Appendix 3

Traffic Impact Assessment (TIA)

Proposed Social Welfare Facilities (Residential Care Home for the Elderly (RCHE)) in "Village Type Development" Zone, Lots 3670 RP (Part), 3671 RP (Part), 3672 RP (Part), 3673 RP (Part) and adjoining Government Land in D.D.104, Nam Sang Wai, Yuen Long

Traffic Impact Assessment Final Report May 2025

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Proposed Social Welfare Facilities (Residential Care Home for the Elderly (RCHE)) in "Village Type Development" Zone, Lots 3670 RP (Part), 3671 RP (Part), 3672 RP (Part), 3673 RP (Part) and adjoining Government Land in D.D.104,Nam Sang Wai, Yuen Long

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Proposed Social Welfare Facilities (Residential Care Home for the Elderly (RCHE)) in "Village Type Development" Zone, Lots 3670 RP (Part), 3671 RP (Part), 3672 RP (Part), 3673 RP (Part) and adjoining Government Land in D.D.104,Nam Sang Wai, Yuen Long

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1.0 INTRODUCTION

Background

- 1.1 The Subject Site is located at lots 3670 RP (Part), 3671 RP (Part), 3672 RP (Part), 3673 RP (Part) and adjoining Government Land in D.D.104, Nam Sang Wai, Yuen Long. The location of the Subject Site is shown in Figure 1.1.
- 1.2 The owner has the intention to develop the Subject Site into a Residential Care Home for the Elderly with no more than 240 beds (the "Proposed RCHE").
- 1.3 Against this background, CKM Asia Limited, a traffic and transportation planning consultancy firm, was commissioned to conduct a Traffic Impact Assessment ("TIA") in support of the Proposed RCHE. The report presents the findings and recommendations of the TIA for the Proposed RCHE.

Scope of the Assessment

- 1.4 The main objectives of this TIA are as follows:
 - To assess the existing traffic issues in the vicinity of the Subject Site;
 - To quantify the amount of traffic generated by the Proposed RCHE; and
 - To examine the traffic impact on the local road network in the vicinity of the Subject Site.

Contents of the Report

1.5 After this introduction, the remaining chapters contain the following:

Chapter Two - describes the existing situation;
Chapter Three - outlines the development proposal;
Chapter Four - presents the traffic impact analysis; and
Chapter Five - summarises the overall conclusion

2.0 THE EXISTING SITUATION

The Subject Site

2.1 The Subject Site is located to the immediate north of Kam Pok Road East. At present, the Subject Site has no vehicular access.

Existing Road Network

- 2.2 Kam Pok Road East is a local distributor, and it is of single carriageway 2-lane standard. It connects with Kam Pok Road to the west and Castle Peak Road Tam Mi to the east.
- 2.3 Castle Peak Road Tam Mi is a rural road, and it is of single carriageway2-lane standard. It connects with The Fairview Park Roundabout to the north and Kam Pok Road East to the south.

Traffic Survey

- 2.4 To quantify the traffic flows at the junctions chosen for the capacity analysis, manual classified counts were conducted on Friday, 7th March 2025 during the AM and PM peak periods. The locations of the surveyed junctions are presented in Figure 2.1 and their layouts are shown in Figures 2.2 to 2.4.
- 2.5 The surveyed junctions include the following:
 - J1: Kam Pok Road / Kam Pok Road East;
 - J2: Castle Peak Road Tam Mi / Kam Pok Road; and
 - J3: The Fairview Park Roundabout
- 2.6 The counts were classified by vehicle type to enable traffic flows in passenger car units ("pcu") to be calculated. From the survey, the AM and PM peak hours were found to be between 0800 0900 and 1700 1800 hours respectively, and the existing AM and PM peak hour traffic flows are presented in Figure 2.5.

Operational Performance of the Surveyed Junctions

2.7 The existing operational performance of the surveyed junctions is calculated based on the observed traffic counts and the analysis is undertaken using the methods outlined in Volume 2 of Transport Planning and Design Manual ("TPDM"). The existing operational performance of the junctions are summarised in Table 2.1 and the detailed calculations are found in Appendix 1.

TABLE 2.1 EXISTING JUNCTION OPERATIONAL PERFORMANCE

| Ref. | Junction | Type of Junction | Parameter ⁽¹⁾ | AM Peak Hour | PM Peak Hour |
|------|----------------------------------|---------------------|--------------------------|-----------------|-----------------|
| J1 | Kam Pok Road / Kam Pok Road East | Priority | RFC | 0.31 | 0.22 |
| J2 | Castle Peak Road – Tam Mi / Kam | Signal | RC | 24% | 38% |
| | Pok Road | | | | |
| J3 | The Fairview Roundabout | Roundabout | RFC | 0.45 | 0.45 |

Notes: (1) RC – reserve capacity RFC – Ratio of Flow to Capacity

2.8 Table 2.1 shows that the junctions now operate with capacity.

Public Transport Facilities

2.9 The Subject Site is located close to public transport services with franchised bus and public light bus routes operating in the vicinity. Details of the franchised bus and green minibus ("GMB") routes operating in the vicinity of the Subject Site are presented in Figure 2.6 and Table 2.2.

TABLE 2.2 FRANCHISED BUS AND GMB SERVICES OPERATING CLOSE TO THE SUBJECT SITE

| Route | Routing | Frequency (minutes) |
|----------|--|------------------------|
| KMB 76K | Long Ping Estate – Ching Ho Estate | 20 – 30 |
| KMB 268 | Sham Tseng – Kwun Tong (Tsui Ping North Estate) | 30 – 35 |
| CTB 976 | Sai Wan Ho – Lok Ma Chau (San Tin) | 6 per day |
| CTB 976A | Siu Sai Wan (Island Resort) – Lok Ma Chau (San Tin) | 2 per day |
| GMB 36 | Yuen Long (Fook Hong Street) – Tai Sang Wai Rural Office | 10 – 15 |
| GMB 37 | Yuen Long (Fook Hong Street) – Yau Tan Mei Village Office | 12 – 15 |
| GMB 38 | Yuen Long (Fook Hong Street) – Yau Tam Mei West | 10 – 15 |
| GMB 75 | Yuen Long (Fook Hong Street) – Lok Ma Chau Spur Line Public | 7 – 9 |
| | Transport Interchange | |
| GMB 76 | Yuen Long (Fook Hong Street) – Siu Hum Tsuen | 15 – 20 |
| GMB 78 | Pat Heung Road (near Tai Lam Bus-Bus Interchange) – Lok Ma Chau (San Tin) Public Transport Interchange | 20 – 25 |

Note: KMB – Kowloon Motor Bus

CTB – Citybus

GMB - Green Minibus

Trip Generation Rates for RCHE

2.10 In view that the TPDM does not have trip generation rates for RCHE, trip generation surveys were conducted at 3 RCHEs. Details of these RCHEs are found in Table 2.3, and survey results are presented in Table 2.4.

