.750                  | 49                      |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |
| NOTE : 'O' - OPPOSING TRAFFIC    N - NEAR SIDE LANE    SG - STEADY GREEN    FG - FLASHING GREEN    PEDESTRIAN WALKING SPEED = 0.9m/s    QUEUING LENGTH =   |                       |                         |       |               |                         |       |    |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |             |                         |            |     |                          |                   |       |       |                  |                                |                 |                   |                         |                         |    |                   |            |                  |               |                        |                   |            |                |             |                   |          |      |                 |            |      |         |         |         |                       |        |   |     |      |      |    |    |      |       |    |    |    |    |       |    |    |   |      |    |   |    |  |   |      |     |  |  |     |      |      |       |      |      |       |       |  |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |    |  |  |      |  |  |     |     |      |      |  |  |      |       |       |   |    |    |       |    |

## PROPOSED JUNCTION IMPROVEMENT

Ove Arup & Partners

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_REF\_IMP\_PM

PROJECT NO: 299277-02  
DATE : 21-Jan-25

Junction No. J3  
FILENAME :

The site plan shows a vertical road labeled "Lai King Hill Road" intersecting a horizontal road labeled "Kwai Chung Interchange". Traffic flows are indicated by arrows and numbers: B1 (down) 367, B2 (up) 400, C1 (right) 305, C2 (left) 424, A1 (up) 378, A2 (down) 342. A north arrow points upwards.

|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 3          |
| No. of stage using for calculation | N =                   | 3          |
| Cycle time                         | C =                   | 120 sec    |
| Sum(y)                             | Y =                   | 0.629      |
| Loss time                          | L =                   | 12 sec     |
| Total Flow                         | =                     | 2216 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 61.9 sec |
| Cm                                 | = L/(1-Y)             | = 32.3 sec |
| Yult                               |                       | = 0.810    |
| R.C.ult                            | = (Yult-Y)/Y*100%     | = 28.8 %   |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 39.8 sec |
| Ymax                               | = 1-L/C               | = 0.900    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 29 %     |

|    |   |   |   |    |  |
|----|---|---|---|----|--|
| X2 | P | Q | Y | Z2 |  |
| X1 |   | R |   | Z1 |  |

|         |        |         |        |         |        |  |  |
|---------|--------|---------|--------|---------|--------|--|--|
| STAGE 1 | INT= 5 | STAGE 2 | INT= 5 | STAGE 3 | INT= 5 |  |  |
|---------|--------|---------|--------|---------|--------|--|--|

|                  |           |                         |       |    |                         |       |    |       |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |
| P                | 5         | 6                       | 1     | 5  | 38                      | 1     | 5  | OK    |
| Q                | 10        | 6                       | 2     | 11 | 26                      | 2     | 11 | OK    |
| R                | 12        | 13                      | 5     | 12 | 22                      | 5     | 12 | OK    |
| S                | 11        | 12                      | 5     | 11 | 20                      | 5     | 11 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow |     |     | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------|-----|-----|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| A1       | 1     | 3.75          | X1    | 1           | 15        |   | N | 1990                     | 342  |     |     | 342              | 1.00                           | 1809            |                   |                         | 1809                    | 0.189 |           | 12    | 32               | 40            | 0.567                  | 46                |
| C1       | 1     | 3.50          | X2    | 1           | 18        |   | N | 1965                     | 305  |     |     | 305              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.186 | 0.234     |       | 32               | 40            | 0.557                  | 41                |
| C2       | 1     | 3.50          | X2    | 1           | 25        |   |   | 2105                     |      |     | 424 | 424              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.234 |           |       | 40               | 40            | 0.701                  | 57                |
| A2       | 3     | 3.75          | Z1    | 1           |           |   |   | 2130                     |      | 378 |     | 378              | 0.00                           | 2130            |                   |                         | 2130                    | 0.177 |           |       | 30               | 32            | 0.665                  | 55                |
| B1       | 3     | 3.30          | Z2    | 1           |           |   | N | 1945                     |      | 367 |     | 367              | 0.00                           | 1945            |                   |                         | 1945                    | 0.189 | 0.189     |       | 32               | 32            | 0.708                  | 54                |
| B2       | 2     | 3.30          | Y     | 1           | 20        |   |   | 2085                     |      |     | 400 | 400              | 1.00                           | 1940            |                   |                         | 1940                    | 0.206 | 0.206     |       | 35               | 35            | 0.707                  | 57                |

NOTE :   'O' - OPPOSING TRAFFIC       N - NEAR SIDE LANE       SG - STEADY GREEN       FG - FLASHING GREEN       PEDESTRIAN WALKING SPEED = 0.9m/s       QUEUING LENGTH = AVERAGE QUEUE \* 6m

## PROPOSED JUNCTION IMPROVEMENT

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_DES\_IMP\_AM

PROJECT NO:299277-02Junction No. J3

DATE :21-Jan-25FILENAME :

The site plan shows a T-junction where Kwai Chung Interchange meets Lai King Hill Road. Traffic flows are indicated by arrows: Stage A1/A2 (left/right turn from interchange), Stage B1/B2 (through/right turn onto road), and Stage C1/C2 (left/right turn off road). Flow volumes are provided for each movement.

|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 3          |
| No. of stage using for calculation | N =                   | 3          |
| Cycle time                         | C =                   | 120 sec    |
| Sum(y)                             | Y =                   | 0.699      |
| Loss time                          | L =                   | 13 sec     |
| Total Flow                         | =                     | 2735 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 81.5 sec |
| Cm                                 | = L/(1-Y)             | = 43.2 sec |
| Yult                               | =                     | 0.803      |
| R.C. ult                           | = (Yult-Y)/Y*100%     | = 14.8 %   |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 58.3 sec |
| Ymax                               | = 1-L/C               | = 0.892    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 15 %     |

|         |        |         |        |         |        |  |  |
|---------|--------|---------|--------|---------|--------|--|--|
| X2      | P      | Q       | Z2     |         |        |  |  |
| X1      |        | Y       | S      | Z1      |        |  |  |
|         |        | R       |        |         |        |  |  |
| STAGE 1 | INT= 5 | STAGE 2 | INT= 5 | STAGE 3 | INT= 5 |  |  |

|                  |           |  |   |    |  |   |    |       |
|------------------|-----------|--|---|----|--|---|----|-------|
| Pedestrian Phase | Width (m) | Green Time Required (s)<br>SG Delay FG |   |    | Green Time Provided (s)<br>SG Delay FG |   |    | Check |
| P                | 5         | 6                                      | 1 | 5  | 51                                     | 1 | 5  | OK    |
| Q                | 10        | 6                                      | 2 | 11 | 17                                     | 2 | 11 | OK    |
| R                | 12        | 13                                     | 5 | 12 | 13                                     | 5 | 12 | OK    |
| S                | 11        | 12                                     | 5 | 11 | 17                                     | 5 | 11 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow |     |     | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------|-----|-----|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| A1       | 1     | 3.75          | X1    | 1           | 15        |   | N | 1990                     | 528  |     |     | 528              | 1.00                           | 1809            |                   |                         | 1809                    | 0.292 |           | 12    | 45               | 53            | 0.661                  | 59                |
| C1       | 1     | 3.50          | X2    | 1           | 18        |   | N | 1965                     | 565  |     |     | 565              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344 | 0.344     |       | 53               | 53            | 0.779                  | 63                |
| C2       | 1     | 3.50          | X2    | 1           | 25        |   |   | 2105                     |      |     | 600 | 600              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.331 |           |       | 51               | 53            | 0.749                  | 67                |
| A2       | 3     | 3.75          | Z1    | 1           |           |   |   | 2130                     |      | 352 |     | 352              | 0.00                           | 2130            |                   |                         | 2130                    | 0.165 |           |       | 25               | 29            | 0.684                  | 53                |
| B1       | 3     | 3.30          | Z2    | 1           |           |   | N | 1945                     |      | 375 |     | 375              | 0.00                           | 1945            |                   |                         | 1945                    | 0.193 | 0.193     |       | 29               | 29            | 0.798                  | 57                |
| B2       | 2     | 3.30          | Y     | 1           | 20        |   |   | 2085                     |      |     | 315 | 315              | 1.00                           | 1940            |                   |                         | 1940                    | 0.162 | 0.162     | 1     | 25               | 26            | 0.750                  | 49                |

NOTE : 'O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN

PEDESTRIAN WALKING SPEED = 0.9m/s

QUEUING LENGTH = AVERAGE QUEUE \* 6m

## PROPOSED JUNCTION IMPROVEMENT

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng  
Lai King Hill Road / Kwai Chung Interchange

J3\_DES\_IMP\_PM

PROJECT NO:  
DATE :

299277-02  
21-Jan-25

Junction No.  
FILENAME :

J3

No.

No. of stages per cycle N = 3  
No. of stage using for calculation N = 3  
  
Cycle time C = 120 sec  
Sum(y) Y = 0.646  
Loss time L = 12 sec  
Total Flow = 2267 pcu  
  
Co = (1.5\*L+5)/(1-Y) = 64.9 sec  
Cm = L/(1-Y) = 33.9 sec  
Yult = 0.810  
R.C. ult = (Yult-Y)/Y\*100% = 25.4 %  
Cp = 0.9\*L/(0.9-Y) = 42.5 sec  
Ymax = 1-L/C = 0.900  
R.C.(C) = (0.9\*Ymax-Y)/Y\*100% = 25 %

P  
X2  
X1

Q  
R

Z2  
Z1  
S

STAGE 1INT= 5STAGE 2INT= 5STAGE 3INT= 5

| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |
| P                | 5         | 6                       | 1     | 5  | 41                      | 1     | 5  | OK    |
| Q                | 10        | 6                       | 2     | 11 | 25                      | 2     | 11 | OK    |
| R                | 12        | 13                      | 5     | 12 | 21                      | 5     | 12 | OK    |
| S                | 11        | 12                      | 5     | 11 | 18                      | 5     | 11 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|          |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| A1       | 1     | 3.75          | X1    | 1           | 15        |   | N | 1990                     | 378        |                |             | 378              | 1.00                           | 1809            |                   |                         | 1809                    | 0.209 |           | 12    | 35               | 43            | 0.583                  | 49                |
| C1       | 1     | 3.50          | X2    | 1           | 18        |   | N | 1965                     | 305        |                |             | 305              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.186 | 0.258     |       | 31               | 43            | 0.518                  | 39                |
| C2       | 1     | 3.50          | X2    | 1           | 25        |   |   | 2105                     |            |                | 468         | 468              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.258 |           |       | 43               | 43            | 0.720                  | 60                |
| A2       | 3     | 3.75          | Z1    | 1           |           |   |   | 2130                     |            | 363            |             | 363              | 0.00                           | 2130            |                   |                         | 2130                    | 0.170 |           |       | 29               | 30            | 0.682                  | 54                |
| B1       | 3     | 3.30          | Z2    | 1           |           |   | N | 1945                     |            | 353            |             | 353              | 0.00                           | 1945            |                   |                         | 1945                    | 0.181 | 0.181     |       | 30               | 30            | 0.726                  | 53                |
| B2       | 2     | 3.30          | Y     | 1           | 20        |   |   | 2085                     |            |                | 400         | 400              | 1.00                           | 1940            |                   |                         | 1940                    | 0.206 | 0.206     |       | 34               | 34            | 0.728                  | 57                |

NOTE : O - OPPOSING TRAFFIC N - NEAR SIDE LANE SG - STEADY GREEN FG - FLASHING GREEN PEDESTRIAN WALKING SPEED = 0.9m/s QUEUING LENGTH = AVERAGE QUEUE \* 6m



## PROPOSED JUNCTION IMPROVEMENT

Ove Arup & Partners

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_INT\_A\_IMP\_AM

PROJECT NO: 299277-02  
DATE : 21-Jan-25

Junction No. J3  
FILENAME :

|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 3          |
| No. of stage using for calculation | N =                   | 3          |
| Cycle time                         | C =                   | 120 sec    |
| Sum(y)                             | Y =                   | 0.695      |
| Loss time                          | L =                   | 13 sec     |
| Total Flow                         | =                     | 2397 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 80.3 sec |
| Cm                                 | = L/(1-Y)             | = 42.6 sec |
| Yult                               |                       | = 0.803    |
| R.C.ult                            | = (Yult-Y)/Y*100%     | = 15.5 %   |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 57.0 sec |
| Ymax                               | = 1-L/C               | = 0.892    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 16 %     |

|    |   |   |   |    |
|----|---|---|---|----|
| X2 | P | Q | Y | Z2 |
| X1 |   | R |   | S  |
|    |   |   |   | Z1 |

|         |        |         |        |         |        |
|---------|--------|---------|--------|---------|--------|
| STAGE 1 | INT= 5 | STAGE 2 | INT= 5 | STAGE 3 | INT= 5 |
|---------|--------|---------|--------|---------|--------|

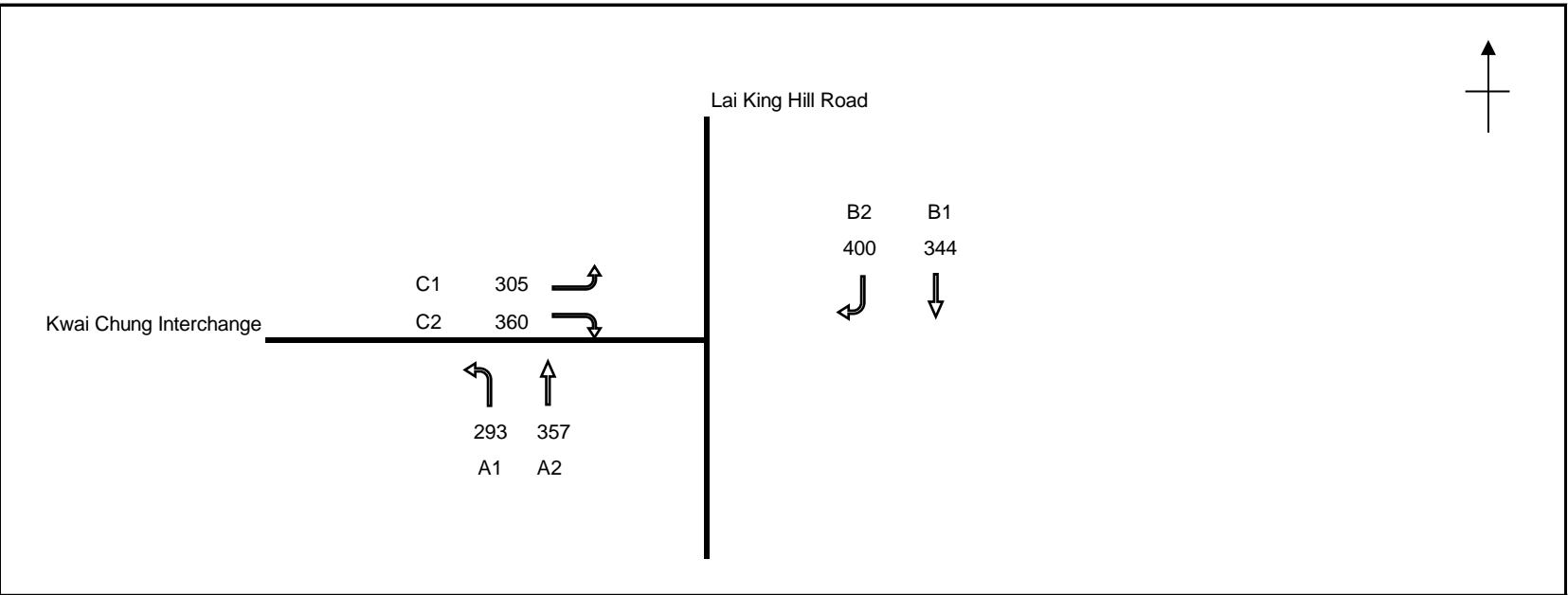
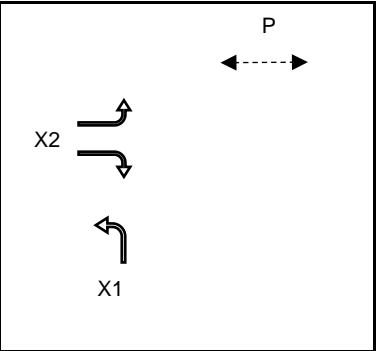
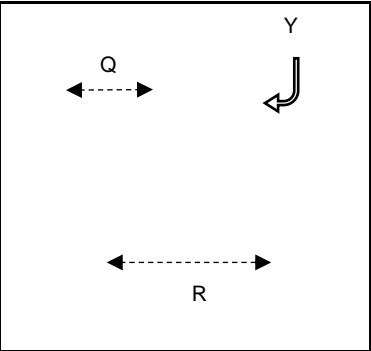
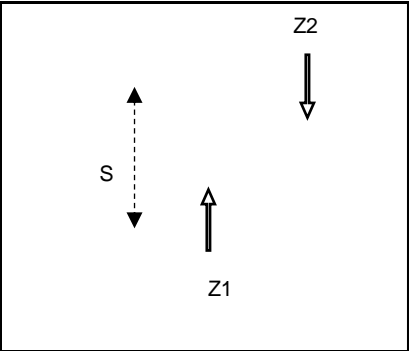
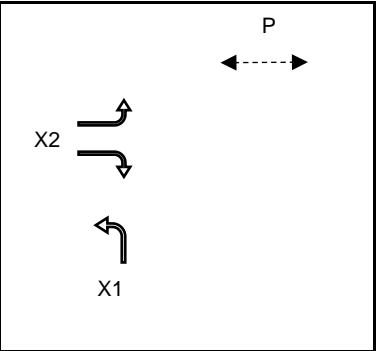
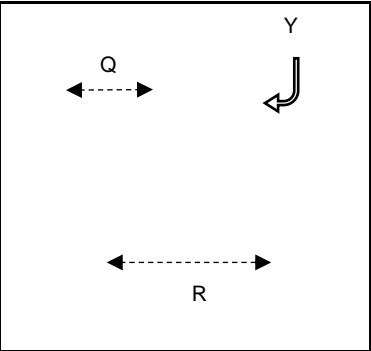
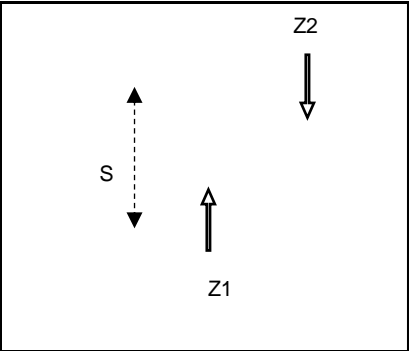
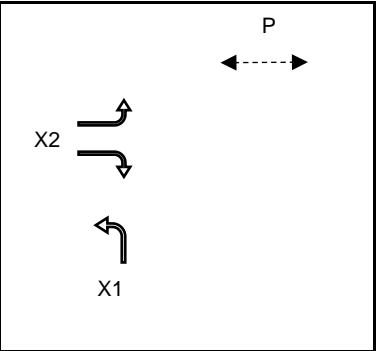
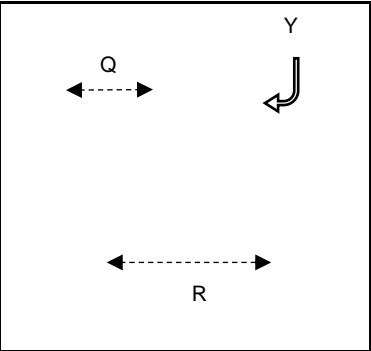
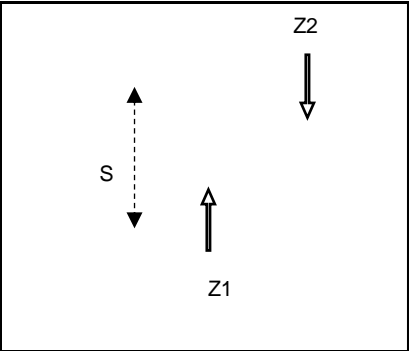
|                  |           |                         |       |    |                         |       |    |       |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |
| P                | 5         | 6                       | 1     | 5  | 51                      | 1     | 5  | OK    |
| Q                | 10        | 6                       | 2     | 11 | 17                      | 2     | 11 | OK    |
| R                | 12        | 13                      | 5     | 12 | 13                      | 5     | 12 | OK    |
| S                | 11        | 12                      | 5     | 11 | 17                      | 5     | 11 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow |     |     | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------|-----|-----|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| A1       | 1     | 3.75          | X1    | 1           | 15        |   | N | 1990                     | 329  |     |     | 329              | 1.00                           | 1809            |                   |                         | 1809                    | 0.182 |           | 12    | 28               | 53            | 0.412                  | 37                |
| C1       | 1     | 3.50          | X2    | 1           | 18        |   | N | 1965                     | 565  |     |     | 565              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344 | 0.344     |       | 53               | 53            | 0.779                  | 63                |
| C2       | 1     | 3.50          | X2    | 1           | 25        |   |   | 2105                     |      |     | 485 | 485              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.267 |           |       | 41               | 53            | 0.605                  | 54                |
| A2       | 3     | 3.75          | Z1    | 1           |           |   |   | 2130                     |      | 337 |     | 337              | 0.00                           | 2130            |                   |                         | 2130                    | 0.158 |           |       | 24               | 29            | 0.655                  | 51                |
| B1       | 3     | 3.30          | Z2    | 1           |           |   | N | 1945                     |      | 366 |     | 366              | 0.00                           | 1945            |                   |                         | 1945                    | 0.188 | 0.188     |       | 29               | 29            | 0.779                  | 56                |
| B2       | 2     | 3.30          | Y     | 1           | 20        |   |   | 2085                     |      |     | 315 | 315              | 1.00                           | 1940            |                   |                         | 1940                    | 0.162 | 0.162     | 1     | 25               | 26            | 0.750                  | 49                |

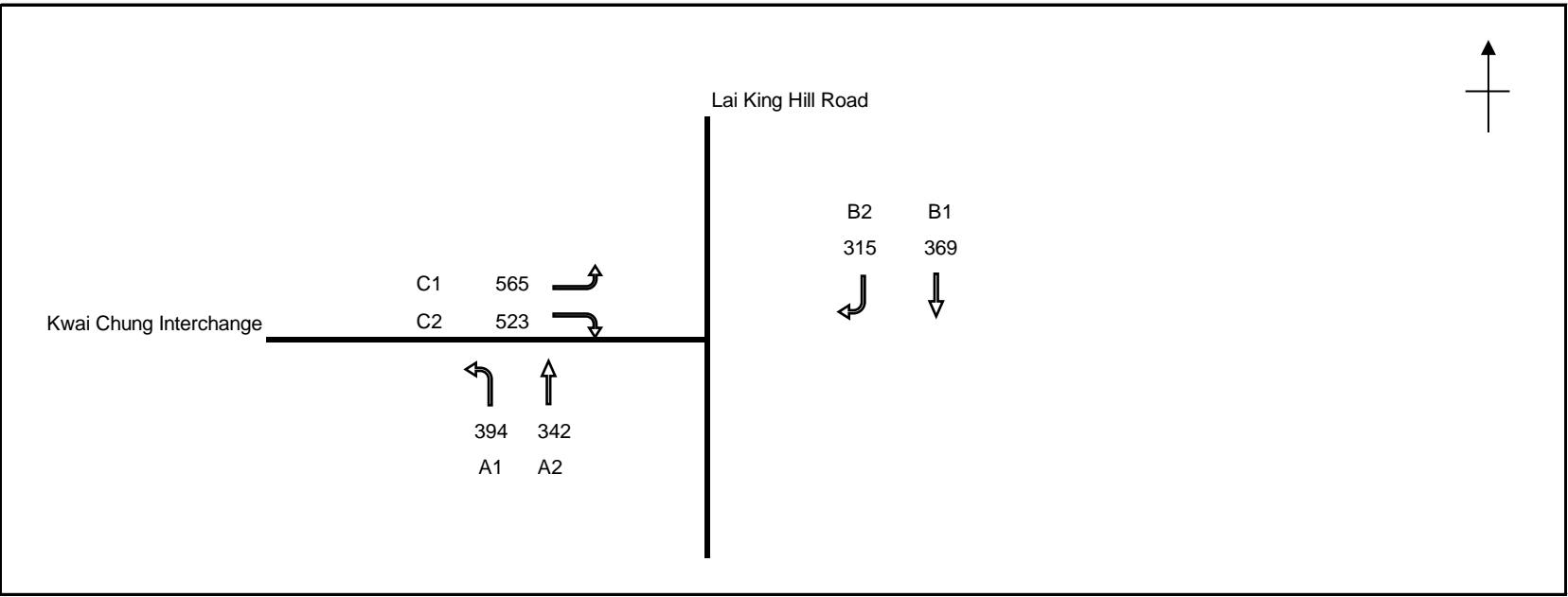
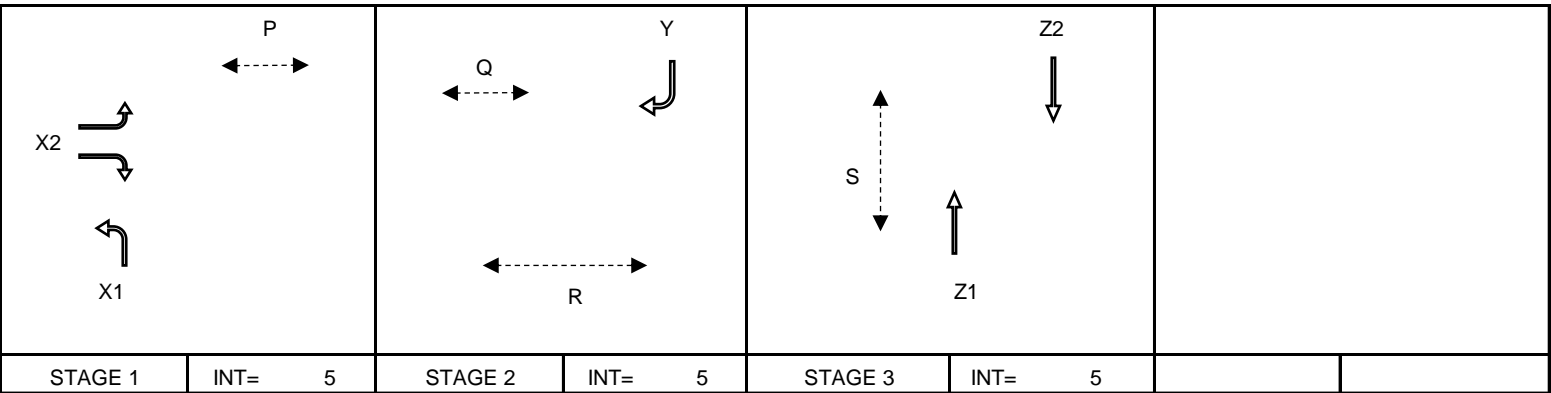
NOTE : 'O' - OPPOSING TRAFFIC    N - NEAR SIDE LANE    SG - STEADY GREEN    FG - FLASHING GREEN

