

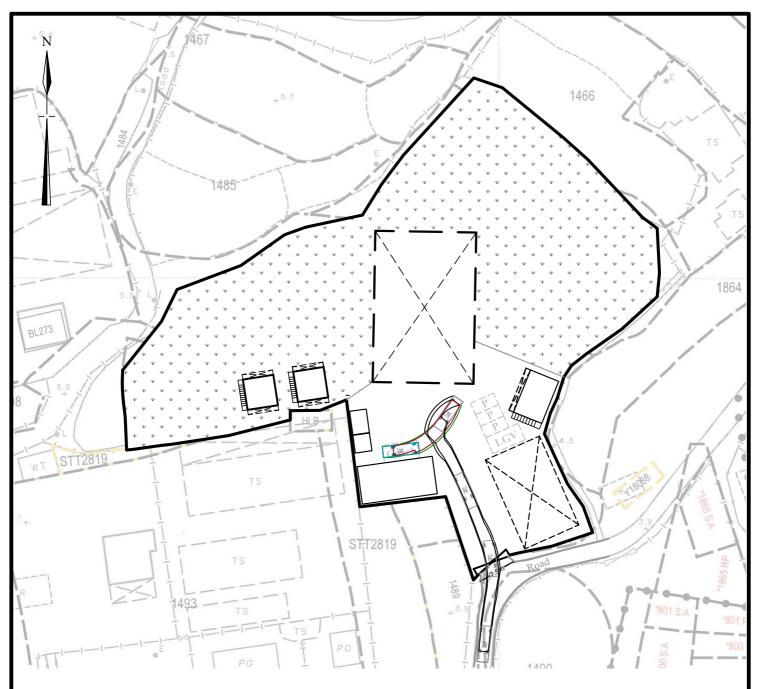
- (/	III (L) X 3.3III (W))	Site in	ca. abou	ι ,,,	Jun
No.	Structure / Use	Floor Area (about)	Covered Area (about)	Height	No. of Storeys
1	Open Shed	600m ²	600m ²	7m	1
2	G/F: Multi-function Room (Animal activity room, social event room and ancillary office)	56m²	56m²	7	2
2	1/F: Roof	37m²	1	7m	2
3	G/F: Multi-function Room (Animal activity room, social event room and ancillary office)	56m²	56m²	7	2
	1/F: Roof	37m²		7m	
4	G/F: Multi-function Room (Animal activity room, social event room and ancillary office)	67m²	67m²	_	2
4	1/F: Roof	58m²	0/111-	7m	2
5	Open Shed	226m²	226m²	7m	1
6	Multi-function Room (Animal activity room, social event room and ancillary office)	225m²	112.5m ²	7m	2
7	Toilet	15m²	15m²	5m	1
8	Toilet	<u>12m²</u>	<u>12m²</u>	5m	1
	Total:	1,389m ²	1,144.5m ²		•

Layout Plan Lots 1464(part), 1466(part), 1486(Part), 1489(Part), 1494(part) and adjoining Government Land in D. D. 107 Yuen Long, New Territories

Goldrich Planners & Surveyors Ltd.

> Plan 3 (P22034)

1:750



Legend

Vehicular Ingress / Egress

 $\begin{bmatrix} P \end{bmatrix}$

Parking space for private cars (5m (L) x 2.5m (W))

LGV

Parking space for light goods vehicles

 $(7m (L) \times 3.5m (W))$

Coach

Parking space for coaches (7m (L) x 3.5m (W))