TABLE 2.3 DETAILS OF THE SURVEYED RCHES

| Ref. | RCHE | Address | No. of beds | Distance from nearest MTR Station |
|------|------------------------------------|----------------------|-------------------|---|
| 1 | The Hong Kong Society for the Aged | 60 - 62 Tin Wan | 392 | 2.8 km (Wong |
| | Bradbury Home for the Elderly and | Street, Tin Wan | | Chuk Hang |
| | Quan Chuen Home for the Elderly | | | Station) |
| 2 | Caritas Li Ka Shing Care and | 16 Wah Fat Street, | 260 | 2.2 km (Tuen |
| | Attention Home, Tuen Mun | Tuen Mun | | Mun Station) |
| 3 | Chuk Lam Ming Tong Care and | 5 Sha Wan Drive, Pok | 175 | 3.5km (Kennedy |
| | Attention Home for the Aged | Fu Lam, Hong Kong | | Town Station) |

TABLE 2.4 TRIP RATES OF THE SURVEYED RCHES

| Ref. | RCHE | AM Peak Hour | | PM Peak Hour | |
|--------|--|--------------|--------|--------------|--------|
| | | IN | OUT | IN | OUT |
| Traff | ic Generation (pcu/hr) | | | | |
| 1 | The Hong Kong Society for the Aged Bradbury | 6 | 3 | 4 | 6 |
| | Home for the Elderly and Quan Chuen Home for | | | | |
| | the Elderly | | | | |
| 2 | Caritas Li Ka Shing Care and Attention Home, | 9 | 6 | 7 | 13 |
| | Tuen Mun | | | | |
| 3 | Chuk Lam Ming Tong Care and Attention Home | 6 | 2 | 3 | 7 |
| | for the Aged | | | | |
| Trip I | Rates (pcu/hour/ bed) | | | | |
| 1 | The Hong Kong Society for the Aged Bradbury | 0.0153 | 0.0077 | 0.0102 | 0.0153 |
| | Home for the Elderly and Quan Chuen Home for | | | | |
| | the Elderly | | | | |
| 2 | Caritas Li Ka Shing Care and Attention Home, | 0.0346 | 0.0231 | 0.0269 | 0.0500 |
| | Tuen Mun | | | | |
| 3 | Chuk Lam Ming Tong Care and Attention Home | 0.0343 | 0.0114 | 0.0171 | 0.0400 |
| | for the Aged | | | | |
| | Adopted (maximum rates) = | 0.0346 | 0.0231 | 0.0269 | 0.0500 |

Pedestrian Generation Rates for RCHE

2.11 In view that the TPDM does not have pedestrian generation rates for RCHE, pedestrian generation surveys were also conducted at the 3 RCHEs found in Table 2.3. The survey results are presented in Table 2.5.

TABLE 2.5 PEDESTRIAN TRIP RATES OF THE SURVEYED RCHES

| Ref. | RCHE | AM Pea | ak Hour | PM Peak Hour | |
|-------|--|--------|---------|--------------|--------|
| | | IN | OUT | IN | OUT |
| Pedes | strian Generation (pedestrian/15 min) | | | | |
| 1 | The Hong Kong Society for the Aged Bradbury Home for the Elderly and Quan Chuen Home for the Elderly | 16 | 7 | 5 | 18 |
| 2 | Caritas Li Ka Shing Care and Attention Home, Tuen Mun | 16 | 5 | 3 | 17 |
| 3 | Chuk Lam Ming Tong Care and Attention Home for the Aged | 9 | 2 | 1 | 7 |
| Pedes | strian Generation Rates (pedestrian/15 min/bed) | | | | |
| 1 | The Hong Kong Society for the Aged Bradbury Home for the Elderly and Quan Chuen Home for the Elderly | 0.0408 | 0.0179 | 0.0128 | 0.0459 |
| 2 | Caritas Li Ka Shing Care and Attention Home, Tuen Mun | 0.0615 | 0.0192 | 0.0115 | 0.0654 |
| 3 | Chuk Lam Ming Tong Care and Attention Home for the Aged | 0.0514 | 0.0114 | 0.0057 | 0.0400 |
| | Adopted (maximum rates) = | 0.0615 | 0.0192 | 0.0128 | 0.0654 |

Utilisation of Surveyed Bus Stops

An utilisation survey was conducted during the AM and PM peak periods at Tai Sang Wai (towards San Tin) and Long Ha (towards Yuen Long) bus stops and the results are presented in Tables 2.6 and 2.7 respectively.

TABLE 2.6 RESULTS OF THE UTILISATION SURVEY AT TAI SANG WAI (TOWARDS SAN TIN) BUS STOP

| (1017110007111111) 2000101 | | | | | | |
|----------------------------|-------------------|--|--------------------------------|----------------------|------------------------|--|
| Route ⁽¹⁾ | No. of Vehicle | No. of Passengers on-board ⁽²⁾ [a] | Capacity ⁽³⁾ [b] | Vacancy [b] – [a] | Occupancy [a] / [b] | |
| AM Peak | | | | | | |
| KMB 76K | 3 | 146 | 384 | 238 | 38.0% | |
| KMB 268 | 2 | 14 | 124 | 110 | 11.3% | |
| GMB 37 | 5 | 65 | 86 | 21 | 75.6% | |
| GMB 38 | 6 | 77 | 102 | 25 | 75.5% | |
| GMB 75 | 3 | 27 | 51 | 24 | 52.9% | |
| GMB 76 | 2 | 15 | 32 | 17 | 46.9% | |
| GMB 78 | 2 | 12 | 38 | 26 | 31.6% | |
| Total | <u>23</u> | <u>356</u> | <u>817</u> | <u>461</u> | 43.6% | |
| PM Peak | | | | | | |
| KMB 76K | 3 | 154 | 384 | 230 | 40.1% | |
| KMB 268 | 2 | 14 | 124 | 110 | 11.3% | |
| GMB 37 | 7 | 93 | 118 | 25 | 78.8% | |
| GMB 38 | 9 | 95 | 147 | 52 | 64.6% | |
| GMB 75 | 3 | 36 | 48 | 12 | 75.0% | |
| GMB 76 | 1 | 10 | 19 | 9 | 52.6% | |
| GMB 78 | 2 | 12 | 38 | 26 | 31.6% | |
| Total | <u>27</u> | <u>414</u> | <u>878</u> | <u>464</u> | <u>47.2%</u> | |

Note: (1) KMB – Kowloon Motor Bus

GMB - Green Minibus

TABLE 2.7 RESULTS OF THE UTILISATION SURVEY AT LONG HA (TOWARDS YUEN LONG) BUS STOP

| Route ⁽¹⁾ | No. of Vehicle | No. of Passengers on-board ⁽²⁾ [a] | Capacity ⁽³⁾ [b] | Vacancy [b] – [a] | Occupancy [a] / [b] |
|----------------------|-------------------|--|--------------------------------|----------------------|------------------------|
| AM Peak | | | | | |
| KMB 76K | 3 | 89 | 384 | 295 | 23.2% |
| KMB 268 | 2 | 14 | 124 | 110 | 11.3% |
| GMB 37 | 6 | 71 | 99 | 28 | 71.7% |
| GMB 38 | 2 | 22 | 32 | 10 | 68.8% |
| GMB 75 | 2 | 83 | 102 | 19 | 81.4% |
| GMB 76 | 2 | 16 | 32 | 16 | 50.0% |
| Total | <u>17</u> | <u>295</u> | 773 | 478 | 38.2% |
| PM Peak | | | | | |
| KMB 76K | 2 | 70 | 256 | 186 | 27.3% |
| KMB 268 | 3 | 21 | 186 | 165 | 11.3% |
| GMB 37 | 5 | 46 | 86 | 40 | 53.5% |
| GMB 38 | 4 | 40 | 67 | 27 | 59.7% |
| GMB 75 | 3 | 38 | 48 | 10 | 79.2% |
| GMB 76 | 2 | 33 | 51 | 18 | 64.7% |
| Total | <u>19</u> | <u>248</u> | 694 | <u>446</u> | <u>35.7%</u> |

Note: (1) KMB – Kowloon Motor Bus

GMB - Green Minibus

2.13 Table 2.6 shows that the utilisation of the franchised buses at Tai Sang Wai (towards San Tin) bus stop is <u>43.6%</u> during the AM Peak Hour and <u>47.2%</u> during the PM Peak Hour. Whilst, Table 2.7 shows that the utilisation of the franchised buses at Long Ha (towards Yuen Long)) bus stop is <u>38.2%</u> during the AM Peak Hour and 35.7% during the PM Peak Hour.