PEDESTRIAN WALKING SPEED = 0.9m/s      QUEUING LENGTH = AVERAGE QUEUE \* 6m

## PROPOSED JUNCTION IMPROVEMENT

| OVE ARUP & PARTNERS  |                       |   |               |  |                         |           |    | TRAFFIC SIGNAL CALCULATION |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
|--|-----------------------|---|---------------|--|-------------------------|-----------|----|----------------------------|--------------------------|-------|---------------|------------|------------------|--|-----------------|---|-------------------------|--|-------------------------|-----------|-------|------------------|---------------|-------------------------|-------------------|-------------|------------------------------------|-------------|----|--------------------------|------|---------|--------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|---|-----------|-------|-------------------|---------------|------------------------|-------------------|------------|------|----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|-----|----|--|-----|------|------|-------|------|------|-------|-------|----|----|-------|----|----|---|------|----|---|----|--|--|------|--|--|-----|-----|------|------|-------|------|------|-------|--|----|----|-------|----|----|---|------|----|---|--|--|--|------|--|-----|--|-----|------|------|--|--|------|-------|--|----|----|-------|----|----|---|------|----|---|--|--|---|------|--|-----|--|-----|------|------|--|--|------|-------|-------|----|----|-------|----|----|---|------|---|-----|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |   |               |  |                         |           |    | PROJECT NO: 299277-02      |                          |       |               |            |                  |  |                 | Junction No. J3   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Lai King Hill Road / Kwai Chung Interchange  |                       |   |               | J3_INT_A_IMP_PM  |                         |           |    | DATE : 21-Jan-25           |                          |       |               | FILENAME : |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
|    |                       |   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.582</td></tr> <tr> <td>Loss time</td><td>L =</td><td>12 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2059 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 55.0 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 28.7 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.810</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 39.3 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 33.9 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.900</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 39 %</td></tr> </table> |                         |  |                         |           |       |                  |               | No. of stages per cycle | N =               | 3           | No. of stage using for calculation | N =         | 3  | Cycle time               | C =  | 120 sec | Sum(y) | Y =              | 0.582                          | Loss time       | L =               | 12 sec                  | Total Flow              | = | 2059 pcu  | Co    | = (1.5*L+5)/(1-Y) | = 55.0 sec    | Cm                     | = L/(1-Y)         | = 28.7 sec | Yult | =  | 0.810 | R.C.ult | = (Yult-Y)/Y*100% | = 39.3 % | Cp | = 0.9*L/(0.9-Y) | = 33.9 sec | Ymax | = 1-L/C | = 0.900 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 39 % |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| No. of stages per cycle  | N =                   | 3   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| No. of stage using for calculation   | N =                   | 3   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Cycle time   | C =                   | 120 sec   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Sum(y)   | Y =                   | 0.582   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Loss time  | L =                   | 12 sec  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Total Flow   | =                     | 2059 pcu  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Co   | = (1.5*L+5)/(1-Y)     | = 55.0 sec  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Cm   | = L/(1-Y)             | = 28.7 sec  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Yult   | =                     | 0.810   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 39.3 %  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Cp   | = 0.9*L/(0.9-Y)       | = 33.9 sec  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Ymax   | = 1-L/C               | = 0.900   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 39 %  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| <table> <tr> <td colspan="2">  </td><td colspan="2">  </td><td colspan="2">  </td><td colspan="2"></td></tr> <tr> <td>STAGE 1</td><td>INT= 5</td><td>STAGE 2</td><td>INT= 5</td><td>STAGE 3</td><td>INT= 5</td><td></td><td></td></tr> </table>   |                       |   |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |    |                         |  |                         |           |       | STAGE 1          | INT= 5        | STAGE 2                 | INT= 5            | STAGE 3     | INT= 5                             |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
|    |                       |  |               |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| STAGE 1  | INT= 5                | STAGE 2   | INT= 5        | STAGE 3  | INT= 5                  |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>P</td><td>5</td><td>6</td><td>1</td><td>5</td><td>35</td><td>1</td><td>5</td><td>OK</td></tr> <tr> <td>Q</td><td>10</td><td>6</td><td>2</td><td>11</td><td>29</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>R</td><td>12</td><td>13</td><td>5</td><td>12</td><td>25</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>S</td><td>11</td><td>12</td><td>5</td><td>11</td><td>21</td><td>5</td><td>11</td><td>OK</td></tr> </table>   |                       |   |               |  |                         |           |    |                            |                          |       |               |            |                  | Pedestrian Phase   | Width (m)       | Green Time Required (s)   |                         |  | Green Time Provided (s) |           |       | Check            | SG            | Delay                   | FG                | SG          | Delay                              | FG          | P  | 5                        | 6    | 1       | 5      | 35               | 1                              | 5               | OK                | Q                       | 10                      | 6 | 2         | 11    | 29                | 2             | 11                     | OK                | R          | 12   | 13 | 5     | 12      | 25                | 5        | 12 | OK              | S          | 11   | 12      | 5       | 11      | 21                    | 5      | 11  | OK |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Pedestrian Phase   | Width (m)             | Green Time Required (s)   |               |  | Green Time Provided (s) |           |    | Check                      |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
|  |                       | SG  | Delay         | FG   | SG                      | Delay     | FG |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| P  | 5                     | 6   | 1             | 5  | 35                      | 1         | 5  | OK                         |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| Q  | 10                    | 6   | 2             | 11   | 29                      | 2         | 11 | OK                         |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| R  | 12                    | 13  | 5             | 12   | 25                      | 5         | 12 | OK                         |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| S  | 11                    | 12  | 5             | 11   | 21                      | 5         | 11 | OK                         |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| <table> <tr> <th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr> <tr> <th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr> <tr> <td>A1</td><td>1</td><td>3.75</td><td>X1</td><td>1</td><td>15</td><td></td><td>N</td><td>1990</td><td>293</td><td></td><td></td><td>293</td><td>1.00</td><td>1809</td><td></td><td></td><td>1809</td><td>0.162</td><td></td><td rowspan="5">12</td><td>30</td><td>37</td><td>0.525</td><td>41</td></tr> <tr> <td>C1</td><td>1</td><td>3.50</td><td>X2</td><td>1</td><td>18</td><td></td><td>N</td><td>1965</td><td>305</td><td></td><td></td><td>305</td><td>1.00</td><td>1814</td><td>4.10%</td><td>-172</td><td>1642</td><td>0.186</td><td>0.198</td><td>34</td><td>37</td><td>0.602</td><td>42</td></tr> <tr> <td>C2</td><td>1</td><td>3.50</td><td>X2</td><td>1</td><td>25</td><td></td><td></td><td>2105</td><td></td><td></td><td>360</td><td>360</td><td>1.00</td><td>1986</td><td>4.10%</td><td>-172</td><td>1814</td><td>0.198</td><td></td><td>37</td><td>37</td><td>0.644</td><td>50</td></tr> <tr> <td>A2</td><td>3</td><td>3.75</td><td>Z1</td><td>1</td><td></td><td></td><td></td><td>2130</td><td></td><td>357</td><td></td><td>357</td><td>0.00</td><td>2130</td><td></td><td></td><td>2130</td><td>0.168</td><td></td><td>31</td><td>33</td><td>0.609</td><td>52</td></tr> <tr> <td>B1</td><td>3</td><td>3.30</td><td>Z2</td><td>1</td><td></td><td></td><td>N</td><td>1945</td><td></td><td>344</td><td></td><td>344</td><td>0.00</td><td>1945</td><td></td><td></td><td>1945</td><td>0.177</td><td>0.177</td><td>33</td><td>33</td><td>0.643</td><td>50</td></tr> <tr> <td>B2</td><td>2</td><td>3.30</td><td>Y</td><td>1&lt;/</td></tr></table> | Move-ment             | Stage   | Lane Width m. | Phase  | No. of lane             | Radius m. | O  | N                          | Straight-Ahead Sat. Flow | Flow  |               |            | Total Flow pcu/h | Proportion of Turning Vehicles   | Sat. Flow pcu/h | Uphill Gradient %   | Short lane Effect pcu/h | Revised Sat. Flow pcu/h  | y                       | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. | Left pcu/h  | Straight pcu/h                     | Right pcu/h | A1 | 1                        | 3.75 | X1      | 1      | 15               |                                | N               | 1990              | 293                     |                         |   | 293       | 1.00  | 1809              |               |                        | 1809              | 0.162      |      | 12 | 30    | 37      | 0.525             | 41       | C1 | 1               | 3.50       | X2   | 1       | 18      |         | N                     | 1965   | 305 |    |  | 305 | 1.00 | 1814 | 4.10% | -172 | 1642 | 0.186 | 0.198 | 34 | 37 | 0.602 | 42 | C2 | 1 | 3.50 | X2 | 1 | 25 |  |  | 2105 |  |  | 360 | 360 | 1.00 | 1986 | 4.10% | -172 | 1814 | 0.198 |  | 37 | 37 | 0.644 | 50 | A2 | 3 | 3.75 | Z1 | 1 |  |  |  | 2130 |  | 357 |  | 357 | 0.00 | 2130 |  |  | 2130 | 0.168 |  | 31 | 33 | 0.609 | 52 | B1 | 3 | 3.30 | Z2 | 1 |  |  | N | 1945 |  | 344 |  | 344 | 0.00 | 1945 |  |  | 1945 | 0.177 | 0.177 | 33 | 33 | 0.643 | 50 | B2 | 2 | 3.30 | Y | 1</ |
| Move-ment  |                       |   |               |  |                         |           |    |                            |                          | Stage | Lane Width m. | Phase      |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   | No. of lane | Radius m.                          | O           | N  | Straight-Ahead Sat. Flow | Flow |         |        | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y | Greater y | L sec | g (required) sec  | g (input) sec | Degree of Saturation X | Queuing Length m. |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
|  | Left pcu/h            | Straight pcu/h  | Right pcu/h   |  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| A1   | 1                     | 3.75  | X1            | 1  | 15                      |           | N  | 1990                       | 293                      |       |               | 293        | 1.00             | 1809   |                 |   | 1809                    | 0.162  |                         | 12        | 30    | 37               | 0.525         | 41                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| C1   | 1                     | 3.50  | X2            | 1  | 18                      |           | N  | 1965                       | 305                      |       |               | 305        | 1.00             | 1814   | 4.10%           | -172  | 1642                    | 0.186  | 0.198                   |           | 34    | 37               | 0.602         | 42                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| C2   | 1                     | 3.50  | X2            | 1  | 25                      |           |    | 2105                       |                          |       | 360           | 360        | 1.00             | 1986   | 4.10%           | -172  | 1814                    | 0.198  |                         |           | 37    | 37               | 0.644         | 50                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| A2   | 3                     | 3.75  | Z1            | 1  |                         |           |    | 2130                       |                          | 357   |               | 357        | 0.00             | 2130   |                 |   | 2130                    | 0.168  |                         |           | 31    | 33               | 0.609         | 52                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| B1   | 3                     | 3.30  | Z2            | 1  |                         |           | N  | 1945                       |                          | 344   |               | 344        | 0.00             | 1945   |                 |   | 1945                    | 0.177  | 0.177                   |           | 33    | 33               | 0.643         | 50                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |
| B2   | 2                     | 3.30  | Y             | 1</  |                         |           |    |                            |                          |       |               |            |                  |  |                 |   |                         |  |                         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |    |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |      |    |   |    |  |  |      |  |  |     |     |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |    |    |       |    |    |   |      |   |     |

## PROPOSED JUNCTION IMPROVEMENT

| OVE ARUP & PARTNERS  |                       |                         |         |                 |                         |         |      | TRAFFIC SIGNAL CALCULATION |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
|--|-----------------------|-------------------------|---------|-----------------|-------------------------|---------|------|----------------------------|------------|----------------|-------------|---|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|---------|-----------|-------|------------------|---------------|------------------------|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-------|-------|-----------|-------|--------|------------|---|----------|----|-------------------|------------|----|-----------|------------|------|----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|---|----|----|---|----|----|---|----|----|---|----|----|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |         |                 |                         |         |      |                            |            |                |             | PROJECT NO: 299277-02   |                                |                 |                   | Junction No. J3         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                         |         | J3_INT_B_IMP_AM |                         |         |      | DATE : 21-Jan-25           |            |                |             | FILENAME :  |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
|    |                       |                         |         |                 |                         |         |      |                            |            |                |             | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.696</td></tr> <tr> <td>Loss time</td><td>L =</td><td>13 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2508 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 80.7 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 42.8 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.803</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 15.3 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 57.4 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.892</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 15 %</td></tr> </table> |                                |                 |                   |                         |                         |         |           |       |                  |               |                        | No. of stages per cycle | N =       | 3                       | No. of stage using for calculation | N = | 3                       | Cycle time | C = | 120 sec | Sum(y) | Y =   | 0.696 | Loss time | L =   | 13 sec | Total Flow | = | 2508 pcu | Co | = (1.5*L+5)/(1-Y) | = 80.7 sec | Cm | = L/(1-Y) | = 42.8 sec | Yult | =  | 0.803 | R.C.ult | = (Yult-Y)/Y*100% | = 15.3 % | Cp | = 0.9*L/(0.9-Y) | = 57.4 sec | Ymax | = 1-L/C | = 0.892 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 15 % |   |    |    |   |    |    |   |    |    |   |    |    |
| No. of stages per cycle  | N =                   | 3                       |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| No. of stage using for calculation   | N =                   | 3                       |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Cycle time   | C =                   | 120 sec                 |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Sum(y)   | Y =                   | 0.696                   |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Loss time  | L =                   | 13 sec                  |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Total Flow   | =                     | 2508 pcu                |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 80.7 sec              |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Cm   | = L/(1-Y)             | = 42.8 sec              |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Yult   | =                     | 0.803                   |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 15.3 %                |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 57.4 sec              |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Ymax   | = 1-L/C               | = 0.892                 |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 15 %                  |         |                 |                         |         |      |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
|   |                       |                         |         |                 |                         |         |      |                            |            |                |             | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>P</td><td>5</td><td>6</td><td>1</td><td>5</td><td>51</td><td>1</td><td>5</td><td>OK</td></tr> <tr> <td>Q</td><td>10</td><td>6</td><td>2</td><td>11</td><td>17</td><td>2</td><td>11</td><td>OK</td></tr> <tr> <td>R</td><td>12</td><td>13</td><td>5</td><td>12</td><td>13</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>S</td><td>11</td><td>12</td><td>5</td><td>11</td><td>17</td><td>5</td><td>11</td><td>OK</td></tr> </table>  |                                |                 |                   |                         |                         |         |           |       |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   | SG     | Delay | FG    | SG        | Delay | FG     | P          | 5 | 6        | 1  | 5                 | 51         | 1  | 5         | OK         | Q    | 10 | 6     | 2       | 11                | 17       | 2  | 11              | OK         | R    | 12      | 13      | 5       | 12                    | 13     | 5 | 12 | OK | S | 11 | 12 | 5 | 11 | 17 | 5 | 11 | OK |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |         |                 | Green Time Provided (s) |         |      | Check                      |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
|  |                       | SG                      | Delay   | FG              | SG                      | Delay   | FG   |                            |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| P  | 5                     | 6                       | 1       | 5               | 51                      | 1       | 5    | OK                         |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Q  | 10                    | 6                       | 2       | 11              | 17                      | 2       | 11   | OK                         |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| R  | 12                    | 13                      | 5       | 12              | 13                      | 5       | 12   | OK                         |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| S  | 11                    | 12                      | 5       | 11              | 17                      | 5       | 11   | OK                         |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| <table> <tr> <td>STAGE 1</td><td>INT=</td><td>5</td><td>STAGE 2</td><td>INT=</td><td>5</td><td>STAGE 3</td><td>INT=</td><td>5</td><td></td><td></td></tr> </table> |                       |                         |         |                 |                         |         |      |                            |            |                |             | STAGE 1   | INT=                           | 5               | STAGE 2           | INT=                    | 5                       | STAGE 3 | INT=      | 5     |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| STAGE 1  | INT=                  | 5                       | STAGE 2 | INT=            | 5                       | STAGE 3 | INT= | 5                          |            |                |             |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| Move-ment  | Stage                 | Lane Width m.           | Phase   | No. of lane     | Radius m.               | O       | N    | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h  | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y       | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.       |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
|  |                       |                         |         |                 |                         |         |      |                            | Left pcu/h | Straight pcu/h | Right pcu/h |   |                                |                 |                   |                         |                         |         |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| A1   | 1                     | 3.75                    | X1      | 1               | 15                      |         | N    | 1990                       | 394        |                |             | 394   | 1.00                           | 1809            |                   |                         | 1809                    | 0.218   |           | 12    | 33               | 53            | 0.493                  | 44                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| C1   | 1                     | 3.50                    | X2      | 1               | 18                      |         | N    | 1965                       | 565        |                |             | 565   | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344   | 0.344     |       | 53               | 53            | 0.779                  | 63                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| C2   | 1                     | 3.50                    | X2      | 1               | 25                      |         |      | 2105                       |            |                | 523         | 523   | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.288   |           |       | 44               | 53            | 0.653                  | 58                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| A2   | 3                     | 3.75                    | Z1      | 1               |                         |         |      | 2130                       |            | 342            |             | 342   | 0.00                           | 2130            |                   |                         | 2130                    | 0.161   |           |       | 25               | 29            | 0.664                  | 52                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| B1   | 3                     | 3.30                    | Z2      | 1               |                         |         | N    | 1945                       |            | 369            |             | 369   | 0.00                           | 1945            |                   |                         | 1945                    | 0.190   | 0.190     |       | 29               | 29            | 0.785                  | 56                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |
| B2   | 2                     | 3.30                    | Y       | 1               | 20                      |         |      | 2085                       |            |                | 315         | 315   | 1.00                           | 1940            |                   |                         | 1940                    | 0.162   | 0.162     | 1     | 25               | 26            |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |   |          |    |                   |            |    |           |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |   |    |    |   |    |    |   |    |    |

## PROPOSED JUNCTION IMPROVEMENT

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_INT\_B\_IMP\_PM

PROJECT NO:299277-02Junction No. J3

DATE :21-Jan-25FILENAME :

## PROPOSED JUNCTION IMPROVEMENT

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng

Lai King Hill Road / Kwai Chung Interchange

J3\_INT\_C\_IMP\_AM

PROJECT NO:  
DATE :

299277-02  
21-Jan-25

Junction No.  
FILENAME :

J3

The diagram illustrates the intersection of Lai King Hill Road and Kwai Chung Interchange. It shows three stages of traffic control: Stage 1 (left-turning vehicles from the interchange), Stage 2 (through and right-turning vehicles from the interchange), and Stage 3 (vehicles approaching from the main road). Traffic volumes are provided for each movement.

| Movement                | Vehicles per Cycle |
|-------------------------|--------------------|
| C1 (Left Turn)          | 565                |
| C2 (Through/Right Turn) | 562                |
| A1 (Left Turn)          | 463                |
| A2 (Through/Right Turn) | 347                |
| B1 (Through/Right Turn) | 372                |
| B2 (Left Turn)          | 315                |

|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 3          |
| No. of stage using for calculation | N =                   | 3          |
| Cycle time                         | C =                   | 120 sec    |
| Sum(y)                             | Y =                   | 0.698      |
| Loss time                          | L =                   | 13 sec     |
| Total Flow                         | =                     | 2624 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 81.1 sec |
| Cm                                 | = L/(1-Y)             | = 43.0 sec |
| Yult                               | =                     | 0.803      |
| R.C. ult                           | = (Yult-Y)/Y*100%     | = 15.0 %   |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 57.9 sec |
| Ymax                               | = 1-L/C               | = 0.892    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 15 %     |

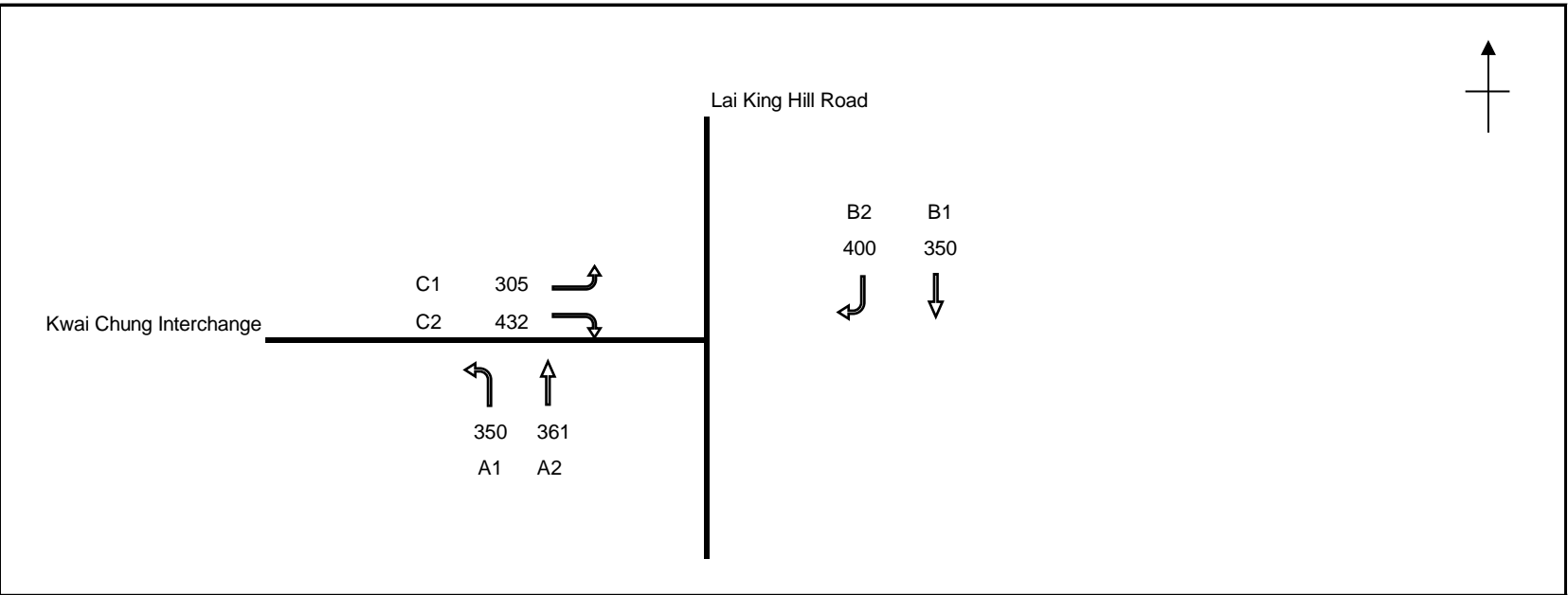
|                  |           |  |  |       |
|------------------|-----------|--|--|-------|
| Pedestrian Phase | Width (m) | Green Time Required (s)<br>SG Delay FG | Green Time Provided (s)<br>SG Delay FG | Check |
| P                | 5         | 6 1 5                                  | 51 1 5                                 | OK    |
| Q                | 10        | 6 2 11                                 | 17 2 11                                | OK    |
| R                | 12        | 13 5 12                                | 13 5 12                                | OK    |
| S                | 11        | 12 5 11                                | 17 5 11                                | OK    |

| Move-ment | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|-----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|           |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| A1        | 1     | 3.75          | X1    | 1           | 15        |   | N | 1990                     | 463        |                |             | 463              | 1.00                           | 1809            |                   |                         | 1809                    | 0.256 |           | 12    | 39               | 53            | 0.579                  | 52                |
| C1        | 1     | 3.50          | X2    | 1           | 18        |   | N | 1965                     | 565        |                |             | 565              | 1.00                           | 1814            | 4.10%             | -172                    | 1642                    | 0.344 | 0.344     |       | 53               | 53            | 0.779                  | 63                |
| C2        | 1     | 3.50          | X2    | 1           | 25        |   |   | 2105                     |            |                | 562         | 562              | 1.00                           | 1986            | 4.10%             | -172                    | 1814                    | 0.310 |           |       | 48               | 53            | 0.702                  | 63                |
| A2        | 3     | 3.75          | Z1    | 1           |           |   |   | 2130                     |            | 347            |             | 347              | 0.00                           | 2130            |                   |                         | 2130                    | 0.163 |           |       | 25               | 29            | 0.674                  | 53                |
| B1        | 3     | 3.30          | Z2    | 1           |           |   | N | 1945                     |            | 372            |             | 372              | 0.00                           | 1945            |                   |                         | 1945                    | 0.191 | 0.191     |       | 29               | 29            | 0.791                  | 56                |
| B2        | 2     | 3.30          | Y     | 1           | 20        |   |   | 2085                     |            |                | 315         | 315              | 1.00                           | 1940            |                   |                         | 1940                    | 0.162 | 0.162     | 1     | 25               | 26            | 0.750                  | 49                |

