

**Proposed Temporary Animal Boarding Establishment and Associated Land Filling  
for a Period of 3 Years at Lot 1070 RP (Part) in D.D. 109, Kam Tin North, Yuen Long**

元朗錦田北丈量約份第 109 約地段第 1070 號餘段（部分）

擬議臨時動物寄養所連相關填土工程（為期 3 年）

**P08\_Drainage Proposal**

**Date: 2025-06-12**

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## **REFERENCES**

1. Stormwater Drainage Manual, Planning Design and Management by DSD
2. Geotechnical Manual for Slopes by GEO
3. Standard Drawings by DSD

## 1. Introduction

This proposal is prepared for the proposed stormwater drainage works for the proposed temporary animal boarding establishment and associated land filling for a period of 3 years at lot 1070 RP (Part) in D.D.109, Kam Tin North, Yuen Long.

## 2. Existing Drainage Condition

A plan showing the existing catchments is enclosed in **Appendix B**. Currently, the surface runoff collected from the site is discharging to the existing Kam Tin River located at the west of the site as shown in **Appendix A**. As per the existing site condition, an additional peripheral U-channels area is considered necessary for the proposed development. A drainage proposal is required to be carried out for the proposed development.

## 3. Design Parameters & Assumptions

The design criteria to be used for the modeling assessment are based on the standards set out in the Stormwater Drainage Manual, Third Edition (SDM). According to Section 6.6.1 of the SDM, the existing village drainage system in the vicinity of the development is classified as main rural catchment drainage system. Table 10 of the SDM recommends to be adopted a 50 year design return period storm event for the urban drainage branch system.

### Stormwater Runoff (Q)

The rate of stormwater runoff used in this assessment report is estimated by the “Rational method” in which the peak runoff is calculated from the formula:

$$Q = K \times i \times A / 3600$$

|       |   |   |                                           |
|-------|---|---|-------------------------------------------|
| where | Q | = | maximum runoff (L/s)                      |
|       | i | = | design mean intensity of rainfall (mm/hr) |
|       | A | = | area of catchment (m <sup>2</sup> )       |
|       | K | = | runoff coefficient                        |

#### **4. Proposed Stormwater Drainage**

The proposed stormwater drainage works include surface U-channels at the peripheral of the site collecting the runoff from catchments within the site. The U-channels will connect and discharge the surface runoff to the existing Kam Tin River located at the west of the site. Catchpits with 300mm sump are proposed at the discharged points of the proposed U-Channel to desilt the surface water before discharging to the drainage outside. The proposed stormwater drainage layout plan is shown in **Appendix A**.

#### **5. Effect on Drainage Characteristics and Potential Drainage Impact**

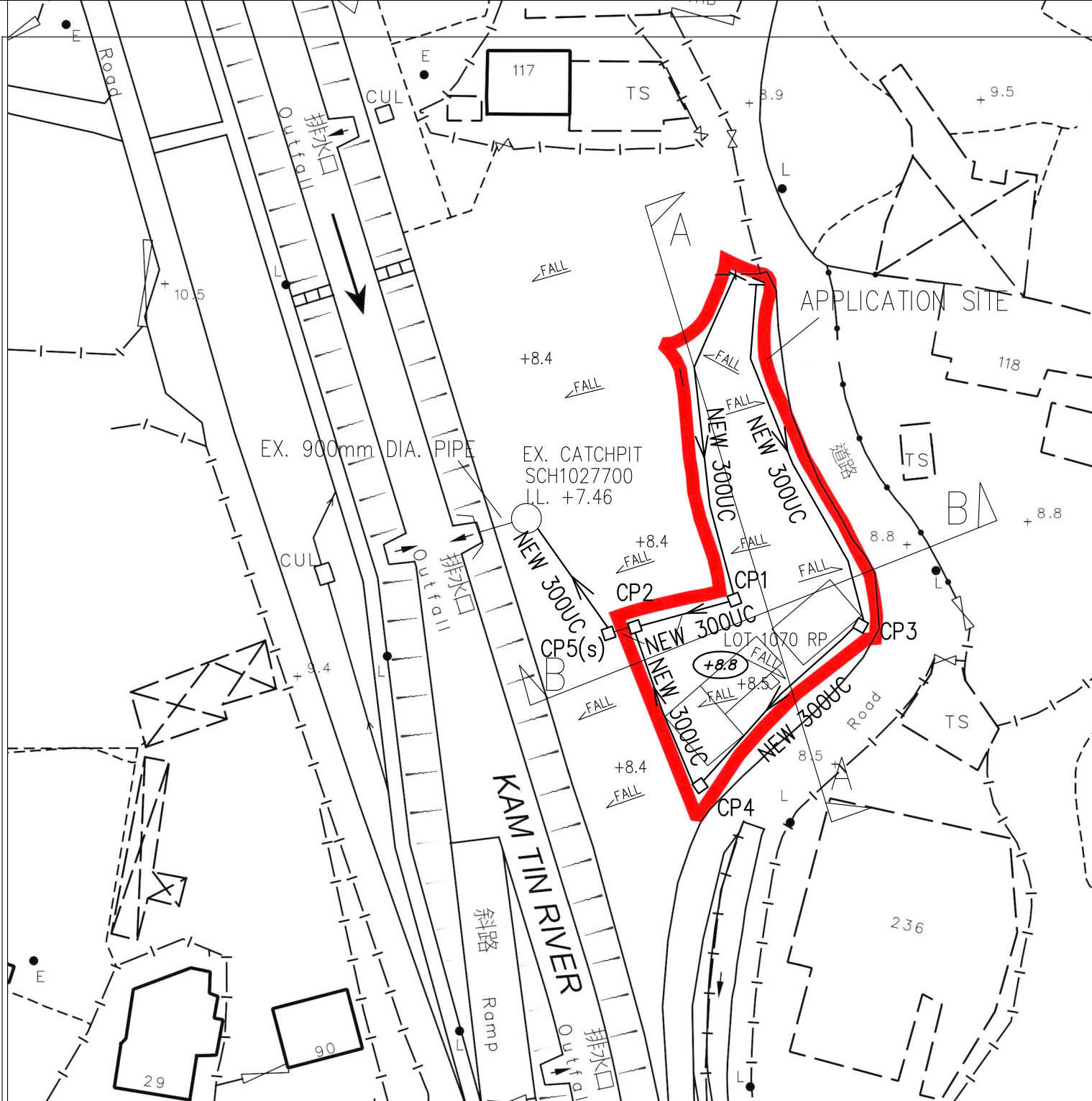
The drainage design of the proposed U-channel is presented in **Appendix B**. Since no wall or hoarding would be erected in this development, it is considered that the existing overland flow passing through the site would not be affected.