⁽²⁾ Passengers counted the moment before the vehicles departed from the bus stop

⁽³⁾ Assumed capacities: Double-decker = 128, Single-decker = 62

⁽²⁾ Passengers counted the moment before the vehicles departed from the bus stop

⁽³⁾ Assumed capacities: Double-decker = 128, Single-decker = 62

3.0 THE PROPOSED RCHE

Proposed RCHE

3.1 The Proposed RCHE consists of 1 building block with no more than 240 beds and is targeted for completion by 2030. The vehicular assess of Proposed RCHE is provided at Kam Pok Road East.

Provision of Internal Transport Facilities

3.2 The HKPSG has no recommendation on the provision of internal transport facilities for RCHE, hence, reference is made to the 3 RCHEs listed in Table 2.3. The internal transport facilities provision rate derived from the 3 RCHEs are found in Table 3.1.

TABLE 3.1 INTERNAL TRANSPORT FACILITIES PROVIDED IN SURVEYED RCHEs

| | Notice | | | | | | |
|-------|--|----------|--------|--------------------------|-------|--|--|
| Ref. | RCHE | No. of | Intern | nal Transport Facilities | | | |
| | | beds | Car | Light Bus / | LGV | | |
| | | | | Ambulance | | | |
| Parki | ng Provision | | | | | | |
| 1 | The Hong Kong Society for the Aged | 392 | 8 | 0 | 1 | | |
| | Bradbury Home for the Elderly and Quan | | | | | | |
| | Chuen Home for the Elderly | | | | | | |
| 2 | Caritas Li Ka Shing Care and Attention | 260 | 5 | 1 | 0 | | |
| | Home, Tuen Mun | | | | | | |
| 3 | Chuk Lam Ming Tong Care and Attention | 175 | 8 | 0 | 0 | | |
| | Home for the Aged | | | | | | |
| Provi | sion rate (space / bed) | | | | | | |
| 1 | The Hong Kong Society for the Aged | 392 | 0.020 | 0.000 | 0.003 | | |
| | Bradbury Home for the Elderly and Quan | | | | | | |
| | Chuen Home for the Elderly | | | | | | |
| 2 | Caritas Li Ka Shing Care and Attention | 260 | 0.019 | 0.004 | 0.000 | | |
| | Home, Tuen Mun | | | | | | |
| 3 | Chuk Lam Ming Tong Care and Attention | 175 | 0.045 | 0.000 | 0.000 | | |
| | Home for the Aged | | | | | | |
| | Adopted provision | n rate = | 0.045 | 0.004 | 0.003 | | |

3.3 Based on the adopted provision rate in Table 3.1, the calculated internal transport facilities for the Proposed RCHE are presented in Table 3.2.

TABLE 3.2 PROVISION OF INTERNAL TRANSPORT FACILITIES THE FOR PROPOSED RCHE

| Use | No. of beds | Internal Transport facilities | Provision | Dimensions |
|------|-------------|--|-----------|--|
| RCHE | 240 | Car Parking Space | 11 | 10 @ 5m (L) x 2.5m (W) x 2.4m (H) 1 @ 5m (L) x 3.5m (W) x 2.4m (H) for persons with disabilities |
| | | LGV loading / unloading bay | 1 | 1 @ 7m (L) x 3.5m (W) x 3.6m (H) |
| | | Light Bus / Ambulance Parking Space | 1 | 1 @ 9m (L) x 3.0m (W) x 3.3m (H) |

3.4 The carpark layout plans for G/F and B/F are shown in Figures 3.1 - 3.2.

Proposed Social Welfare Facilities (Residential Care Home for the Elderly (RCHE)) in "Village Type Development" Zone, Lots 3670 RP (Part), 3671 RP (Part), 3672 RP (Part), 3673 RP (Part) and adjoining Government Land in D.D.104, Nam Sang Wai, Yuen Long

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Swept Path Analysis

3.5 The CAD-based swept path analysis program, Autodesk Vehicle Tracking, was used to check the ease of vehicle manoeuvring. Vehicles are found to have no manoeuvring problems and all vehicles could enter and leave the spaces with ease. The swept path analysis drawings for critical movements are found in Appendix 2.

4.0 TRAFFIC IMPACT

Design Year

4.1 The Proposed RCHE is expected to be completed by 2030, and the design year adopted for the capacity analysis is 2033, i.e. 3 years after the completion of the Proposed RCHE.

Traffic Forecasting

- 4.2 The 2033 traffic flows used for the junction analysis are produced with reference to the following:
 - (i) 2031 traffic flows derived based on the NTW1 Base District Traffic Model ("BDTM");
 - (ii) estimated traffic growth from 2031 to 2033 based on the higher of: (a) Hong Kong Population Projections 2022 2046, published by Census and Statistics Department, or (b) historic Annual Average Daily Traffic ("AADT") produced by Transport Department;
 - (iii) the other developments in the vicinity of the Proposed RCHE; and
 - (iv) Traffic generated by the Proposed RCHE.
- 4.3 The (ii) estimated traffic growth from 2031 to 2033, (iii) the other development in the vicinity of the Proposed RCHE and (iv) traffic generated by the Proposed RCHE are presented in the paragraphs below.

Estimated Growth Rate from 2031 to 2033

4.4 The (a) Hong Kong Population Projections 2022 – 2046, and (b) historic AADT are summarised in Tables 4.1 – 4.2 respectively.

TABLE 4.1 HONG KONG POPULATION PROJECTIONS 2022 – 2046

| Whole Territo | ory Population | Annual Growth Rate |
|---------------|----------------|--------------------|
| Year 2031 | Year 2033 | 2031 to 2033 |
| 7,820,200 | 7,903,600 | 0.53% |

TABLE 4.2 AADT OF THE STATION IN THE VICINITY OF THE SUBJECT SITE

| Year \ | | | | | | | | |
|---------|--------|--------|------------|-----------|--------------|--------|--------|---------|
| Station | 5016 | 5019 | 5257 | 5297 | 5505 | 5508 | 5496 | Overall |
| 2013 | 90,610 | 34,530 | 12,620 | 8,220 | 9,030 | 68,040 | 35,980 | 259,030 |
| 2014 | 88,800 | 36,490 | 10,600 | 6,200 | 11,990 | 72,580 | 30,750 | 257,410 |
| 2015 | 86,180 | 34,380 | 10,510 | 6,140 | 12,090 | 85,910 | 27,750 | 262,960 |
| 2016 | 92,230 | 31,990 | 10,940 | 6,400 | 12,590 | 90,760 | 28,900 | 273,810 |
| 2017 | 90,650 | 30,040 | 10,770 | 6,300 | 6,300 12,390 | | 28,450 | 268,710 |
| 2018 | 86,230 | 29,300 | 11,980 | 8,540 | 12,700 | 92,980 | 29,150 | 270,880 |
| 2019 | 90,860 | 30,160 | 11,910 | 7,530 | 13,330 | 80,460 | 26,970 | 261,220 |
| 2020 | 81,870 | 27,640 | 11,420 | 7,220 | 13,420 | 82,010 | 13,100 | 236,680 |
| 2021 | 86,620 | 29,600 | 11,880 | 7,510 | 13,960 | 86,000 | 13,630 | 249,200 |
| 2022 | 82,820 | 28,180 | 11,520 | 7,280 | 13,540 | 82,190 | 13,210 | 238,740 |
| 2023 | 88,760 | 55,700 | 10,740 | 10,960 | 13,860 | 87,340 | 13,520 | 280,880 |
| | | A | verage Anr | nual Grow | th | | | 0.81% |