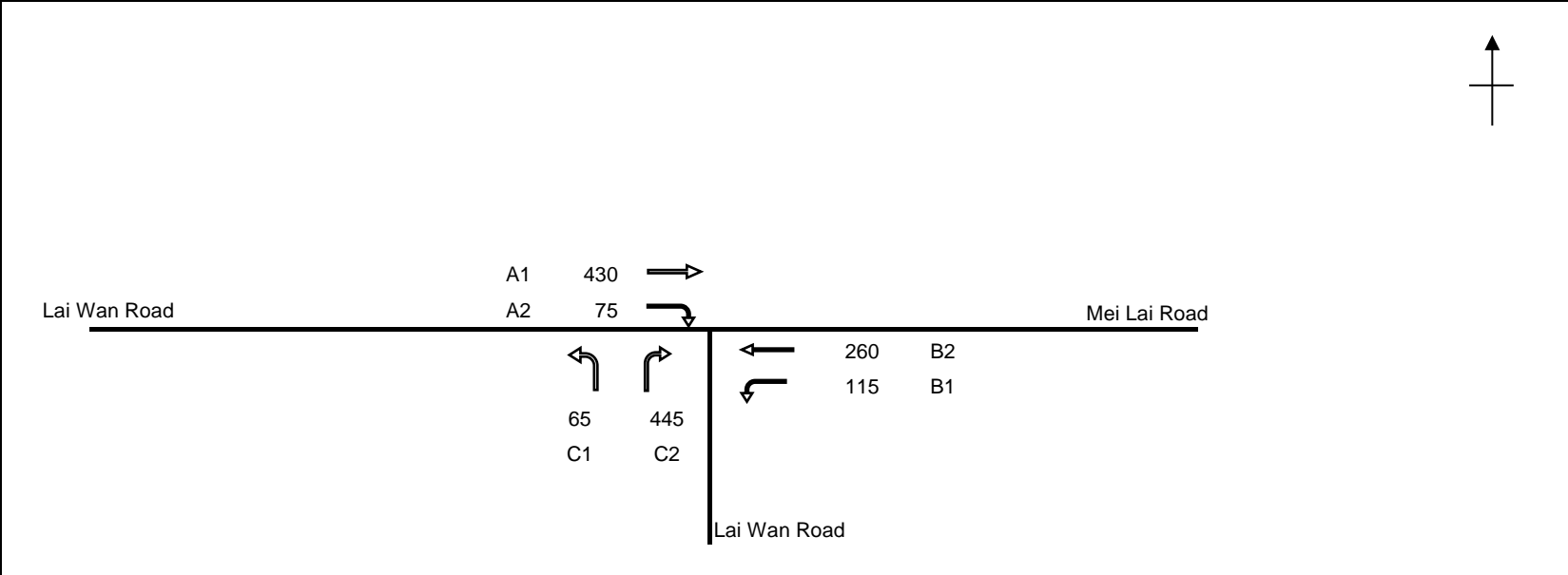
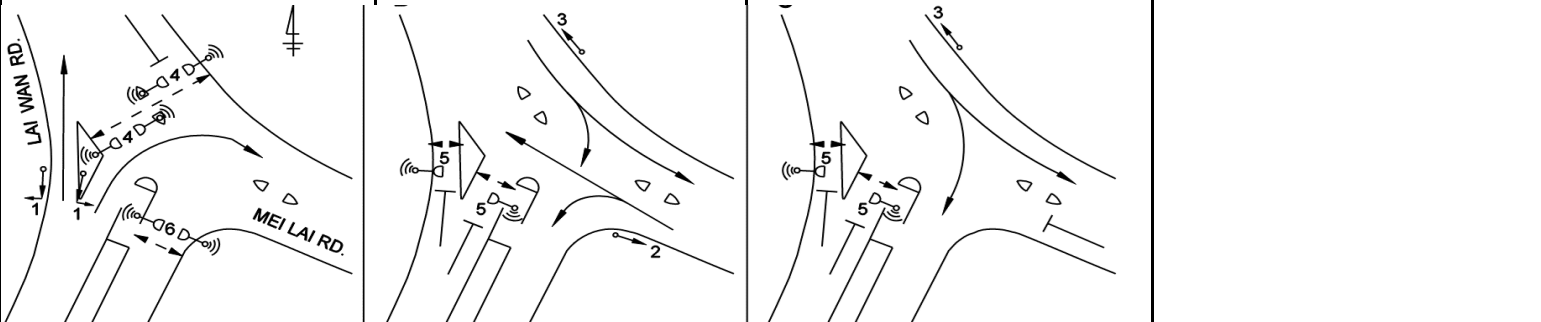
NOTE :   'O' - OPPOSING TRAFFIC       N - NEAR SIDE LANE       SG - STEADY GREEN       FG - FLASHING GREEN                 PEDESTRIAN WALKING SPEED = 0.9m/s                 QUEUING LENGTH = AVERAGE QUEUE \* 6m



## PROPOSED JUNCTION IMPROVEMENT

| OVE ARUP & PARTNERS  |                       |                |               |                 |             |           |   | TRAFFIC SIGNAL CALCULATION |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|--|-----------------------|----------------|---------------|-----------------|-------------|-----------|---|----------------------------|--------------------------|-------|---------------|------------|------------------|--------------------------------|-----------------|---|-------------------------|-------------------------|---------|-----------|-------|------------------|---------------|-------------------------|-------------------|-------------|------------------------------------|-------------|----|--------------------------|------|---------|--------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|---|-----------|-------|-------------------|---------------|------------------------|-------------------|------------|------|----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|-----|--|--|-----|------|------|-------|------|------|-------|-------|----|----|-------|----|----|---|---------|----|------|----|---------|--|------|---|---------|-----|------|------|------|-------|------|------|-------|--|----|----|-------|----|----|---|------|----|---|--|--|--|------|--|-----|--|-----|------|------|--|--|------|-------|--|----|----|-------|----|----|---|------|----|---|--|--|---|------|--|-----|--|-----|------|------|--|--|------|-------|---------|
| S16 Application for Proposed Development at Kau Wa Keng  |                       |                |               |                 |             |           |   | PROJECT NO: 299277-02      |                          |       |               |            |                  |                                |                 | Junction No. J3   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Lai King Hill Road / Kwai Chung Interchange  |                       |                |               | J3_INT_C_IMP_PM |             |           |   | DATE : 21-Jan-25           |                          |       |               | FILENAME : |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|    |                       |                |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>3</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.624</td></tr> <tr> <td>Loss time</td><td>L =</td><td>12 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>2198 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 61.2 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 31.9 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.810</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 29.7 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 39.2 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.900</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 30 %</td></tr> </table> |                         |                         |         |           |       |                  |               | No. of stages per cycle | N =               | 3           | No. of stage using for calculation | N =         | 3  | Cycle time               | C =  | 120 sec | Sum(y) | Y =              | 0.624                          | Loss time       | L =               | 12 sec                  | Total Flow              | = | 2198 pcu  | Co    | = (1.5*L+5)/(1-Y) | = 61.2 sec    | Cm                     | = L/(1-Y)         | = 31.9 sec | Yult | =  | 0.810 | R.C.ult | = (Yult-Y)/Y*100% | = 29.7 % | Cp | = 0.9*L/(0.9-Y) | = 39.2 sec | Ymax | = 1-L/C | = 0.900 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 30 % |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| No. of stages per cycle  | N =                   | 3              |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| No. of stage using for calculation   | N =                   | 3              |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Cycle time   | C =                   | 120 sec        |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Sum(y)   | Y =                   | 0.624          |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Loss time  | L =                   | 12 sec         |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Total Flow   | =                     | 2198 pcu       |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Co   | = (1.5*L+5)/(1-Y)     | = 61.2 sec     |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Cm   | = L/(1-Y)             | = 31.9 sec     |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Yult   | =                     | 0.810          |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 29.7 %       |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Cp   | = 0.9*L/(0.9-Y)       | = 39.2 sec     |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Ymax   | = 1-L/C               | = 0.900        |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 30 %         |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| <table> <tr> <td rowspan="5">Pedestrian Phase</td><td colspan="2">P</td><td colspan="3"></td><td colspan="3">Y</td><td colspan="3">Z2</td><td colspan="2"></td></tr> <tr> <td colspan="2">X2</td><td colspan="3">Q</td><td colspan="3">S</td><td colspan="3">Z1</td><td colspan="2"></td></tr> <tr> <td colspan="2">X1</td><td colspan="3">R</td><td colspan="3"></td><td colspan="3"></td><td colspan="2"></td></tr> <tr> <td colspan="2"></td><td colspan="3"></td><td colspan="3"></td><td colspan="3"></td><td colspan="2"></td></tr> <tr> <td colspan="2"></td><td colspan="3"></td><td colspan="3"></td><td colspan="3"></td><td colspan="2"></td></tr> <tr> <td colspan="2">STAGE 1</td><td>INT=</td><td>5</td><td colspan="2">STAGE 2</td><td>INT=</td><td>5</td><td colspan="2">STAGE 3</td><td>INT=</td><td>5</td><td colspan="2"></td></tr> </table>  |                       |                |               |                 |             |           |   |                            |                          |       |               |            |                  | Pedestrian Phase               | P               |   |                         |                         |         | Y         |       |                  | Z2            |                         |                   |             |                                    | X2          |    | Q                        |      |         | S      |                  |                                | Z1              |                   |                         |                         |   | X1        |       | R                 |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   | STAGE 1 |    | INT= | 5  | STAGE 2 |  | INT= | 5 | STAGE 3 |     | INT= | 5    |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| Pedestrian Phase   | P                     |                |               |                 |             | Y         |   |                            | Z2                       |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|  | X2                    |                | Q             |                 |             | S         |   |                            | Z1                       |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|  | X1                    |                | R             |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|  |                       |                |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|  |                       |                |               |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| STAGE 1  |                       | INT=           | 5             | STAGE 2         |             | INT=      | 5 | STAGE 3                    |                          | INT=  | 5             |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| <table> <tr> <th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr> <tr> <th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr> <tr> <td>A1</td><td>1</td><td>3.75</td><td>X1</td><td>1</td><td>15</td><td></td><td>N</td><td>1990</td><td>350</td><td></td><td></td><td>350</td><td>1.00</td><td>1809</td><td></td><td></td><td>1809</td><td>0.193</td><td></td><td rowspan="4">12</td><td>33</td><td>41</td><td>0.566</td><td>46</td></tr> <tr> <td>C1</td><td>1</td><td>3.50</td><td>X2</td><td>1</td><td>18</td><td></td><td>N</td><td>1965</td><td>305</td><td></td><td></td><td>305</td><td>1.00</td><td>1814</td><td>4.10%</td><td>-172</td><td>1642</td><td>0.186</td><td>0.238</td><td>32</td><td>41</td><td>0.544</td><td>40</td></tr> <tr> <td>C2</td><td>1</td><td>3.50</td><td>X2</td><td>1</td><td>25</td><td></td><td></td><td>2105</td><td></td><td></td><td>432</td><td>432</td><td>1.00</td><td>1986</td><td>4.10%</td><td>-172</td><td>1814</td><td>0.238</td><td></td><td>41</td><td>41</td><td>0.697</td><td>57</td></tr> <tr> <td>A2</td><td>3</td><td>3.75</td><td>Z1</td><td>1</td><td></td><td></td><td></td><td>2130</td><td></td><td>361</td><td></td><td>361</td><td>0.00</td><td>2130</td><td></td><td></td><td>2130</td><td>0.169</td><td></td><td>29</td><td>31</td><td>0.656</td><td>54</td></tr> <tr> <td>B1</td><td>3</td><td>3.30</td><td>Z2</td><td>1</td><td></td><td></td><td>N</td><td>1945</td><td></td><td>350</td><td></td><td>350</td><td>0.00</td><td>1945</td><td></td><td></td><td>1945</td><td>0.180</td><td>0.180&lt;/</td></tr></table> | Move-ment             | Stage          | Lane Width m. | Phase           | No. of lane | Radius m. | O | N                          | Straight-Ahead Sat. Flow | Flow  |               |            | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient %   | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y       | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. | Left pcu/h  | Straight pcu/h                     | Right pcu/h | A1 | 1                        | 3.75 | X1      | 1      | 15               |                                | N               | 1990              | 350                     |                         |   | 350       | 1.00  | 1809              |               |                        | 1809              | 0.193      |      | 12 | 33    | 41      | 0.566             | 46       | C1 | 1               | 3.50       | X2   | 1       | 18      |         | N                     | 1965   | 305 |  |  | 305 | 1.00 | 1814 | 4.10% | -172 | 1642 | 0.186 | 0.238 | 32 | 41 | 0.544 | 40 | C2 | 1 | 3.50    | X2 | 1    | 25 |         |  | 2105 |   |         | 432 | 432  | 1.00 | 1986 | 4.10% | -172 | 1814 | 0.238 |  | 41 | 41 | 0.697 | 57 | A2 | 3 | 3.75 | Z1 | 1 |  |  |  | 2130 |  | 361 |  | 361 | 0.00 | 2130 |  |  | 2130 | 0.169 |  | 29 | 31 | 0.656 | 54 | B1 | 3 | 3.30 | Z2 | 1 |  |  | N | 1945 |  | 350 |  | 350 | 0.00 | 1945 |  |  | 1945 | 0.180 | 0.180</ |
| Move-ment  |                       |                |               |                 |             |           |   |                            |                          | Stage | Lane Width m. | Phase      |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   | No. of lane | Radius m.                          | O           | N  | Straight-Ahead Sat. Flow | Flow |         |        | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y | Greater y | L sec | g (required) sec  | g (input) sec | Degree of Saturation X | Queuing Length m. |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
|  | Left pcu/h            | Straight pcu/h | Right pcu/h   |                 |             |           |   |                            |                          |       |               |            |                  |                                |                 |   |                         |                         |         |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| A1   | 1                     | 3.75           | X1            | 1               | 15          |           | N | 1990                       | 350                      |       |               | 350        | 1.00             | 1809                           |                 |   | 1809                    | 0.193                   |         | 12        | 33    | 41               | 0.566         | 46                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| C1   | 1                     | 3.50           | X2            | 1               | 18          |           | N | 1965                       | 305                      |       |               | 305        | 1.00             | 1814                           | 4.10%           | -172  | 1642                    | 0.186                   | 0.238   |           | 32    | 41               | 0.544         | 40                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| C2   | 1                     | 3.50           | X2            | 1               | 25          |           |   | 2105                       |                          |       | 432           | 432        | 1.00             | 1986                           | 4.10%           | -172  | 1814                    | 0.238                   |         |           | 41    | 41               | 0.697         | 57                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| A2   | 3                     | 3.75           | Z1            | 1               |             |           |   | 2130                       |                          | 361   |               | 361        | 0.00             | 2130                           |                 |   | 2130                    | 0.169                   |         |           | 29    | 31               | 0.656         | 54                      |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |
| B1   | 3                     | 3.30           | Z2            | 1               |             |           | N | 1945                       |                          | 350   |               | 350        | 0.00             | 1945                           |                 |   | 1945                    | 0.180                   | 0.180</ |           |       |                  |               |                         |                   |             |                                    |             |    |                          |      |         |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |      |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |     |  |  |     |      |      |       |      |      |       |       |    |    |       |    |    |   |         |    |      |    |         |  |      |   |         |     |      |      |      |       |      |      |       |  |    |    |       |    |    |   |      |    |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |    |    |       |    |    |   |      |    |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |         |

## J4 YEAR 2024 AM TRAFFIC FLOW

| OVE ARUP & PARTNERS   |                       |                         |       |             |                         |           |      | TRAFFIC SIGNAL CALCULATION |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|-----------|------|----------------------------|------------|----------------|-------------|---|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------------|-----------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|---------|--------|-------|-------|-----------|-------|--------|------------|-----|----------|----|-------------------|------------|----|-----------|------------|------|-----|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng                             |                       |                         |       |             |                         |           |      |                            |            |                |             | PROJECT NO: 299277-02   |                                |                 | Junction No. J4   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Lai Wan Road / Mei Lai Road   |                       |                         |       |             |                         | J4_OBS_AM |      |                            |            |                |             | DATE : 21-Jan-25  |                                |                 | FILENAME :        |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
|   |                       |                         |       |             |                         |           |      |                            |            |                |             | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.271</td></tr> <tr> <td>Loss time</td><td>L =</td><td>10 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1390 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 27.4 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 13.7 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.825</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 204.5 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 14.3 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.917</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 204 %</td></tr> </table> |                                |                 |                   |                         |                         |       |           |       |                  |               |                        | No. of stages per cycle | N =       | 3                       | No. of stage using for calculation | N = | 2                       | Cycle time | C = | 120 sec | Sum(y) | Y =   | 0.271 | Loss time | L =   | 10 sec | Total Flow | =   | 1390 pcu | Co | = (1.5*L+5)/(1-Y) | = 27.4 sec | Cm | = L/(1-Y) | = 13.7 sec | Yult | =   | 0.825 | R.C.ult | = (Yult-Y)/Y*100% | = 204.5 % | Cp | = 0.9*L/(0.9-Y) | = 14.3 sec | Ymax | = 1-L/C | = 0.917 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 204 % |   |   |    |
| No. of stages per cycle   | N =                   | 3                       |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| No. of stage using for calculation  | N =                   | 2                       |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Cycle time  | C =                   | 120 sec                 |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Sum(y)  | Y =                   | 0.271                   |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Loss time   | L =                   | 10 sec                  |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Total Flow  | =                     | 1390 pcu                |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 27.4 sec              |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Cm  | = L/(1-Y)             | = 13.7 sec              |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Yult  | =                     | 0.825                   |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 204.5 %               |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 14.3 sec              |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Ymax  | = 1-L/C               | = 0.917                 |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 204 %                 |       |             |                         |           |      |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
|  |                       |                         |       |             |                         |           |      |                            |            |                |             | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Dp</td><td>9.6</td><td>11</td><td>2</td><td>9</td><td>50</td><td>2</td><td>9</td><td>OK</td></tr> <tr> <td>Ep</td><td>7.3</td><td>5</td><td>1</td><td>8</td><td>50</td><td>1</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>7.3</td><td>5</td><td>7</td><td>8</td><td>46</td><td>7</td><td>8</td><td>OK</td></tr> </table>  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        | Pedestrian Phase        | Width (m) | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check   | SG     | Delay | FG    | SG        | Delay | FG     | Dp         | 9.6 | 11       | 2  | 9                 | 50         | 2  | 9         | OK         | Ep   | 7.3 | 5     | 1       | 8                 | 50        | 1  | 8               | OK         | Fp   | 7.3     | 5       | 7       | 8                     | 46      | 7 | 8 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |           |      | Check                      |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
|   |                       | SG                      | Delay | FG          | SG                      | Delay     | FG   |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Dp  | 9.6                   | 11                      | 2     | 9           | 50                      | 2         | 9    | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Ep  | 7.3                   | 5                       | 1     | 8           | 50                      | 1         | 8    | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Fp  | 7.3                   | 5                       | 7     | 8           | 46                      | 7         | 8    | OK                         |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| STAGE 1   | INT= 7                | STAGE 2                 | INT=  | STAGE 3     | INT= 5                  | STAGE 4   | INT= |                            |            |                |             |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O         | N    | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h  | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m.       |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
|   |                       |                         |       |             |                         |           |      |                            | Left pcu/h | Straight pcu/h | Right pcu/h |   |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| C1,C2   | 1                     | 3.30                    | C     | 1           | 16                      |           | N    | 1945                       | 65         |                | 177         | 242   | 1.00                           | 1778            |                   |                         | 1778                    | 0.136 | 0.136     | 10    | 55               | 55            | 0.297                  | 26                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| C2  | 1                     | 4.00                    | C     | 1           | 16                      |           | N    | 2155                       |            |                | 268         | 268   | 1.00                           | 1970            |                   |                         | 1970                    | 0.136 |           |       | 55               | 55            | 0.297                  | 29                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| B1,B2   | 2                     | 2.70                    | B     | 1           | 6                       |           | N    | 1885                       | 115        | 49             |             | 164   | 0.70                           | 1604            |                   |                         | 1604                    | 0.102 |           |       | 42               | 42            | 0.292                  | 21                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| B2  | 2                     | 3.00                    | B     | 1           |                         |           | N    | 2055                       |            | 211            |             | 211   | 0.00                           | 2055            |                   |                         | 2055                    | 0.103 |           |       | 42               | 42            | 0.293                  | 27                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| A1  | 2,3                   | 3.20                    | A     | 1           |                         |           | N    | 1935                       |            | 261            |             | 261   | 0.00                           | 1935            |                   |                         | 1935                    | 0.135 | 0.135     |       | 55               | 55            | 0.294                  | 28                      |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |
| A1,A2   | 2,3                   | 3.20                    | A     | 1           | 25                      | O         |      | 2075                       |            | 169            | 75          | 244   | 0.31                           | 1               |                   |                         |                         |       |           |       |                  |               |                        |                         |           |                         |                                    |     |                         |            |     |         |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |   |   |    |

## J4 YEAR 2024 PM TRAFFIC FLOW

OVE ARUP & PARTNERS

S16 Application for Proposed Development at Kau Wa Keng

J4\_OBS\_PM

PROJECT NO:  
DATE :

299277-02  
21-Jan-25

Junction No.  
FILENAME :

J4

Lai Wan Road / Mei Lai Road

No. of stages per cycle N =  
No. of stage using for calculation N =

3  
2

Cycle time C =  
Sum(y) Y =  
Loss time L =  
Total Flow =

120 sec  
0.211  
20 sec  
1200 pcu

Co = (1.5\*L+5)/(1-Y)  
Cm = L/(1-Y)  
Yult  
R.C. ult = (Yult-Y)/Y\*100%  
Cp = 0.9\*L/(0.9-Y)  
Ymax = 1-L/C  
  
R.C.(C)

= 44.4 sec  
= 25.4 sec  
= 0.750  
= 255.2 %  
= 26.1 sec  
= 0.833  
  
= 255 %

The main diagram shows an intersection where Lai Wan Road crosses over Mei Lai Road via two bridges. On the left side of Lai Wan Road, there are four lanes labeled A1 (left-turn), A2 (through/right-turn), C1 (left-turn), and C2 (right-turn). Traffic volumes are given as A1: 330, A2: 90, C1: 95, and C2: 330. On the right side of Mei Lai Road, there are two through lanes B1 and B2 with traffic volumes of 115 and 240 respectively. An arrow indicates north is towards the top-right.

| Pedestrian Phase | Width (m) | Green Time Required (s)<br>SG Delay FG | Green Time Provided (s)<br>SG Delay FG | Check |
|------------------|-----------|--|--|-------|
| Dp               | 9.6       | 11 2 9                                 | 49 2 9                                 | OK    |
| Ep               | 7.3       | 5 1 8                                  | 51 1 8                                 | OK    |
| Fp               | 7.3       | 5 7 8                                  | 45 7 8                                 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|          |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| C1,C2    | 1     | 3.30          | C     | 1           | 16        |   | N | 1945                     | 95         |                | 106         | 201              | 1.00                           | 1778            |                   |                         | 1778                    | 0.113 | 0.114     | 20    | 54               | 54            | 0.251                  | 22                |
| C2       | 1     | 4.00          | C     | 1           | 16        |   | N | 2155                     |            |                | 224         | 224              | 1.00                           | 1970            |                   |                         | 1970                    | 0.114 |           |       | 54               | 54            | 0.253                  | 25                |
| B1,B2    | 2     | 2.70          | B     | 1           | 6         |   | N | 1885                     | 115        | 40             |             | 155              | 0.74                           | 1590            |                   |                         | 1590                    | 0.097 | 0.097     |       | 46               | 46            | 0.254                  | 19                |
| B2       | 2     | 3.00          | B     | 1           |           |   |   | 2055                     |            | 200            |             | 200              | 0.00                           | 2055            |                   |                         | 2055                    | 0.097 |           |       | 46               | 46            | 0.254                  | 25                |
| A1       | 2,3   | 3.20          | A     | 1           |           |   | N | 1935                     |            | 217            |             | 217              | 0.00                           | 1935            |                   |                         | 1935                    | 0.112 |           |       | 53               | 53            | 0.254                  | 24                |
| A1,A2    | 2,3   | 3.20          | A     | 1           | 25        | O |   | 2075                     |            | 113            | 90          | 203              | 0.44                           | 1797            |                   |                         | 1797                    | 0.113 |           |       | 53               | 53            | 0.256                  | 23                |

NOTE :   'O' - OPPOSING TRAFFIC                  N - NEAR SIDE LANE                  SG - STEADY GREEN                  FG - FLASHING GREEN

