寄件者: Rich Gold

寄件日期: 2025年09月04日星期四 17:26

收件者: tpbpd/PLAND

副本: David Chi Chiu CHENG/PLAND

主旨: Re: Planning Application No. A/YL-KTN/1149 - Submission of Further Information

附件: KTN1149_P25020B_FI_4.9.2025.pdf

類別: Internet Email

Dear Sir/Madam,

Attached please find our further information for the captioned application, which serves to supersede our previous submission in the preceding email dated 3.9.2025 at 5:13pm. Thank you.

Regards, Janice Tang

Rich Gold 於 2025 年 9 月 3 日 週三 下午 5:13 寫道:

Dear Sir/Madam,

Attached please find our further information for the captioned application. Thank you.

Regards, Janice Tang

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Goldrich Planners and Surveyors Ltd.

Gold Rich Planners & surveyors Ltd.

金潤規劃測量師行有限公司

Your Ref.: A/YL-KTN/1149

Our Ref.: P25020B/TL25295

4 September 2025

The Secretary

By Post and E-mail

Town Planning Board

tpbpd@pland.gov.hk

15/F., North Point Government Offices

333 Java Road, North Point, Hong Kong

Dear Sir,

Submission of Further Information (FI)

Proposed Temporary Warehouse (Excluding Dangerous Goods Godown) with Ancillary Facilities and Associated Filling of Land and Pond for a Period of 3 Years in "Agriculture" Zone, Lots 176 (Part), 179 RP (Part), 207 RP (Part) and 224 (Part) in D.D. 110, Yuen Long, New Territories

(Application No. A/YL-KTN/1149)

We would like to submit a drainage proposal (Plans 6.1 & 6.2) with hydraulic calculations and FSI proposal (Plan 7) for the captioned application. It serves to supersede our previous FI submission under our reference P25020B/TL25294 dated 3.9.2025.

We would like to clarify that about 1,326 m² of the site has been filled with concrete of about 0.2 m in depth (from 17.5mPD to 17.7mPD) and the pond (about 175 m²) within the site has been filled with soil and concrete of about 1.5 m in depth (from 16.2mPD to 17.7mPD).

Fencing (about 3 m high) will be erected along the site boundary by the applicant.

The applicant undertakes that no open storage activities will be carried out within the site. The construction materials will be stored in the enclosed structures. No maintenance, repairing, dismantling, cleaning or other workshop activities are proposed within the site.

