## Gold Rich Planners & Surveyors Ltd.

#### 金潤規劃測量師行有限公司

Your Ref.: A/YL-KTS/1090

Our Ref.: P25040/TL25411

2 December 2025

The Secretary
Town Planning Board
15/F., North Point Government Offices
333 Java Road, North Point, Hong Kong

By Post and E-mail tpbpd@pland.gov.hk

Dear Sir,

**Submission of Further Information (FI)** 

Proposed Temporary Private Vehicle Park (Private Cars Only) for a Period of 3 Years in "Village Type Development" Zone, Lot 343 (Part) in D.D. 113, Kam Tin, Yuen Long, New Territories (Application No. A/YL-KTS/1090)

We write to submit FI in response to departmental comment(s) conveyed by the Planning Department for the captioned application.

Yours faithfully, For and on behalf of Goldrich Planners & Surveyors Ltd.

Francis LAU

Encl.

c.c.

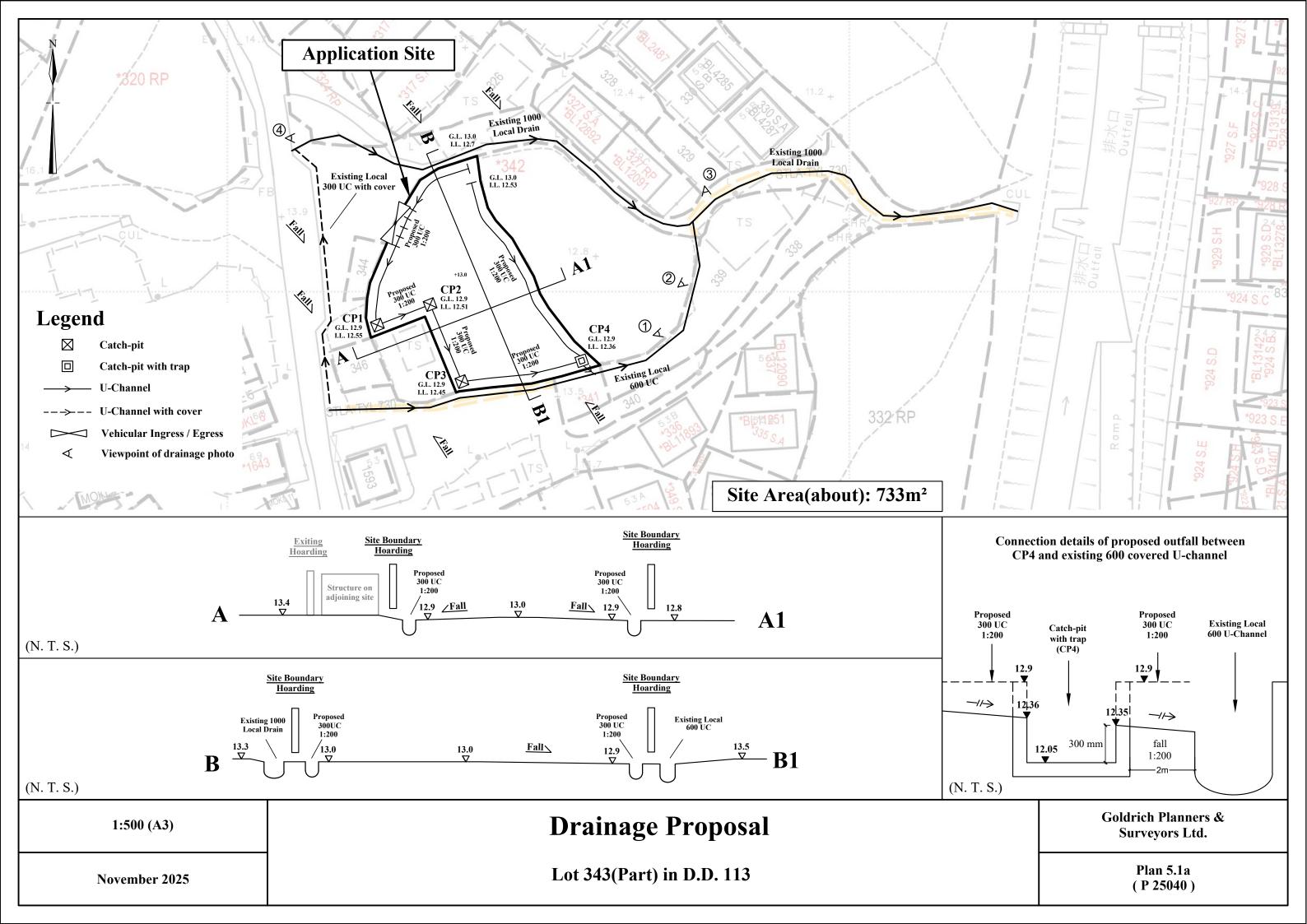
DPO/FS&YLE, PlanD (Attn.: Ms. Anna TONG) By E-mail only