PEDESTRIAN WALKING SPEED = 0.9m/s

QUEUING LENGTH = AVERAGE QUEUE \* 6m

## J4 YEAR 2035 AM TRAFFIC FLOW BASELINE SCENARIO

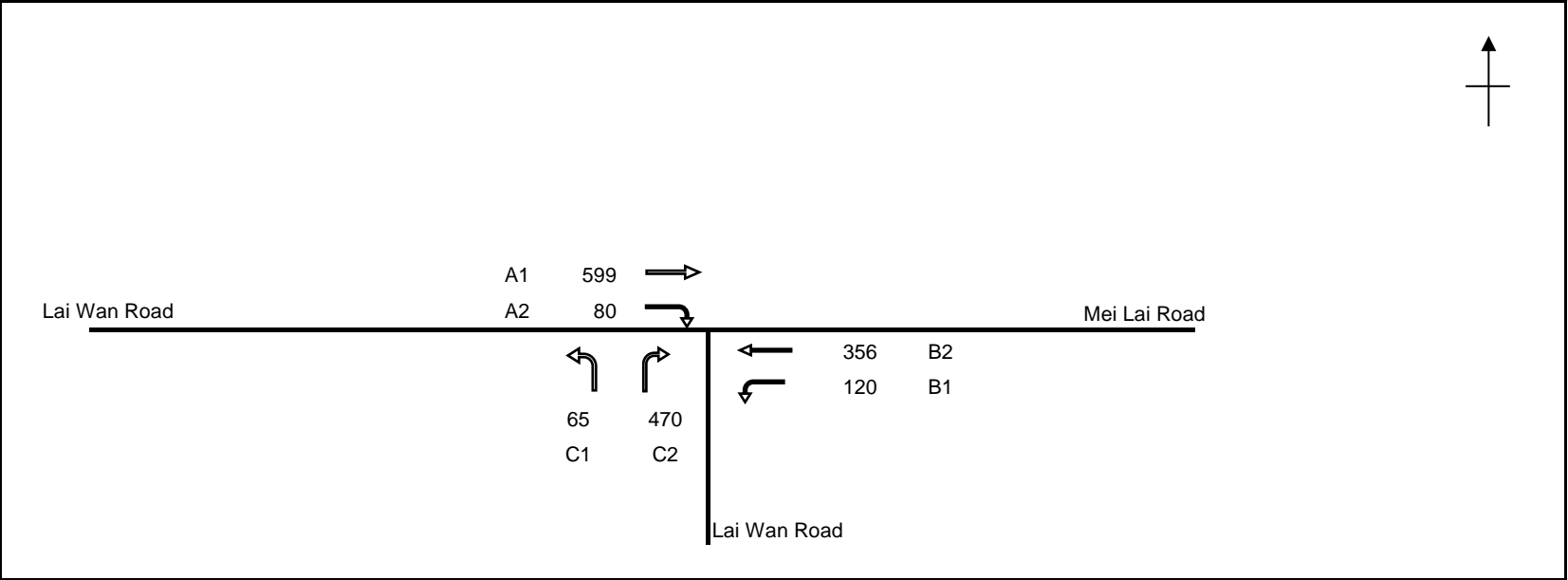
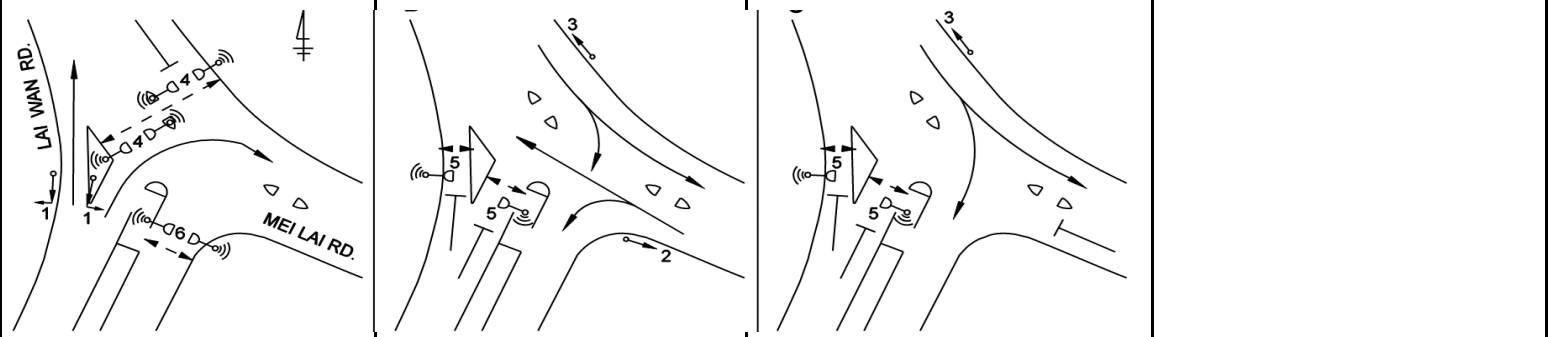
[illegible]

## J4 YEAR 2035 PM TRAFFIC FLOW BASELINE SCENARIO

[illegible]



## J4 YEAR 2035 AM TRAFFIC FLOW REFERENCE SCENARIO

| OVE ARUP & PARTNERS   |                       |                         |       |               |                         |       |    | TRAFFIC SIGNAL CALCULATION |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|---|-----------------------|-------------------------|-------|---------------|-------------------------|-------|----|----------------------------|--|-------------|--|-----------|--|--------------|---|--------------------------|--|------|--|------------|--|----------------|--|------------------|-----------|-------------------------|--|--------------------------------|-------------------------|-------------------------|-----|-------------------|------------------------------------|-------------------------|----|-------------------------|-----|---------|--------|-----------|-------|-----------|-----|------------------|------------|---------------|----------|------------------------|-------------------|-------------------|----|-----------|------------|------|---|-------|---------|-------------------|-----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|---------|
| S16 Application for Proposed Development at Kau Wa Keng                             |                       |                         |       |               |                         |       |    |                            |  | PROJECT NO: |  | 299277-02 |  | Junction No. |   | J4                       |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Lai Wan Road / Mei Lai Road   |                       |                         |       |               | J4_REF_AM               |       |    |                            |  | DATE :      |  | 21-Jan-25 |  | FILENAME :   |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       |                         |       |               |                         |       |    |                            |  |             |  |           |  |              | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>3</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>120 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.324</td></tr> <tr> <td>Loss time</td><td>L =</td><td>10 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1690 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 29.6 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 14.8 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.825</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 154.8 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 15.6 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.917</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 155 %</td></tr> </table> |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         | No. of stages per cycle | N = | 3                 | No. of stage using for calculation | N =                     | 2  | Cycle time              | C = | 120 sec | Sum(y) | Y =       | 0.324 | Loss time | L = | 10 sec           | Total Flow | =             | 1690 pcu | Co                     | = (1.5*L+5)/(1-Y) | = 29.6 sec        | Cm | = L/(1-Y) | = 14.8 sec | Yult | = | 0.825 | R.C.ult | = (Yult-Y)/Y*100% | = 154.8 % | Cp | = 0.9*L/(0.9-Y) | = 15.6 sec | Ymax | = 1-L/C | = 0.917 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 155 % |
| No. of stages per cycle   | N =                   | 3                       |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| No. of stage using for calculation  | N =                   | 2                       |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cycle time  | C =                   | 120 sec                 |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Sum(y)  | Y =                   | 0.324                   |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Loss time   | L =                   | 10 sec                  |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Total Flow  | =                     | 1690 pcu                |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Co  | = (1.5*L+5)/(1-Y)     | = 29.6 sec              |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cm  | = L/(1-Y)             | = 14.8 sec              |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Yult  | =                     | 0.825                   |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 154.8 %               |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Cp  | = 0.9*L/(0.9-Y)       | = 15.6 sec              |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ymax  | = 1-L/C               | = 0.917                 |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 155 %                 |       |               |                         |       |    |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|  |                       |                         |       |               |                         |       |    |                            |  |             |  |           |  |              | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <td></td><td></td><td>SG</td><td>Delay</td><td>FG</td><td>SG</td><td>Delay</td><td>FG</td><td></td></tr> <tr> <td>Dp</td><td>9.6</td><td>11</td><td>2</td><td>9</td><td>44</td><td>2</td><td>9</td><td>OK</td></tr> <tr> <td>Ep</td><td>7.3</td><td>5</td><td>1</td><td>8</td><td>56</td><td>1</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>7.3</td><td>5</td><td>7</td><td>8</td><td>40</td><td>7</td><td>8</td><td>OK</td></tr> </table>   |                          |  |      |  |            |  |                |  | Pedestrian Phase | Width (m) | Green Time Required (s) |  |                                | Green Time Provided (s) |                         |     | Check             |                                    |                         | SG | Delay                   | FG  | SG      | Delay  | FG        |       | Dp        | 9.6 | 11               | 2          | 9             | 44       | 2                      | 9                 | OK                | Ep | 7.3       | 5          | 1    | 8 | 56    | 1       | 8                 | OK        | Fp | 7.3             | 5          | 7    | 8       | 40      | 7       | 8                     | OK      |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |               | Green Time Provided (s) |       |    | Check                      |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
|   |                       | SG                      | Delay | FG            | SG                      | Delay | FG |                            |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Dp  | 9.6                   | 11                      | 2     | 9             | 44                      | 2     | 9  | OK                         |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Ep  | 7.3                   | 5                       | 1     | 8             | 56                      | 1     | 8  | OK                         |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Fp  | 7.3                   | 5                       | 7     | 8             | 40                      | 7     | 8  | OK                         |  |             |  |           |  |              |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| STAGE 1   |                       | INT= 7                  |       | STAGE 2       |                         | INT=  |    | STAGE 3                    |  | INT= 5      |  | STAGE 4   |  | INT=         |   |                          |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| Move-ment   |                       | Stage                   |       | Lane Width m. |                         | Phase |    | No. of lane                |  | Radius m.   |  | O         |  | N            |   | Straight-Ahead Sat. Flow |  | Flow |  | Left pcu/h |  | Straight pcu/h |  | Right pcu/h      |           | Total Flow pcu/h        |  | Proportion of Turning Vehicles |                         | Sat. Flow pcu/h         |     | Uphill Gradient % |                                    | Short lane Effect pcu/h |    | Revised Sat. Flow pcu/h |     | y       |        | Greater y |       | L sec     |     | g (required) sec |            | g (input) sec |          | Degree of Saturation X |                   | Queuing Length m. |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| C1,C2   |                       | 1                       |       | 3.30          |                         | C     |    | 1                          |  | 16          |  |           |  | N            |   | 1945                     |  |      |  | 65         |  |                |  | 189              |           | 254                     |  | 1.00                           |                         | 1778                    |     |                   |                                    | 1778                    |    | 0.143                   |     | 0.143   |        | 10        |       | 49        |     | 49               |            | 0.350         |          | 30                     |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |
| C2  |                       | 1                       |       | 4.00          |                         | C     |    | 1                          |  | 16          |  |           |  | N            |   | 2155                     |  |      |  |            |  |                |  |                  |           |                         |  |                                |                         |                         |     |                   |                                    |                         |    |                         |     |         |        |           |       |           |     |                  |            |               |          |                        |                   |                   |    |           |            |      |   |       |         |                   |           |    |                 |            |      |         |         |         |                       |         |

## J4 YEAR 2035 PM TRAFFIC FLOW REFERENCE SCENARIO

[illegible]

## J4 YEAR 2035 AM TRAFFIC FLOW

OVE ARUP & PARTNERS
TRAFFIC SIGNAL CALCULATION

S16 Application for Proposed Development at Kau Wa Keng

PROJECT NO:

299277-02

Junction No.

J4

Lai Wan Road / Mei Lai Road

J4\_DES\_AM

DATE :

21-Jan-25

FILENAME :

↑

A1    632 →  
A2     80 ↘  
  
← 65      470  
C1       C2  
  
Lai Wan Road                  Mei Lai Road

No. of stages per cycle N = 3

No. of stage using for calculation N = 2

Cycle time C = 120 sec

Sum(y) Y = 0.332

Loss time L = 10 sec

Total Flow = 1744 pcu

Co = (1.5\*L+5)/(1-Y) = 30.0 sec

Cm = L/(1-Y) = 15.0 sec

Yult = 0.825

R.C. ult = (Yult-Y)/Y\*100% = 148.1 %

Cp = 0.9\*L/(0.9-Y) = 15.9 sec

Ymax = 1-L/C = 0.917

R.C.(C) = (0.9\*Ymax-Y)/Y\*100% = 148 %

STAGE 1 | INT= 7 | STAGE 2 | INT= | STAGE 3 | INT= 5 | STAGE 4 | INT=

| Pedestrian Phase | Width (m) | Green Time Required (s)<br>SG Delay FG |   |   | Green Time Provided (s)<br>SG Delay FG |   |   | Check |
|------------------|-----------|--|---|---|--|---|---|-------|
| Dp               | 9.6       | 11                                     | 2 | 9 | 42                                     | 2 | 9 | OK    |
| Ep               | 7.3       | 5                                      | 1 | 8 | 58                                     | 1 | 8 | OK    |
| Fp               | 7.3       | 5                                      | 7 | 8 | 38                                     | 7 | 8 | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow<br>Left Straight Right |     |     | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|-----------------------------|-----|-----|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| C1,C2    | 1     | 3.30          | C     | 1           | 16        |   | N | 1945                     | 65                          |     | 189 | 254              | 1.00                           | 1778            |                   |                         | 1778                    | 0.143 | 0.143     | 10    | 47               | 47            | 0.365                  | 31                |
| C2       | 1     | 4.00          | C     | 1           | 16        |   | N | 2155                     |                             |     | 281 | 281              | 1.00                           | 1970            |                   |                         | 1970                    | 0.143 |           |       | 47               | 47            | 0.364                  | 34                |
| B1,B2    | 2     | 2.70          | B     | 1           | 6         |   | N | 1885                     | 120                         | 102 |     | 222              | 0.54                           | 1661            |                   |                         | 1661                    | 0.134 |           |       | 44               | 44            | 0.365                  | 28                |
| B2       | 2     | 3.00          | B     | 1           |           |   | N | 2055                     |                             | 275 |     | 275              | 0.00                           | 2055            |                   |                         | 2055                    | 0.134 |           |       | 44               | 44            | 0.365                  | 35                |
| A1       | 2,3   | 3.20          | A     | 1           |           |   | N | 1935                     |                             | 367 |     | 367              | 0.00                           | 1935            |                   |                         | 1935                    | 0.190 | 0.190     |       | 63               | 63            | 0.361                  | 35                |
| A1,A2    | 2,3   | 3.20          | A     | 1           | 25        | O |   | 2075                     |                             | 265 | 80  | 345              | 0.23                           | 1820            |                   |                         | 1820                    | 0.190 |           |       | 63               | 63            | 0.361                  | 33                |

NOTE :    'O' - OPPOSING TRAFFIC    'N' - NEAR SIDE LANE    SG - STEADY GREEN    FG - FLASHING GREEN    PEDESTRIAN WALKING SPEED = 0.9m/s    QUEUING LENGTH = AVERAGE QUEUE \* 6m

## J4 YEAR 2035 PM TRAFFIC FLOW

S16 Application for Proposed Development at Kau Wa Keng

Lai Wan Road / Mei Lai Road

J4\_DES\_PM

PROJECT NO:

299277-02

Junction No.

J4

DATE :

21-Jan-25

FILENAME :

A1      428 →  
A2      95 ↘

← 355 B2  
↙ 120 B1

→ 345 C2  
← 100 C1

Lai Wan Road

Mei Lai Road

Lai Wan Road

No. of stages per cycle N = 3  
No. of stage using for calculation N = 2  
  
Cycle time C = 120 sec  
Sum(y) Y = 0.247  
Loss time L = 20 sec  
Total Flow = 1443 pcu  
  
Co = (1.5\*L+5)/(1-Y) = 46.5 sec  
Cm = L/(1-Y) = 26.6 sec  
Yult = 0.750  
R.C. ult = (Yult-Y)/Y\*100% = 203.5 %  
Cp = 0.9\*L/(0.9-Y) = 27.6 sec  
Ymax = 1-L/C = 0.833  
R.C.(C) = (0.9\*Ymax-Y)/Y\*100% = 203 %

STAGE 1

INT= 7

STAGE 2

INT=

STAGE 3

INT= 15

STAGE 4

INT=

Pedestrian Phase

Width (m)

Green Time Required (s)  
SG Delay FG

Green Time Provided (s)  
SG Delay FG

Check

Dp Ep Fp

9.6 7.3 7.3

11 5 5

2 1 7

9 8 8

43 57 39

2 1 7

9 8 8

OK OK OK

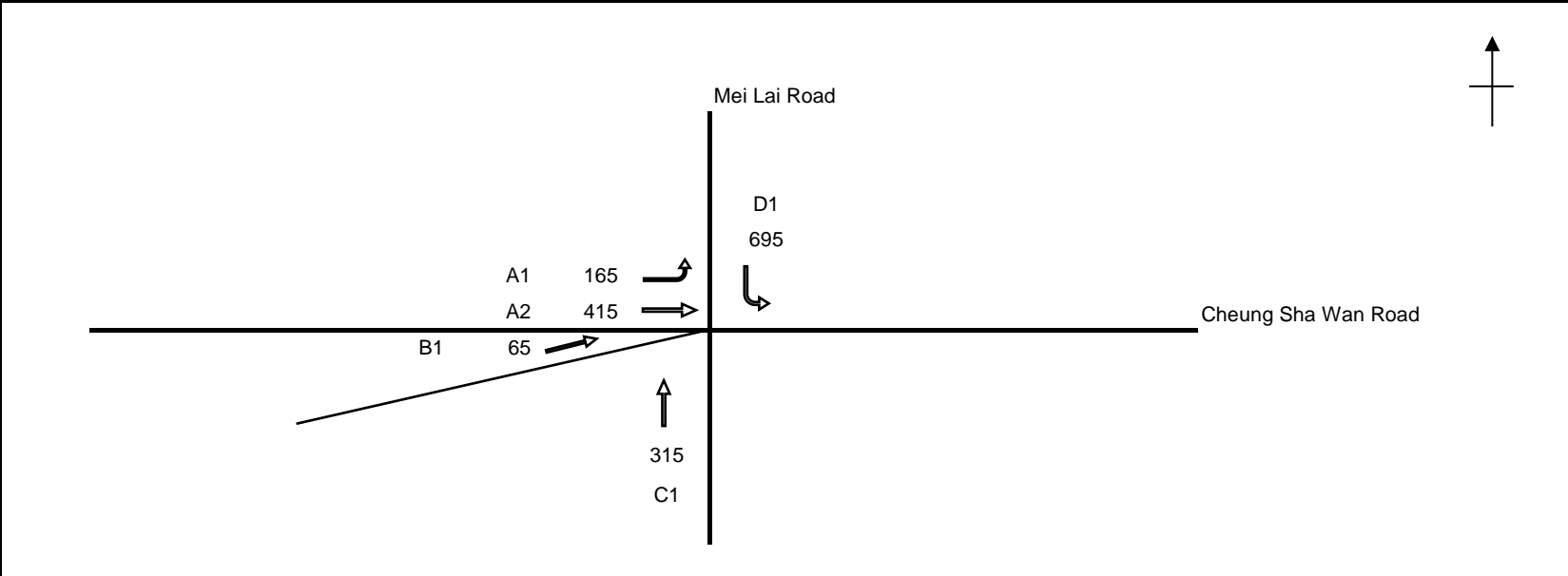
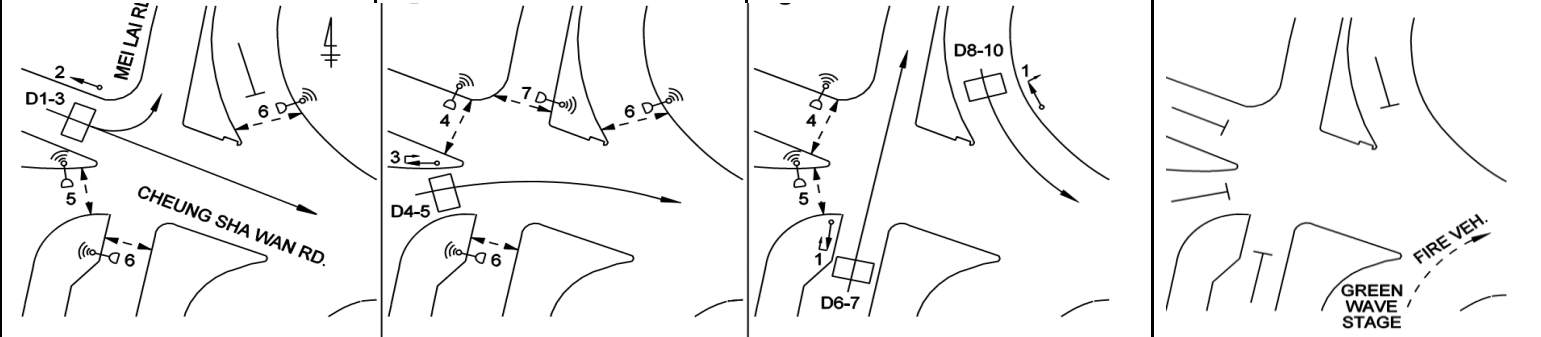
| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | <div>FlowLeftpcu/hStraightpcu/hRightpcu/h</div> | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|---|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
| C1,C2    | 1     | 3.30          | C     | 1           | 16        |   | N | 1945                     | 100   |                  | 111                            | 211             |                   | 1.00                    | 1778                    |       |           | 20    | 48               | 48            | 0.297                  | 25                |
| C2       | 1     | 4.00          | C     | 1           | 16        |   | N | 2155                     |   |                  | 234                            | 234             |                   | 1.00                    | 1970                    | 0.119 |           |       | 48               | 48            | 0.297                  | 28                |
| B1,B2    | 2     | 2.70          | B     | 1           | 6         |   | N | 1885                     | 120   | 92               |                                | 212             |                   | 0.57                    | 1651                    | 0.128 | 0.128     |       | 52               | 52            | 0.296                  | 24                |
| B2       | 2     | 3.00          | B     | 1           |           |   | N | 2055                     |   | 263              |                                | 263             |                   | 0.00                    | 2055                    | 0.128 |           |       | 52               | 52            | 0.295                  | 30                |
| A1       | 2,3   | 3.20          | A     | 1           |           |   | N | 1935                     |   | 270              |                                | 270             |                   | 0.00                    | 1935                    | 0.140 |           |       | 56               | 57            | 0.294                  | 28                |
| A1,A2    | 2,3   | 3.20          | A     | 1           | 25        | O |   | 2075                     |   | 158              | 95                             | 253             |                   | 0.38                    | 1804                    | 0.140 |           |       | 57               | 57            | 0.295                  | 27                |

NOTE : 'O' - OPPOSING TRAFFICN - NEAR SIDE LANESG - STEADY GREENFG - FLASHING GREENPEDESTRIAN WALKING SPEED = 0.9m/ssQUEUING LENGTH = AVERAGE QUEUE \* 6m

## J5 YEAR 2024 AM TRAFFIC FLOW

[illegible]