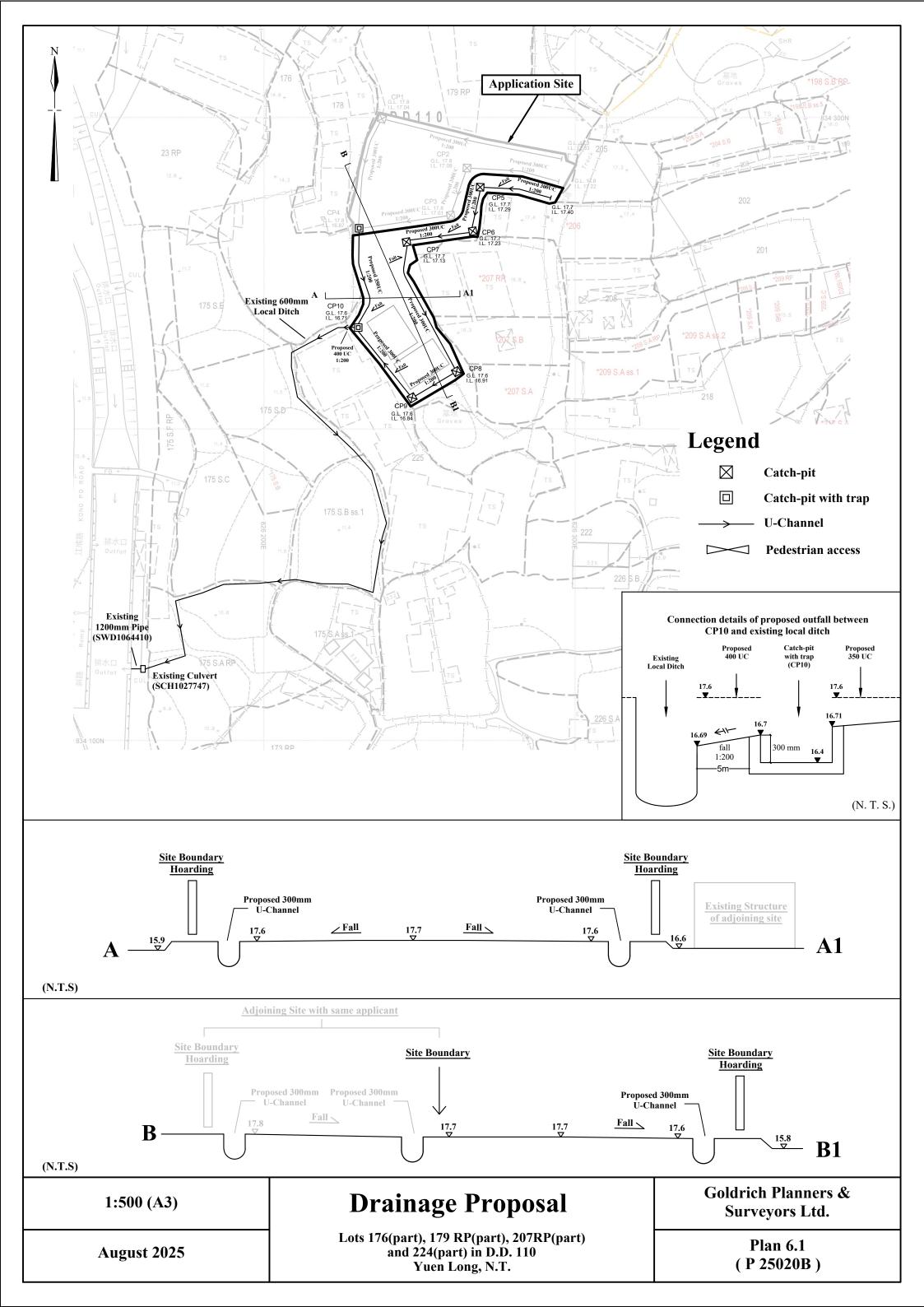
Yours faithfully, For and on behalf of Goldrich Planners & Surveyors Ltd.