#### **6. Conclusion**

Peripheral channels are to be provided along the site boundary where necessary to intercept runoff from crossing the site. The drainage conditions of adjacent areas will not be adversely affected.

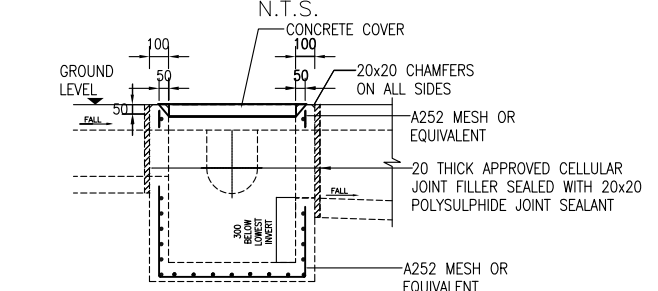
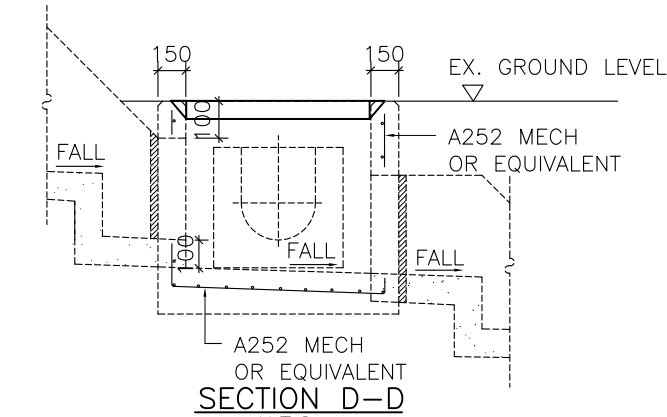
## **Appendix A**

### **Stormwater Drainage Proposal Plan**

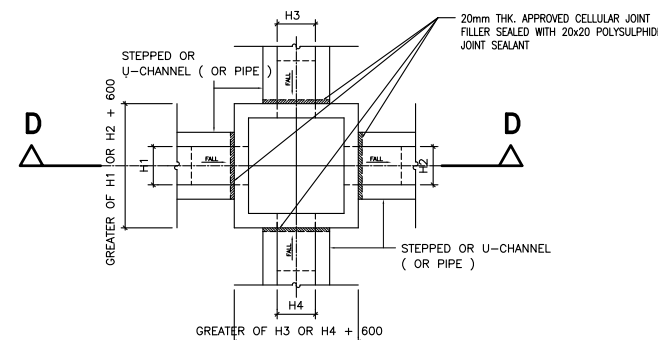


### LEGEND:

- +8.8  
NEW 300UC  
CP5(s)  
CP1  
+8.8  
PROPOSED BUILDING
- EXISTING GROUND LEVEL AT +8.8mPD  
PROPOSED 300mm U-CHANNEL WITH GRATING AT FALL 1: 100 (MIN)  
PROPOSED COVERED DESILTED CATCHPIT NO. CP5  
PROPOSED COVERED CATCHPIT NO. CP1  
PROPOSED SITE FORMATION LEVEL  
PROPOSED BUILDING



### SECTION D - D WITH DESILTED TRAP COMPLY WITH CEDD'S DRAWING NO. DS C2405 AND C2406I

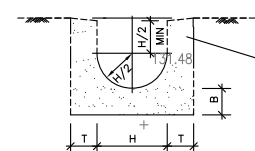


### PLAN

### TYPICAL DETAILS OF CATCHPIT

SLOT FOR LIFTING KEY

20 x 20 CHAMFER



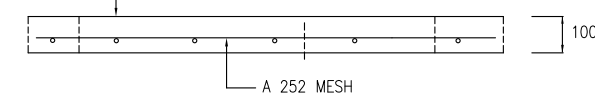
### U-CHANNEL

COMPLY WITH FIG 8.11 OF GEOTECHNICAL MANUAL FOR SLOPES

### NOTES:

1. H = NOMINAL CHANNEL SIZE.  
N.T.S. GRADE 25D CONCRETE WITH ONE LAYER OF A 252 MESH REINFORCEMENT PLACED CENTRALLY F2 AND U2 FINISH

### PLAN



### PRECAST CONCRETE COVERS FOR CATCHPIT

N.T.S.