Note: 5016 – San Tin Highway, Castle Peak Road & San Tam Road (From Kam Tin Road to Fairview Park Boulevard)

5019 - Castle Peak Road - Yuen Long (From Yuen Long On Lok Road to Kam Tin Road)

5257 – Castle Peak Road – Tam Mi, Mai Po & San Tin (From Fairview Park Boulevard to Lok Ma Chau Road)

5297 - San Tam Road (From Castle Peak Road - Mai Po to Fairview Park Boulevard Roundabout)

5505 – Sam Tam Road (From Fairview Park Boulevard RA to End)

5508 – San Tin Highway (From Fairview Park Boulevard to Lok Ma Chau Road)

5496 – San Sham Road (From San Tin Interchange to End of San Sham Road)

4.5 Table 4.1 shows that the annual growth rate from 2031 to 2033 is +0.53%. Table 4.2 shows that in the historic AADT of the stations between 2013 and 2023 in the vicinity has average annual growth rate of +0.81% per annum. To be conservative, the growth rate of +1.00% per annum is adopted for the traffic growth between 2031 and 2033.

Other Developments in the Vicinity of the Proposed RCHE

4.6 The major planned developments in the vicinity of the Proposed RCHE are summarized in Table 4.3, and are included in the traffic forecast.

TABLE 4.3 DETAILS OF MAJOR PLANNED DEVELOPMENTS

| Site | Address | Use | Development Parameter (Approx.) |
|------|---|-------------|---------------------------------------|
| 1 | TPB ref.: A/YL-KTN/663-1: Lots 1783 (Part), 1784 RP, 1788 RP, 1789 RP, 1790 RP (Part), 1791 RP, 1795 (Part), 1796 (Part), 1797 (Part), 1836 (Part), 1927 S.A and 1927 RP (Part) in D.D. 107 and Adjoining Government Land, Kam Tin, Yuen Long | Residential | Around 1,154 flats |
| 2 | TPB ref.: A/YL-MP/205-1: Lots 3054 S.A RP, 3098 RP (Part), 3108 (Part), 3109 (Part), 3100 (Part), 3110, 3111, 3112, 3113, 3114, 3115 RP, 3119 RP, 3122 RP, 3123, 3124, 3126, 3131 S.A, 3131 S.B, 3131 S.C, 3131 S.D, 3131 RP, 3132, 3138, 3146, 3147 RP (Part), 3148, 3150 RP, 3156 RP, 3158 RP, 3162, 3163, 3164 S.A, 3164 RP, 3167, 3168, 3171, 3173, 3176, 3177, 3178, 3179, 3180 RP, 3181 RP, 3182 RP, 3189 RP, 3190, 3191, 3192 RP, 3193RP and 3194 RP in D.D. 104 and Adjoining Government Land, Mai Po, Yuen Long, New Territories | Residential | Around 71 flats |
| 3 | TPB ref.: A/YL-MP/344: Lots 50 S.A and 77 in D.D.101, Wo Shang Wai, Mai | Residential | Around 789 flats |

| Site | Address | Use | Development Parameter (Approx.) |
|------|--|------------------------------------|--|
| | Po, Yuen Long | | , , , |
| 4 | TPB ref.: A/YL-NTM/178: | Residential | Around 322 |
| | Lots 435(Part), 436(Part), 438, 439, 442-444, 445(Part), 446-454, 456(Part), 457(Part), 459, 460, 461(Part), 462(Part), 463(Part), 464(Part), 465-474, 476, 478-483, 484(Part), 485, 486(Part), 492495(Part), 516-518, 520, 521(Part), 522(Part), 541(Part), 542(Part), 543-545, 547-552, 555, 556, 559, 560, 562, 563(Part), 564(Part), 572(Part), 573, 574, 575(Part), 576(Part) and Adjoining Government Land in DD 105, Shek Wu Wai, Ngau Tam Mei, Yuen Long | | flats |
| 5 | TPB ref.: A/YL-MP/341: Various Lots in D.D. 104 and Adjoining Government Land, Yau Pok Road, Mai Po, Yuen Long | Residential | Around 2150 flats |
| 6 | TPB ref.: A/YL-MP/247: Lots 3054 S.B RP and 3055 in D.D.104, near Yau Mei San Tsuen, Yuen Long | Residential | Around 105 flats |
| 7 | TPB ref.: A/YL-MP/287: Lots 3207 RP, 3209 RP, 3220 RP, 3221 RP, 3224 RP, 3225 S.A RP, 3225 S.C RP, 3225 RP, 3226 S.A RP, 3226 RP, 3228, 3229, 3230 RP, 3250 S.B ss.21 RP, 3250 S.B ss.33 S.B, 3250 S.B ss.40 S.A RP, 3250 S.B ss.40 RP and 4658 RP in D.D. 104 and Adjoining Government Land, Mai Po, Yuen Long, New Territories | Residential | Around 65 flats |
| 8 | TPB ref.: Y/YL-NSW/4: Lots 594, 595 (Part), 600 (Part), 1288 S.B RP (Part), 1289 S.B RP (Part) and 1292 S.B RP (Part) in D.D. 115, Nam Sang Wai, Yuen Long | Residential | Around 57 flats |
| 9 | TPB ref.: A/YL-NSW/274: Lots 592 S.C ss.1 S.A, 592 S.C ss.4 and 1252 S.C in D.D. 115, Tung Shing Lei, Yuen Long | Residential, Office and RCHE | Around 1518 flats, office with 1800m² GFA and RCHE with no more than 10 beds |
| 10 | TPB ref.: A/YL-NSW/314: Various lots in D.D.104, North of Kam Pok Road East, Pok Wai, Yuen Long, New Territories | Residential | Around 90 flats |

Traffic Generated by the Proposed RCHE

4.7 Traffic generation associated with the Proposed RCHE is calculated based on results presented in Table 2.4, and the calculation is presented in Table 4.4.

TABLE 4.4 TRAFFIC GENERATION OF THE PROPOSED RCHE

| TABLE 1.1 HOURTO GENERATIO | 714 01 1 | 1121110 | 1 OOLD | INOTIL | | | | | | | |
|--|----------|-----------|-----------|--------------|-----------|-------|--|--|--|--|--|
| Item | AM | 1 Peak Ho | ur | PM Peak Hour | | | | | | | |
| | In | Out | 2-way | In | Out | 2-way | | | | | |
| Trip Generation Rates for RCHE (pcu/hour/bed) in Table 2.4 | | | | | | | | | | | |
| RCHE | 0.0346 | 0.0231 | NA | 0.0269 | 0.0500 | NA | | | | | |
| Traffic Generation of Proposed RCHE (po | u/hour) | • | | • | • | | | | | | |
| RCHE: 240 beds | 9 | 6 | <u>15</u> | 7 | <u>12</u> | 19 | | | | | |

4.8 Table 4.4 shows that the total 2-way traffic generated by the Proposed Development is only 14 and 17 pcu/hour (2-way) during the AM and PM peak hours respectively.