## J5 YEAR 2024 PM TRAFFIC FLOW

| OVE ARUP & PARTNERS   |                       |                         |               |       |                         |           |    | TRAFFIC SIGNAL CALCULATION |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
|---|-----------------------|-------------------------|---------------|-------|-------------------------|-----------|----|----------------------------|--------------------------|------------------|---------------|------------|------------------|--|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|------------------|-------------------------|-------------------------|-------------|------------------------------------|-------------------------|--------|--------------------------|-------|--------|--------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|---|-----------|-------|-------------------|---------------|------------------------|-------------------|------------|-------|----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|----|-----|---|-----|------|------|-----|-----|------|-------|---|---|----|----|-------|----|----|---|------|---|---|--|--|---|------|--|----|--|----|------|------|--|--|------|-------|--|--|---|----|-------|---|----|---|------|---|---|--|--|--|------|--|----|--|----|------|------|--|--|------|-------|--|--|---|----|-------|---|----|---|------|---|---|--|--|---|------|--|-----|--|-----|------|------|--|--|------|-------|-------|--|----|----|-------|----|----|---|------|---|---|--|--|--|------|--|-----|--|-----|------|------|--|--|------|-------|--|--|----|----|-------|----|----|---|------|---|---|----|--|---|------|-----|--|--|-----|------|------|--|--|------|-------|--|--|----|----|-------|----|----|---|------|---|
| S16 Application for Proposed Development at Kau Wa Keng   |                       |                         |               |       |                         |           |    |                            |                          |                  |               |            |                  | PROJECT NO: 299277-02  |                 | Junction No. J5   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Cheung Sha Wan Road / Mei Lai Road  |                       |                         |               |       | J5_OBS_PM               |           |    |                            |                          | DATE : 21-Jan-25 |               | FILENAME : |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
|   |                       |                         |               |       |                         |           |    |                            |                          |                  |               |            |                  | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>90 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.308</td></tr> <tr> <td>Loss time</td><td>L =</td><td>38 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1655 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 89.6 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 54.9 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.615</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 99.6 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 57.8 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.578</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 69 %</td></tr> </table> |                 |                   |                         |                         |       |           |       |                  |                  | No. of stages per cycle | N =                     | 4           | No. of stage using for calculation | N =                     | 2      | Cycle time               | C =   | 90 sec | Sum(y) | Y =              | 0.308                          | Loss time       | L =               | 38 sec                  | Total Flow              | = | 1655 pcu  | Co    | = (1.5*L+5)/(1-Y) | = 89.6 sec    | Cm                     | = L/(1-Y)         | = 54.9 sec | Yult  | =  | 0.615 | R.C.ult | = (Yult-Y)/Y*100% | = 99.6 % | Cp | = 0.9*L/(0.9-Y) | = 57.8 sec | Ymax | = 1-L/C | = 0.578 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 69 % |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| No. of stages per cycle   | N =                   | 4                       |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| No. of stage using for calculation  | N =                   | 2                       |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Cycle time  | C =                   | 90 sec                  |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Sum(y)  | Y =                   | 0.308                   |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Loss time   | L =                   | 38 sec                  |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Total Flow  | =                     | 1655 pcu                |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Co  | = (1.5*L+5)/(1-Y)     | = 89.6 sec              |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Cm  | = L/(1-Y)             | = 54.9 sec              |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Yult  | =                     | 0.615                   |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 99.6 %                |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Cp  | = 0.9*L/(0.9-Y)       | = 57.8 sec              |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Ymax  | = 1-L/C               | = 0.578                 |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 69 %                  |               |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
|    |                       |                         |               |       |                         |           |    |                            |                          |                  |               |            |                  | <table> <tr> <th>Pedestrian Phase</th><th>Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th>Check</th></tr> <tr> <th></th><th></th><th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th><th></th></tr> <tr> <td>Ep</td><td>4.9</td><td>5</td><td>3</td><td>8</td><td>39</td><td>3</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>4.5</td><td>5</td><td>3</td><td>6</td><td>53</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>4</td><td>5</td><td>5</td><td>12</td><td>33</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>Hp</td><td>3.7</td><td>5</td><td>7</td><td>9</td><td>5</td><td>7</td><td>9</td><td>OK</td></tr> </table>  |                 |                   |                         |                         |       |           |       |                  | Pedestrian Phase | Width (m)               | Green Time Required (s) |             |                                    | Green Time Provided (s) |        |                          | Check |        |        | SG               | Delay                          | FG              | SG                | Delay                   | FG                      |   | Ep        | 4.9   | 5                 | 3             | 8                      | 39                | 3          | 8     | OK | Fp    | 4.5     | 5                 | 3        | 6  | 53              | 3          | 6    | OK      | Gp      | 4       | 5                     | 5      | 12 | 33  | 5 | 12  | OK   | Hp   | 3.7 | 5   | 7    | 9     | 5 | 7 | 9  | OK |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |               |       | Green Time Provided (s) |           |    | Check                      |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
|   |                       | SG                      | Delay         | FG    | SG                      | Delay     | FG |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Ep  | 4.9                   | 5                       | 3             | 8     | 39                      | 3         | 8  | OK                         |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Fp  | 4.5                   | 5                       | 3             | 6     | 53                      | 3         | 6  | OK                         |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Gp  | 4                     | 5                       | 5             | 12    | 33                      | 5         | 12 | OK                         |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| Hp  | 3.7                   | 5                       | 7             | 9     | 5                       | 7         | 9  | OK                         |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| <table> <tr> <th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr> <tr> <th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr> <tr> <td>A1, A2</td><td>1</td><td>3.20</td><td>A</td><td>1</td><td>6.5</td><td></td><td>N</td><td>1935</td><td>165</td><td>66</td><td></td><td>231</td><td>0.71</td><td>1661</td><td></td><td></td><td>1661</td><td>0.139</td><td>0.140</td><td>28</td><td>23</td><td>24</td><td>0.521</td><td>25</td></tr> <tr> <td>A2</td><td>1</td><td>3.40</td><td>A</td><td>1</td><td></td><td></td><td></td><td>2095</td><td></td><td>349</td><td></td><td>349</td><td>0.00</td><td>2095</td><td></td><td>400</td><td>2495</td><td>0.140</td><td></td><td></td><td>24</td><td>24</td><td>0.525</td><td>38</td></tr> <tr> <td>B1</td><td>2</td><td>3.80</td><td>B</td><td>1</td><td></td><td></td><td>N</td><td>1995</td><td></td><td>31</td><td></td><td>31</td><td>0.00</td><td>1995</td><td></td><td></td><td>1995</td><td>0.016</td><td></td><td></td><td>3</td><td>14</td><td>0.100</td><td>4</td></tr> <tr> <td>B1</td><td>2</td><td>3.80</td><td>B</td><td>1</td><td></td><td></td><td></td><td>2135</td><td></td><td>34</td><td></td><td>34</td><td>0.00</td><td>2135</td><td></td><td></td><td>2135</td><td>0.016</td><td></td><td></td><td>3</td><td>14</td><td>0.102</td><td>4</td></tr> <tr> <td>C1</td><td>3</td><td>3.00</td><td>C</td><td>1</td><td></td><td></td><td>N</td><td>1915</td><td></td><td>151</td><td></td><td>151</td><td>0.00</td><td>1915</td><td></td><td></td><td>1915</td><td>0.079</td><td>0.168</td><td></td><td>13</td><td>28</td><td>0.253</td><td>16</td></tr> <tr> <td>C1</td><td>3</td><td>3.40</td><td>C</td><td>1</td><td></td><td></td><td></td><td>2095</td><td></td><td>164</td><td></td><td>164</td><td>0.00</td><td>2095</td><td></td><td></td><td>2095</td><td>0.078</td><td></td><td></td><td>13</td><td>28</td><td>0.252</td><td>17</td></tr> <tr> <td>D1</td><td>3</td><td>3.20</td><td>C</td><td>1</td><td>30</td><td></td><td>N</td><td>1935</td><td>310</td><td></td><td></td><td>310</td><td>1.00</td><td>1843</td><td></td><td></td><td>1843</td><td>0.168</td><td></td><td></td><td>28</td><td>28</td><td>0.541</td><td>32</td></tr> <tr> <td>D1</td><td>3</td><td>3.20</td><td>C</td>&lt;</tr></table> | Move-ment             | Stage                   | Lane Width m. | Phase | No. of lane             | Radius m. | O  | N                          | Straight-Ahead Sat. Flow | Flow             |               |            | Total Flow pcu/h | Proportion of Turning Vehicles   | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec    | Degree of Saturation X  | Queuing Length m.       | Left pcu/h  | Straight pcu/h                     | Right pcu/h             | A1, A2 | 1                        | 3.20  | A      | 1      | 6.5              |                                | N               | 1935              | 165                     | 66                      |   | 231       | 0.71  | 1661              |               |                        | 1661              | 0.139      | 0.140 | 28 | 23    | 24      | 0.521             | 25       | A2 | 1               | 3.40       | A    | 1       |         |         |                       | 2095   |    | 349 |   | 349 | 0.00 | 2095 |     | 400 | 2495 | 0.140 |   |   | 24 | 24 | 0.525 | 38 | B1 | 2 | 3.80 | B | 1 |  |  | N | 1995 |  | 31 |  | 31 | 0.00 | 1995 |  |  | 1995 | 0.016 |  |  | 3 | 14 | 0.100 | 4 | B1 | 2 | 3.80 | B | 1 |  |  |  | 2135 |  | 34 |  | 34 | 0.00 | 2135 |  |  | 2135 | 0.016 |  |  | 3 | 14 | 0.102 | 4 | C1 | 3 | 3.00 | C | 1 |  |  | N | 1915 |  | 151 |  | 151 | 0.00 | 1915 |  |  | 1915 | 0.079 | 0.168 |  | 13 | 28 | 0.253 | 16 | C1 | 3 | 3.40 | C | 1 |  |  |  | 2095 |  | 164 |  | 164 | 0.00 | 2095 |  |  | 2095 | 0.078 |  |  | 13 | 28 | 0.252 | 17 | D1 | 3 | 3.20 | C | 1 | 30 |  | N | 1935 | 310 |  |  | 310 | 1.00 | 1843 |  |  | 1843 | 0.168 |  |  | 28 | 28 | 0.541 | 32 | D1 | 3 | 3.20 | C |
| Move-ment   |                       |                         |               |       |                         |           |    |                            |                          | Stage            | Lane Width m. | Phase      |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         | No. of lane | Radius m.                          | O                       | N      | Straight-Ahead Sat. Flow | Flow  |        |        | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y | Greater y | L sec | g (required) sec  | g (input) sec | Degree of Saturation X | Queuing Length m. |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
|   | Left pcu/h            | Straight pcu/h          | Right pcu/h   |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| A1, A2  | 1                     | 3.20                    | A             | 1     | 6.5                     |           | N  | 1935                       | 165                      | 66               |               | 231        | 0.71             | 1661   |                 |                   | 1661                    | 0.139                   | 0.140 | 28        | 23    | 24               | 0.521            | 25                      |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| A2  | 1                     | 3.40                    | A             | 1     |                         |           |    | 2095                       |                          | 349              |               | 349        | 0.00             | 2095   |                 | 400               | 2495                    | 0.140                   |       |           | 24    | 24               | 0.525            | 38                      |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| B1  | 2                     | 3.80                    | B             | 1     |                         |           | N  | 1995                       |                          | 31               |               | 31         | 0.00             | 1995   |                 |                   | 1995                    | 0.016                   |       |           | 3     | 14               | 0.100            | 4                       |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| B1  | 2                     | 3.80                    | B             | 1     |                         |           |    | 2135                       |                          | 34               |               | 34         | 0.00             | 2135   |                 |                   | 2135                    | 0.016                   |       |           | 3     | 14               | 0.102            | 4                       |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| C1  | 3                     | 3.00                    | C             | 1     |                         |           | N  | 1915                       |                          | 151              |               | 151        | 0.00             | 1915   |                 |                   | 1915                    | 0.079                   | 0.168 |           | 13    | 28               | 0.253            | 16                      |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| C1  | 3                     | 3.40                    | C             | 1     |                         |           |    | 2095                       |                          | 164              |               | 164        | 0.00             | 2095   |                 |                   | 2095                    | 0.078                   |       |           | 13    | 28               | 0.252            | 17                      |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| D1  | 3                     | 3.20                    | C             | 1     | 30                      |           | N  | 1935                       | 310                      |                  |               | 310        | 1.00             | 1843   |                 |                   | 1843                    | 0.168                   |       |           | 28    | 28               | 0.541            | 32                      |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |
| D1  | 3                     | 3.20                    | C             |       |                         |           |    |                            |                          |                  |               |            |                  |  |                 |                   |                         |                         |       |           |       |                  |                  |                         |                         |             |                                    |                         |        |                          |       |        |        |                  |                                |                 |                   |                         |                         |   |           |       |                   |               |                        |                   |            |       |    |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |    |     |   |     |      |      |     |     |      |       |   |   |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |



## J5 YEAR 2035 AM TRAFFIC FLOW BASELINE SCENARIO

| OVE ARUP & PARTNERS  |                       |                         |               |            |                         |           |    | TRAFFIC SIGNAL CALCULATION |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
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| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |               |            |                         |           |    |                            |                          |            |               |       |                  | PROJECT NO: 299277-02  |                 | Junction No. J5   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Cheung Sha Wan Road / Mei Lai Road   |                       |                         |               | J5_BASE_AM |                         |           |    | DATE : 21-Jan-25           |                          | FILENAME : |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
|  |                       |                         |               |            |                         |           |    |                            |                          |            |               |       |                  | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>90 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.334</td></tr> <tr> <td>Loss time</td><td>L =</td><td>38 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1655 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 93.1 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 57.1 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.615</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 84.0 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 60.5 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.578</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 56 %</td></tr> </table> |                 |                   |                         |                         |       |           |       |                  | No. of stages per cycle | N =                    | 4                       | No. of stage using for calculation | N =            | 2                       | Cycle time | C =                      | 90 sec | Sum(y) | Y =   | 0.334            | Loss time                      | L =             | 38 sec            | Total Flow              | =                       | 1655 pcu | Co        | = (1.5*L+5)/(1-Y) | = 93.1 sec       | Cm            | = L/(1-Y)              | = 57.1 sec        | Yult  | =     | 0.615 | R.C.ult | = (Yult-Y)/Y*100% | = 84.0 % | Cp | = 0.9*L/(0.9-Y) | = 60.5 sec | Ymax | = 1-L/C | = 0.578 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 56 % |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| No. of stages per cycle  | N =                   | 4                       |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| No. of stage using for calculation   | N =                   | 2                       |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Cycle time   | C =                   | 90 sec                  |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Sum(y)   | Y =                   | 0.334                   |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Loss time  | L =                   | 38 sec                  |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Total Flow   | =                     | 1655 pcu                |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Co   | = (1.5*L+5)/(1-Y)     | = 93.1 sec              |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Cm   | = L/(1-Y)             | = 57.1 sec              |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Yult   | =                     | 0.615                   |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 84.0 %                |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Cp   | = 0.9*L/(0.9-Y)       | = 60.5 sec              |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Ymax   | = 1-L/C               | = 0.578                 |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 56 %                  |               |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
|  |                       |                         |               |            |                         |           |    |                            |                          |            |               |       |                  | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>4.9</td><td>5</td><td>3</td><td>8</td><td>43</td><td>3</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>4.5</td><td>5</td><td>3</td><td>6</td><td>53</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>4</td><td>5</td><td>5</td><td>12</td><td>37</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>Hp</td><td>3.7</td><td>5</td><td>7</td><td>9</td><td>5</td><td>7</td><td>9</td><td>OK</td></tr> </table>   |                 |                   |                         |                         |       |           |       |                  | Pedestrian Phase        | Width (m)              | Green Time Required (s) |                                    |                | Green Time Provided (s) |            |                          | Check  | SG     | Delay | FG               | SG                             | Delay           | FG                | Ep                      | 4.9                     | 5        | 3         | 8                 | 43               | 3             | 8                      | OK                | Fp    | 4.5   | 5     | 3       | 6                 | 53       | 3  | 6               | OK         | Gp   | 4       | 5       | 5       | 12                    | 37     | 5    | 12 | OK  | Hp | 3.7 | 5    | 7    | 9 | 5   | 7    | 9     | OK |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |               |            | Green Time Provided (s) |           |    | Check                      |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
|  |                       | SG                      | Delay         | FG         | SG                      | Delay     | FG |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Ep   | 4.9                   | 5                       | 3             | 8          | 43                      | 3         | 8  | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Fp   | 4.5                   | 5                       | 3             | 6          | 53                      | 3         | 6  | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Gp   | 4                     | 5                       | 5             | 12         | 37                      | 5         | 12 | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| Hp   | 3.7                   | 5                       | 7             | 9          | 5                       | 7         | 9  | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| <table> <tr> <th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr> <tr> <th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr> <tr> <td>A1, A2</td><td>1</td><td>3.20</td><td>A</td><td>1</td><td>6.5</td><td></td><td>N</td><td>1935</td><td>190</td><td>12</td><td></td><td>202</td><td>0.94</td><td>1590</td><td></td><td></td><td>1590</td><td>0.127</td><td>0.127</td><td>28</td><td>20</td><td>20</td><td>0.572</td><td>24</td></tr> <tr> <td>A2</td><td>1</td><td>3.40</td><td>A</td><td>1</td><td></td><td></td><td></td><td>2095</td><td></td><td>318</td><td></td><td>318</td><td>0.00</td><td>2095</td><td></td><td>400</td><td>2495</td><td>0.127</td><td></td><td></td><td>20</td><td>20</td><td>0.574</td><td>37</td></tr> <tr> <td>B1</td><td>2</td><td>3.80</td><td>B</td><td>1</td><td></td><td></td><td>N</td><td>1995</td><td></td><td>22</td><td></td><td>22</td><td>0.00</td><td>1995</td><td></td><td></td><td>1995</td><td>0.011</td><td></td><td></td><td>2</td><td>14</td><td>0.071</td><td>3</td></tr> <tr> <td>B1</td><td>2</td><td>3.80</td><td>B</td><td>1</td><td></td><td></td><td></td><td>2135</td><td></td><td>23</td><td></td><td>23</td><td>0.00</td><td>2135</td><td></td><td></td><td>2135</td><td>0.011</td><td></td><td></td><td>2</td><td>14</td><td>0.069</td><td>3</td></tr> <tr> <td>C1</td><td>3</td><td>3.00</td><td>C</td><td>1</td><td></td><td></td><td>N</td><td>1915</td><td></td><td>112</td><td></td><td>112</td><td>0.00</td><td>1915</td><td></td><td></td><td>1915</td><td>0.058</td><td>0.207</td><td></td><td>9</td><td>32</td><td>0.164</td><td>11</td></tr> <tr> <td>C1</td><td>3</td><td>3.40</td><td>C</td><td>1</td><td></td><td></td><td></td><td>2095</td><td></td><td>123</td><td></td><td>123</td><td>0.00</td><td>2095</td><td></td><td></td><td>2095</td><td>0.059</td><td></td><td></td><td>9</td><td>32</td><td>0.165</td><td>12</td></tr> <tr> <td>D1</td><td>3</td><td>3.20</td><td>C</td><td>1</td><td>30</td><td></td><td>N</td><td>1935</td><td>380</td><td></td><td></td><td>380</td><td>1.00</td><td>1843</td><td></td><td></td><td>1843</td><td>0.206</td><td></td><td></td><td>32</td><td>32</td><td>0.</td></tr></table> | Move-ment             | Stage                   | Lane Width m. | Phase      | No. of lane             | Radius m. | O  | N                          | Straight-Ahead Sat. Flow | Flow       |               |       | Total Flow pcu/h | Proportion of Turning Vehicles   | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec           | Degree of Saturation X | Queuing Length m.       | Left pcu/h                         | Straight pcu/h | Right pcu/h             | A1, A2     | 1                        | 3.20   | A      | 1     | 6.5              |                                | N               | 1935              | 190                     | 12                      |          | 202       | 0.94              | 1590             |               |                        | 1590              | 0.127 | 0.127 | 28    | 20      | 20                | 0.572    | 24 | A2              | 1          | 3.40 | A       | 1       |         |                       |        | 2095 |    | 318 |    | 318 | 0.00 | 2095 |   | 400 | 2495 | 0.127 |    |  | 20 | 20 | 0.574 | 37 | B1 | 2 | 3.80 | B | 1 |  |  | N | 1995 |  | 22 |  | 22 | 0.00 | 1995 |  |  | 1995 | 0.011 |  |  | 2 | 14 | 0.071 | 3 | B1 | 2 | 3.80 | B | 1 |  |  |  | 2135 |  | 23 |  | 23 | 0.00 | 2135 |  |  | 2135 | 0.011 |  |  | 2 | 14 | 0.069 | 3 | C1 | 3 | 3.00 | C | 1 |  |  | N | 1915 |  | 112 |  | 112 | 0.00 | 1915 |  |  | 1915 | 0.058 | 0.207 |  | 9 | 32 | 0.164 | 11 | C1 | 3 | 3.40 | C | 1 |  |  |  | 2095 |  | 123 |  | 123 | 0.00 | 2095 |  |  | 2095 | 0.059 |  |  | 9 | 32 | 0.165 | 12 | D1 | 3 | 3.20 | C | 1 | 30 |  | N | 1935 | 380 |  |  | 380 | 1.00 | 1843 |  |  | 1843 | 0.206 |  |  | 32 | 32 | 0. |
| Move-ment  |                       |                         |               |            |                         |           |    |                            |                          | Stage      | Lane Width m. | Phase |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         | No. of lane                        | Radius m.      | O                       | N          | Straight-Ahead Sat. Flow | Flow   |        |       | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y        | Greater y | L sec             | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
|  | Left pcu/h            | Straight pcu/h          | Right pcu/h   |            |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| A1, A2   | 1                     | 3.20                    | A             | 1          | 6.5                     |           | N  | 1935                       | 190                      | 12         |               | 202   | 0.94             | 1590   |                 |                   | 1590                    | 0.127                   | 0.127 | 28        | 20    | 20               | 0.572                   | 24                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| A2   | 1                     | 3.40                    | A             | 1          |                         |           |    | 2095                       |                          | 318        |               | 318   | 0.00             | 2095   |                 | 400               | 2495                    | 0.127                   |       |           | 20    | 20               | 0.574                   | 37                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| B1   | 2                     | 3.80                    | B             | 1          |                         |           | N  | 1995                       |                          | 22         |               | 22    | 0.00             | 1995   |                 |                   | 1995                    | 0.011                   |       |           | 2     | 14               | 0.071                   | 3                      |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| B1   | 2                     | 3.80                    | B             | 1          |                         |           |    | 2135                       |                          | 23         |               | 23    | 0.00             | 2135   |                 |                   | 2135                    | 0.011                   |       |           | 2     | 14               | 0.069                   | 3                      |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| C1   | 3                     | 3.00                    | C             | 1          |                         |           | N  | 1915                       |                          | 112        |               | 112   | 0.00             | 1915   |                 |                   | 1915                    | 0.058                   | 0.207 |           | 9     | 32               | 0.164                   | 11                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| C1   | 3                     | 3.40                    | C             | 1          |                         |           |    | 2095                       |                          | 123        |               | 123   | 0.00             | 2095   |                 |                   | 2095                    | 0.059                   |       |           | 9     | 32               | 0.165                   | 12                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |
| D1   | 3                     | 3.20                    | C             | 1          | 30                      |           | N  | 1935                       | 380                      |            |               | 380   | 1.00             | 1843   |                 |                   | 1843                    | 0.206                   |       |           | 32    | 32               | 0.                      |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |  |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |   |    |       |    |    |   |      |   |   |  |  |  |      |  |     |  |     |      |      |  |  |      |       |  |  |   |    |       |    |    |   |      |   |   |    |  |   |      |     |  |  |     |      |      |  |  |      |       |  |  |    |    |    |

## J5 YEAR 2035 PM TRAFFIC FLOW BASELINE SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |       |             |                         |         |    | TRAFFIC SIGNAL CALCULATION |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|---------|----|----------------------------|------------|----------------|-------------|------------------|--------------------------------|--|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|-------------------------|-------------------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|--------|--------|-------|-------|-----------|-------|--------|------------|-----|----------|----|-------------------|------------|----|-----------|------------|------|-----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|---|----|----|----|-----|---|---|---|---|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |       |             |                         |         |    |                            |            |                |             |                  |                                | PROJECT NO: 299277-02  |                   | Junction No. J5         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cheung Sha Wan Road / Mei Lai Road                      |                       |                         |       | J5_BASE_PM  |                         |         |    | DATE : 21-Jan-25           |            | FILENAME :     |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                         |       |             |                         |         |    |                            |            |                |             |                  |                                | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>90 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.326</td></tr> <tr> <td>Loss time</td><td>L =</td><td>38 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1750 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 91.9 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 56.4 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.615</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 88.8 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 59.5 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.578</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 60 %</td></tr> </table> |                   |                         |                         |       |           |       |                  |               | No. of stages per cycle | N =               | 4                       | No. of stage using for calculation | N = | 2                       | Cycle time | C = | 90 sec | Sum(y) | Y =   | 0.326 | Loss time | L =   | 38 sec | Total Flow | =   | 1750 pcu | Co | = (1.5*L+5)/(1-Y) | = 91.9 sec | Cm | = L/(1-Y) | = 56.4 sec | Yult | =   | 0.615 | R.C.ult | = (Yult-Y)/Y*100% | = 88.8 % | Cp | = 0.9*L/(0.9-Y) | = 59.5 sec | Ymax | = 1-L/C | = 0.578 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 60 % |   |    |    |    |     |   |   |   |   |   |   |    |
| No. of stages per cycle                                 | N =                   | 4                       |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| No. of stage using for calculation                      | N =                   | 2                       |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cycle time  | C =                   | 90 sec                  |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Sum(y)  | Y =                   | 0.326                   |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Loss time   | L =                   | 38 sec                  |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Total Flow  | =                     | 1750 pcu                |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 91.9 sec              |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cm  | = L/(1-Y)             | = 56.4 sec              |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Yult  | =                     | 0.615                   |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 88.8 %                |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 59.5 sec              |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Ymax  | = 1-L/C               | = 0.578                 |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 60 %                  |       |             |                         |         |    |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                         |       |             |                         |         |    |                            |            |                |             |                  |                                | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>4.9</td><td>5</td><td>3</td><td>8</td><td>39</td><td>3</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>4.5</td><td>5</td><td>3</td><td>6</td><td>53</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>4</td><td>5</td><td>5</td><td>12</td><td>33</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>Hp</td><td>3.7</td><td>5</td><td>7</td><td>9</td><td>5</td><td>7</td><td>9</td><td>OK</td></tr> </table>   |                   |                         |                         |       |           |       |                  |               | Pedestrian Phase        | Width (m)         | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check  | SG     | Delay | FG    | SG        | Delay | FG     | Ep         | 4.9 | 5        | 3  | 8                 | 39         | 3  | 8         | OK         | Fp   | 4.5 | 5     | 3       | 6                 | 53       | 3  | 6               | OK         | Gp   | 4       | 5       | 5       | 12                    | 33     | 5 | 12 | OK | Hp | 3.7 | 5 | 7 | 9 | 5 | 7 | 9 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |         |    | Check                      |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       | SG                      | Delay | FG          | SG                      | Delay   | FG |                            |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Ep  | 4.9                   | 5                       | 3     | 8           | 39                      | 3       | 8  | OK                         |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Fp  | 4.5                   | 5                       | 3     | 6           | 53                      | 3       | 6  | OK                         |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Gp  | 4                     | 5                       | 5     | 12          | 33                      | 5       | 12 | OK                         |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Hp  | 3.7                   | 5                       | 7     | 9           | 5                       | 7       | 9  | OK                         |            |                |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| STAGE 1   |                       | INT= 7                  |       | STAGE 2     |                         | INT= 13 |    | STAGE 3                    |            | INT= 5         |             | STAGE 4          |                                | INT= 5   |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O       | N  | Straight-Ahead Sat. Flow   | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h  | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                         |       |             |                         |         |    |                            | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| A1, A2  | 1                     | 3.20                    | A     | 1           | 6.5                     |         | N  | 1935                       | 175        | 71             |             | 246              | 0.71                           | 1662   |                   |                         | 1662                    | 0.148 | 0.148     | 28    | 24               | 24            | 0.555                   | 27                |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| A2  | 1                     | 3.40                    | A     | 1           |                         |         | N  | 2095                       |            | 369            |             | 369              | 0.00                           | 2095   |                   | 400                     | 2495                    | 0.148 |           |       | 24               | 24            | 0.555                   | 41                |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| B1  | 2                     | 3.80                    | B     | 1           |                         |         | N  | 1995                       |            | 33             |             | 33               | 0.00                           | 1995   |                   |                         | 1995                    | 0.017 |           |       | 3                | 14            | 0.106                   | 4                 |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| B1  | 2                     | 3.80                    | B     | 1           |                         |         | N  | 2135                       |            | 37             |             | 37               | 0.00                           | 2135   |                   |                         | 2135                    | 0.017 |           |       | 3                | 14            | 0.111                   | 5                 |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| C1  | 3                     | 3.00                    | C     | 1           |                         |         | N  | 1915                       |            | 157            |             | 157              | 0.00                           | 1915   |                   |                         | 1915                    | 0.082 | 0.178     |       | 13               | 28            | 0.264                   | 1                 |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |

## J5 YEAR 2035 AM TRAFFIC FLOW REFERENCE SCENARIO

[illegible]

## J5 YEAR 2035 PM TRAFFIC FLOW REFERENCE SCENARIO

| OVE ARUP & PARTNERS                                     |                       |                         |       |             |                         |         |    | TRAFFIC SIGNAL CALCULATION |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|---|-----------------------|-------------------------|-------|-------------|-------------------------|---------|----|----------------------------|------------|------------------|-------------|------------------|--------------------------------|--|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|-------------------------|-------------------|-------------------------|------------------------------------|-----|-------------------------|------------|-----|--------|--------|-------|-------|-----------|-------|--------|------------|-----|----------|----|-------------------|------------|----|-----------|------------|------|-----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|---|----|----|----|-----|---|---|---|---|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                         |       |             |                         |         |    |                            |            |                  |             |                  |                                | PROJECT NO: 299277-02  |                   | Junction No. J5         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cheung Sha Wan Road / Mei Lai Road                      |                       |                         |       |             | J5_REF_PM               |         |    |                            |            | DATE : 21-Jan-25 |             | FILENAME :       |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                         |       |             |                         |         |    |                            |            |                  |             |                  |                                | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>90 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.346</td></tr> <tr> <td>Loss time</td><td>L =</td><td>38 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1893 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 94.9 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 58.1 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.615</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 77.5 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 61.8 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.578</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 50 %</td></tr> </table> |                   |                         |                         |       |           |       |                  |               | No. of stages per cycle | N =               | 4                       | No. of stage using for calculation | N = | 2                       | Cycle time | C = | 90 sec | Sum(y) | Y =   | 0.346 | Loss time | L =   | 38 sec | Total Flow | =   | 1893 pcu | Co | = (1.5*L+5)/(1-Y) | = 94.9 sec | Cm | = L/(1-Y) | = 58.1 sec | Yult | =   | 0.615 | R.C.ult | = (Yult-Y)/Y*100% | = 77.5 % | Cp | = 0.9*L/(0.9-Y) | = 61.8 sec | Ymax | = 1-L/C | = 0.578 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 50 % |   |    |    |    |     |   |   |   |   |   |   |    |
| No. of stages per cycle                                 | N =                   | 4                       |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| No. of stage using for calculation                      | N =                   | 2                       |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cycle time  | C =                   | 90 sec                  |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Sum(y)  | Y =                   | 0.346                   |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Loss time   | L =                   | 38 sec                  |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Total Flow  | =                     | 1893 pcu                |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 94.9 sec              |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cm  | = L/(1-Y)             | = 58.1 sec              |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Yult  | =                     | 0.615                   |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 77.5 %                |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 61.8 sec              |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Ymax  | = 1-L/C               | = 0.578                 |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 50 %                  |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                         |       |             |                         |         |    |                            |            |                  |             |                  |                                | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>4.9</td><td>5</td><td>3</td><td>8</td><td>40</td><td>3</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>4.5</td><td>5</td><td>3</td><td>6</td><td>53</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>4</td><td>5</td><td>5</td><td>12</td><td>34</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>Hp</td><td>3.7</td><td>5</td><td>7</td><td>9</td><td>5</td><td>7</td><td>9</td><td>OK</td></tr> </table>   |                   |                         |                         |       |           |       |                  |               | Pedestrian Phase        | Width (m)         | Green Time Required (s) |                                    |     | Green Time Provided (s) |            |     | Check  | SG     | Delay | FG    | SG        | Delay | FG     | Ep         | 4.9 | 5        | 3  | 8                 | 40         | 3  | 8         | OK         | Fp   | 4.5 | 5     | 3       | 6                 | 53       | 3  | 6               | OK         | Gp   | 4       | 5       | 5       | 12                    | 34     | 5 | 12 | OK | Hp | 3.7 | 5 | 7 | 9 | 5 | 7 | 9 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s) |       |             | Green Time Provided (s) |         |    | Check                      |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       | SG                      | Delay | FG          | SG                      | Delay   | FG |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Ep  | 4.9                   | 5                       | 3     | 8           | 40                      | 3       | 8  | OK                         |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Fp  | 4.5                   | 5                       | 3     | 6           | 53                      | 3       | 6  | OK                         |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Gp  | 4                     | 5                       | 5     | 12          | 34                      | 5       | 12 | OK                         |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Hp  | 3.7                   | 5                       | 7     | 9           | 5                       | 7       | 9  | OK                         |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| STAGE 1   |                       | INT= 7                  |       | STAGE 2     |                         | INT= 13 |    | STAGE 3                    |            | INT= 5           |             | STAGE 4          |                                | INT= 5   |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Move-ment   | Stage                 | Lane Width m.           | Phase | No. of lane | Radius m.               | O       | N  | Straight-Ahead Sat. Flow   | Flow       |                  |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h  | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X  | Queuing Length m. |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                         |       |             |                         |         |    |                            | Left pcu/h | Straight pcu/h   | Right pcu/h |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| A1, A2  | 1                     | 3.20                    | A     | 1           | 6.5                     |         | N  | 1935                       | 195        | 57               |             | 252              | 0.77                           | 1642   |                   |                         | 1642                    | 0.153 | 0.154     | 28    | 23               | 23            | 0.601                   | 28                |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| A2  | 1                     | 3.40                    | A     | 1           |                         |         | N  | 2095                       |            | 383              |             | 383              | 0.00                           | 2095   |                   | 400                     | 2495                    | 0.154 |           |       | 23               | 23            | 0.601                   | 43                |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| B1  | 2                     | 3.80                    | B     | 1           |                         |         | N  | 1995                       |            | 33               |             | 33               | 0.00                           | 1995   |                   |                         | 1995                    | 0.017 |           |       | 2                | 14            | 0.106                   | 4                 |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| B1  | 2                     | 3.80                    | B     | 1           |                         |         | N  | 2135                       |            | 37               |             | 37               | 0.00                           | 2135   |                   |                         | 2135                    | 0.017 |           |       | 3                | 14            | 0.111                   | 5                 |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| C1  | 3                     | 3.00                    | C     | 1           |                         |         | N  | 1915                       |            | 187              |             | 187              | 0.00                           | 1915   |                   |                         | 1915                    | 0.098 | 0.193     |       | 15               | 29            | 0.303                   | 19                |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| C1  | 3                     |                         |       |             |                         |         |    |                            |            |                  |             |                  |                                |  |                   |                         |                         |       |           |       |                  |               |                         |                   |                         |                                    |     |                         |            |     |        |        |       |       |           |       |        |            |     |          |    |                   |            |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |

## J5 YEAR 2035 AM TRAFFIC FLOW DESIGN SCENARIO

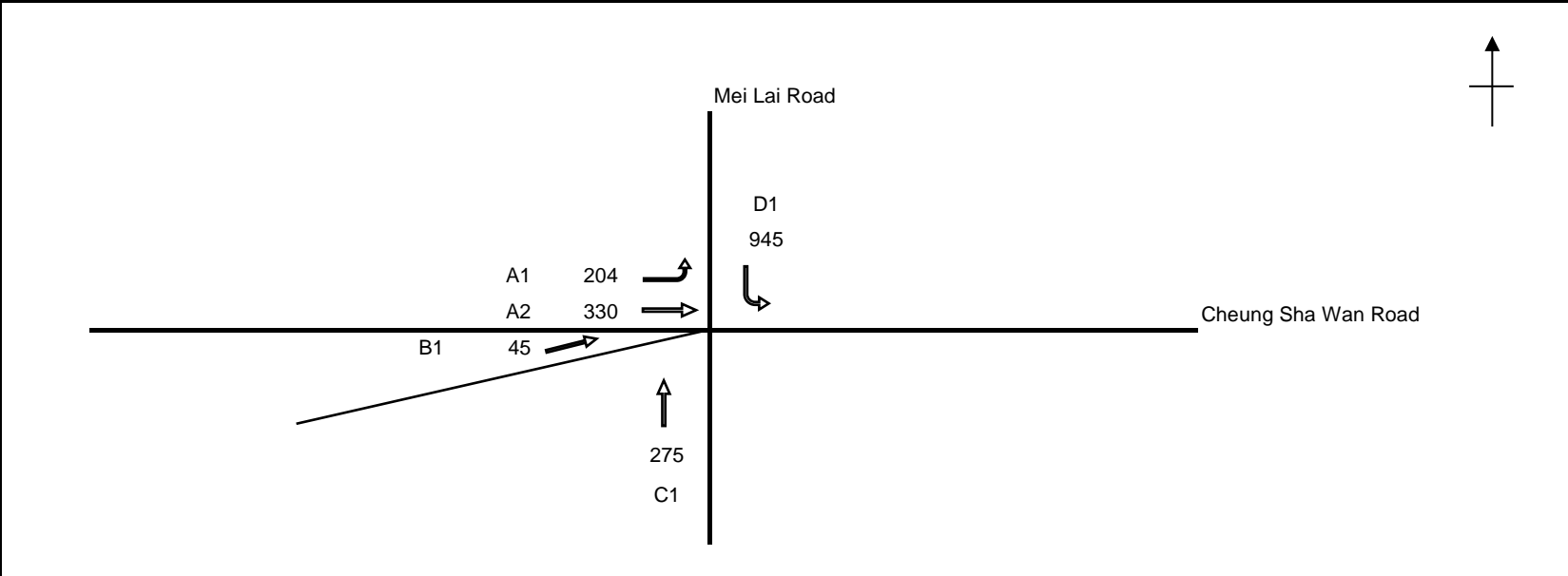
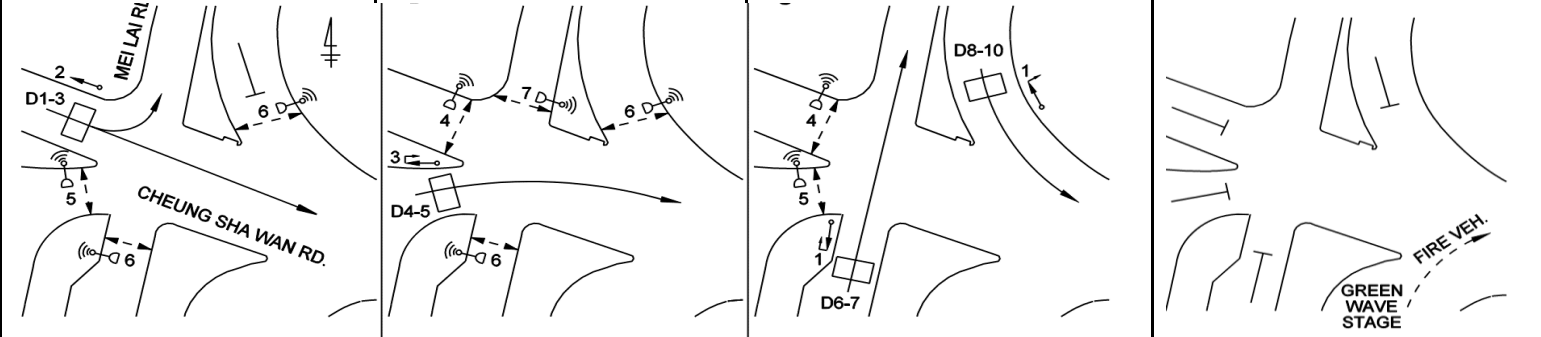
| OVE ARUP & PARTNERS                                     |                       | TRAFFIC SIGNAL CALCULATION |       |             |                         |         |    |                          |            |   |             | PROJECT NO: 299277-02 |                                | Junction No. J5 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|---|-----------------------|----------------------------|-------|-------------|-------------------------|---------|----|--------------------------|------------|---|-------------|-----------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------------------------|------------------------------------|-------|-------------------------|---------------|------------------------|-------------------|--------|-------|-------|-----------|-------|--------|------------|-----|----------|----|-------------------|-------------|----|-----------|------------|------|-----|-------|---------|-------------------|----------|----|-----------------|------------|------|---------|---------|---------|-----------------------|--------|---|----|----|----|-----|---|---|---|---|---|---|----|
| S16 Application for Proposed Development at Kau Wa Keng |                       |                            |       |             |                         |         |    |                          |            | DATE : 21-Jan-25  |             | FILENAME :            |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cheung Sha Wan Road / Mei Lai Road                      |                       |                            |       |             | J5_DES_AM               |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                            |       |             |                         |         |    |                          |            | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>90 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.389</td></tr> <tr> <td>Loss time</td><td>L =</td><td>38 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1944 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 101.5 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 62.2 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.615</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 58.1 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 66.9 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.578</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 34 %</td></tr> </table> |             |                       |                                |                 |                   | No. of stages per cycle | N =                     | 4                       | No. of stage using for calculation | N =   | 2                       | Cycle time    | C =                    | 90 sec            | Sum(y) | Y =   | 0.389 | Loss time | L =   | 38 sec | Total Flow | =   | 1944 pcu | Co | = (1.5*L+5)/(1-Y) | = 101.5 sec | Cm | = L/(1-Y) | = 62.2 sec | Yult | =   | 0.615 | R.C.ult | = (Yult-Y)/Y*100% | = 58.1 % | Cp | = 0.9*L/(0.9-Y) | = 66.9 sec | Ymax | = 1-L/C | = 0.578 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 34 % |   |    |    |    |     |   |   |   |   |   |   |    |
| No. of stages per cycle                                 | N =                   | 4                          |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| No. of stage using for calculation                      | N =                   | 2                          |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cycle time  | C =                   | 90 sec                     |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Sum(y)  | Y =                   | 0.389                      |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Loss time   | L =                   | 38 sec                     |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Total Flow  | =                     | 1944 pcu                   |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Co  | = (1.5*L+5)/(1-Y)     | = 101.5 sec                |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cm  | = L/(1-Y)             | = 62.2 sec                 |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Yult  | =                     | 0.615                      |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| R.C.ult   | = (Yult-Y)/Y*100%     | = 58.1 %                   |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Cp  | = 0.9*L/(0.9-Y)       | = 66.9 sec                 |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Ymax  | = 1-L/C               | = 0.578                    |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| R.C.(C)   | = (0.9*Ymax-Y)/Y*100% | = 34 %                     |       |             |                         |         |    |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                            |       |             |                         |         |    |                          |            | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>4.9</td><td>5</td><td>3</td><td>8</td><td>45</td><td>3</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>4.5</td><td>5</td><td>3</td><td>6</td><td>53</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>4</td><td>5</td><td>5</td><td>12</td><td>39</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>Hp</td><td>3.7</td><td>5</td><td>7</td><td>9</td><td>5</td><td>7</td><td>9</td><td>OK</td></tr> </table>  |             |                       |                                |                 |                   | Pedestrian Phase        | Width (m)               | Green Time Required (s) |                                    |       | Green Time Provided (s) |               |                        | Check             | SG     | Delay | FG    | SG        | Delay | FG     | Ep         | 4.9 | 5        | 3  | 8                 | 45          | 3  | 8         | OK         | Fp   | 4.5 | 5     | 3       | 6                 | 53       | 3  | 6               | OK         | Gp   | 4       | 5       | 5       | 12                    | 39     | 5 | 12 | OK | Hp | 3.7 | 5 | 7 | 9 | 5 | 7 | 9 | OK |
| Pedestrian Phase  | Width (m)             | Green Time Required (s)    |       |             | Green Time Provided (s) |         |    | Check                    |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       | SG                         | Delay | FG          | SG                      | Delay   | FG |                          |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Ep  | 4.9                   | 5                          | 3     | 8           | 45                      | 3       | 8  | OK                       |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Fp  | 4.5                   | 5                          | 3     | 6           | 53                      | 3       | 6  | OK                       |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Gp  | 4                     | 5                          | 5     | 12          | 39                      | 5       | 12 | OK                       |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Hp  | 3.7                   | 5                          | 7     | 9           | 5                       | 7       | 9  | OK                       |            |   |             |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| STAGE 1   |                       | INT= 7                     |       | STAGE 2     |                         | INT= 13 |    | STAGE 3                  |            | INT= 5  |             | STAGE 4               |                                | INT= 5          |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| Move-ment   | Stage                 | Lane Width m.              | Phase | No. of lane | Radius m.               | O       | N  | Straight-Ahead Sat. Flow | Flow       |   |             | Total Flow pcu/h      | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y                       | Greater y                          | L sec | g (required) sec        | g (input) sec | Degree of Saturation X | Queuing Length m. |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
|   |                       |                            |       |             |                         |         |    |                          | Left pcu/h | Straight pcu/h  | Right pcu/h |                       |                                |                 |                   |                         |                         |                         |                                    |       |                         |               |                        |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| A1, A2  | 1                     | 3.20                       | A     | 1           | 6.5                     |         | N  | 1935                     | 217        | 0   |             | 217                   | 1.00                           | 1572            |                   | 400                     | 1572                    | 0.138                   | 0.138                              | 28    | 18                      | 18            | 0.690                  | 26                |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| A2  | 1                     | 3.40                       | A     | 1           |                         |         |    | 2095                     |            | 330   |             | 330                   | 0.00                           | 2095            |                   |                         | 2495                    | 0.132                   |                                    |       | 18                      | 18            | 0.661                  | 40                |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| B1  | 2                     | 3.80                       | B     | 1           |                         |         | N  | 1995                     |            | 22  |             | 22                    | 0.00                           | 1995            |                   |                         | 1995                    | 0.011                   |                                    |       | 1                       | 14            | 0.071                  | 3                 |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| B1  | 2                     | 3.80                       | B     | 1           |                         |         |    | 2135                     |            | 23  |             | 23                    | 0.00                           | 2135            |                   |                         | 2135                    | 0.011                   |                                    |       | 1                       | 14            | 0.069                  | 3                 |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| C1  | 3                     | 3.00                       | C     | 1           |                         |         | N  | 1915                     |            | 150   |             | 150                   | 0.00                           | 1915            |                   |                         | 1915                    | 0.078                   |                                    |       | 10                      | 34            | 0.207                  | 14                |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| C1  | 3                     | 3.40                       | C     | 1           |                         |         |    | 2095                     |            | 165   |             | 165                   | 0.00                           | 2095            |                   |                         | 2095                    | 0.079                   |                                    |       | 11                      | 34            | 0.208                  | 15                |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |
| D1  | 3                     | 3.20                       | C     | 1           | 30                      |         | N  | 1935                     | 461        |   |             | 461                   | 1.00                           | 1843            |                   | 320                     | 1843                    | 0.250                   |                                    |       | 33                      | 34            | 0.662                  |                   |        |       |       |           |       |        |            |     |          |    |                   |             |    |           |            |      |     |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |   |    |    |    |     |   |   |   |   |   |   |    |

## J5 YEAR 2035 PM TRAFFIC FLOW DESIGN SCENARIO

[illegible]