### GENERAL NOTE

1. THE PROPOSED DRAINAGE WORK, WHETHER WITHIN OR OUTSIDE THE LOT BOUNDARY, SHOULD BE CONSTRUCTED AND MAINTAINED BY THE LOT OWNER AT HIS OWN EXPENSE. FOR WORKS TO BE UNDERTAKEN OUTSIDE THE LOT BOUNDARY, PRIOR CONSENT AND AGREEMENT FROM DLO AND/OR RELEVANT PRIVATE LOT OWNER SHOULD BE SOUGHT.

### CONCRETE STRENGTH AND STEEL REINFORCEMENT SPECIFICATION FOR DRAINAGE DETAILS

1. CONCRETE GRADE FOR CATCHPITS AND U-CHANNEL SHALL BE 30D DESIGN IN COMPLIANCE WITH CS1 : 2010  
FOR BLINDING LAYER SHALL BE 15D, DESIGN COMPLY WITH CS1-2010.
2. ALL MAIN BARS TO BE HOT ROLLED HIGH YIELD STEEL DEFORMED BAR COMPLY WITH CS2 : 2012  
Y - HIGH YIELD BAR 500 MPa  
M - MILD STEEL BAR 250 MPa
3. CONCRETE COVER TO MAIN REINFORCEMENT TO BE 50mm.
4. LAP LENGTH FOR ALL BARS TO BE 46x DIAMETER OF LARGER BAR TO BE LAPPED.
5. REACTIVE ALKALI CONTENT EXPRESSED IN SODIUM OXIDE PER CUBIC METER OF CONCRETE SHOULD NOT EXCEED 3KG AS PER PNAP APP-74.

### HALF ROUND, U, AND STEPPED - CHANNELS

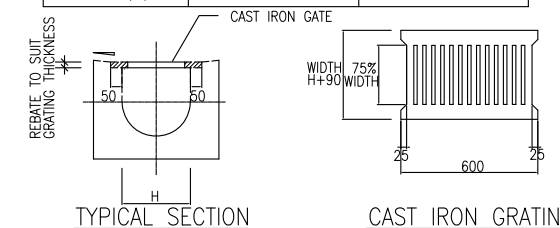
- 1 ALL DIMENSIONS ARE IN MILLIMETERS
- 2 CONCRETE SURFACE FINISHING SHALL BE CLASS U2 OR F2 AS APPROPRIATE
- 3 FOR HALF ROUND AND U - CHANNEL, SPACING OF EXPANSION JOINT IN CHANNELS, BERMS AND APRON TO BE 10m MAXIMUM. FOR STEPPED CHANNELS, EXPANSION JOINTS TO BE PROVIDED AT A MAXIMUM SPACING OF 10m.
- 4 DIMENSIONS FOR HALF ROUND AND U-CHANNELS SEE TABLE 1.
- 5 THE COVER FOR U-CHANNELS AND CATCHPIT SHALL COMPLY WITH CEDD'S STANDARD DRAWINGS NO. C2405 TO C2407 AND C2412.
- 6 ALL PROPOSED U-CHANNELS SHALL BE COVERED WITH GRATING

### TABLE 1 : DIMENSION OF U-CHANNEL AND HALF-ROUND CHANNEL

| NORMAL SIZE H | T   | B   | REINFORCING                |
|---------------|-----|-----|----------------------------|
| <300          | 100 | 100 | NIL                        |
| 375 - 675     | 150 | 150 | NIL                        |
| 750 - 900     | 175 | 175 | A252 MESH PLACED CENTRALLY |

### PROPOSED CATCHPIT SCHEDULE

| CATCHPIT NO. | C.L. (mPD) | I.L. (mPD) |
|--------------|------------|------------|
| CP1          | 8.80       | 8.11       |
| CP2          | 8.80       | 7.62       |
| CP3          | 8.80       | 8.06       |
| CP4          | 8.80       | 7.81       |
| CP5(s)       | 8.80       | 7.60       |



### TYPICAL SECTION

### CAST IRON GRATING

( DIMENSIONS ARE FOR GUIDANCE ONLY. CONTRACTOR MAY SUBMIT EQUIVALENT TYPE )