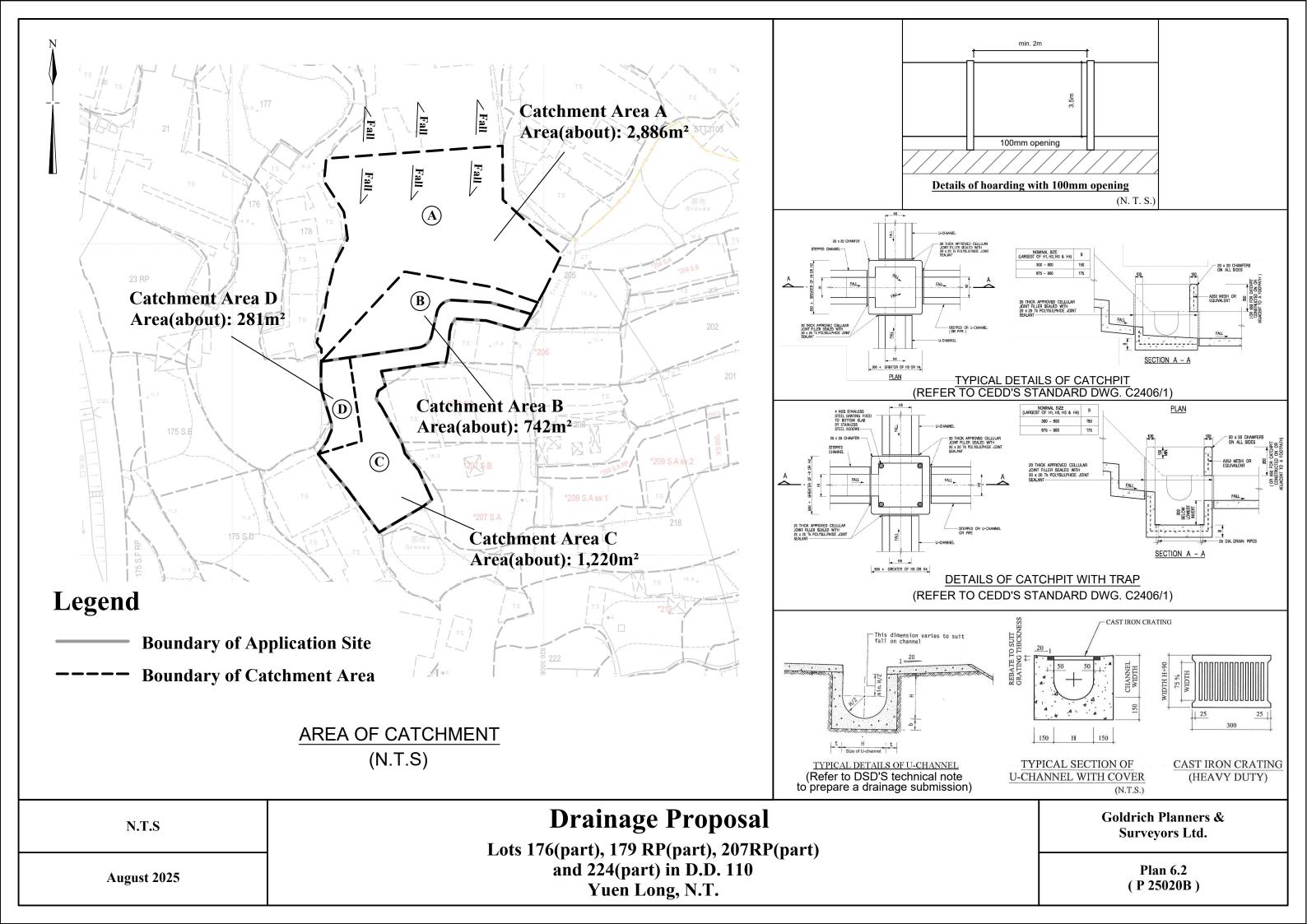
Francis LAU

Encl.