2033 Traffic Flows

4.9 Year 2033 traffic flows for the following cases are derived:

2033 without the = (i) 2031 traffic flows derived with reference to BDTM + (ii) estimated total growth from 2031 to 2033 + (iii) Other Developments in the Vicinity of the

Proposed RCHE

2033 with the = [A] + (iv) traffic generated by the Proposed RCHE Proposed RCHE [B] (Table 4.4)

4.10 The 2033 peak hour traffic flows for the cases without and with the Proposed RCHE, are shown in Figures 4.1 - 4.2, respectively.

2033 Junction Operational Performance

4.11 Year 2033 capacity analysis for the cases without and with the Proposed RCHE are summarised in Table 4.5 and detailed calculations are found in the Appendix 1.

TABLE 4.5 2033 JUNCTION OPERATIONAL PERFORMANCE

| Ref. | Junction | Type of Junction / | | out the ed RCHE | With the Proposed RCHE | | |
|-------------------|---|--------------------------|---------|--------------------|---------------------------|---------|--|
| | | Parameter ⁽¹⁾ | AM Peak | PM Peak | AM Peak | PM Peak | |
| J1 | Kam Pok Road / Kam Pok Road East | Priority / RFC | 0.34 | 0.24 | 0.34 | 0.24 | |
| J2 ⁽²⁾ | Castle Peak Road – Tam Mi / Kam Pok Road | Signal / RC | 26% | 34% | 25% | 33% | |
| J3 | The Fairview Roundabout | Roundabout / RFC | 0.66 | 0.71 | 0.66 | 0.72 | |

Notes: (1) RC – reserve capacity RFC – Ratio of Flow to Capacity

4.12 Table 4.5 shows that the junctions operate with capacities during the AM and PM peak hours for the cases without and with the Proposed RCHE.

Impact on Utilisation of Surveyed bus stops

4.13 To be conservative, it is assumed that all pedestrians generated by the Proposed RCHE will use public transport services. The number of public transport passengers generated by the Proposed RCHE is calculated based on the pedestrian generation of the Proposed RCHE, as presented in Table 2.5, and the calculation is found in Table 4.6.

⁽²⁾ Cycle time increased from 94s to 120s as proposed by the approved A/YL-NSW/314

Traffic Impact Assessment Final Report

TABLE 4.6 PUBLIC TRANSPORT PASSENGERS GENERATED BY THE PROPOSED RCHE

| Item | A۱۸ | 1 Peak Ho | ur | PM | ur | | | | | | | |
|---|------------|------------|-------|--------|--------|-------|--|--|--|--|--|--|
| | In | Out | 2-way | In | Out | 2-way | | | | | | |
| Pedestrian Generation Rates for RCHE (pedestrian/15 min/bed) in Table 2.5 | | | | | | | | | | | | |
| RCHE | 0.0615 | 0.0192 | NA | 0.0128 | 0.0654 | NA | | | | | | |
| | | | | | | | | | | | | |
| Pedestrian Generation of Proposed RCHE | (pedestri | an/15 mir | ٦) | | | | | | | | | |
| RCHE: 240 beds | 15 | 5 | 20 | 4 | 16 | 20 | | | | | | |
| Pedestrian Generation of Proposed RCHE | E (pedestr | ian/1 houi | ^) | | | | | | | | | |
| RCHE: 240 beds | 60 | 20 | 80 | 16 | 64 | 80 | | | | | | |

4.14 The public transport utilisation analysis is presented in Table 4.7.

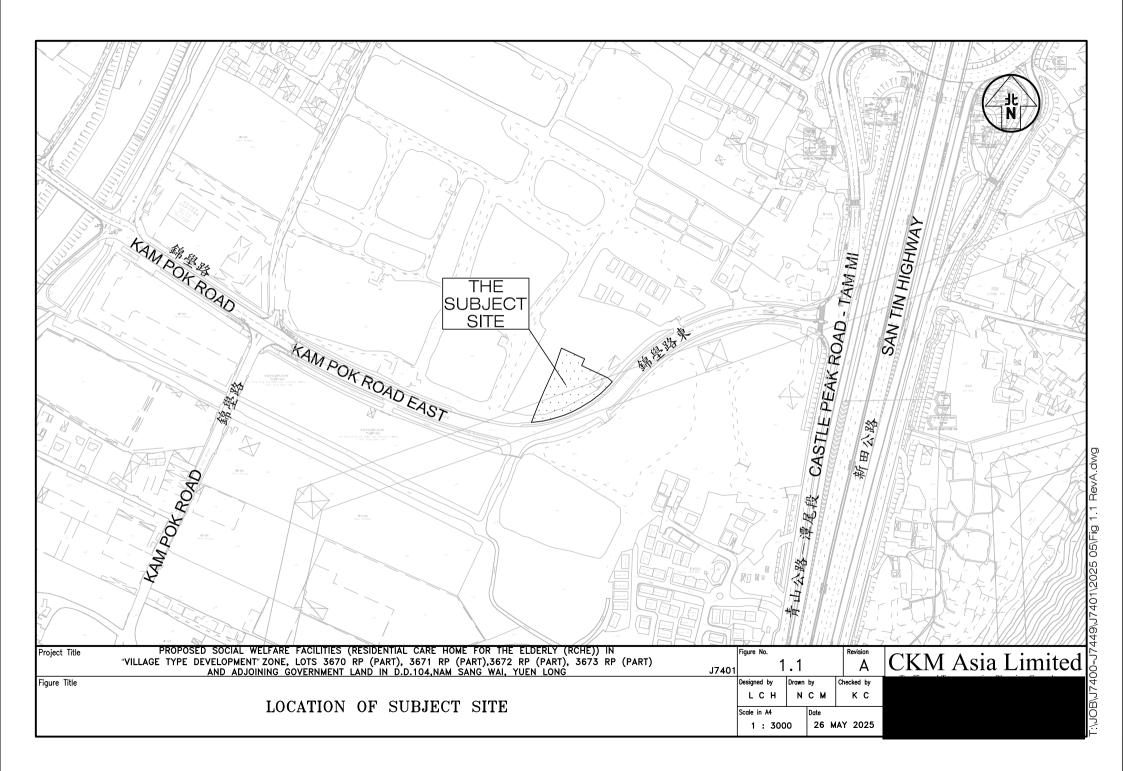
TABLE 4.7 THE UTILISATION OF THE PUBLIC TRANSPORT SERVICES FOR THE CASE WITH THE PROPOSED RCHE