### U-CHANNEL WITH CAST IRON GRATING

|                                               |                     |                           |          |     |         |
|-----------------------------------------------|---------------------|---------------------------|----------|-----|---------|
|                                               |                     |                           |          |     |         |
|                                               |                     |                           |          |     |         |
|                                               | PLANNING SUBMISSION | RC                        | AY       | RY  | JUNE 25 |
| REV                                           | DESCRIPTION         | CHECKED                   | APPROVED | DWN | DATE    |
| PROJECT TITLE:                                |                     |                           |          |     |         |
| STORMWATER DRAINAGE PROPOSAL                  |                     |                           |          |     |         |
| LOT 1070 RP IN D.D. 109                       |                     |                           |          |     |         |
| DRAWING TITLE:                                |                     |                           |          |     |         |
| DRAINAGE PROPOSAL PLAN<br>AND TYPICAL DETAILS |                     |                           |          |     |         |
| SCALE : N.T.S.                                |                     | CAD FILE: CAD_REF         |          |     |         |
| DRAWN                                         | RY                  | DRAWING NO.<br><br>SDP001 |          |     |         |
| S.D                                           | RY                  |                           |          |     |         |
| DESIGNED                                      | RC                  |                           |          |     |         |
| CHECKED                                       | AY                  |                           |          |     |         |
|                                               |                     | B.D. REF. NO.:            |          |     |         |

**Appendix B**

**Surface Drainage Design**

### Time of Concentration (tc)

The time of concentration is defined as the time required for stormwater runoff to flow from the most remote part of the catchment area to the point in the drainage system under consideration. Based on the assumptions adopted in the Rational Method, this is the time taken for the peak runoff to become established at the considered section.

The time of concentration comprises the time for water flowing within natural catchments and along the man-made drainage pipes/channels. For natural catchments, the time of concentration is estimated by the modified form of the Brandsby William's equation.

$$t_o = \frac{0.14465L}{H^{0.2} A^{0.1}}$$

Where  $t_o$  = time of concentration of a natural catchment (min.)

A = catchment area ( $m^2$ )

H = average slope (m per 100m), measured along the line of natural flow, from the summit of the catchment to the point under consideration

L = distance (on plan) measured on the line of natural flow between the summit and the point under consideration (m)

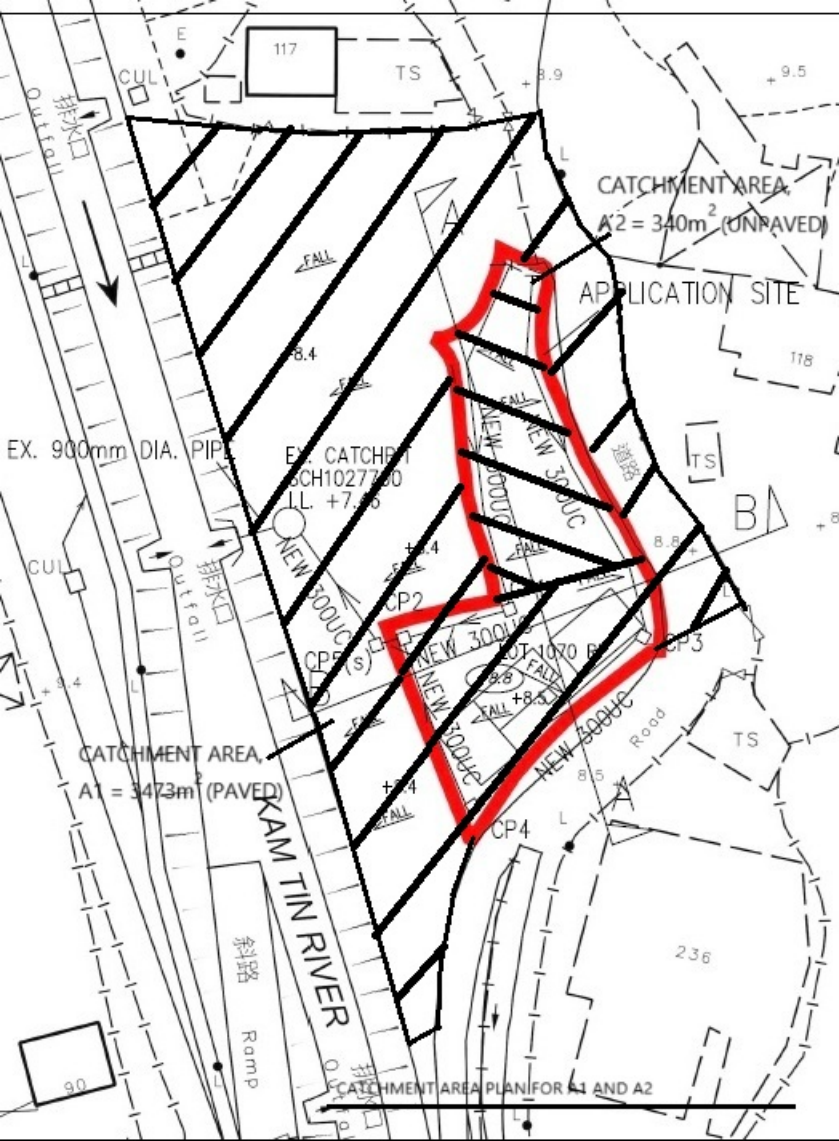
### Mean Rainfall Intensity (i)

Mean rainfall intensity-duration curves attached in this report are based on the Statistical analysis of long term rainfall records from the Hong Kong Observatory. A return period of 50 years is adopted.

### Runoff Coefficient (K)

The value of K is taken as 1 for developed area. For vegetated ground, the value of K is taken as 0.3.