Cook

Coach

 $(7m (L) \times 2.5m (W))$

1	•	7511
1	•	130

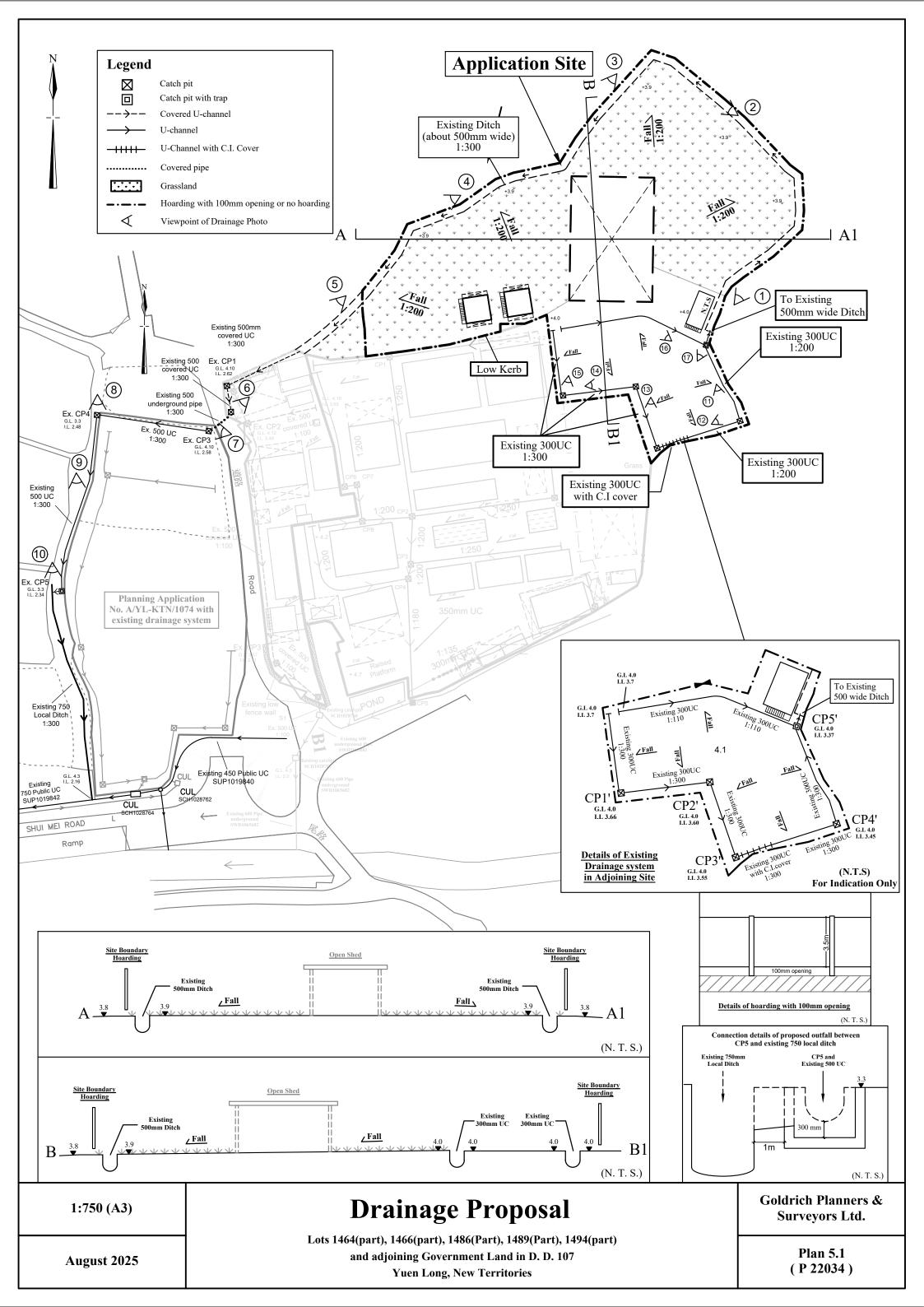
Swept Path Analysis

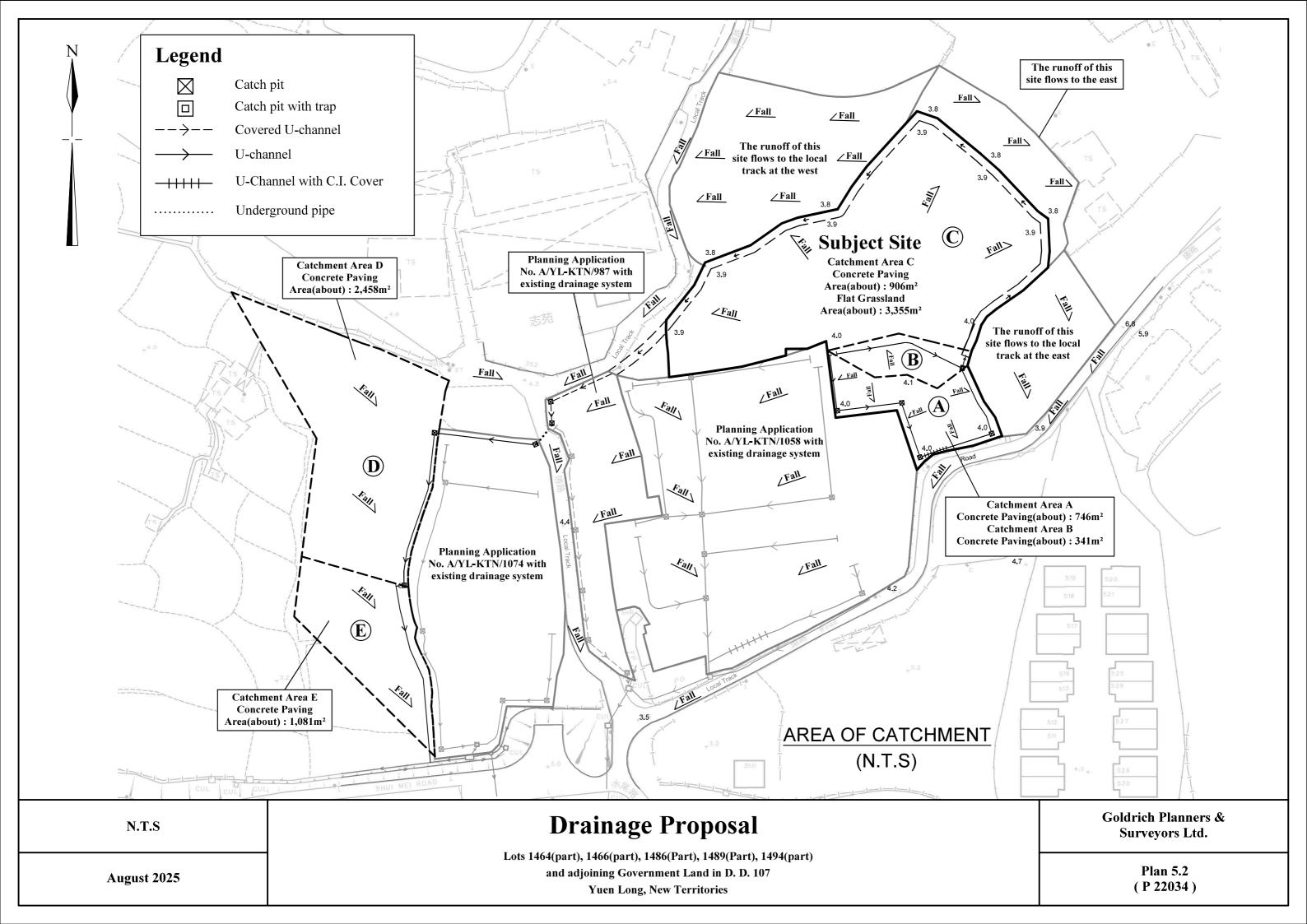
Lots 1464(part), 1466(part), 1486(Part), 1489(Part), 1494(part) and adjoining Government Land in D. D. 107
Yuen Long, New Territories