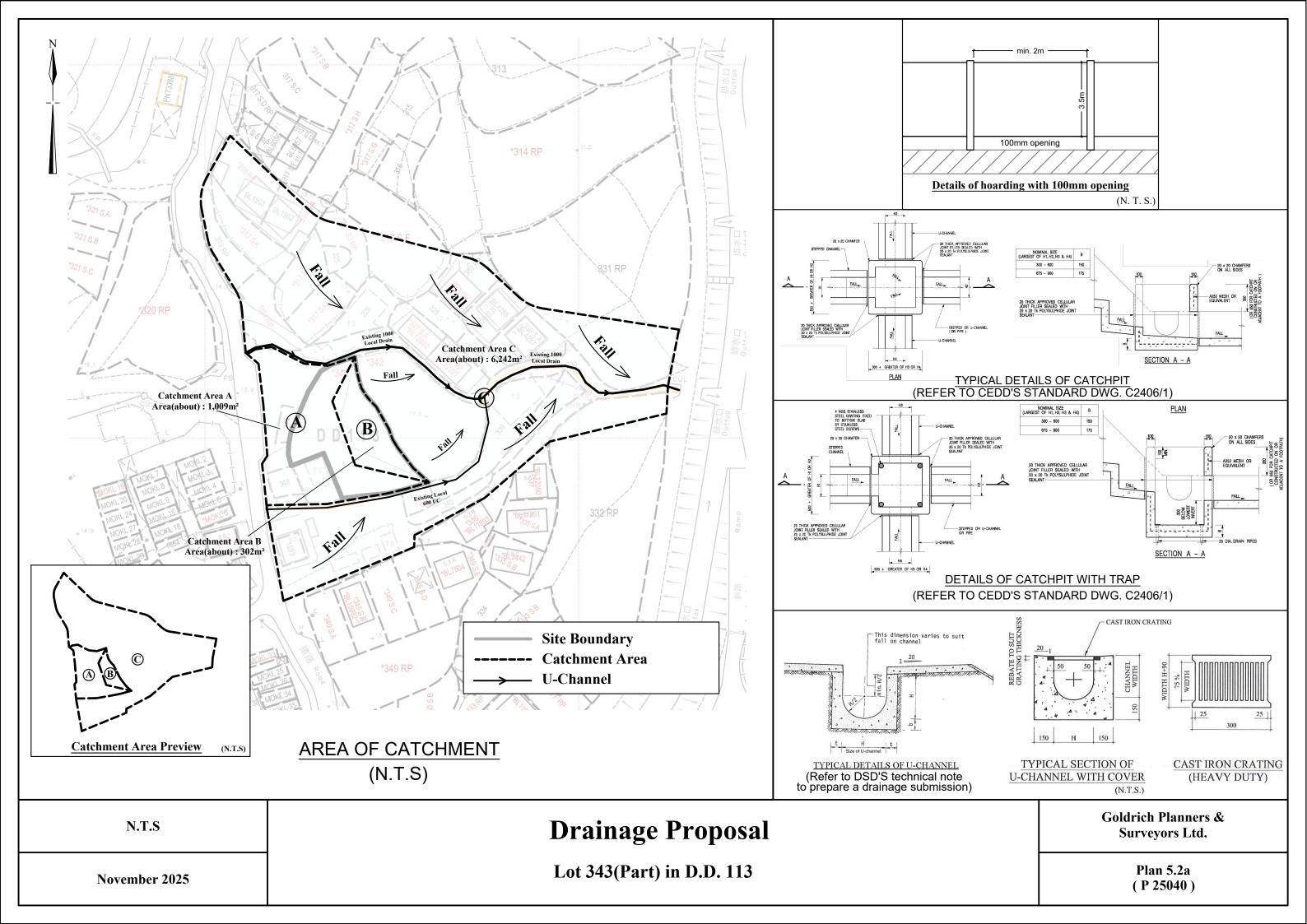
#### Further Information for Planning Application No. A/YL-KTS/1090 Response-to-Comments