Drainage Design at lot 1070 RP in

Project No.: D.D.109 Kam Tin Village

Date:

31-May-25

Prepared by:

Ray Cheng

Check for the drainage capacity of existing 900mm dia. pipe

|                 |    |   |                |                |                                    |
|-----------------|----|---|----------------|----------------|------------------------------------|
| Catchment area, | A1 | = | 3473           | m <sup>2</sup> | Assume k = 1.0 for paved surface   |
|                 | A2 | = | 340            | m <sup>2</sup> | Assume k = 0.3 for unpaved surface |
| Total Area, A   |    | = | 3473 + 0.3x340 |                |                                    |
|                 |    | = | 3575           | m <sup>2</sup> |                                    |

Use Rational Method from Geo-Manual

$$Q = kiA/3600$$

where,

Q = Maximum runoff (lit/sec)

k = Runoff coefficient

i = Design mean intensity of rainfall (mm/hr)

A = Total catchment area (m<sup>2</sup>)

Longest distance from summit point to outlet, PtZ

$$(L_d) = 114.00 \text{ m}$$

Shortest distance from summit point to outlet, PtZ

$$(L_s) = 46.00 \text{ m}$$

Elevation of remote point (Pt A)

$$= 8.80 \text{ mPD}$$

Elevation of outlet point, PtZ

$$= 7.46 \text{ mPD}$$

Average fall, H

$$= (z_1 - z_2)/L_s \times 100$$

$$= 2.91 \text{ m per 100m}$$

From TGN30

$$T_c = 0.14465 \times L_d / (H^{0.2} \times A^{0.1})$$

$$= 5.84 \text{ min}$$

Assume a 1 in 50 year design rainfall return period for rural area

From SDM Corrigendum No. 1/2024

$$i = 215 \text{ mm/hr}$$

$$Q = \frac{kiA}{60} \times 1.16$$

$$14860 \text{ lit/min}$$

From TGN 43A1

For existing 900mm dia. pipe with 1 in 100 gradient

$$\text{Maximum capacity} = 1.992 \times 1000 \times 60 = 119520 \text{ lit/min} > 14860 \text{ o.k.}$$