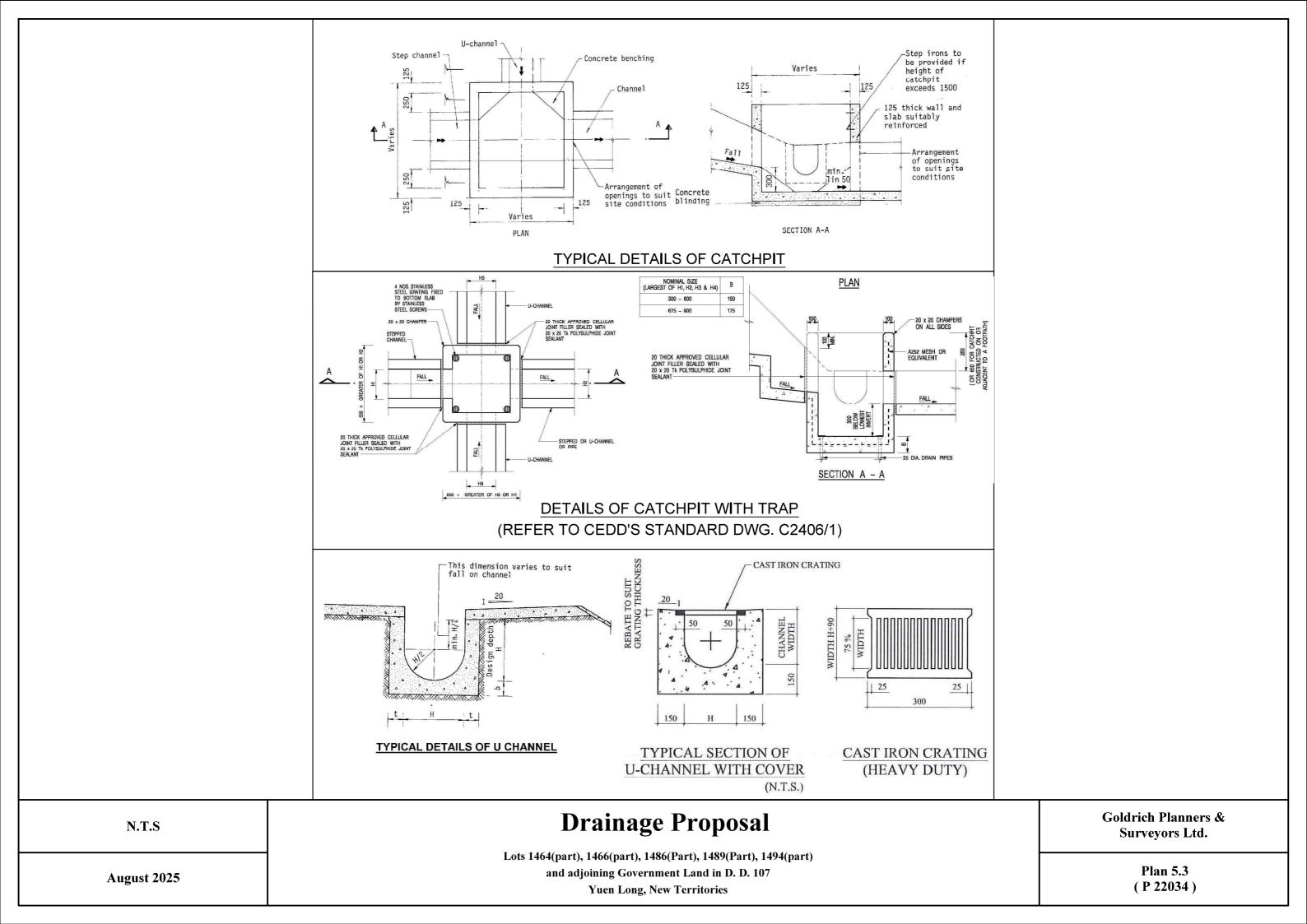
Goldrich Planners & Surveyors Ltd.

Plan 4 (P22034)