#### **Comments from the Drainage Services Department**

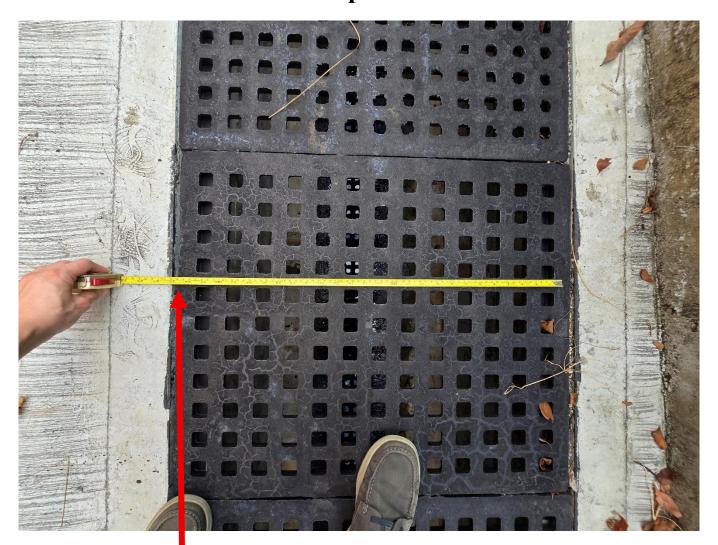
Contact person: Mr. CHAN Yue Lap (Tel.: 2300 1259)

I.	Comments	Responses
1.	Please take into account the 16% rainfall increase due to	Noted. Please refer to the revised
	climate change as stated in the Stormwater Drainage	hydraulic calculations.
	Manual Corrigendum No. 1/2022 for the design	
	calculation.	
2.	The application site is in the vicinity of existing channels.	Noted. The applicant will place all the
	The applicant shall be required to place all the proposed	proposed works 3m away from the top
	works 3m away from the top of the bank of the channel.	of the bank of the channel.
	All the proposed works in the vicinity of the channel	
	should not create any adverse drainage impacts, both	
	during and after construction.	
3.	Calculation to demonstrate the downstream drainage	Noted. Please refer to the revised
	system receiving the discharge from the development has	hydraulic calculations.
	adequate spare capacity to accommodate the runoff is	
	required.	
4.	Colour photos to indicate the current conditions of the	We revisited the site. The width of the
	existing drainage facilities i.e. the existing 350UC should	existing drainage facilities is updated.
	be included in the submission. The photos taken locations	Please refer to Plan 5.1a and viewpoint
	and angles should be shown on the layout plan.	photos.
5.	Adequate opening should be provided to walls/hoardings	Hoardings with 100mm opening will
	erected/laid along the site boundary for intercepting the	be provided along the site boundary.
	existing overland flow passing through the site.	
6.	The existing 350UC of the proposed discharge point is	Noted.
	not maintained by this Department, consent from the	
	concerned departments/maintenance parties/owners	
	should be obtained for the proposed connections to their	
	drainage systems.	
7.	The applicant shall resolve any conflict/disagreement	Noted.
	with relevant lot owner(s) and seek LandsD's permission	
	for laying new drains/channels and/or	
	modifying/upgrading existing ones in other private lots or	
	on Government land outside the application site.	