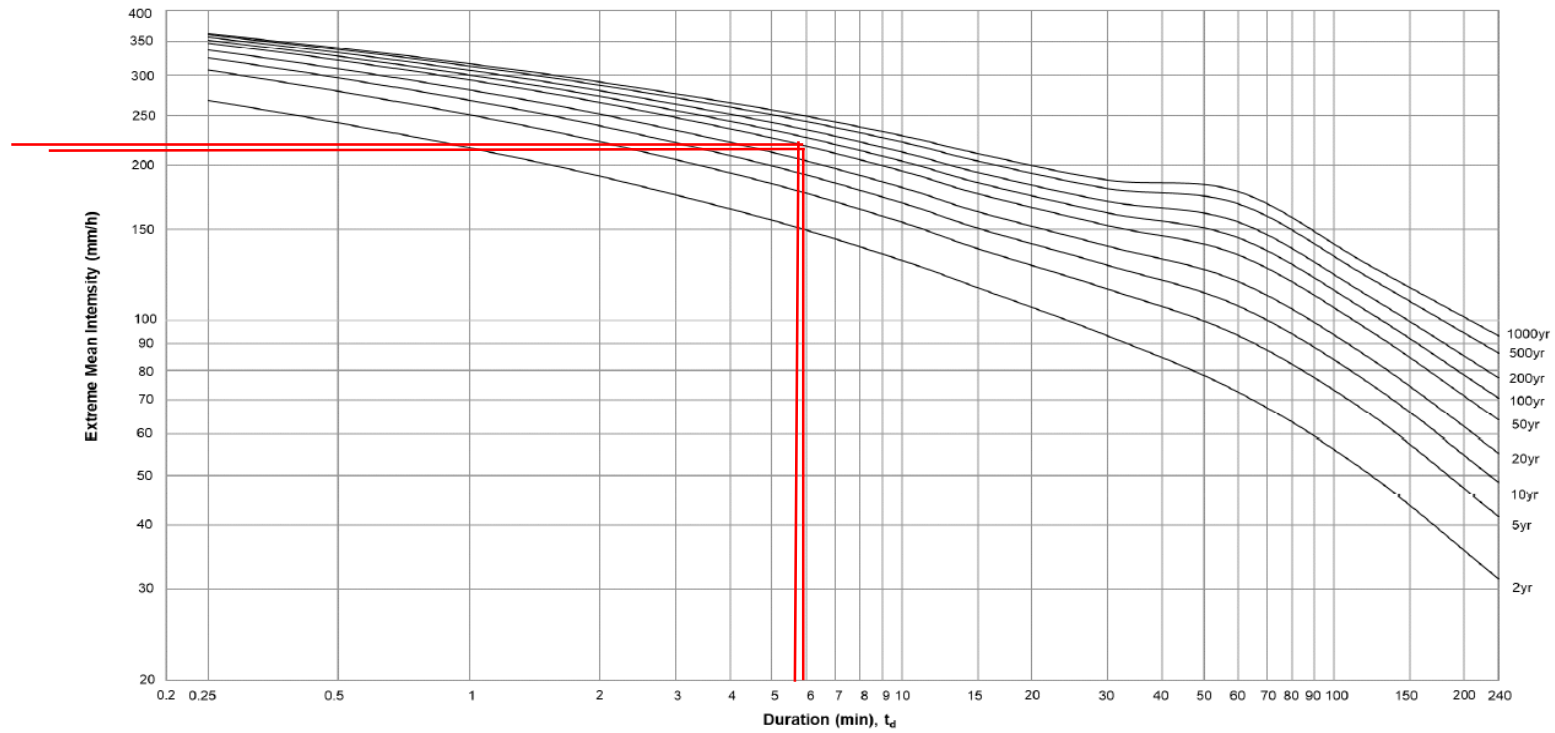


Figure 4a – Intensity-Duration-Frequency Curves of HKO Headquarters  
(for durations not exceeding 4 hours)

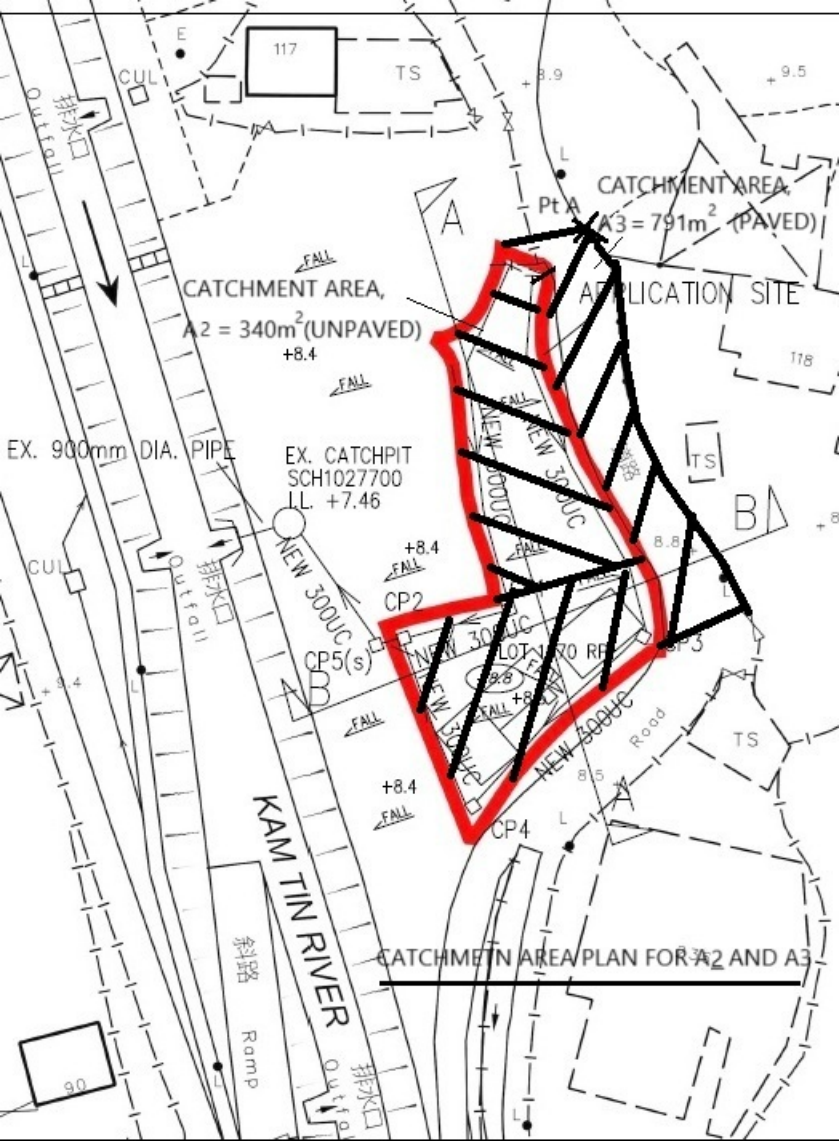
continued

 $\frac{1}{1 \text{ in } 333 \text{ to } 1 \text{ in } 13}$ 
 $\frac{\text{velocities in m/s}}{\text{discharges in m}^3/\text{s}}$ 