August 2025







1 For Catchment Area A					Ref.
A	•	= 742	2		
Area, Average slope,			m per 100m		
Distance on the line of natural flow,					
Time of concentraction,	t _o =	•	= 0.14465 (21) / (0.1^0.2*) min	742^0.1)	SDM 7.5.2 (d)
2 For Existing U-Channel in ca	tchn	nent area A			
	From	то То			
Ground level (mPD)	4.00	4.00	-		
Invert level (mPD)	3.70	3.37	-		
Width of u-channel,	١٨/ =	300	mm		
Length of u-channel,					
Depth of vertical part of u-channel,			mm		
Gradient of u-channel,					
		,			
Cross-Section Area,		= $0.5 \pi r^2 + w d$ = 0.178	$= 0.5 \times 3.14 \times 150^{2} + 300 \times 476$	5	
Wetted Perimeter,		- υ.۱/δ - π r + 2 d	m = 3.14 x 150 + 2 x 476		
welled Fellinelel,	р - =		m		
Hydralic radius,		= a/p			SDM 8.2.1
,	- =		m		
3 Use Manning Equation for es	stima	ating velocity of s	tormwater		
•					
Take			for concrete lined channels:-		SDM Table 13
Allowable velocity,	v =	$= R^{1/6}x (RS_f)^{1/2}/n$	= (0.125)^1/6 x (0.125 x 0.003)^	1/2 / 0.016	SDM Table 12
T'	_ =	0.00			
Time of flow,	·		min		
4 Use "Rational Method" for ca		_	OW		
Design intensity,					SDM 4.3.2
	=	= 505.5 / (2.9+0.5+3.	29)^0.35{ for return period T = 50	years	Corrigendum 1/2024
	=	= 246			SDM Table 3a
Type of surface		Runoff Coefficient C	Catchment Area A (m ²)	<u>C x A</u>	SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	0.0	0.0	
Concrete Paving		0.95	742.0	704.9	
			SUM =	704.9	
Upstream flow,	Q _u =	- 0	m ³ /s		
Danier Brown	0	- 0.270; \(\cap \cap \cap \cap \cap \cap \cap \cap	whore A is in k-2		CDM 7 F O (-)
Design flow,			where A _j is in km ²		SDM 7.5.2 (a)
	=	0.278 x 246 x 704.9			
	=	0.048	m~/s		
Allowable flow,	Q. =	= axv			
		= 0.178 x 0.9			
	=	= 0.161	m³/s		
	>	Q_d (O.K.)			
Reference was made to Stormwate	er Dra	inage Manual (SDM)	by DSD		
Scale: NA		Hydraul	ic Calculation		Planners &
		T / 1421 @ 1 115	C (D. A. 1400 (D. A. 1404 (D.)	Surve	eyors Ltd.
Dagamhar 2024			6 (Part), 1489 (Part), 1494 (Part) vernment Land in D. D. 107	P	age 1
December 2024			en Long, N. T.		22034)
		1 0		(4.5	,