<u>c.c.</u>

DPO/FSYLE, PlanD (Attn.: Mr. David CHENG) By E-mail only





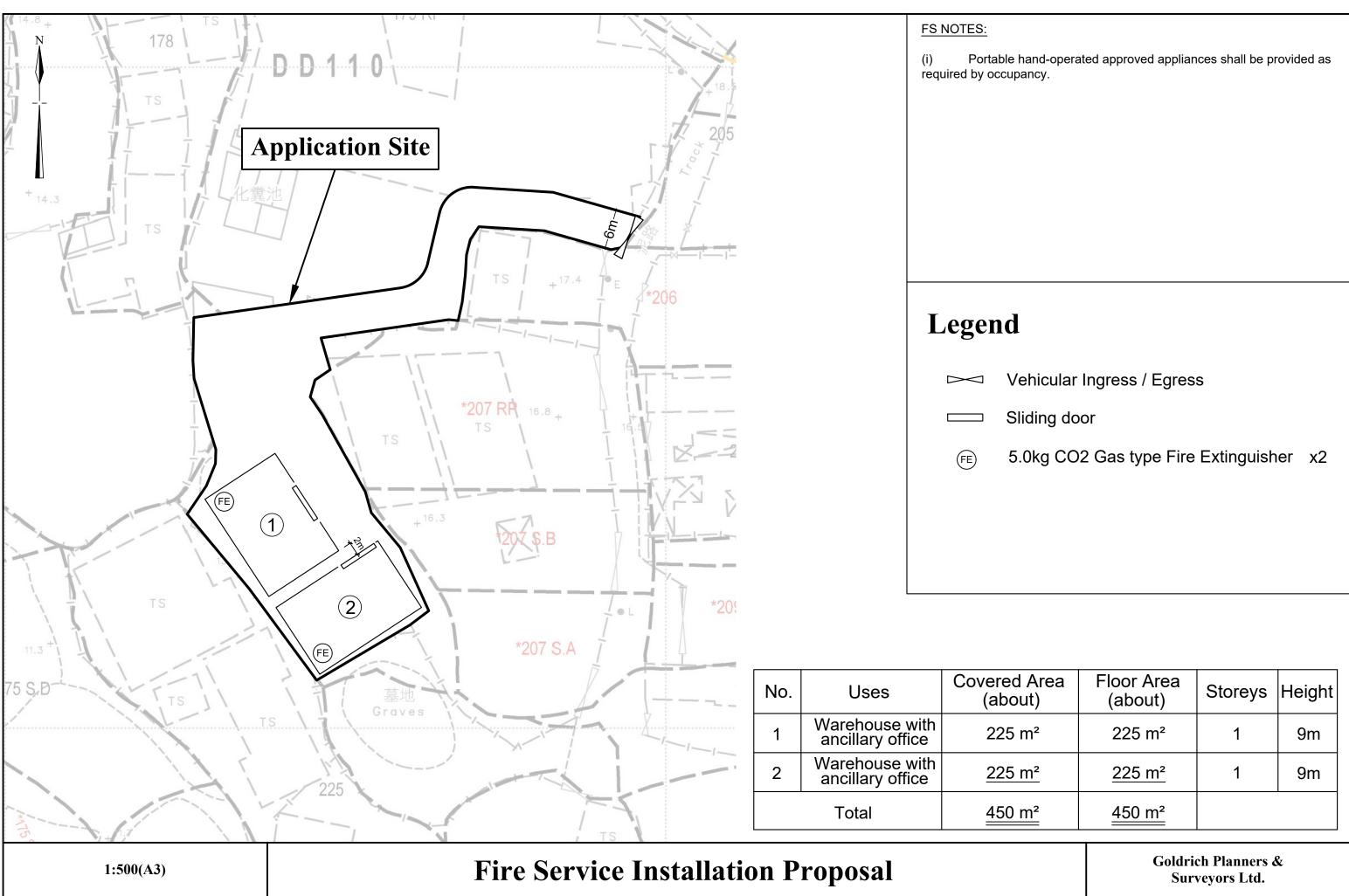
1 For Catchment Area A					Ref.	
Average slope Distance on the line of natural flow	H = L =	9	m per 100m m			
Time of concentraction	t _o = =	0.14465L / (H ^{0.2} A ^{0.1}) 0.9	= 0.14465 (9) / (0.1^0.2*28 min	386^0.1)	SDM 7.5.2 (d)	
2 For Proposed UC in Catchme	nt Are	а А				
Ground level (mPD) Invert level (mPD)	From 17.80 17.33					
Width of u-channel, Length of u-channel,	L _c =		m			
Depth of vertical part of u-channel Gradient of u-channel						
Cross-Section Area			= 0.5 x 3.14 x 150^2 + 300 x 780	1		
	=	π r + 2 d 2.031	$= 3.14 \times 150 + 2 \times 780$			
Hydralic radius,	R =	a/p			SDM 8.2.1	
3 Use Manning Equation for estimating velocity of stormwater						
	n = v =	$R^{1/6}x (RS_f)^{1/2}/n$	for concrete lined channels:- = (0.133)^1/6 x (0.133 x 0.005)^^	1/2 / 0.016	SDM Table 13 SDM Table 12	
Time of flow	t _f =	1.15 1.3	m/s min			
4 Use "Rational Method" for calculation of design flow						
Design intensity,			29)^0.355 for return period T = 50 y	/ears	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a	
Type of surface Flat Glassland(heavy soil) Concrete Paving		Runoff Coefficient C 0.25 0.95	0.0 2886.0	C x A 0.0 2741.7 2741.7	SDM 7.5.2 (b)	
Upstream flow	Q _u =	0	m ³ /s			
Design flow		$0.278i \Sigma C_j A_j + Q_u$ $0.278 \times 275 \times 2741.$ 0.210			SDM 7.5.2 (a)	
Allowable flow		a x v 0.269 x 1.15 0.309	m³/s			
> Q _d (O.K.)						
Reference was made to Stormwater Drainage Manual (SDM) by DSD						
Scale: NA		Hydraul	ic Calculation	Goldrich Pl Surveyor		
September 2025	Lots		207 RP (Part) and 224 (Part) in D.D. 110 Yuen Long, New Territories	Page (P2502		