Gradient

Pipe diameters in mm

|                   | 900   | 975   | 1000  | 1050  | 1100  | 1200  | 1350  | 1500  | 1650   | 1800   | 1950   | 2100   |
|-------------------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|
| 0.00300<br>1/ 333 | 1.709 | 1.796 | 1.824 | 1.880 | 1.935 | 2.042 | 2.195 | 2.342 | 2.483  | 2.619  | 2.750  | 2.877  |
|                   | 1.087 | 1.341 | 1.433 | 1.628 | 1.839 | 2.309 | 3.142 | 4.139 | 5.309  | 6.663  | 8.212  | 9.963  |
| 0.00320<br>1/ 313 | 1.765 | 1.855 | 1.885 | 1.942 | 1.999 | 2.109 | 2.268 | 2.419 | 2.565  | 2.705  | 2.840  | 2.971  |
|                   | 1.123 | 1.385 | 1.480 | 1.682 | 1.900 | 2.385 | 3.246 | 4.275 | 5.484  | 6.883  | 8.482  | 10.292 |
| 0.00340<br>1/ 294 | 1.820 | 1.913 | 1.943 | 2.003 | 2.061 | 2.175 | 2.338 | 2.494 | 2.644  | 2.789  | 2.928  | 3.063  |
|                   | 1.158 | 1.428 | 1.526 | 1.734 | 1.959 | 2.459 | 3.347 | 4.408 | 5.654  | 7.096  | 8.745  | 10.610 |
| 0.00360<br>1/ 278 | 1.873 | 1.969 | 2.000 | 2.061 | 2.121 | 2.238 | 2.406 | 2.567 | 2.721  | 2.870  | 3.013  | 3.153  |
|                   | 1.192 | 1.470 | 1.571 | 1.785 | 2.016 | 2.531 | 3.444 | 4.536 | 5.819  | 7.303  | 9.000  | 10.919 |
| 0.00380<br>1/ 263 | 1.925 | 2.023 | 2.055 | 2.118 | 2.180 | 2.300 | 2.473 | 2.638 | 2.796  | 2.949  | 3.096  | 3.239  |
|                   | 1.225 | 1.510 | 1.614 | 1.834 | 2.071 | 2.601 | 3.539 | 4.661 | 5.979  | 7.504  | 9.247  | 11.220 |
| 0.00400<br>1/ 250 | 1.975 | 2.076 | 2.109 | 2.173 | 2.237 | 2.360 | 2.537 | 2.707 | 2.869  | 3.026  | 3.177  | 3.324  |
|                   | 1.257 | 1.550 | 1.656 | 1.882 | 2.126 | 2.669 | 3.632 | 4.783 | 6.135  | 7.700  | 9.489  | 11.513 |
| 0.00420<br>1/ 238 | 2.025 | 2.127 | 2.161 | 2.227 | 2.292 | 2.419 | 2.600 | 2.774 | 2.940  | 3.101  | 3.256  | 3.406  |
|                   | 1.288 | 1.588 | 1.697 | 1.929 | 2.178 | 2.735 | 3.722 | 4.902 | 6.287  | 7.891  | 9.724  | 11.798 |
| 0.00440<br>1/ 227 | 2.072 | 2.178 | 2.212 | 2.280 | 2.346 | 2.476 | 2.662 | 2.839 | 3.010  | 3.174  | 3.333  | 3.487  |
|                   | 1.318 | 1.626 | 1.738 | 1.974 | 2.230 | 2.800 | 3.810 | 5.018 | 6.436  | 8.078  | 9.954  | 12.077 |
| 0.00460<br>1/ 217 | 2.119 | 2.227 | 2.262 | 2.332 | 2.400 | 2.532 | 2.722 | 2.904 | 3.078  | 3.248  | 3.408  | 3.566  |
|                   | 1.348 | 1.663 | 1.777 | 2.019 | 2.280 | 2.863 | 3.896 | 5.131 | 6.582  | 8.260  | 10.179 | 12.350 |
| 0.00480<br>1/ 208 | 2.165 | 2.275 | 2.311 | 2.382 | 2.451 | 2.587 | 2.781 | 2.966 | 3.145  | 3.316  | 3.482  | 3.643  |
|                   | 1.378 | 1.699 | 1.815 | 2.063 | 2.330 | 2.925 | 3.980 | 5.242 | 6.724  | 8.438  | 10.399 | 12.616 |
| 0.00500<br>1/ 200 | 2.210 | 2.323 | 2.359 | 2.431 | 2.502 | 2.640 | 2.838 | 3.028 | 3.210  | 3.385  | 3.554  | 3.718  |
|                   | 1.406 | 1.734 | 1.853 | 2.105 | 2.378 | 2.986 | 4.063 | 5.351 | 6.863  | 8.613  | 10.614 | 12.877 |
| 0.00550<br>1/ 182 | 2.319 | 2.437 | 2.475 | 2.551 | 2.625 | 2.770 | 2.978 | 3.176 | 3.367  | 3.551  | 3.728  | 3.900  |
|                   | 1.475 | 1.819 | 1.944 | 2.209 | 2.495 | 3.132 | 4.262 | 5.613 | 7.200  | 9.035  | 11.134 | 13.509 |
| 0.00600<br>1/ 167 | 2.423 | 2.546 | 2.586 | 2.665 | 2.743 | 2.894 | 3.111 | 3.318 | 3.517  | 3.709  | 3.895  | 4.074  |
|                   | 1.541 | 1.901 | 2.031 | 2.308 | 2.606 | 3.273 | 4.453 | 5.864 | 7.521  | 9.439  | 11.631 | 14.111 |
| 0.00650<br>1/ 154 | 2.522 | 2.650 | 2.692 | 2.774 | 2.855 | 3.012 | 3.238 | 3.454 | 3.662  | 3.861  | 4.054  | 4.241  |
|                   | 1.604 | 1.979 | 2.114 | 2.402 | 2.713 | 3.407 | 4.635 | 6.104 | 7.829  | 9.826  | 12.108 | 14.690 |
| 0.00700<br>1/ 143 | 2.618 | 2.751 | 2.794 | 2.880 | 2.963 | 3.127 | 3.361 | 3.585 | 3.800  | 4.008  | 4.208  | 4.402  |
|                   | 1.665 | 2.054 | 2.195 | 2.493 | 2.816 | 3.536 | 4.811 | 6.336 | 8.126  | 10.198 | 12.567 | 15.246 |
| 0.00750<br>1/ 133 | 2.710 | 2.848 | 2.893 | 2.981 | 3.068 | 3.237 | 3.480 | 3.712 | 3.934  | 4.149  | 4.356  | 4.557  |
|                   | 1.724 | 2.126 | 2.272 | 2.581 | 2.916 | 3.661 | 4.981 | 6.559 | 8.413  | 10.557 | 13.009 | 15.783 |
| 0.00800<br>1/ 125 | 2.800 | 2.942 | 2.988 | 3.079 | 3.169 | 3.343 | 3.594 | 3.834 | 4.064  | 4.285  | 4.499  | 4.707  |
|                   | 1.781 | 2.196 | 2.347 | 2.667 | 3.012 | 3.781 | 5.145 | 6.775 | 8.689  | 10.905 | 13.437 | 16.302 |
| 0.00850<br>1/ 118 | 2.886 | 3.033 | 3.081 | 3.175 | 3.267 | 3.447 | 3.705 | 3.952 | 4.189  | 4.418  | 4.638  | 4.852  |
|                   | 1.836 | 2.264 | 2.419 | 2.749 | 3.105 | 3.898 | 5.304 | 6.984 | 8.958  | 11.242 | 13.852 | 16.806 |
| 0.00900<br>1/ 111 | 2.970 | 3.121 | 3.170 | 3.267 | 3.362 | 3.547 | 3.813 | 4.067 | 4.311  | 4.546  | 4.773  | 4.993  |
|                   | 1.890 | 2.330 | 2.490 | 2.829 | 3.195 | 4.012 | 5.458 | 7.188 | 9.219  | 11.569 | 14.255 | 17.295 |
| 0.00950<br>1/ 105 | 3.052 | 3.207 | 3.258 | 3.357 | 3.455 | 3.645 | 3.918 | 4.179 | 4.430  | 4.671  | 4.904  | 5.130  |
|                   | 1.942 | 2.394 | 2.558 | 2.907 | 3.283 | 4.122 | 5.608 | 7.385 | 9.472  | 11.887 | 14.647 | 17.770 |
| 0.01000<br>1/ 100 | 3.132 | 3.291 | 3.343 | 3.445 | 3.545 | 3.740 | 4.020 | 4.288 | 4.545  | 4.793  | 5.032  | 5.264  |
|                   | 1.992 | 2.457 | 2.625 | 2.983 | 3.369 | 4.230 | 5.754 | 7.578 | 9.719  | 12.197 | 15.029 | 18.233 |
| 0.01100<br>1/ 91  | 3.285 | 3.452 | 3.506 | 3.614 | 3.719 | 3.923 | 4.217 | 4.498 | 4.768  | 5.028  | 5.279  | 5.522  |
|                   | 2.090 | 2.577 | 2.754 | 3.129 | 3.534 | 4.437 | 6.036 | 7.949 | 10.195 | 12.794 | 15.764 | 19.125 |