4. For Cotohmont Area B					Def
1 For Catchment Area B					Ref.
		343			
Average slope, Distance on the line of natural flow,	H =	0.1 25	m per 100m m		
Time of concentraction,	t _o =	•	.1) = 0.14465 (25) / (0.1^0.2*3	343^0.1)	SDM 7.5.2 (d)
2 For Existing U-Channel in ca	tchn	nent area B			
	From		_		
Ground level (mPD) Invert level (mPD)	4.00 3.70	4.00 3.37			
<u> </u>			-		
Width of u-channel, Length of u-channel, Depth of vertical part of u-channel, Gradient of u-channel,	w =	300	mm		
Length of u-channel,	L _c =	36.2	m		
Depth of vertical part of u-channel,	d =	480	mm		
Gradient of u-channel,	S _f =	(3.7-3.37)/36.2	= 0.009		
Cross-Section Area,		$0.5 \pi r^2 + w d$ 0.179	= 0.5 x 3.14 x 150 ² + 300 x 480 m ²		
Wetted Perimeter,	p =	$\pi r + 2 d$	$= 3.14 \times 150 + 2 \times 480$		
Hydralic radius,	R =	: a/p			SDM 8.2.1
•	=	0.125	m		
3 Use Manning Equation for es			stormwater for concrete lined channels:-		SDM Table 13
Allowable velocity,	v =	$= R^{1/6}x (RS_f)^{1/2}/n$	= $(0.125)^1/6 \times (0.125 \times 0.009)^1$	1/2 / 0.016	SDM Table 12
	=	1.49			
Time of flow,	t _f =	0.4	min		
4 Use "Rational Method" for ca	alcul	ation of design f	low		
Design intensity,	i =	: a / (t _a + t _i +b) ^c			SDM 4.3.2
		505.5 / (2.9+0.5+3	3.29)^0.35:for return period T = 50 y	/ears	Corrigendum 1/2024 SDM Table 3a
Type of surface		Runoff Coefficient (C Catchment Area A (m ²)	<u>C x A</u>	SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	0.0	0.0	- ()
Concrete Paving		0.95	343.0	325.9	
			SUM =	325.9	
Upstream flow,	Q _u =	. 0	m ³ /s		
Design flow.	Q _d =	: 0.278i Σ C _i A _i + Q ₁₁	where A _i is in km ²		SDM 7.5.2 (a)
,		: 0.278 x 255 x 325.			` ,
	=	0.023	m^3/s		
AH. 11.6	0				
Allowable flow,		: a x v : 0.179 x 1.49			
	=		m ³ /s		
= 0.268 m /s > Q _d (O.K.)					
Reference was made to Stormwate) by DSD		
Scale: NA		Hydraul	lic Calculation		Planners &
~~~~		•		Survey	ors Ltd.
December 2024		and adjoining Go	6 (Part), 1489 (Part), 1494 (Part) overnment Land in D. D. 107	Pag	
		Yu	en Long, N. T.	(P22	034)

1 For Catchment Area C					Ref.
					1.0
Area,	A =	3944			
Average slope,			m per 100m		
Distance on the line of natural flow,	L =	66	m		
Time of concentraction,	t _o =		) = 0.14465 (66) / (0.1^0.2*3	3944^0.1)	SDM 7.5.2 (d)
2 For Existing Ditch in catchm	ent a	rea C			
	From	То			
Ground level (mPD)	4.00	3.90	-		
Invert level (mPD)	3.37	2.68	-		
Width of u-channel,	w =	500	mm		
Length of u-channel,	L _c =	206.7	m		
Depth of vertical part of u-channel,	d =	969	mm		
Gradient of u-channel,	S _f =	(3.37-2.681)/206.7	= 0.0033		
Cross-Section Area.	a =	$0.5 \pi r^2 + w d$	= 0.5 x 3.14 x 250^2 + 500 x 969	)	
			2		
Wetted Perimeter	n =	π r + 2 d	m ² = 3.14 x 250 + 2 x 969		
	=	2.123	m		
Hydralic radius,		a / p			SDM 8.2.1
. , , a.	=	0.214	m		02 0.2
3 Use Manning Equation for es	stima	ting velocity of st	tormwater		
Take	n =	0.0225	for earth lined channels:-		SDM Table 13
			$= (0.214)^{1/6} \times (0.214 \times 0.003)^{1/6}$	1/2 / 0 0225	SDM Table 12
/ illowable velocity,	=	0.92		172 7 0.0220	OBIVI TUBIC 12
Time of flow,	t _f =	3.8	min		
4 Use "Rational Method" for ca	alcula	ation of design flo	ow		
Design intensity,	i =	$a / (t_0 + t_f + b)^c$			SDM 4.3.2
			$(29)^0.355$ for return period T = 50 y	/ears	Corrigendum 1/2024
	=				SDM Table 3a
Type of surface		Runoff Coefficient C	Catchment Area A (m ² )	<u>C x A</u>	SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	2765.0	691.3	(-)
Concrete Paving		0.95	1179.0	1120.1	
·			SUM =	1811.3	
Upstream flow,	Q ₁₁ =	0.071	m³/s		
·			_		
Design flow,			where A _j is in km ²		SDM 7.5.2 (a)
	=	0.278 x 200 x 1811			
	=	0.172	m ³ /s		