1 For Catchment Area B					Ref.	
Area, Average slope, Distance on the line of natural flow,	A = H = L =	742 0.1 10	m ² m per 100m m			
Time of concentraction,	t _o = =		= 0.14465 (10) / (0.1^0.2*7 min	7 42^0.1)	SDM 7.5.2 (d)	
2 For Proposed UC in Catchmer	nt Area	а В				
Ground level (mPD) Invert level (mPD)	From 17.80 17.22					
Width of u-channel, Length of u-channel, Depth of vertical part of u-channel,	L _c =	300 69.6 780	m			
Gradient of u-channel,						
Cross-Section Area,		0.5 π r ² + w d 0.269	$= 0.5 \times 3.14 \times 150^2 + 300 \times 780$ m^2)		
Wetted Perimeter,		π r + 2 d	$= 3.14 \times 150 + 2 \times 780$			
Hydralic radius,	R = =	a / p 0.133	m		SDM 8.2.1	
3 Use Manning Equation for esti	matin	g velocity of storm	water			
			for concrete lined channels:- = (0.133)^1/6 x (0.133 x 0.005)^^- m/s	1/2 / 0.016	SDM Table 13 SDM Table 12	
Time of flow,	t _f =					
4 Use "Rational Method" for calculation of design flow						
Design intensity,)^0.355 for return period T = 50 y	/ears	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a	
<u>Type of surface</u> Flat Glassland(heavy soil) Concrete Paving		Runoff Coefficient C 0.25 0.95	0.0 742.0	C x A 0.0 704.9 704.9	SDM 7.5.2 (b)	
Upstream flow,	Q _u =	0	m ³ /s			
Design flow,		$0.278i \Sigma C_j A_j + Q_u$ $0.278 \times 276 \times 704.9$ 0.054			SDM 7.5.2 (a)	
Allowable flow,		a x v 0.269 x 1.15 0.310	m³/s			
> Q _d (O.K.)						
Reference was made to Stormwater Drainage Manual (SDM) by DSD						
Scale: NA		Hydraul	ic Calculation	Goldrich Pl Surveyor		
September 2025	Lots		207 RP (Part) and 224 (Part) in D.D. 110 Yuen Long, New Territories	Page (P2502		