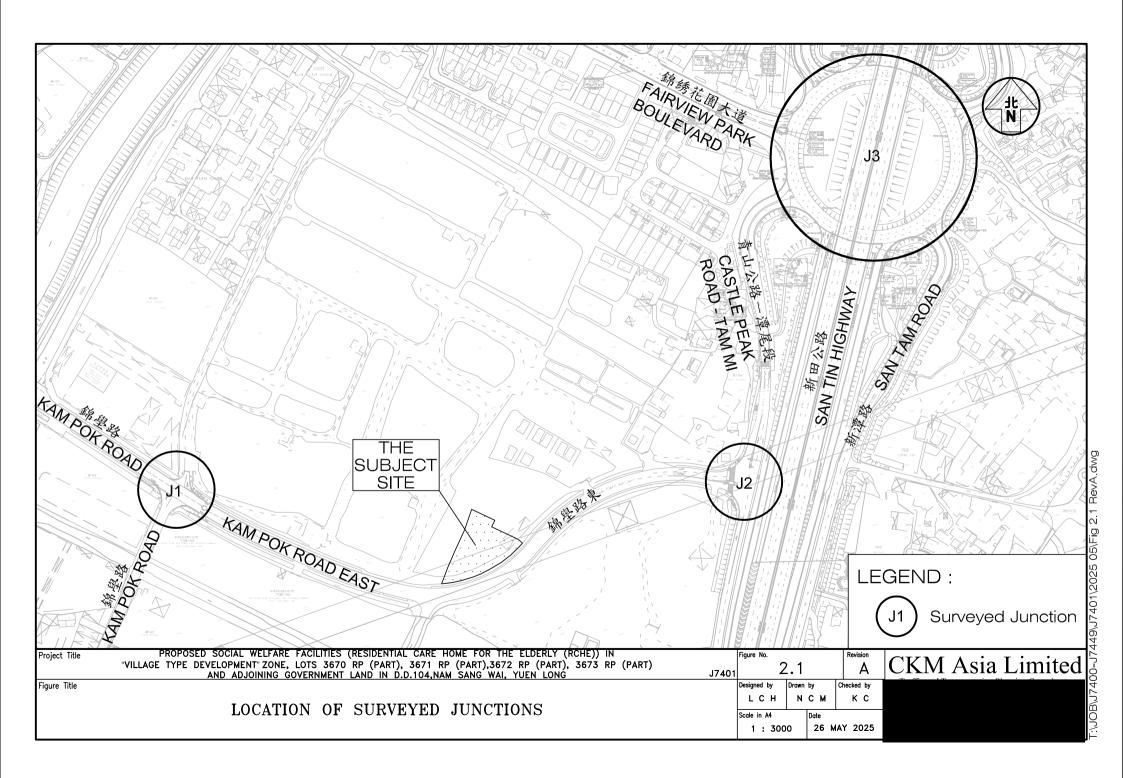
| No. | Location | Occupancy of Public Transport Service | | | | | |
|-----|---|---------------------------------------|---------|--|--|--|--|
| | | AM Peak | PM Peak | | | | |
| 1 | Tai Sang Wai (towards San Tin) Bus Stop | 48.5% | 51.7% | | | | |
| 2 | Long Ha (towards Yuen Long) Bus Stop | 43.3% | 41.5% | | | | |

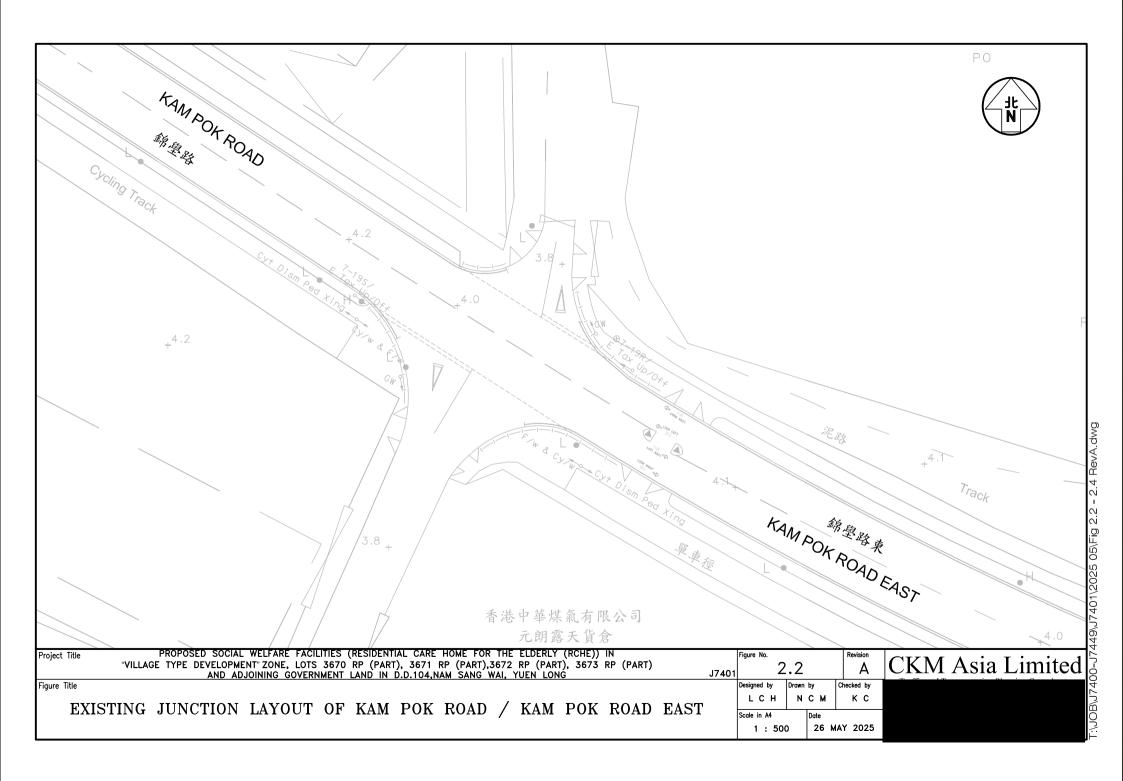
4.15 Table 4.7 shows that the public transport service have capacity to accommodate the passenger demand generated by the Proposed RCHE.