### **Viewpoint 1**



Existing Local 600 UC

### Viewpoint 2



Existing Local 600 UC

#### **Viewpoint 3**

Existing Local 600 UC



Existing 1000 Local Drain

# Viewpoint 4

Our Ref.: P25040



1 For Catchment Area A					Ref.
Area	ı, A	= 1009	m <sup>2</sup>		
Average slope	, Н		m per 100m		
Distance on the line of natural flow	, L	= 18	m		
Time of concentraction	ı, t <sub>o</sub>		) = 0.14465 (18) / (0.1^0.2 <sup>2</sup>	1009^0.1)	SDM 7.5.2 (d)
2 For Proposed UC in Catchme	ent A	rea A			
	Fro	m To			
Ground level (mPD)	13.	00 12.90	-		
Invert level (mPD)	12.	70 12.36	_		
Midth of a shown		_ 200			
Width of u-channel Length of u-channel			mm m		
Depth of vertical part of u-channel	, L <sub>C</sub>	= 67.6	mm		
Credient of u channel	, u	= (12.7-12.36)/67.6			
Gradient of d-channel	, o <sub>f</sub>	- (12.7-12.30)/07.0	- 0.005		
			= 0.5 x 3.14 x 150 <sup>2</sup> + 300 x 39	0	
W		= 0.152	m <sup>2</sup> = 3.14 x 150 + 2 x 390 m		
Wetted Perimeter	, p	$= \pi r + 2 d$	$= 3.14 \times 150 + 2 \times 390$		
Hydrolio rodino	D	= 1.251 $=$ a/p	m		SDM 8.2.1
Hydralic radius	, K	= 0.122	m		3DIVI 0.2.1
3 Use Manning Equation for est	imat				
					001171110
			for concrete lined channels:-		SDM Table 13
Allowable velocity	, v		= $(0.122)^1/6 \times (0.122 \times 0.005)^n$	1/2 / 0.016	SDM Table 12
Time of flow	t,	= 1.09	m/s min		
Use "Rational Method" for cal					
Design intensity		- 01/4 14 16\C			CDM 4 2 2
Design intensity		= $a/(t_0 + t_f + b)^c$ = $605.5/(2.1+1+3.20)$	0°0.355 for return period T = 50	vooro	SDM 4.3.2
		= 262	10.555 for return period 1 = 50	years	Corrigendum 1/2024 SDM Table 3a
					ODIVI Table da
Type of surface		Runoff Coefficient C	Catchment Area A (m <sup>2</sup> )	CxA	SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	0.0	0.0	
Concrete Paving		0.95	1009.0	958.6	
			SUM =	958.6	
Upstream flow	Q	= 0	m³/s		
Opsitean now,	×u	U			
Design flow.	Qd	= 1.16 x 0.278i Σ C <sub>i</sub> A <sub>i</sub>	+ Q <sub>u</sub> where A <sub>i</sub> is in km <sup>2</sup>		SDM 7.5.2 (a)
		= 1.16 x 0.278 x 262 x			Corrigendum 1/2022
		= 0.081			
		0.001			
Allowable flow,	$Q_a$	= axv			
		= 0.152 x 1.09			
		0.166	m <sup>3</sup> /s		
		0 (0 (1)			
	>	• Q <sub>d</sub> (O.K.)			
Reference was made to Stormwate	er Dra	ainage Manual (SDM) b	by DSD		6
				0-11/1-21	
Scale: NA		77 1 1	S- G-11 4	Goldrich Pl	
Hydraulic Calculation Surveyors			's Lta.		
October 2025 Lot 343 (Part) in D.D. 113, Kam Tin, Yuen Long, New Territories Page 1				1	
October 2025		Lot 272 (1 att) III D.D. 113, N	an in, i den Long, ivew Territories	(P250-	was a second
(r23040)					,