Drainage Design at lot 1070 RP in

Project No.: D.D.109 Kam Tin Village

Date: 31-May-25

Prepared by: Ray Cheng

Check for the drainage capacity of proposed 300UC

|                 |    |   |               |                |                                    |
|-----------------|----|---|---------------|----------------|------------------------------------|
| Catchment area, | A3 | = | 791           | m <sup>2</sup> | Assume k = 1.0 for paved surface   |
|                 | A2 | = | 340           | m <sup>2</sup> | Assume k = 0.3 for unpaved surface |
| Total Area, A   |    | = | 791 + 0.3x340 |                |                                    |
|                 |    | = | 893           | m <sup>2</sup> |                                    |

Use Rational Method from Geo-Manual

$$Q = kiA/3600$$

where,

Q = Maximum runoff (lit/sec)

k = Runoff coefficient

i = Design mean intensity of rainfall (mm/hr)

A = Total catchment area (m<sup>2</sup>)

Longest distance from summit point to outlet, CP5(s)

(Ld) = 98.00 m

Shortest distance from summit point to outlet, CP5(s)

(Ls) = 45.00 m

Elevation of remote point (Pt A)

= 8.80 mPD

Elevation of outlet point, CP5(s)

= 7.60 mPD

Average fall, H

=  $(z_1 - z_2)/L_s \times 100$ 

= 2.67 m per 100m

From TGN30

$$T_c = 0.14465 \times L_d / (H^{0.2} \times A^{0.1})$$

$$= 5.77 \text{ min}$$

Assume a 1 in 50 year design rainfall return period for rural area

From SDM Corrigendum No. 1/2024

$$i = 220 \text{ mm/hr}$$

$$Q = \frac{kiA}{60} \times 1.16$$

$$= 3798 \text{ lit/min}$$

From TGN 43A1

For proposed 300 UC with 1 in 100 gradient

Maximum capacity = 8000 lit/min &gt; 3798 o.k.

The corresponding velocity = 1.75 m/s &lt; 4 o.k.