Allowable flow,	Q ₂ =	axv			
		0.583 x 0.92			
	=		$m^3/s$		
	>	Q _d (O.K.)			
Reference was made to Stormwater Drainage Manual (SDM) by DSD					
Scale: NA		Hydraul	ic Calculation		Planners &
Scare. 141		•		Survey	ors Ltd.
_			6 (Part), 1489 (Part), 1494 (Part)	Pя	ge 3
December 2024			vernment Land in D. D. 107		2034)
		Yue	en Long, N. T.	(1.7.	2037 <i>)</i>

1 For Catchment Area between	n Exi	sting Ditch and C	P2		Ref.
Area,	Δ =	. 0	$m^2$		
Average slope,			m per 100m		
Distance on the line of natural flow,	L =	. 0	m		
Time of concentraction,	t _o =	•	) = 0.14465 (0) / (0.1^0.2*0 ⁴ min	^0.1)	SDM 7.5.2 (d)
2 For Existing U-Channel betw	een	Existing Ditch an	d CP2		
	From				
Ground level (mPD)	3.90	4.10			
Invert level (mPD)	2.68	2.59	-		
Width of u-channel,	w =	500	mm		
Length of u-channel,	L _c =	27.7	m		
Depth of vertical part of u-channel,			mm		
Gradient of u-channel,	S _f =	(2.68-2.59)/27.7	= 0.0033		
Cross-Section Area,	a =	$0.5 \pi r^2 + w d$	= 0.5 x 3.14 x 250^2 + 500 x 126	60	
,		0.728			
Wetted Perimeter,	p =	$\pi r + 2 d$	= 3.14 x 250 + 2 x 1260		
	=	3.305			
Hydralic radius,	R =	: a/p			SDM 8.2.1
	=	0.220	m		
3 Use Manning Equation for es	stima	nting velocity of s	tormwater		
Take	n =	0.0160	for concrete lined channels:-		SDM Table 13
Allowable velocity,	v =	$= R^{1/6}x (RS_f)^{1/2}/n$	$= (0.22)^{1/6} \times (0.22 \times 0.003)^{1/2}$	2 / 0.016	SDM Table 12
•	=	1.31			
Time of flow,	t _f =	0.4	min		
4 Use "Rational Method" for c	alcul	ation of design flo	ow		
Design intensity,	i =	$= a / (t_o + t_f + b)^c$			SDM 4.3.2
			29) 0 .355 for return period T = 50	years	Corrigendum 1/2024
	=			•	SDM Table 3a
Type of surface		Runoff Coefficient C	Catchment Area A (m ² )	<u>C x A</u>	SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	0.0	0.0	, ,
Concrete Paving		0.95	0.0	0.0	
			SUM =	0.0	
Upstream flow,	Q _u =	0.172	m ³ /s		
Dosign flow	0	: 0 278i 5 CA + O	where A _i is in km ²		SDM 7.5.2 (a)
Design flow,		: 0.2781			ואוטט (a) אוטט (a)
		0.270 X 319 X 07 10 0.172			
	=	0.172	m /s		
Allowable flow,	Q _a =	axv			
		: 0.728 x 1.31			
	=	0.951	m ³ /s		
	>	Q _d (O.K.)			
Reference was made to Stormwate			by DSD		
G 1 31		Hydraul	ic Calculation	Goldrich	Planners &
Scale: NA		11yur aur	ic Caiculativii		yors Ltd.
		· //	6 (Part), 1489 (Part), 1494 (Part)		ge 4
December 2024			vernment Land in D. D. 107		2034)
		Yue	en Long, N. T.	(P2	203 <del>1</del> )

1 For Catchment Area between	CP2 and CP3	Ref.
Area, A	$\alpha = 0 \text{ m}^2$	
	N = 0 m N = 0.1 m per 100m	
Distance on the line of natural flow, L	= <b>0</b> m	
Time of concentraction, $t_c$	$ = 0.14465L / (H^{0.2}A^{0.1}) = 0.14465 (0) / (0.1^{0.2}0^{0.1}) $ $ = 0.0 min $	SDM 7.5.2 (d)
2 For Underground Pipe betwee	n CP2 and CP3	
Size(Diameter) w		
Length of Pipe Design the pipe to 9/10 full bore		
Area of ventilated portion	= 0.1 of pipe area	
$\frac{1}{2}$ r ² $\theta$ - $\frac{1}{2}$ r ² sin( $\theta$ )	= 0.1 $\pi$ r ²	
$\theta$ - $\sin(\theta)$	= 0.2 π	
heta	= 1.63 rad = $93.4^{\circ}$ (By trial and error)	
Area A	$\alpha = 0.9 \pi r^2$	
	$= 0.9 \times 3.14 \times 500^{2}$ $= 0.707  m^{2}$	SDM 8.2.1
	$\theta = 2 \pi r - r \theta = 2327 \text{ mm}$	
Hydralic radius F	R = A/P $303.7$ mm	
Use Manning Equation for est	imating velocity of stormwater	
	1: 300	
	= 0.016 for concrete lined channels:-	SDM Table 1
Allowable velocity, v	= $R^{1/6}x (RS_f)^{1/2}/n$ = $(303.7)^1/6 * (303.7/300)^1/2 / 0.016$ = $1.35 \text{ m/s}$	SDM Table 1
	= 0.04 min	
Use "Rational Method" for cal	culation of design flow	
Design intensity,	$i = a / (t_o + t_f + b)^c$	SDM 4.3.2
	= 505.5 / (2.9+0.04+3.29)^0.355 for return period T = 50 years = 330	Corrigendum 1/20 SDM Table 3a