1 For Catchment Area B		Ref.		
Area	$A = 302 \text{ m}^2$			
Average slope				
Distance on the line of natural flow				
Time of concentraction	$t_o = 0.14465 L / (H^{0.2}A^{0.1}) = 0.14465 (10) / (0.1^0.2*302^0.1)$ = 1.3 min	SDM 7.5.2 (d)		
2. For Bronnerd HC in Catalana	nt Area D			
2 For Proposed UC in Catchme	nt Area B			
	From To			
Ground level (mPD)	13.00 12.90			
Invert level (mPD)	12.53 12.36			
Width of u-channel				
Length of u-channel				
Depth of vertical part of u-channel				
Gradient of u-channel	$S_f = (12.53-12.36)/33.4 = 0.005$			
	2			
Cross-Section Area		1		
	= 0.152 m <sup>2</sup>			
Wetted Perimeter				
	= 1.251 m			
Hydralic radius		SDM 8.2.1		
	= 0.122 m			
3 Use Manning Equation for estimating velocity of stormwater				
Take	n = 0.016 for concrete lined channels:-	SDM Table 13		
Allowable velocity	$v = R^{1/6}x (RS_f)^{1/2}/n = (0.122)^{1/6} x (0.122 \times 0.005)^{1/2} / 0.016$	SDM Table 12		
,	= 1.10 m/s			
Time of flow,				
4 Use "Rational Method" for calc				
	144 - 1 - 126	0014400		
Design intensity,	$i = a/(t_0 + t_f + b)^c$	SDM 4.3.2		
	= 505.5 / (1.3+0.5+3.29)^0.355 for return period T = 50 years	Corrigendum 1/2024		
	= 284	SDM Table 3a		
Town of sourferen	Duranti Carattaire to Cartabarrant Area A (m²)	CDM 7.5.0 (b)		
Type of surface	Runoff Coefficient C Catchment Area A (m²) C x A 0.25 0.0 0.0	SDM 7.5.2 (b)		
Flat Glassland(heavy soil) Concrete Paving	0.25 <b>0.0</b> 0.0 0.95 <b>302.0</b> 286.9			
Concrete Faving	SUM = 286.9			
	00m - 200.0			
Upstream flow,	$Q_{II} = 0 \text{ m}^3/\text{s}$			
2 pos. 52 11011,	5.00.75			
Design flow	$Q_d = 1.16 \times 0.278i \Sigma C_i A_i + Q_u$ where $A_i$ is in km <sup>2</sup>	SDM 7.5.2 (a)		
Bedigit now,	$= 1.16 \times 0.278 \times 284 \times 286.9 / 1000000 + 0$	Corrigendum 1/2022		
	$= 0.026 \text{ m}^3/\text{s}$	Comgendam 1/2022		
	- U.UZU III /S			
Allowable flow, $Q_a = a \times v$				
Allowable flow,	$Q_a = 0.152 \times 1.1$			
	= 0.167 m <sup>3</sup> /s			
	- 0.107 11178			
	> Q <sub>d</sub> (O.K.)			
Reference was made to Stormwate	er Drainage Manual (SDM) by DSD			
	Caldida	Planners &		
Scale: NA				
Hydraulic Calculation Surveyo				
Lot 343 (Part) in D.D. 113 Kam Tin, Yuen Long, New Territories Page 2				
October 2025	Lot 5 15 (Tart) in D.D. 115, Italii Tili, Taeli Long, Item Territories	Contract of the contract of th		
A. 3000000000000000000000000000000000000		(P25040)		