1 For Catchment Area C					Ref.
Area, Average slope, Distance on the line of natural flow,	A = H = L =	1220 0.1 10			
Time of concentraction,	t _o = =		= 0.14465 (10) / (0.1^0.2*1	220^0.1)	SDM 7.5.2 (d)
2 For Proposed UC in Catchmen	it Area	а С			
Ground level (mPD)	From 17.70 17.40				
Width of u-channel, Length of u-channel, Depth of vertical part of u-channel,	L _c =	300 137.2 740	m		
Gradient of u-channel,					
Cross-Section Area,		$0.5 \pi r^2 + w d$ 0.257	$= 0.5 \times 3.14 \times 150^{2} + 300 \times 740^{2}$ m^{2})	
Wetted Perimeter,		π r + 2 d	$= 3.14 \times 150 + 2 \times 740$		
Hydralic radius,	R = =				SDM 8.2.1
Use Manning Equation for esting	matin	g velocity of storm	water		
			for concrete lined channels:- = (0.132)^1/6 x (0.132 x 0.005)^^	1/2 / 0.046	SDM Table 13 SDM Table 12
-	=	1.15	m/s	1/2 / 0.010	SDIVI TABLE 12
Time of flow, t _f = 2.0 min 4 Use "Rational Method" for calculation of design flow					
Design intensity,	j =	$a / (t_o + t_f + b)^c$)^0.355 for return period T = 50 y	/ears	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a
Type of surface Flat Glassland(heavy soil) Concrete Paving		Runoff Coefficient C 0.25 0.95	0.0 1220.0	<u>C x A</u> 0.0 1159.0 1159.0	SDM 7.5.2 (b)
Upstream flow,	Q _u =	0	m ³ /s		
Design flow,		0.278i Σ C _j A _j + Q _u 0.278 x 261 x 1159 μ 0.084			SDM 7.5.2 (a)
Allowable flow,		a x v 0.257 x 1.15 0.296	m³/s		
> Q _d (O.K.)					
Reference was made to Stormwater Drainage Manual (SDM) by DSD					
Scale: NA		Hydraul	ic Calculation	Goldrich Pl Surveyor	
September 2025	Lots		207 RP (Part) and 224 (Part) in D.D. 110 Yuen Long, New Territories	Page (P2502	

1 For Catchment Area D					Ref.	
Area, Average slope, Distance on the line of natural flow,	A = H = L =	281 0.1 5	m ² m per 100m m			
Time of concentraction,	t _o =	· ·) = 0.14465 (5) / (0.1^0.2*28 min	31^0.1)	SDM 7.5.2 (d)	
2 For Proposed UC in Catchmer	nt Are	ea D				
	From	То	_			
Ground level (mPD)	17.80					
Invert level (mPD)	16.87	16.71	-			
Width of u-channel,	w =	350	mm			
Length of u-channel,						
Depth of vertical part of u-channel,			mm			
Gradient of u-channel,						
,		(10101 1011 1),01				
Cross-Section Area,	a =		= 0.5 x 3.14 x 175 ² + 350 x 715 m ²	;		
Wetted Perimeter,	p =	π r + 2 d	= 3.14 x 175 + 2 x 715			
	=	1.980				
Hydralic radius,	R =	: a/p			SDM 8.2.1	
	=	0.151	m			
3 Use Manning Equation for esti	3 Use Manning Equation for estimating velocity of stormwater					
Take	n =	0.016	for concrete lined channels:-		SDM Table 13	
Allowable velocity.	v =	$R^{1/6}x (RS_f)^{1/2}/n$	$= (0.151)^1/6 \times (0.151 \times 0.005)^1$	1/2 / 0.016	SDM Table 12	
<i>,</i>	=					
Time of flow,	t _f =	0.4	min			
4 Use "Rational Method" for calculation of design flow						
Design intensity,		505.5 / (0.7+0.4+3.2	29)^0.355 for return period T = 50 y	/ears	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a	
Time of audions		Dunest Coefficient C	Catalana ant Ana a A (m²)	O A	CDM 7.5.0 (b)	
Type of surface		Runoff Coefficient C	Catchment Area A (m ²) 0.0	<u>C x A</u>	SDM 7.5.2 (b)	
Flat Glassland(heavy soil) Concrete Paving		0.25 0.95	281.0	0.0 267.0		
Concrete Paving		0.95	201.0 SUM =			
			30W -	201.0		
Upstream flow,	Q _u =	0.264	m ³ /s			
Design flow,		0.278 x 300 x 266.9			SDM 7.5.2 (a)	
		0.200	/0			
Allowable flow,		a x v 0.298 x 1.27				
	=	0.379	m ³ /s			
> Q _d (O.K.)						
Reference was made to Stormwater Drainage Manual (SDM) by DSD						
Scale: NA		II,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	ia Calaulatian	Goldrich Pl		
Scarc. IVA		Hyaraul	ic Calculation	Surveyor	rs Ltd.	
	Lots	176 (Part) 179 RP (Part)	207 RP (Part) and 224 (Part) in D.D. 110	D _c ===	. 1	
September 2025	Lots		Yuen Long, New Territories	Page		
				(P2502	(שטי	