Type of surface	Runoff Coefficient C Catchment Area A (m²) C x A	SDM 7.5.2 (b
Flat Glassland(heavy soil)	0.25 <b>0.0</b> 0.0	
Concrete Paving Macadam Roadways	0.95 <b>0.0</b> 0.0 0.425 <b>0.0</b> 0.0	
Wooded Areas	0.105	
Upstream flow, G	$Q_{\rm u} = 0.172 \text{ m}^3/\text{s}$	
Design flow	$Q_d = 0.278i \Sigma C_i A_i + Q_u$ where $A_i$ is in km ²	SDM 7.5.2 (a
Design now, o	$= 0.278 \times 330 \times 0 / 1000000 + 0.172$ $= 0.172 \text{ m}^3/\text{s}$	3DW 7.3.2 (a
Allowable flow, G	$Q_a = 0.9 \times a \times v$ (10% reduction in flow area due to deposition of sediment) = $0.9 \times 0.3974 \times 1.35$ = $0.856 \text{ m}^3/\text{s}$	
	> Q _d (O.K.)	
Reference was made to Stormwater		
Scale: NA	Hydraulic Calculation Goldrich Pl	
	Surveyor	rs Ltd.
December 2024	Lots 1464 (Part), 1486 (Part), 1489 (Part), 1494 (Part) and adjoining Government Land in D. D. 107  Page	
Describer 2027	Yuen Long, N. T. (P220	34)

1 For Catchment Area D					Ref.
Δτρο	Δ =	2458	$m^2$		
Average slope,			m per 100m		
Distance on the line of natural flow,					
Time of concentraction,	t _o =	•	) = 0.14465 (33) / (0.1^0.2*) min	2458^0.1)	SDM 7.5.2 (d)
2 For U-channel between Exist	ing(	CP3 and CP5			
	From		_		
	4.10	3.30			
Invert level (mPD)	2.58	2.34	-		
Width of u-channel,	w =	500	mm		
Length of u-channel,					
Depth of vertical part of u-channel,			mm		
Gradient of u-channel,					
Cross-Section Area,	a =		= 0.5 x 3.14 x 250^2 + 500 x 710	)	
	=		m ²		
Wetted Perimeter,			= 3.14 x 250 + 2 x 710		
14.3.2.0.0.0	_ =		m		004004
Hydralic radius,	K =		m		SDM 8.2.1
3 Use Manning Equation for es	tima				
Take			for concrete lined channels:-		SDM Table 13
Allowable velocity,	v =		$= (0.205)^{1/6} \times (0.205 \times 0.003)^{1/6}$	1/2 / 0.016	SDM Table 12
Time of flow,			min		
4 Use "Rational Method" for ca	lcul	ation of design flo	ow		
Design intensity,	i =	: a / (t + t, +b) ^c			SDM 4.3.2
Booign interiority,			29) $^{\circ}$ 0.355 for return period T = 50	vears	Corrigendum 1/2024
	=		· · ·	years	SDM Table 3a
Type of surface		Runoff Coefficient C	Catchment Area A (m ² )	CxA	SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	0.0	0.0	(2)
Concrete Paving		0.95	2458.0	2335.1	
			SUM =	2335.1	
Upstream flow,	Q _u =	0.172	m ³ /s		
Design flow	O. =	: 0.278i Σ C:A· + Ω	where A _i is in km ²		SDM 7.5.2 (a)
Design now,			.1 / 1000000 + 0.172		ODW 7.0.2 (a)
	=	0.369			
Allowable flow,	Q _a =	: axv			
	=	0.453 x 1.26			
	=	0.573	m ³ /s		
	>	Q _d (O.K.)			
Reference was made to Stormwate	r Dra	inage Manual (SDM)	by DSD		
Scale: NA		Hydraul	ic Calculation	Goldrich	Planners &
Scale: NA				Survey	yors Ltd.
			6 (Part), 1489 (Part), 1494 (Part)		ge 6
December 2024			vernment Land in D. D. 107		-
		Yue	en Long, N. T.	(P2)	2034)

				I	
For Catchment Area E				Ref.	
Area.	A =	1081	$m^2$		
Average slope,			m per 100m		
Distance on the line of natural flow,					
Time of concentraction,	t _o =	,	) = 0.14465 (33) / (0.1^0.2**) min	(1081^0.1) SDM 7.5.2	<u>?</u> (d
For Existing Local Ditch in c	atch	ment area E			
Crown d lovel (mcDD)	From		-		
Ground level (mPD) Invert level (mPD)	3.30 2.34	4.30 2.16			
invertiever (iiii b)	2.54	2.10	-		
Width of u-channel,	w =	750	mm		
Length of u-channel,	L _c =	53	m		
Depth of vertical part of u-channel,			mm		
Gradient of u-channel,			= 0.0034		
Cross-Section Area,	a =	$0.5 \pi r^2 + w d$	= 0.5 x 3.14 x 375^2 + 750 x 176	55	
,	=				
Wetted Perimeter,	p =		= 3.14 x 375 + 2 x 1765		
	=	4.708			
Hydralic radius,	R =		m	SDM 8.2	<u>.</u> .1
Use Manning Equation for e	stima	ting velocity of s	tormwater		
Take	n =	0.016	for concrete lined channels:-	SDM Table	e 1