					Γ
1 For Connection between CP	4 and	Existing Local 600	UC with C.I. Cover		Ref.
Are	a, A	= 0	m <sup>2</sup>		
Average slope	e, H	= 0.1	m per 100m		
Distance on the line of natural flow	v, L	= 0	m		
Time of concentraction	n, t <sub>o</sub>		) = 0.14465 (0) / (0.1^0.2*0 min	0^0.1)	SDM 7.5.2 (d)
2 For Proposed UC in Connect	ion b	etween CP4 and Ex	isting Local 600 UC with C.I.	Cover	
	Fro	m To			
Ground level (mPD)	12.9	00 12.90	=		
Invert level (mPD)	12.3	36 12.35	-		
Width of u-channe	l, w	= 300	mm		
Length of u-channe	I. La	= 2	m		
Length of u-channe Depth of vertical part of u-channe	l d	= 400	mm		
Gradient of u-channe	l, S <sub>f</sub>	= (12.36-12.35)/2			
Cross-Section Area	a a	$= 0.5 \pi r^2 + wd$	= 0.5 x 3.14 x 150^2 + 300 x 40	0	
OTOUS-OCCION AIGO	., u	= 0.5 %1 + Wd		•	
Wetted Perimete	r, p	$= \pi r + 2 d$	$= 3.14 \times 150 + 2 \times 400$		
Hydralic radius	. P	= 1.271 = a/p	m		SDM 8.2.1
Trydraile radius	o, IX	= 0.122	m		3DIVI 0.2.1
3 Use Manning Equation for es	timat	ng velocity of storm	water		
Tak	e n	= 0.016	for concrete lined channels:-		SDM Table 13
Allowable velocity	/, V	$= R^{1/6}x (RS_f)^{1/2}/n$	$= (0.122)^1/6 \times (0.122 \times 0.005)^7$	1/2 / 0.016	SDM Table 12
-		= 1.09		Section Section Section	
Time of flow			min		
4 Use "Rational Method" for ca	lculat	on of design flow			
Design intensity	/, i	$= a / (t_o + t_f + b)^c$			SDM 4.3.2
		= 505.5 / (0+0+3.29)^0	0.355 for return period $T = 50$	years	Corrigendum 1/202
		= 330			SDM Table 3a
Type of surface		Runoff Coefficient C	Notes to the second sec		SDM 7.5.2 (b)
Flat Glassland(heavy soil)		0.25	0.0	0.0	
Concrete Paving		0.95	<b>0.0</b> SUM =	0.0	
Unatroom flou	. 0	- 0.407			
Upstream flow, $Q_u = 0.107 \text{ m}^3/\text{s}$					
Design flow	, Q <sub>d</sub>	= $1.16 \times 0.278i \Sigma C_i A_i$	+ Q <sub>u</sub> where A <sub>i</sub> is in km <sup>2</sup>		SDM 7.5.2 (a)
		= 1.16 x 0.278 x 330 x			Corrigendum 1/202
		0.107			•
Allowable flow	. Q.	= axv			
Allowable flow		= 0.155 x 1.09			
	;	= 0.133 x 1.09	m³/s		
	2	Q <sub>d</sub> (O.K.)			
Reference was made to Stormwat	er Dra	inage Manual (SDM) b	y DSD		
Scale: NA				Goldrich Pla	nners &
Scale, IVA		Hydrauli	c Calculation	Surveyor	s Ltd.
	1	TO SECURITION OF THE SECURITIO		D.	2
October 2025		Lot 343 (Part) in D.D. 113, K	am Tin, Yuen Long, New Territories	Page	
				(P2504	10)