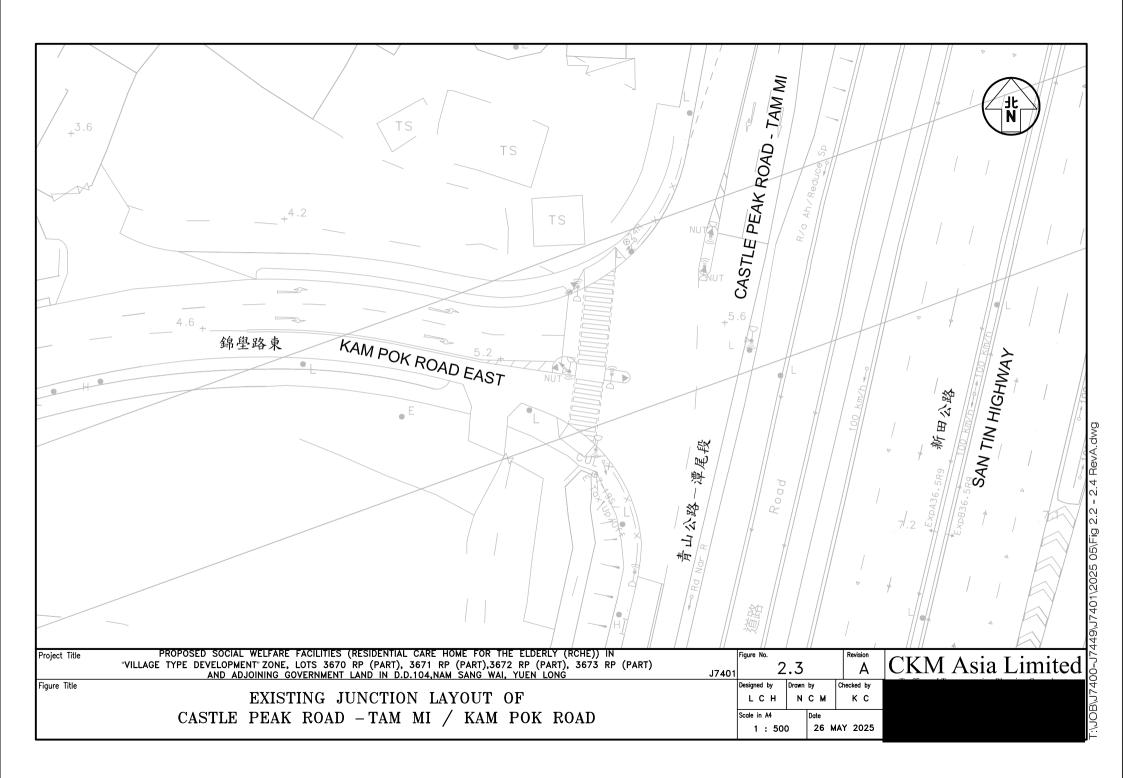
5.0 CONCLUSION

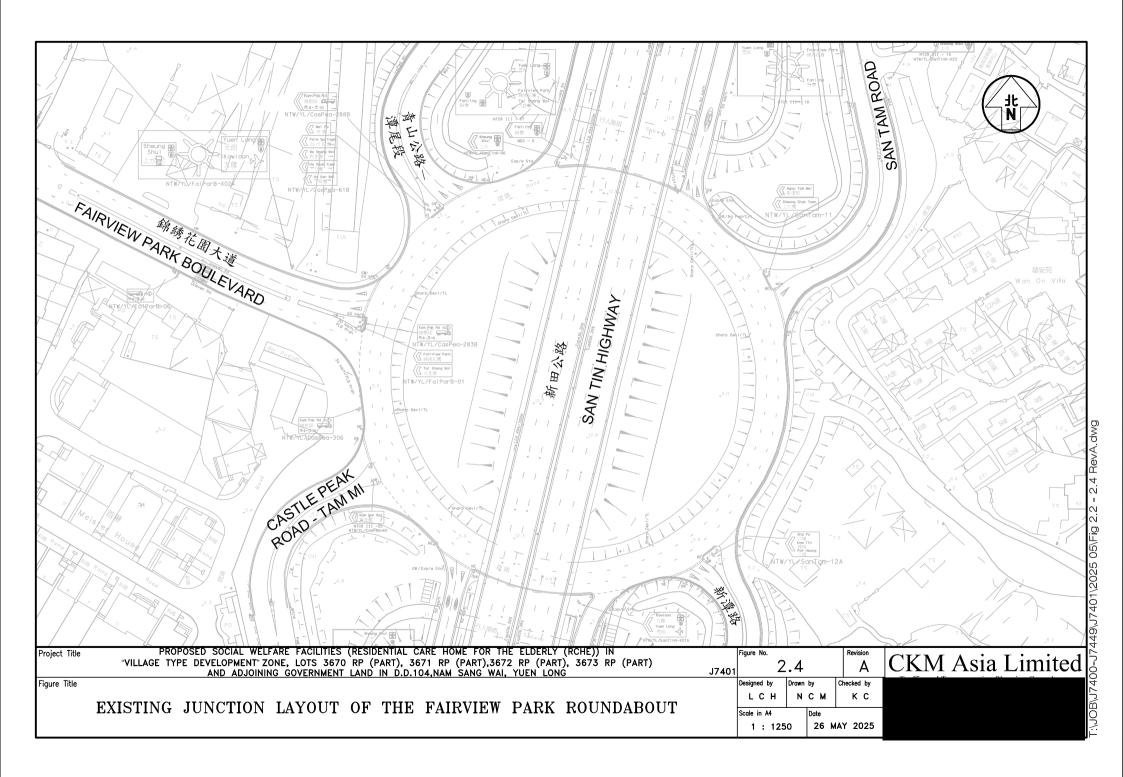
- The Subject Site is located at lots 3670 RP (Part), 3671 RP (Part), 3672 RP (Part), 3673 RP (Part) and adjoining Government Land in D.D.104, Nam Sang Wai, Yuen Long. The owner has the intention to develop the Subject Site into a RCHE with no more than 240 beds.
- 5.2 Manual classified counts were conducted at junctions located in the vicinity of the Proposed RCHE in order to establish the peak hour traffic flows. Currently, these junctions operate with capacities during the AM and PM peak hours.
- 5.3 The internal transport facilities for the Proposed RCHE are provided based on the operational needs with the reference to 3 surveyed RCHEs.
- 5.4 The Proposed RCHE is expected to be completed by 2030, and the junction capacity analysis is undertaken for year 2033. For the design year 2033, the junctions analysed are expected to operate with capacities during the peak hours for the case without and with the Proposed RCHE.
- 5.5 The public transport services at 2 surveyed bus stops have capacity to accommodate the passenger demand generated by the Proposed RCHE.
- 5.6 It is concluded that the Proposed RCHE will result in <u>no adverse traffic impact</u> to the surrounding road network. From traffic engineering grounds, the Proposed RCHE is acceptable.