## J5 YEAR 2035 AM TRAFFIC FLOW INTERIM SCENARIO A

| OVE ARUP & PARTNERS  |                       |                         |               |             |                         |           |    | TRAFFIC SIGNAL CALCULATION |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
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| S16 Application for Proposed Development at Kau Wa Keng  |                       |                         |               |             |                         |           |    |                            |                          |            |               |       |                  | PROJECT NO: 299277-02  |                 | Junction No. J5   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Cheung Sha Wan Road / Mei Lai Road   |                       |                         |               | J5_INT_A_AM |                         |           |    | DATE : 21-Jan-25           |                          | FILENAME : |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
|    |                       |                         |               |             |                         |           |    |                            |                          |            |               |       |                  | <table> <tr> <td>No. of stages per cycle</td><td>N =</td><td>4</td></tr> <tr> <td>No. of stage using for calculation</td><td>N =</td><td>2</td></tr> <tr> <td>Cycle time</td><td>C =</td><td>90 sec</td></tr> <tr> <td>Sum(y)</td><td>Y =</td><td>0.360</td></tr> <tr> <td>Loss time</td><td>L =</td><td>38 sec</td></tr> <tr> <td>Total Flow</td><td>=</td><td>1799 pcu</td></tr> <tr> <td>Co</td><td>= (1.5*L+5)/(1-Y)</td><td>= 96.8 sec</td></tr> <tr> <td>Cm</td><td>= L/(1-Y)</td><td>= 59.4 sec</td></tr> <tr> <td>Yult</td><td>=</td><td>0.615</td></tr> <tr> <td>R.C.ult</td><td>= (Yult-Y)/Y*100%</td><td>= 70.9 %</td></tr> <tr> <td>Cp</td><td>= 0.9*L/(0.9-Y)</td><td>= 63.3 sec</td></tr> <tr> <td>Ymax</td><td>= 1-L/C</td><td>= 0.578</td></tr> <tr> <td>R.C.(C)</td><td>= (0.9*Ymax-Y)/Y*100%</td><td>= 45 %</td></tr> </table> |                 |                   |                         |                         |       |           |       |                  | No. of stages per cycle | N =                    | 4                       | No. of stage using for calculation | N =            | 2                       | Cycle time | C =                      | 90 sec | Sum(y) | Y =   | 0.360            | Loss time                      | L =             | 38 sec            | Total Flow              | =                       | 1799 pcu | Co        | = (1.5*L+5)/(1-Y) | = 96.8 sec       | Cm            | = L/(1-Y)              | = 59.4 sec        | Yult  | =     | 0.615 | R.C.ult | = (Yult-Y)/Y*100% | = 70.9 % | Cp | = 0.9*L/(0.9-Y) | = 63.3 sec | Ymax | = 1-L/C | = 0.578 | R.C.(C) | = (0.9*Ymax-Y)/Y*100% | = 45 % |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| No. of stages per cycle  | N =                   | 4                       |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| No. of stage using for calculation   | N =                   | 2                       |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Cycle time   | C =                   | 90 sec                  |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Sum(y)   | Y =                   | 0.360                   |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Loss time  | L =                   | 38 sec                  |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Total Flow   | =                     | 1799 pcu                |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Co   | = (1.5*L+5)/(1-Y)     | = 96.8 sec              |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Cm   | = L/(1-Y)             | = 59.4 sec              |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Yult   | =                     | 0.615                   |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| R.C.ult  | = (Yult-Y)/Y*100%     | = 70.9 %                |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Cp   | = 0.9*L/(0.9-Y)       | = 63.3 sec              |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Ymax   | = 1-L/C               | = 0.578                 |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| R.C.(C)  | = (0.9*Ymax-Y)/Y*100% | = 45 %                  |               |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
|   |                       |                         |               |             |                         |           |    |                            |                          |            |               |       |                  | <table> <tr> <th rowspan="2">Pedestrian Phase</th><th rowspan="2">Width (m)</th><th colspan="3">Green Time Required (s)</th><th colspan="3">Green Time Provided (s)</th><th rowspan="2">Check</th></tr> <tr> <th>SG</th><th>Delay</th><th>FG</th><th>SG</th><th>Delay</th><th>FG</th></tr> <tr> <td>Ep</td><td>4.9</td><td>5</td><td>3</td><td>8</td><td>44</td><td>3</td><td>8</td><td>OK</td></tr> <tr> <td>Fp</td><td>4.5</td><td>5</td><td>3</td><td>6</td><td>53</td><td>3</td><td>6</td><td>OK</td></tr> <tr> <td>Gp</td><td>4</td><td>5</td><td>5</td><td>12</td><td>38</td><td>5</td><td>12</td><td>OK</td></tr> <tr> <td>Hp</td><td>3.7</td><td>5</td><td>7</td><td>9</td><td>5</td><td>7</td><td>9</td><td>OK</td></tr> </table>   |                 |                   |                         |                         |       |           |       |                  | Pedestrian Phase        | Width (m)              | Green Time Required (s) |                                    |                | Green Time Provided (s) |            |                          | Check  | SG     | Delay | FG               | SG                             | Delay           | FG                | Ep                      | 4.9                     | 5        | 3         | 8                 | 44               | 3             | 8                      | OK                | Fp    | 4.5   | 5     | 3       | 6                 | 53       | 3  | 6               | OK         | Gp   | 4       | 5       | 5       | 12                    | 38     | 5    | 12 | OK  | Hp | 3.7 | 5    | 7    | 9 | 5   | 7    | 9     | OK |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Pedestrian Phase   | Width (m)             | Green Time Required (s) |               |             | Green Time Provided (s) |           |    | Check                      |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
|  |                       | SG                      | Delay         | FG          | SG                      | Delay     | FG |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Ep   | 4.9                   | 5                       | 3             | 8           | 44                      | 3         | 8  | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Fp   | 4.5                   | 5                       | 3             | 6           | 53                      | 3         | 6  | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Gp   | 4                     | 5                       | 5             | 12          | 38                      | 5         | 12 | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| Hp   | 3.7                   | 5                       | 7             | 9           | 5                       | 7         | 9  | OK                         |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| <table> <tr> <th rowspan="2">Move-ment</th><th rowspan="2">Stage</th><th rowspan="2">Lane Width m.</th><th rowspan="2">Phase</th><th rowspan="2">No. of lane</th><th rowspan="2">Radius m.</th><th rowspan="2">O</th><th rowspan="2">N</th><th rowspan="2">Straight-Ahead Sat. Flow</th><th colspan="3">Flow</th><th rowspan="2">Total Flow pcu/h</th><th rowspan="2">Proportion of Turning Vehicles</th><th rowspan="2">Sat. Flow pcu/h</th><th rowspan="2">Uphill Gradient %</th><th rowspan="2">Short lane Effect pcu/h</th><th rowspan="2">Revised Sat. Flow pcu/h</th><th rowspan="2">y</th><th rowspan="2">Greater y</th><th rowspan="2">L sec</th><th rowspan="2">g (required) sec</th><th rowspan="2">g (input) sec</th><th rowspan="2">Degree of Saturation X</th><th rowspan="2">Queuing Length m.</th></tr> <tr> <th>Left pcu/h</th><th>Straight pcu/h</th><th>Right pcu/h</th></tr> <tr> <td>A1, A2</td><td>1</td><td>3.20</td><td>A</td><td>1</td><td>6.5</td><td></td><td>N</td><td>1935</td><td>204</td><td>3</td><td></td><td>207</td><td>0.99</td><td>1576</td><td></td><td></td><td>1576</td><td>0.131</td><td>0.131</td><td>28</td><td>19</td><td>19</td><td>0.622</td><td>24</td></tr> <tr> <td>A2</td><td>1</td><td>3.40</td><td>A</td><td>1</td><td></td><td></td><td>N</td><td>2095</td><td></td><td>327</td><td></td><td>327</td><td>0.00</td><td>2095</td><td></td><td>400</td><td>2495</td><td>0.131</td><td></td><td></td><td>19</td><td>19</td><td>0.621</td><td>39</td></tr> <tr> <td>B1</td><td>2</td><td>3.80</td><td>B</td><td>1</td><td></td><td></td><td>N</td><td>1995</td><td></td><td>22</td><td></td><td>22</td><td>0.00</td><td>1995</td><td></td><td></td><td>1995</td><td>0.011</td><td></td><td></td><td>2</td><td>14</td><td>0.071</td><td>3</td></tr> <tr> <td>B1</td><td>2</td><td>3.80</td><td>B</td><td>1</td><td></td><td></td><td>N</td><td>2135</td><td></td><td>23</td><td></td><td>23</td><td>0.00</td><td>2135</td><td></td><td></td><td>2135</td><td>0.011</td><td></td><td></td><td>2</td><td>14</td><td>0.069</td><td>3</td></tr> <tr> <td>C1</td><td>3</td><td>3.00</td><td>C</td><td>1</td><td></td><td></td><td>N</td><td>1915</td><td></td><td>131</td><td></td><td>131</td><td>0.00</td><td>1915</td><td></td><td></td><td>1915</td><td>0.068</td><td>0.228</td><td></td><td>10</td><td>33</td><td>0.187</td><td>12</td></tr> <tr> <td>C1</td><td>3</td><td>3.40</td><td>C</td><td>1</td><td></td><td></td><td>N</td><td>2095</td><td></td><td>144</td><td></td><td>144</td><td>0.00</td><td>2095</td><td></td><td></td><td>2095</td><td>0.069</td><td></td><td></td><td>10</td><td>33</td><td>0.187</td><td>14</td></tr> <tr> <td>D1</td><td>3</td><td>3.20</td><td>C</td><td>1</td><td>30</td><td></td><td>N</td><td>1935</td><td>421</td></tr></table> | Move-ment             | Stage                   | Lane Width m. | Phase       | No. of lane             | Radius m. | O  | N                          | Straight-Ahead Sat. Flow | Flow       |               |       | Total Flow pcu/h | Proportion of Turning Vehicles   | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec           | Degree of Saturation X | Queuing Length m.       | Left pcu/h                         | Straight pcu/h | Right pcu/h             | A1, A2     | 1                        | 3.20   | A      | 1     | 6.5              |                                | N               | 1935              | 204                     | 3                       |          | 207       | 0.99              | 1576             |               |                        | 1576              | 0.131 | 0.131 | 28    | 19      | 19                | 0.622    | 24 | A2              | 1          | 3.40 | A       | 1       |         |                       | N      | 2095 |    | 327 |    | 327 | 0.00 | 2095 |   | 400 | 2495 | 0.131 |    |  | 19 | 19 | 0.621 | 39 | B1 | 2 | 3.80 | B | 1 |  |  | N | 1995 |  | 22 |  | 22 | 0.00 | 1995 |  |  | 1995 | 0.011 |  |  | 2 | 14 | 0.071 | 3 | B1 | 2 | 3.80 | B | 1 |  |  | N | 2135 |  | 23 |  | 23 | 0.00 | 2135 |  |  | 2135 | 0.011 |  |  | 2 | 14 | 0.069 | 3 | C1 | 3 | 3.00 | C | 1 |  |  | N | 1915 |  | 131 |  | 131 | 0.00 | 1915 |  |  | 1915 | 0.068 | 0.228 |  | 10 | 33 | 0.187 | 12 | C1 | 3 | 3.40 | C | 1 |  |  | N | 2095 |  | 144 |  | 144 | 0.00 | 2095 |  |  | 2095 | 0.069 |  |  | 10 | 33 | 0.187 | 14 | D1 | 3 | 3.20 | C | 1 | 30 |  | N | 1935 | 421 |
| Move-ment  |                       |                         |               |             |                         |           |    |                            |                          | Stage      | Lane Width m. | Phase |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         | No. of lane                        | Radius m.      | O                       | N          | Straight-Ahead Sat. Flow | Flow   |        |       | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y        | Greater y | L sec             | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
|  | Left pcu/h            | Straight pcu/h          | Right pcu/h   |             |                         |           |    |                            |                          |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| A1, A2   | 1                     | 3.20                    | A             | 1           | 6.5                     |           | N  | 1935                       | 204                      | 3          |               | 207   | 0.99             | 1576   |                 |                   | 1576                    | 0.131                   | 0.131 | 28        | 19    | 19               | 0.622                   | 24                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| A2   | 1                     | 3.40                    | A             | 1           |                         |           | N  | 2095                       |                          | 327        |               | 327   | 0.00             | 2095   |                 | 400               | 2495                    | 0.131                   |       |           | 19    | 19               | 0.621                   | 39                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| B1   | 2                     | 3.80                    | B             | 1           |                         |           | N  | 1995                       |                          | 22         |               | 22    | 0.00             | 1995   |                 |                   | 1995                    | 0.011                   |       |           | 2     | 14               | 0.071                   | 3                      |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| B1   | 2                     | 3.80                    | B             | 1           |                         |           | N  | 2135                       |                          | 23         |               | 23    | 0.00             | 2135   |                 |                   | 2135                    | 0.011                   |       |           | 2     | 14               | 0.069                   | 3                      |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| C1   | 3                     | 3.00                    | C             | 1           |                         |           | N  | 1915                       |                          | 131        |               | 131   | 0.00             | 1915   |                 |                   | 1915                    | 0.068                   | 0.228 |           | 10    | 33               | 0.187                   | 12                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| C1   | 3                     | 3.40                    | C             | 1           |                         |           | N  | 2095                       |                          | 144        |               | 144   | 0.00             | 2095   |                 |                   | 2095                    | 0.069                   |       |           | 10    | 33               | 0.187                   | 14                     |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |
| D1   | 3                     | 3.20                    | C             | 1           | 30                      |           | N  | 1935                       | 421                      |            |               |       |                  |  |                 |                   |                         |                         |       |           |       |                  |                         |                        |                         |                                    |                |                         |            |                          |        |        |       |                  |                                |                 |                   |                         |                         |          |           |                   |                  |               |                        |                   |       |       |       |         |                   |          |    |                 |            |      |         |         |         |                       |        |      |    |     |    |     |      |      |   |     |      |       |    |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |    |  |    |      |      |  |  |      |       |  |  |   |    |       |   |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |       |  |    |    |       |    |    |   |      |   |   |  |  |   |      |  |     |  |     |      |      |  |  |      |       |  |  |    |    |       |    |    |   |      |   |   |    |  |   |      |     |

## J5 YEAR 2035 PM TRAFFIC FLOW INTERIM SCENARIO A

[illegible]

## J5 YEAR 2035 AM TRAFFIC FLOW INTERIM SCENARIO B

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## J5 YEAR 2035 PM TRAFFIC FLOW INTERIM SCENARIO B

OVE ARUP & PARTNERS

TRAFFIC SIGNAL CALCULATION

S16 Application for Proposed Development at Kau Wa Keng

PROJECT NO:                299277-02

Junction No.          J5

Cheung Sha Wan Road / Mei Lai Road

J5\_INT\_B\_PM

DATE :                      21-Jan-25

FILENAME :

The site plan shows an intersection between Cheung Sha Wan Road and Mei Lai Road. Traffic movements are labeled as follows:  
A1: Left turn from Westbound Cheung Sha Wan Rd to Southbound Mei Lai Rd (Flow: 191)  
A2: Through/right turn from Westbound Cheung Sha Wan Rd to Southbound Mei Lai Rd (Flow: 440)  
B1: Right turn from Eastbound Cheung Sha Wan Rd to Northbound Mei Lai Rd (Flow: 70)  
C1: Through/left turn from Southbound Mei Lai Rd to Westbound Cheung Sha Wan Rd (Flow: 381)  
D1: Through/right turn from Southbound Mei Lai Rd to Eastbound Cheung Sha Wan Rd (Flow: 787)  
Movements D8-10 are also indicated for the side street.

|                                    |                       |            |
|------------------------------------|-----------------------|------------|
| No. of stages per cycle            | N =                   | 4          |
| No. of stage using for calculation | N =                   | 2          |
| Cycle time                         | C =                   | 90 sec     |
| Sum(y)                             | Y=                    | 0.343      |
| Loss time                          | L =                   | 38 sec     |
| Total Flow                         | =                     | 1869 pcu   |
| Co                                 | = (1.5*L+5)/(1-Y)     | = 94.4 sec |
| Cm                                 | = L/(1-Y)             | = 57.8 sec |
| Yult                               | =                     | 0.615      |
| R.C. ult                           | = (Yult-Y)/Y*100%     | = 79.3 %   |
| Cp                                 | = 0.9*L/(0.9-Y)       | = 61.4 sec |
| Ymax                               | = 1-L/C               | = 0.578    |
| R.C.(C)                            | = (0.9*Ymax-Y)/Y*100% | = 52 %     |

Detailed description: Stage 1 involves two phases. Phase 1 includes movements D1-3 and 6, while Phase 2 includes movements 4, 5, and 6. The total duration for both phases combined is 7 seconds.

Detailed description: Stage 2 involves three phases. Phase 1 includes movement 3, Phase 2 includes movements 4 and 7, and Phase 3 includes movements 6 and 7. The total duration for all three phases is 13 seconds.

Detailed description: Stage 3 involves two phases. Phase 1 includes movements D6-7 and 1, while Phase 2 includes movements 4 and 5. The total duration for both phases is 5 seconds.

Detailed description: Stage 4 includes a single phase for movement 1, lasting 5 seconds.

| Pedestrian Phase | Width (m) | Green Time Required (s) |       |    | Green Time Provided (s) |       |    | Check |
|------------------|-----------|-------------------------|-------|----|-------------------------|-------|----|-------|
|                  |           | SG                      | Delay | FG | SG                      | Delay | FG |       |
| Ep               | 4.9       | 5                       | 3     | 8  | 40                      | 3     | 8  | OK    |
| Fp               | 4.5       | 5                       | 3     | 6  | 53                      | 3     | 6  | OK    |
| Gp               | 4         | 5                       | 5     | 12 | 34                      | 5     | 12 | OK    |
| Hp               | 3.7       | 5                       | 7     | 9  | 5                       | 7     | 9  | OK    |

| Movement | Stage | Lane Width m. | Phase | No. of lane | Radius m. | O | N | Straight-Ahead Sat. Flow | Flow       |                |             | Total Flow pcu/h | Proportion of Turning Vehicles | Sat. Flow pcu/h | Uphill Gradient % | Short lane Effect pcu/h | Revised Sat. Flow pcu/h | y     | Greater y | L sec | g (required) sec | g (input) sec | Degree of Saturation X | Queuing Length m. |
|----------|-------|---------------|-------|-------------|-----------|---|---|--------------------------|------------|----------------|-------------|------------------|--------------------------------|-----------------|-------------------|-------------------------|-------------------------|-------|-----------|-------|------------------|---------------|------------------------|-------------------|
|          |       |               |       |             |           |   |   |                          | Left pcu/h | Straight pcu/h | Right pcu/h |                  |                                |                 |                   |                         |                         |       |           |       |                  |               |                        |                   |
| A1, A2   | 1     | 3.20          | A     | 1           | 6.5       |   | N | 1935                     | 191        | 60             |             | 251              | 0.76                           | 1646            |                   |                         | 1646                    | 0.152 | 0.152     | 28    | 23               | 23            | 0.597                  | 28                |
| A2       | 1     | 3.40          | A     | 1           |           |   | N | 2095                     |            | 380            |             | 380              | 0.00                           | 2095            |                   | 400                     | 2495                    | 0.152 |           |       | 23               | 23            | 0.596                  | 42                |
| B1       | 2     | 3.80          | B     | 1           |           |   | N | 1995                     |            | 33             |             | 33               | 0.00                           | 1995            |                   |                         | 1995                    | 0.017 |           |       | 3                | 14            | 0.106                  | 4                 |
| B1       | 2     | 3.80          | B     | 1           |           |   | N | 2135                     |            | 37             |             | 37               | 0.00                           | 2135            |                   |                         | 2135                    | 0.017 |           |       | 3                | 14            | 0.111                  | 5                 |
| C1       | 3     | 3.00          | C     | 1           |           |   | N | 1915                     |            | 182            |             | 182              | 0.00                           | 1915            |                   |                         | 1915                    | 0.095 | 0.190     |       | 14               | 29            | 0.295                  | 19                |
| C1       | 3     | 3.40          | C     | 1           |           |   | N | 2095                     |            | 199            |             | 199              | 0.00                           | 2095            |                   |                         | 2095                    | 0.095 |           |       | 14               | 29            | 0.295                  | 20                |
| D1       | 3     | 3.20          | C     | 1           | 30        |   | N | 1935                     | 351        |                |             | 351              | 1.00                           | 1843            |                   |                         | 1843                    | 0.190 |           |       | 29               | 29            | 0.591                  | 36                |
| D1       | 3     | 3.20          | C     | 1           | 30        |   | N | 2075                     | 436        |                |             | 436              | 1.00                           | 1976            |                   | 320                     | 2296                    | 0.190 |           |       | 29               | 29            | 0.589                  | 44                |
| X        | 4     |               |       |             |           |   |   |                          |            |                |             |                  |                                |                 |                   |                         |                         |       |           | 5     |                  |               |                        |                   |
| Hp       |       |               |       |             |           |   |   |                          |            |                |             |                  |                                |                 |                   |                         |                         |       |           | 5     |                  |               |                        |                   |

NOTE :     'O' - OPPOSING TRAFFIC        'N' - NEAR SIDE LANE        SG - STEADY GREEN        FG - FLASHING GREEN

PEDESTRIAN WALKING SPEED = 0.9m/s

QUEUING LENGTH = AVERAGE QUEUE \* 6m

## J5 YEAR 2035 AM TRAFFIC FLOW INTERIM SCENARIO C

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## J5 YEAR 2035 PM TRAFFIC FLOW INTERIM SCENARIO C

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## Appendix B

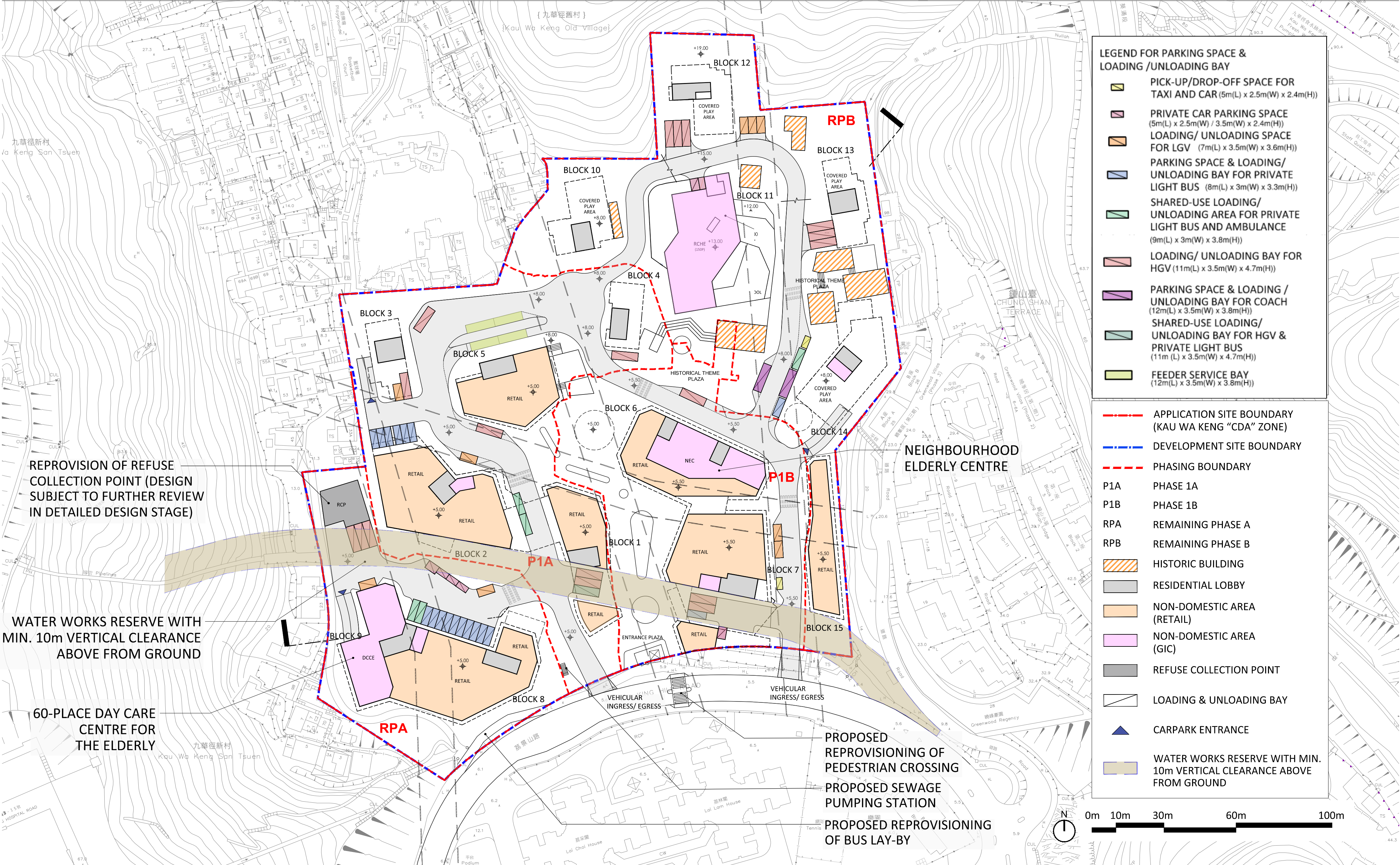
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### Highlighted Plans of Internal Transport Provision



GROUND FLOOR LAYOUT PLAN

1:500@A0 1:1000@A2



PROPOSED COMPREHENSIVE DEVELOPMENT INCLUDING FLATS, RETAIL AND COMMUNITY FACILITIES AND MINOR RELAXATION OF PLOT RATIO AND BUILDING HEIGHT RESTRICTION IN "COMPREHENSIVE DEVELOPMENT AREA" ZONE AT VARIOUS LOTS IN S.D.4 AND ADJOINING GOVERNMENT LAND, KAU WA KENG, KWAI CHUNG

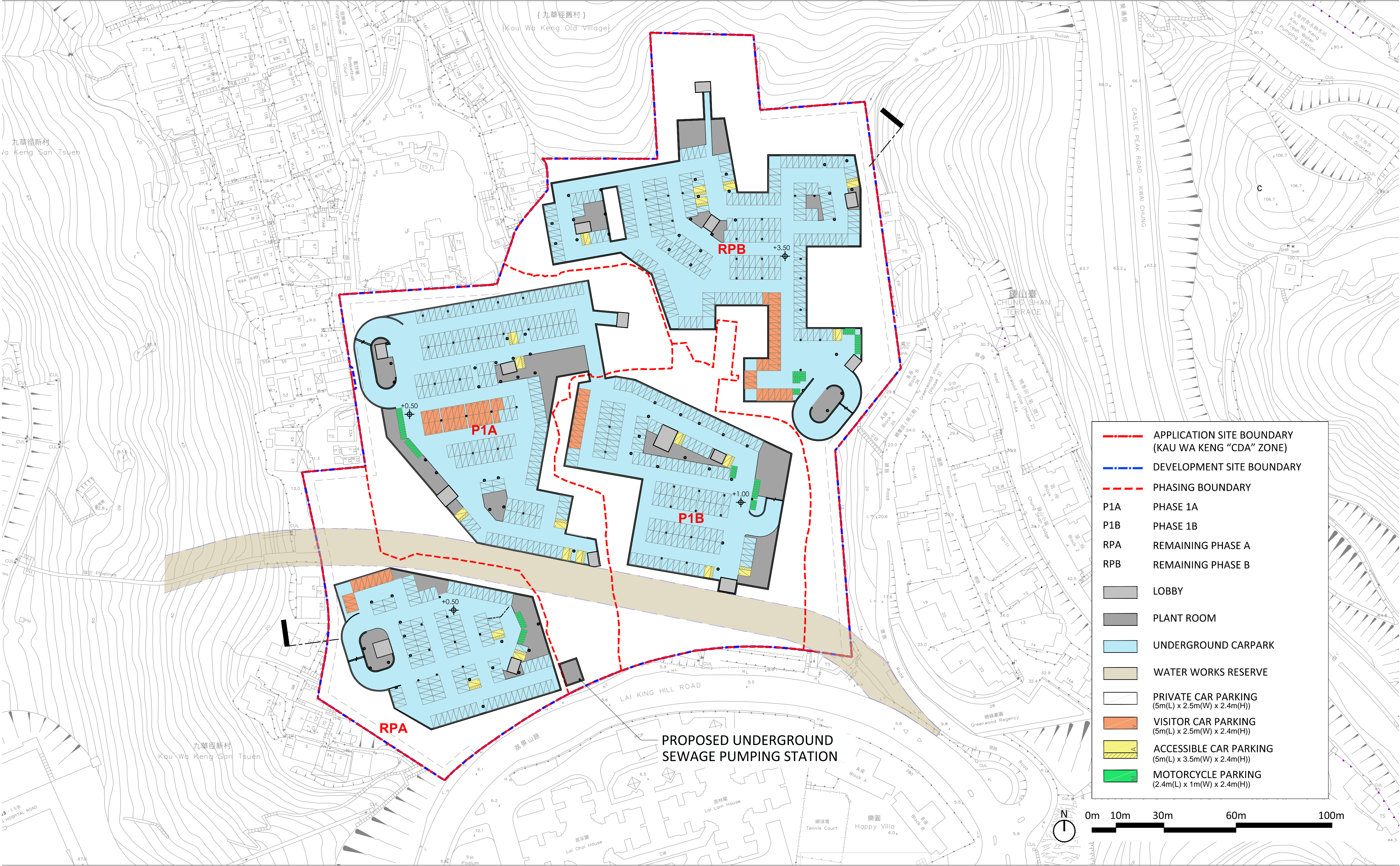
5 JUNE 2025

DRAWING NO.: MLP-SK01\01-R8



BASEMENT 1/F FLOOR LAYOUT PLAN

1:500@A0 1:1000@A2



PROPOSED COMPREHENSIVE DEVELOPMENT INCLUDING FLAT AND COMMUNITY FACILITIES IN "COMPREHENSIVE DEVELOPMENT AREA" ZONE AT VARIOUS LOTS IN S.D.4 AND ADJOINING GOVERNMENT LAND, KAU WA KENG, KWAI CHUNG