Area, A = 6242 m <sup>2</sup> Average slope, H = 0.1 m per 100m  Distance on the line of natural flow, L = 60 m  Time of concentraction, t <sub>o</sub> = 0.14465L / (H <sup>0.2</sup> A <sup>0.1</sup> ) = 0.14465 (60) / (0.1^0.2*6242^0.1) = 5.7 min  2 For Existing 1000 Local Drain in Catchment Area C  From To  Ground level (mPD) 12.00 11.50  Invert level (mPD) 11.00 10.71					
Average slope, H = 0.1 m per 100m  Distance on the line of natural flow, L = 60 m  Time of concentraction, t <sub>o</sub> = 0.14465L / (H <sup>0.2</sup> A <sup>0.1</sup> ) = 0.14465 (60) / (0.1^0.2*6242^0.1) = 5.7 min  2 For Existing 1000 Local Drain in Catchment Area C  From To  Ground level (mPD) 12.00 11.50 Invert level (mPD) 11.00 10.71	5.2 (d)				
Average slope, H = 0.1 m per 100m Distance on the line of natural flow, L = 60 m  Time of concentraction, t <sub>o</sub> = 0.14465L / (H <sup>0.2</sup> A <sup>0.1</sup> ) = 0.14465 (60) / (0.1^0.2*6242^0.1) = 5.7 min  2 For Existing 1000 Local Drain in Catchment Area C  From To Ground level (mPD) 12.00 11.50 Invert level (mPD) 11.00 10.71	5.2 (d)				
Time of concentraction, t <sub>o</sub> = 0.14465L / (H <sup>0.2</sup> A <sup>0.1</sup> ) = 0.14465 (60) / (0.1^0.2*6242^0.1) = 5.7 min  2 For Existing 1000 Local Drain in Catchment Area C  From To  Ground level (mPD) 12.00 11.50 Invert level (mPD) 11.00 10.71	5.2 (d)				
= 5.7 min  2 For Existing 1000 Local Drain in Catchment Area C  From To  Ground level (mPD) 12.00 11.50  Invert level (mPD) 11.00 10.71	5.2 (d)				
From To  Ground level (mPD) 12.00 11.50 Invert level (mPD) 11.00 10.71					
From To  Ground level (mPD) 12.00 11.50 Invert level (mPD) 11.00 10.71					
Ground level (mPD) 12.00 11.50 Invert level (mPD) 11.00 10.71					
Invert level (mPD) 11.00 10.71					
Width of u-channel, w = 1000 mm					
Length of u-channel, $L_c = 58 \text{ m}$					
100 miles - 100 mi					
Gradient of u-channel, $S_f = (11-10.71)/58 = 0.005$					
Cross-Section Area, a = $0.5 \pi r^2 + w d$ = $0.5 \times 3.14 \times 500^2 + 1000 \times 290$					
$= 0.683 \text{ m}^2$					
Wetted Perimeter, p = $\pi r + 2 d$ = 3.14 x 500 + 2 x 290					
= 2.151 m					
Hydralic radius, R = a / p SDM 8	.2.1				
= 0.317 m					
3 Use Manning Equation for estimating velocity of stormwater					
Take n = 0.016 for concrete lined channels:- SDM Tal	ble 13				
Allowable velocity, $v = R^{1/6}x (RS_f)^{1/2}/n = (0.317)^1/6 x (0.317 x 0.005)^1/2 / 0.016$ SDM Tal	ble 12				
= 2.06 m/s					
Time of flow, $t_f = 0.5 \text{ min}$					
4 Use "Rational Method" for calculation of design flow					
Design intensity is a 2/4 of the					
Design intensity, $i = a/(t_0 + t_f + b)^c$ SDM 4					
= 505.5 / (5.7+0.5+3.29)\(^0.355\) for return period T = 50 years Corrigendum					
= 227 SDI					
Type of surface Runoff Coefficient C Catchment Area A (m²) C x A SDM 7.5	.2 (b)				
Flat Glassland(heavy soil) 0.25 0.0 0.0	. ,				
Concrete Paving 0.95 <b>6242.0</b> 5929.9					
SUM = 5929.9					
Upstream flow, Q <sub>II</sub> = <b>0.107</b> m <sup>3</sup> /s					
Upstream flow, $Q_u = 0.107 \text{ m}^3/\text{s}$					
Design flow, $Q_d = 1.16 \times 0.278i \Sigma C_i A_i + Q_u$ where $A_i$ is in km <sup>2</sup> SDM 7.5	.2 (a)				
= 1.16 x 0.278 x 227 x 5929.9 / 1000000 + 0.107 Corrigendum					
= 0.542 m <sup>3</sup> /s	1 1/2022				
= 0.542 m7s					
Allowable flow O = a v ··					
Allowable flow, $Q_a = a \times v$					
= 0.683 x 2.06					
= 1.404 m <sup>3</sup> /s					
> Q <sub>d</sub> (O.K.)					
——————————————————————————————————————					
Reference was made to Stormwater Drainage Manual (SDM) by DSD					
Goldrich Planners &					
I Goldrich Dlannara &					
Scale, NA					
Scale: NA  Hydraulic Calculation  Surveyors Ltd.					
Hydraulic Calculation Surveyors Ltd.					
Scale, MA					