Allowable velocity,	v =	$= R^{1/6}x (RS_f)^{1/2}/n$	$= (0.328)^1/6 \times (0.328 \times 0.003)^4$	1/2 / 0.016 SDM Table	e 1
	_ =	1.73			
Time of flow,	t _f =	0.5	min		
Use "Rational Method" for c	alcul	ation of design flo	DW .		
Design intensity,	j =	a / (t _o + t _f +b) ^c		SDM 4.3	3.2
	=	505.5 / (2.9+0.5+3.2	29) $^0.355$ for return period T = 50 y	/ears Corrigendum 1	1/20
	=	246		SDM Table	э 3
Type of surface		Runoff Coefficient C		<u>C x A</u> SDM 7.5.2	<u>≀</u> (b
Flat Glassland(heavy soil)		0.25	0.0	0.0	
Concrete Paving		0.95	<b>1081.0</b> SUM =	1027.0 1027.0	
Upstream flow,	0 -	0.369	m ³ /s		
•	_				
Design flow,			where A _j is in km²	SDM 7.5.2	<u> 2</u> (a
	=	0.278 x 246 x 1026	.95 / 1000000 + 0.369		
	=	0.439	m ³ /s		
Allowable flow,	Q _a =	: axv			
		: 1.545 x 1.73			
	=	2.676	m ³ /s		
	>	Q _d (O.K.)			
Reference was made to Stormwate			by DSD		
0.1.37	l	Hydraul	ic Calculation	Goldrich Planners &	
Scale: NA		11yur aur	ic Caiculativii	Surveyors Ltd.	
				•	
December 2024	1		6 (Part), 1489 (Part), 1494 (Part) vernment Land in D. D. 107	Page 7	

## **Viewpoint 1**

# Existing Earth Ditch



## Viewpoint 3





## Viewpoint 5





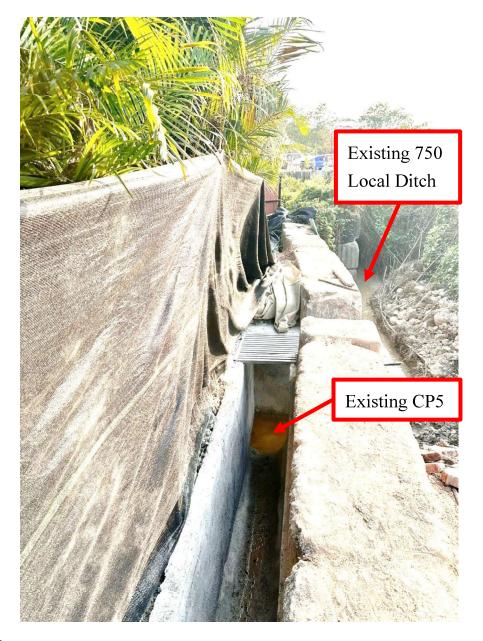
## Viewpoint 7





## Viewpoint 9

## Existing 500 UC



## **Viewpoint 11**





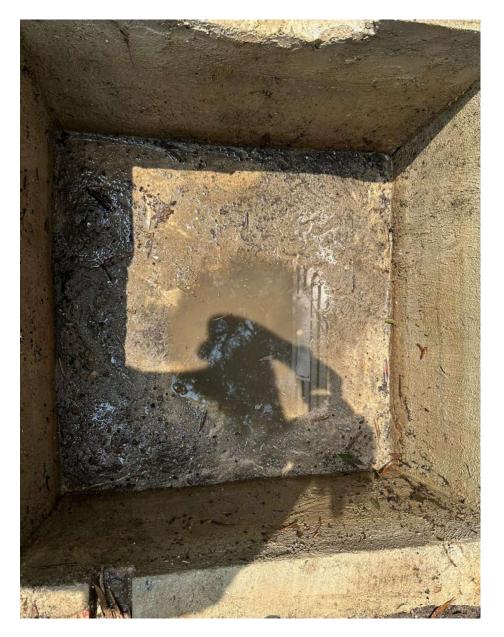
## Viewpoint 13

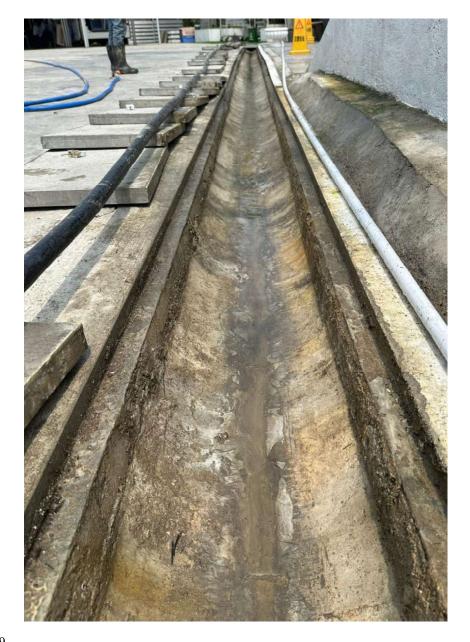




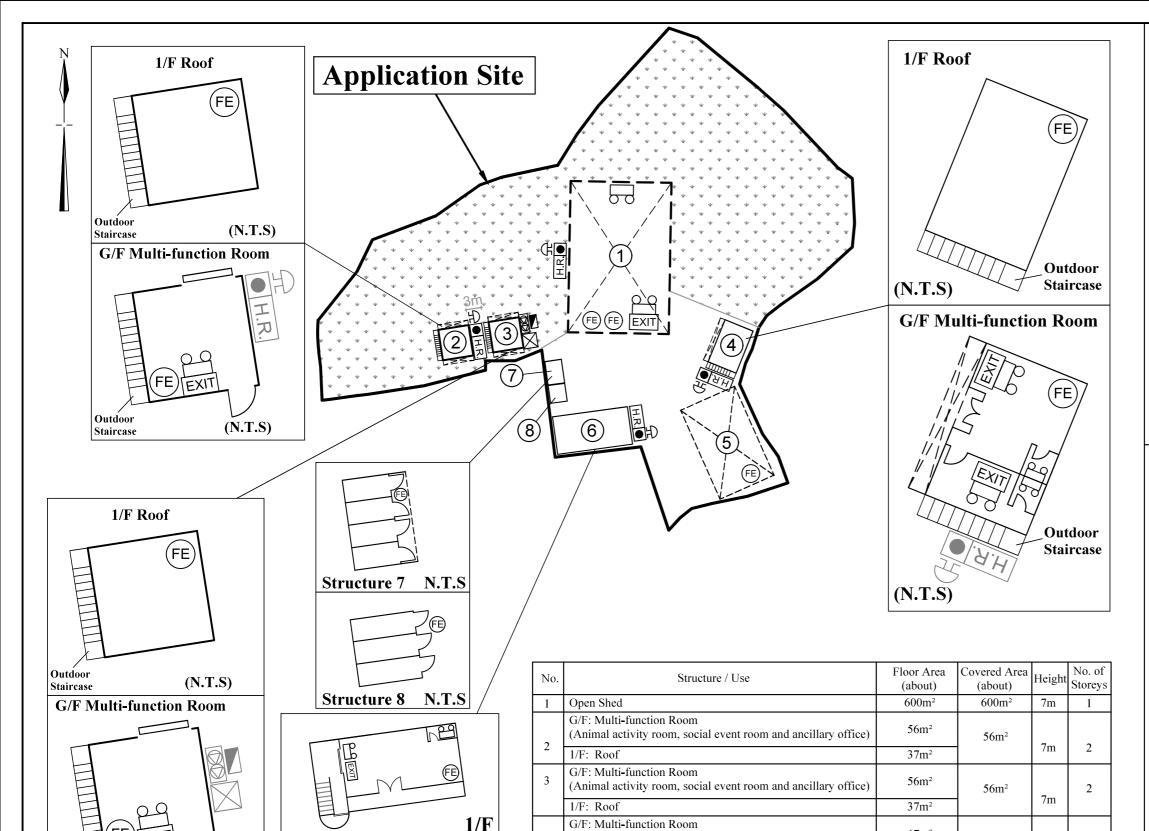
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## Viewpoint 15









1/F: Roof

Open Shed

Toilet

Toilet

G/F

Multi-function Room

### FS NOTES:

- (i) Sufficient emergency lighting shall be provided in accordance with BS 5266-1:2016, BS EN 1838:2013 and the FSD Circular Letter No. 4/2021
- (ii) Sufficient directional and exit sign shall be provided in accordance with BS 5266: Part 1 and FSD Circular Letter 5/2008.
- (iii) Portable hand-operated approved appliances shall be provided as required by occupancy.
- (iv) Fire alarm system shall be provided throughout the entire building in accordance with BS 5839-1:2017 and FSD Circular Letter 6/2021. One actuating point and one audio warning device to be located at each hose reel point. This actuation point should include facilities for fire pump start and audio/visual warning device initiation.
- (v) A modified hose reel system supplied by 2m³ FS water tank shall be provided. There shall be sufficient hose reels to ensure that every part of each building can be reached by a length of not more than 30m of hose reel tubing.
- (vi) Duplicated power supplies for all fire Service Installations comprising a cable connected from electricity mains and other teed off before the main switch shall be provide.

### Legend:

FE	5.0kg CO2 Gas type Fire Extinguisher	x13
29	Emergency Light	x12
EXIT	Exit Sign	<b>x</b> 8
•	Break Glass Call Point	x4
$\rightleftharpoons$	Fire Alarm Bell	x4
H.R.	Fire Hosereel	<b>x4</b>
	F.S pump room	x1
$\boxtimes$	2m³ FS Water Tank	x1
	Fire Alarm / Hosereel Pump Control Panel	<b>x</b> 1
	Sliding Door	

Canopy / Open Shed

## **Fire Service Installation Proposal**

(Animal activity room, social event room and ancillary office)

(Animal activity room, social event room and ancillary office)

Total:

 $67m^2$ 

58m²

226m²

225m²

15m²

12m²

1,389m²

 $67m^2$ 

226m²

112.5m²

15m²

12m²

1,144.5m²

2

2

7m

7m

7m

5m

5m

Lots 1464(part), 1466(part), 1486(Part), 1489(Part), 1494(part) and adjoining Government Land in D. D. 107

Yuen Long, New Territories

1:750 (A3)

(N.T.S)

Outdoor

Staircase

August 2025

Goldrich Planners & Surveyors Ltd.

Plan 6 ( P 22034 )