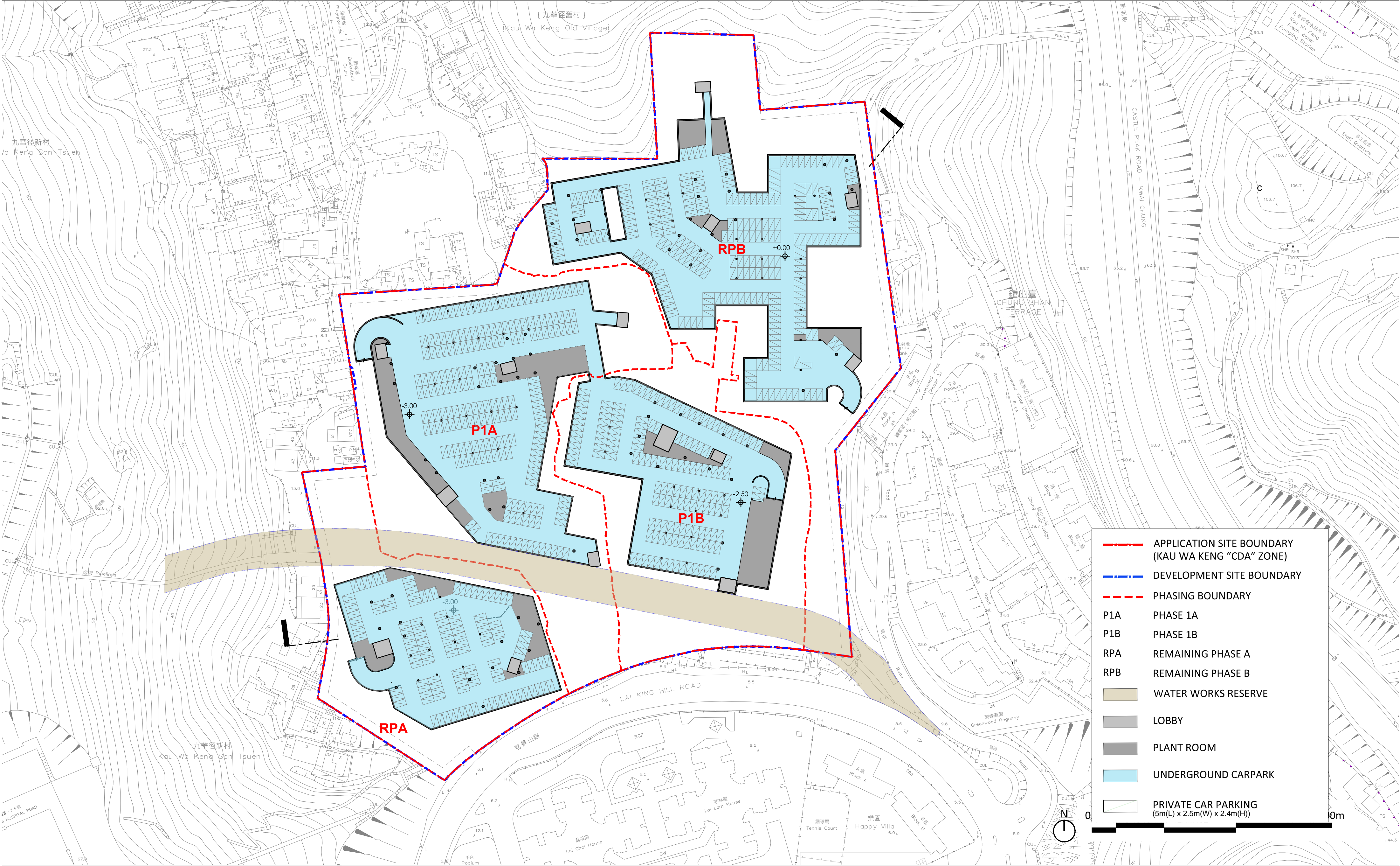
10 FEBRUARY 2025

DRAWING NO.: MLP-SK03\02-R5



BASEMENT 2/F FLOOR LAYOUT PLAN

1:500@A0 1:1000@A2



PROPOSED COMPREHENSIVE DEVELOPMENT INCLUDING FLAT AND COMMUNITY FACILITIES IN "COMPREHENSIVE DEVELOPMENT AREA" ZONE  
AT VARIOUS LOTS IN S.D.4 AND ADJOINING GOVERNMENT LAND, KAU WA KENG, KWAI CHUNG

10 FEBRUARY 2025

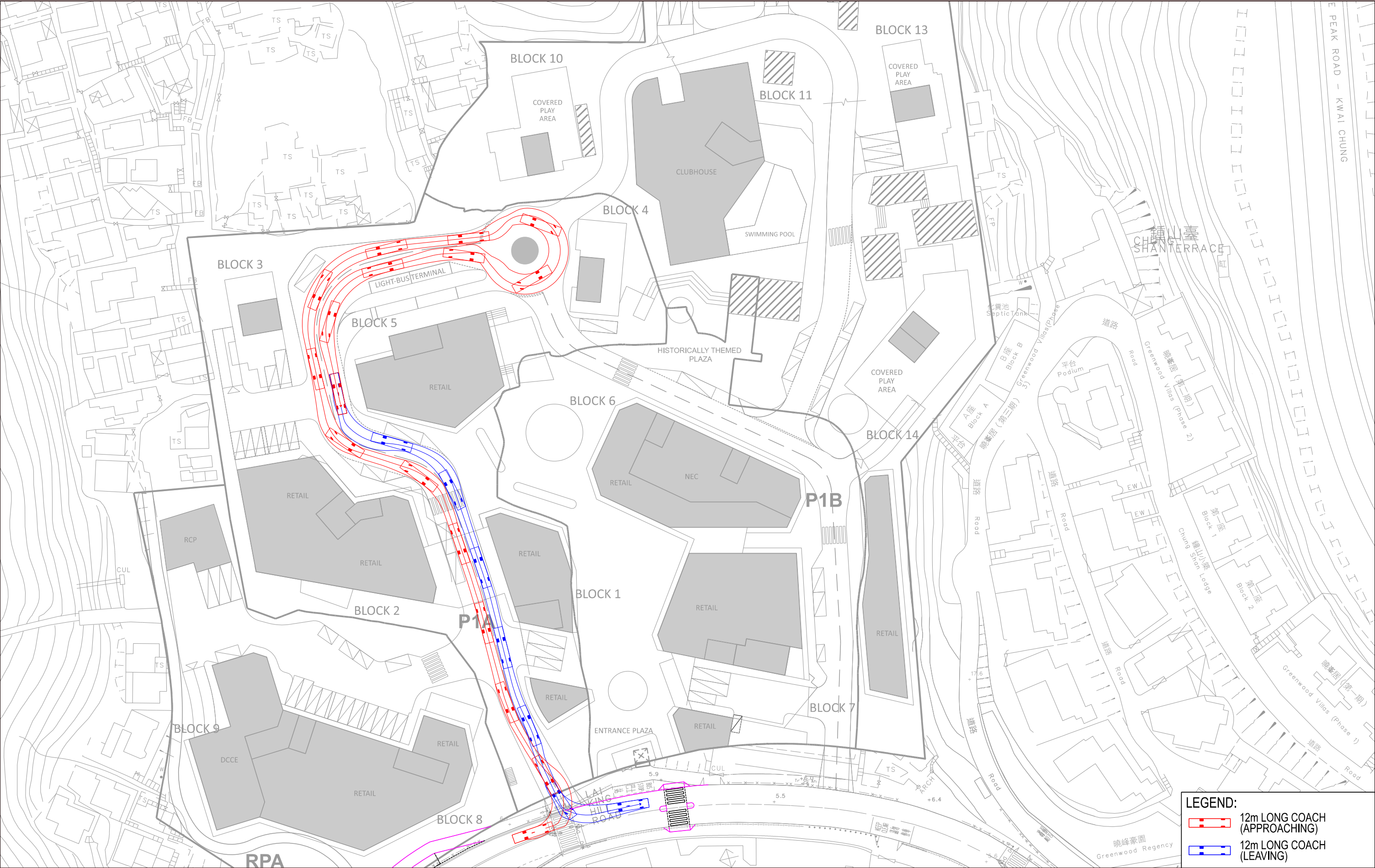
DRAWING NO.: MLP-SK03\01-R5



# Appendix C

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## Critical Swept Path Analysis



|           |           |  |   |  |  |
|-----------|-----------|--|---|--|--|
| Job Title |           |  | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |  |
| Date      | Scale     | Drawing Title                          |   |  |  |
| 15JAN25   | 1:1000@A3 | SWEPT PATH ANALYSIS FOR 12m LONG COACH |   |  |  |
| Drawn     | Job No.   |  |   |  |  |
| WLAC      | 299277-02 |  |   |  |  |

LEGEND:

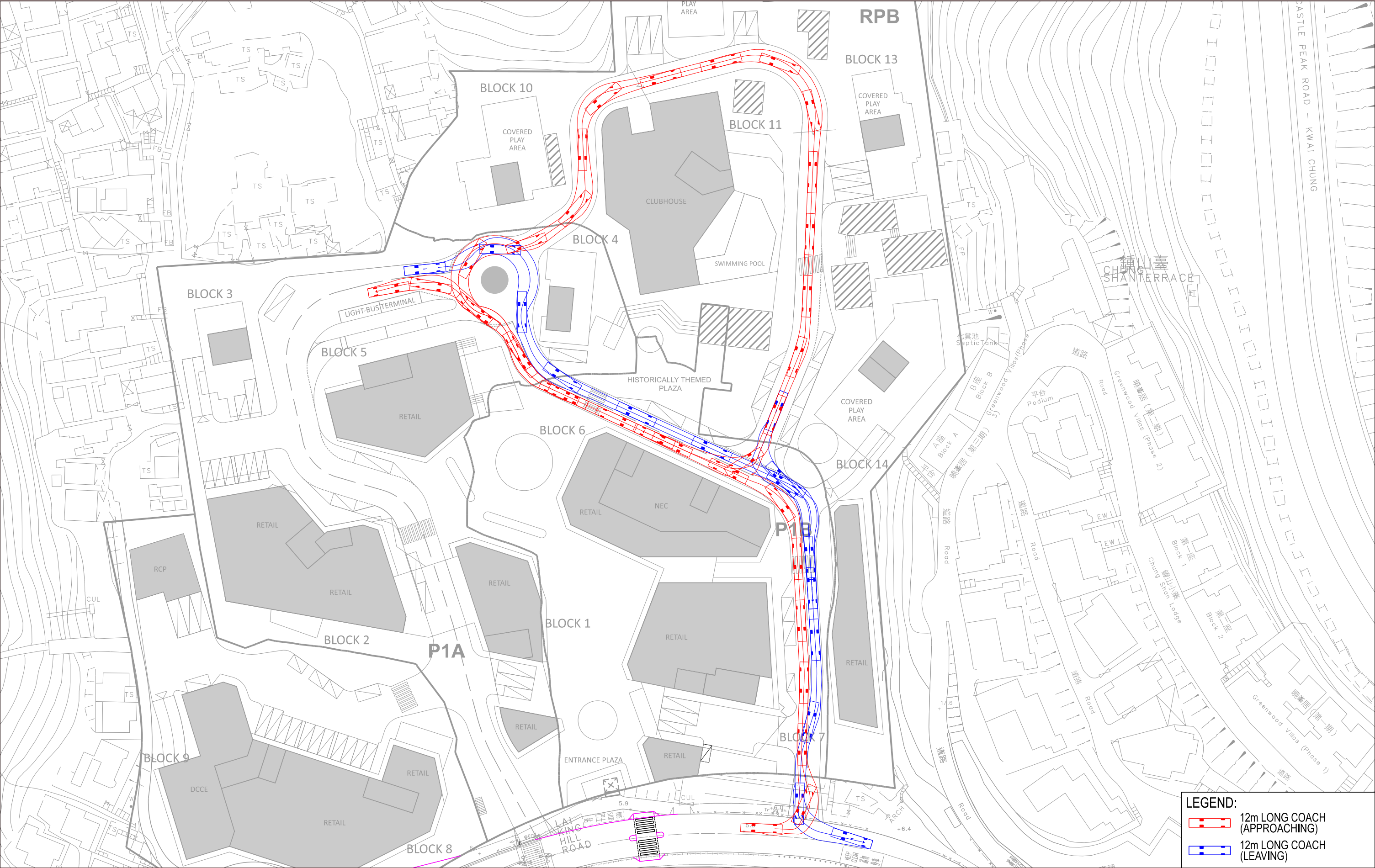
12m LONG COACH (APPROACHING)

12m LONG COACH (LEAVING)

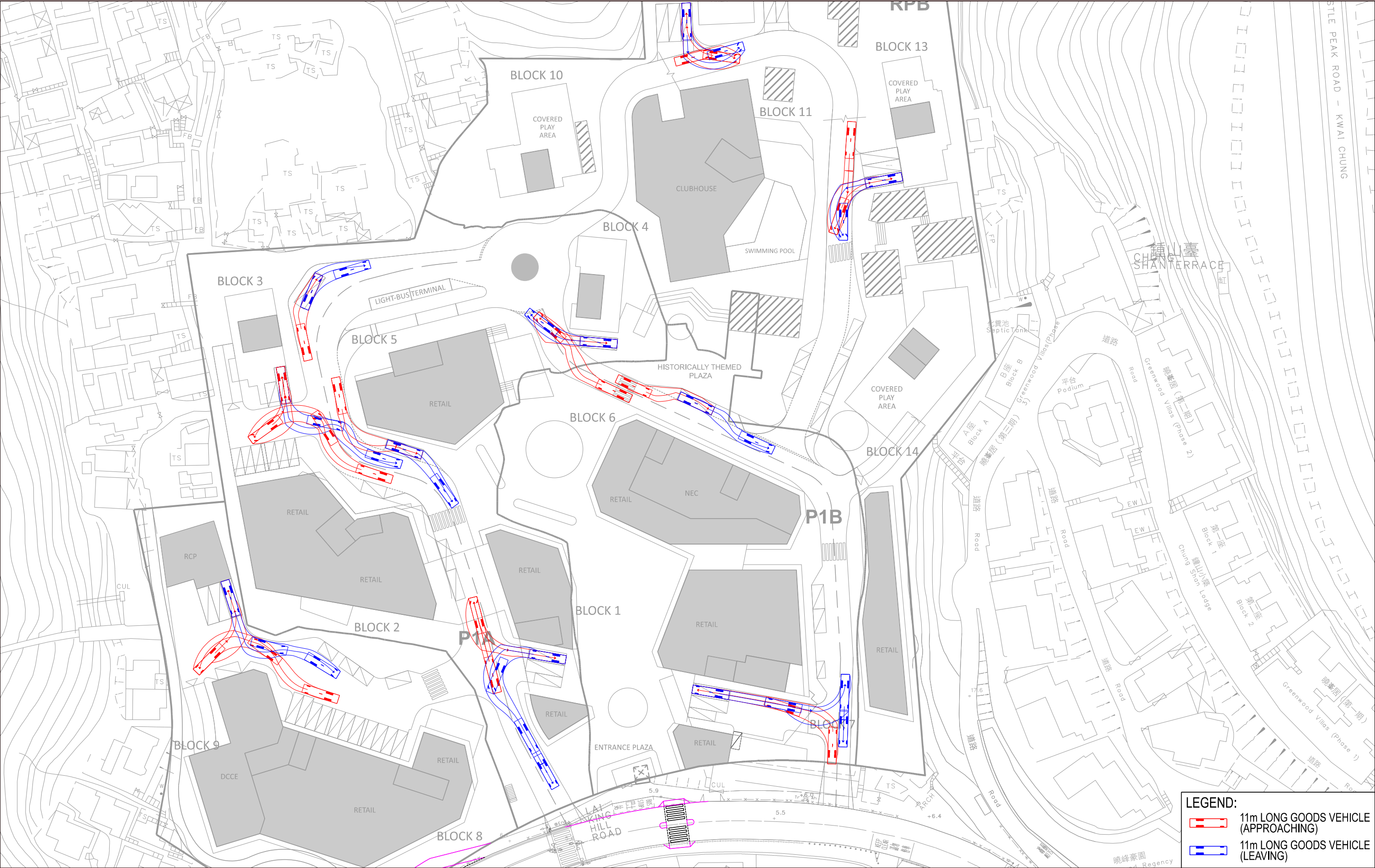
SK-011\_SP5

ARUP





|           |           |  |   |  |  |            |      |  |
|-----------|-----------|--|---|--|--|------------|------|--|
| Job Title |           |  | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |  | SK-011_SP7 |      |  |
| Date      | Scale     | Drawing Title                          |   |  |  |            | ARUP |  |
| 14JAN25   | 1:300@A3  | SWEPT PATH ANALYSIS FOR 12m LONG COACH |   |  |  |            |      |  |
| Drawn     | Job No.   |  |   |  |  |            |      |  |
| WLAC      | 299277-02 |  |   |  |  |            |      |  |

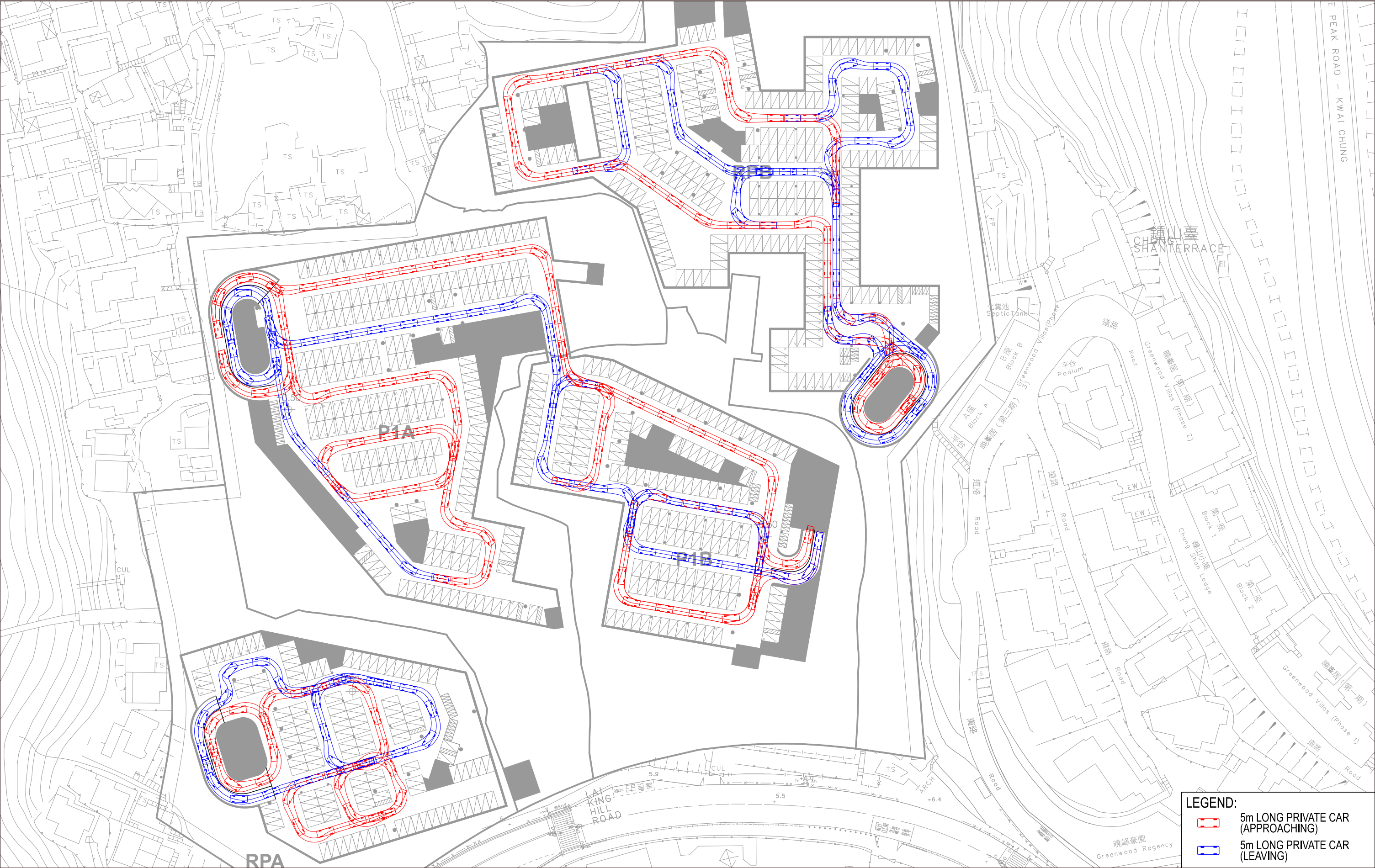


|           |           |  |   |  |  |
|-----------|-----------|--|---|--|--|
| Job Title |           |  | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in "Comprehensive Development Area" Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |  |
| Date      | Scale     | Drawing Title                                  |   |  |  |
| 14JAN25   | 1:1000@A3 | SWEPT PATH ANALYSIS FOR 11m LONG GOODS VEHICLE |   |  |  |
| Drawn     | Job No.   |  |   |  |  |
| WLAC      | 299277-02 |  |   |  |  |

SK-011\_SP3

ARUP





- LEGEND:
- 5m LONG PRIVATE CAR (APPROACHING)
  - 5m LONG PRIVATE CAR (LEAVING)

Job Title    **Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in “Comprehensive Development Area” Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung**

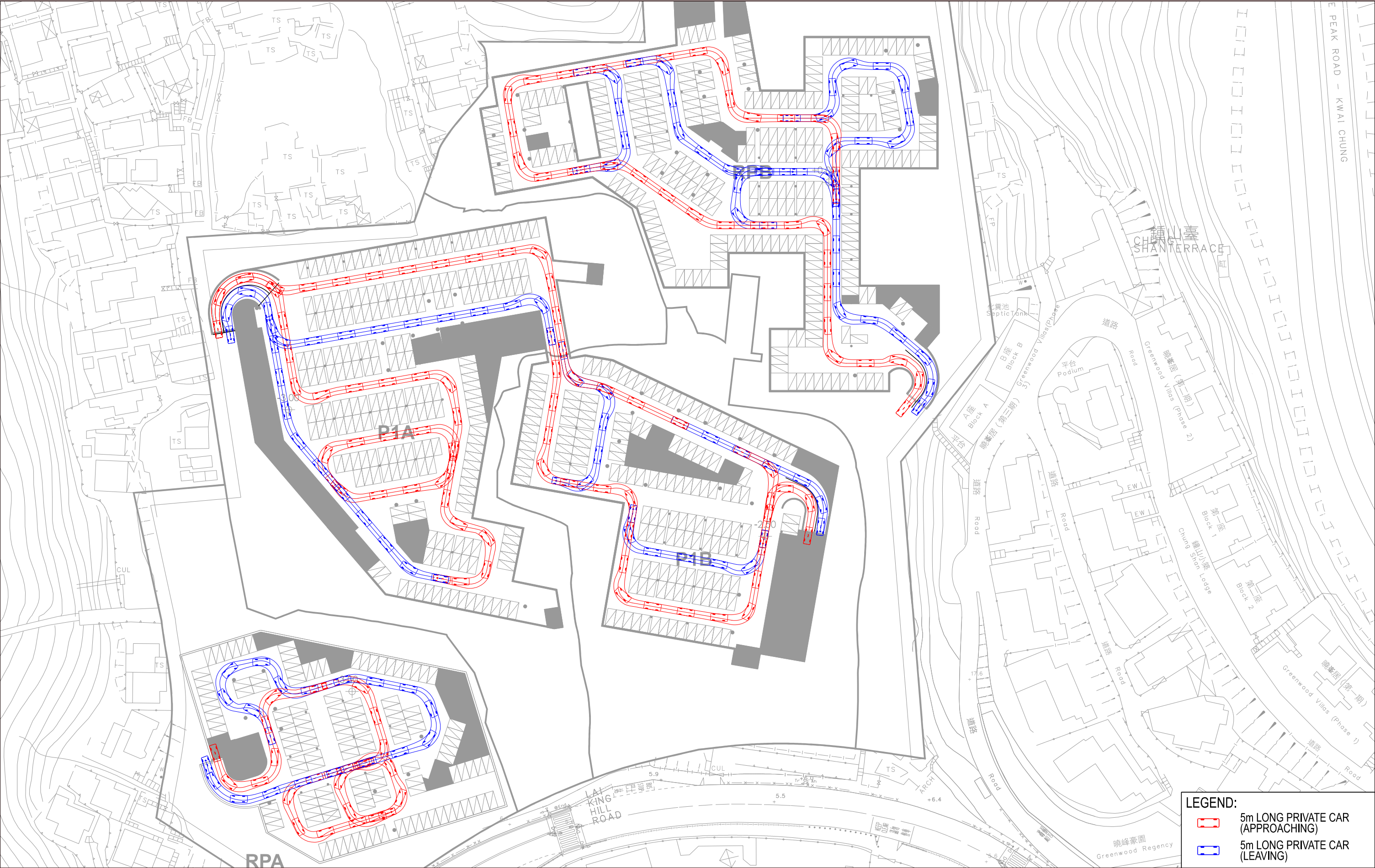
SK-012\_SP1

|         |           |
|---------|-----------|
| Date    | Scale     |
| 14JAN25 | 1:1000@A3 |
| Drawn   | Job No.   |
| WLAC    | 299277-02 |

SWEPT PATH ANALYSIS FOR 5m LONG PRIVATE CAR AT B1

ARUP





|           |           |   |   |  |  |
|-----------|-----------|---|---|--|--|
| Job Title |           |   | Application for Permission Under Section 16 of the Town Planning Ordinance (Cap. 131) for Proposed Comprehensive Development including Flats, Retail and Community Facilities and Minor Relaxation of Plot Ratio and Building Height Restriction in “Comprehensive Development Area” Zone at Various Lots in S.D.4 and Adjoining Government Land, Kau Wa Keng, Kwai Chung |  |  |
| Date      | Scale     | Drawing Title                                     |   |  |  |
| 14JAN25   | 1:1000@A3 | SWEPT PATH ANALYSIS FOR 5m LONG PRIVATE CAR AT B2 |   |  |  |
| Drawn     | Job No.   |   |   |  |  |
| WLAC      | 299277-02 |   |   |  |  |

SK-013\_SP1

ARUP

## Appendix D

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### Planned Junction Improvement Schemes

## TD's planned junction improvement scheme