1 For Connection Between CP10 and Existing 600 Local Ditch				Ref.	
Area, A = 0 m^2 Average slope, H = $0.1 \text{ m per } 100 \text{m}$ Distance on the line of natural flow, L = 0 m					
Average slope,	H =	0.1 m per 100m			
Distance on the line of natural flow,	L =	0 m			
Time of concentraction,	t _o = =	$0.14465L / (H^{0.2}A^{0.1}) = 0.14465 (0) / (0.1^{0.2*0}$ 0.0 min	^ 0.1)	SDM 7.5.2 (d)	
2 For Proposed UC after CP10					
	From	То			
Ground level (mPD) Invert level (mPD)	17.60 16.71				
Width of u-channel,		400 mm			
Length of u-channel,					
Depth of vertical part of u-channel,		(16.71-16.69)/5 = 0.005			
Gradient of d-channel,	o _f –	(10.71-10.09)/3 - 0.003			
Cross-Section Area,	a =	2	5		
Wetted Perimeter,	p =	π r + 2 d = 3.14 x 200 + 2 x 715			
Hydralic radius,	=	2.058 m		SDM 8.2.1	
Hydralic radius,	=	α/ρ 0.169 m		3DIVI 6.2.1	
3 Use Manning Equation for esti	matin	g velocity of stormwater			
Take	n =	0.016 for concrete lined channels:-		SDM Table 13	
Allowable velocity,	v =	$R^{1/6}x (RS_f)^{1/2}/n = (0.169)^{1/6} x (0.169 \times 0.005)^{1/6}$	1/2 / 0.016	SDM Table 12	
	. =	1.00 11/0			
Time of flow, t _f = 0.1 min					
4 Use "Rational Method" for calculation of design flow					
Design intensity,		$a / (t_o + t_f + b)^c$ 505.5 / (0+0.1+3.29)^0.355 for return period T = 50 329	years	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a	
<u>Type of surface</u> Flat Glassland(heavy soil)		Runoff Coefficient C Catchment Area A (m²) 0.25 0.0	<u>C x A</u> 0.0	SDM 7.5.2 (b)	
Concrete Paving		0.95 0.0 SUM =	0.0		
Upstream flow,	Q _u =	0.370 m ³ /s			
Design flow,		0.278i Σ C _j A _j + Q _u where A _j is in km ² 0.278 x 329 x 0 / 1000000 + 0.37		SDM 7.5.2 (a)	
	=	0.370 m ³ /s			
Allowable flow, $Q_a = a \times v$					
$= 0.349 \times 1.35$					
	=	0.472 m ³ /s			
> Q _d (O.K.)					
Reference was made to Stormwater Drainage Manual (SDM) by DSD					
			Goldrich Pl	onners Pr	
Scale: NA		Hydraulic Calculation	Goldrich Pl Surveyor		
		•			
September 2025	Lots	IZ T' NI A NI T 'A '		Page 5	
		Tame Taring, Twen Long, New Territories	(P25020B)		



Lots 176(part), 179 RP(part), 207RP(part) and 224(part) in D.D. 110 Yuen Long, N.T.

September 2025

Plan 7 (P 25020B)