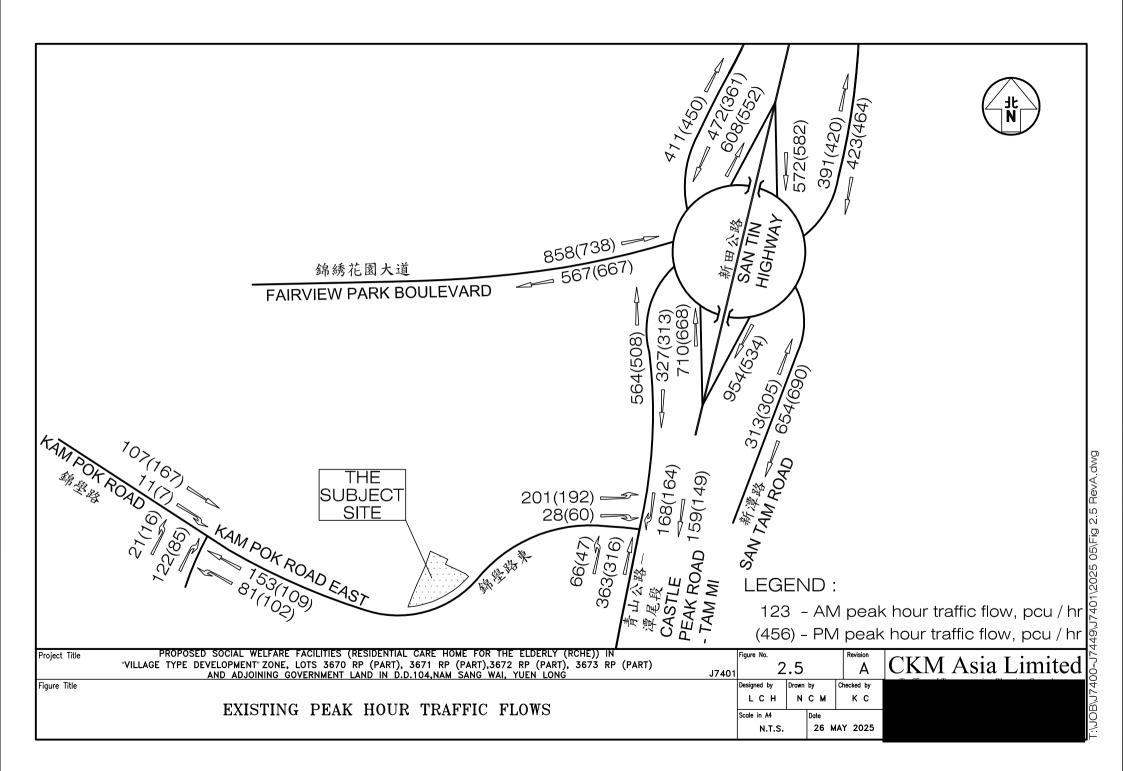


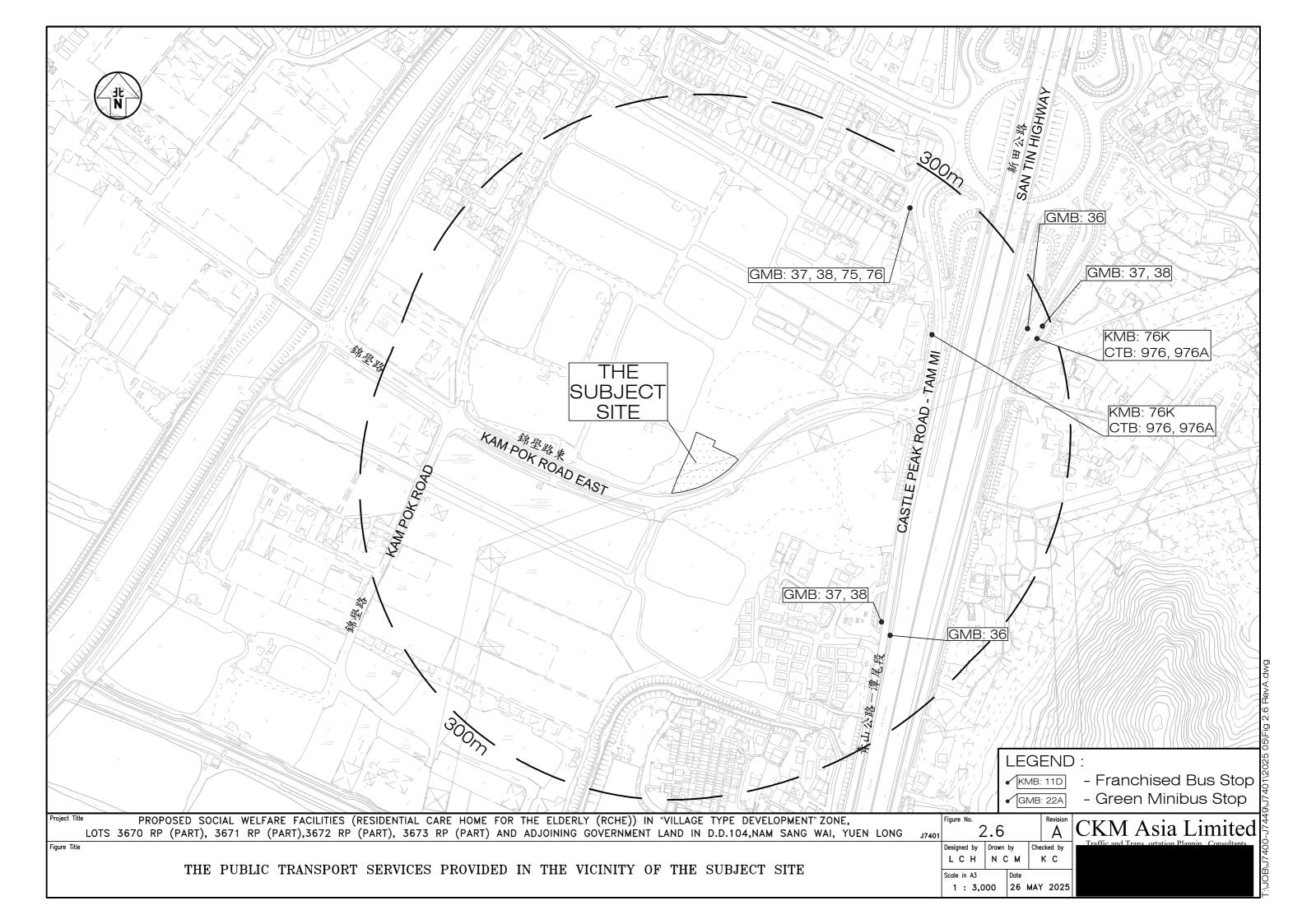


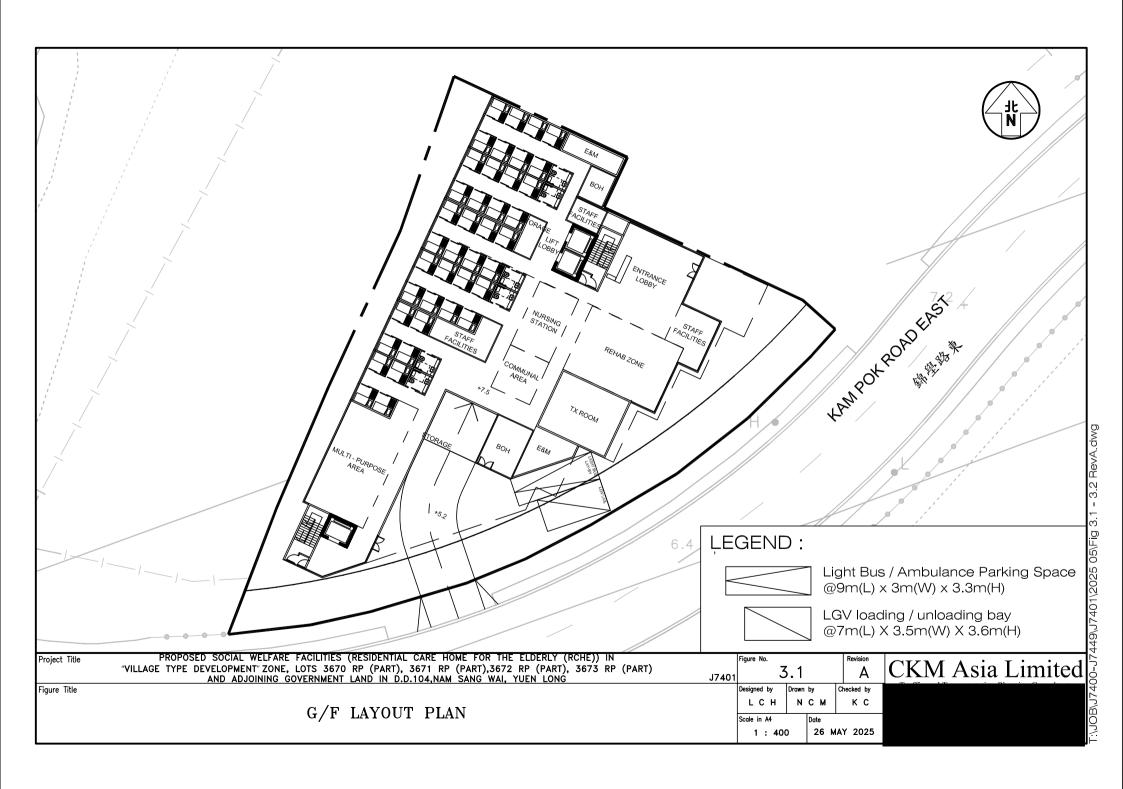


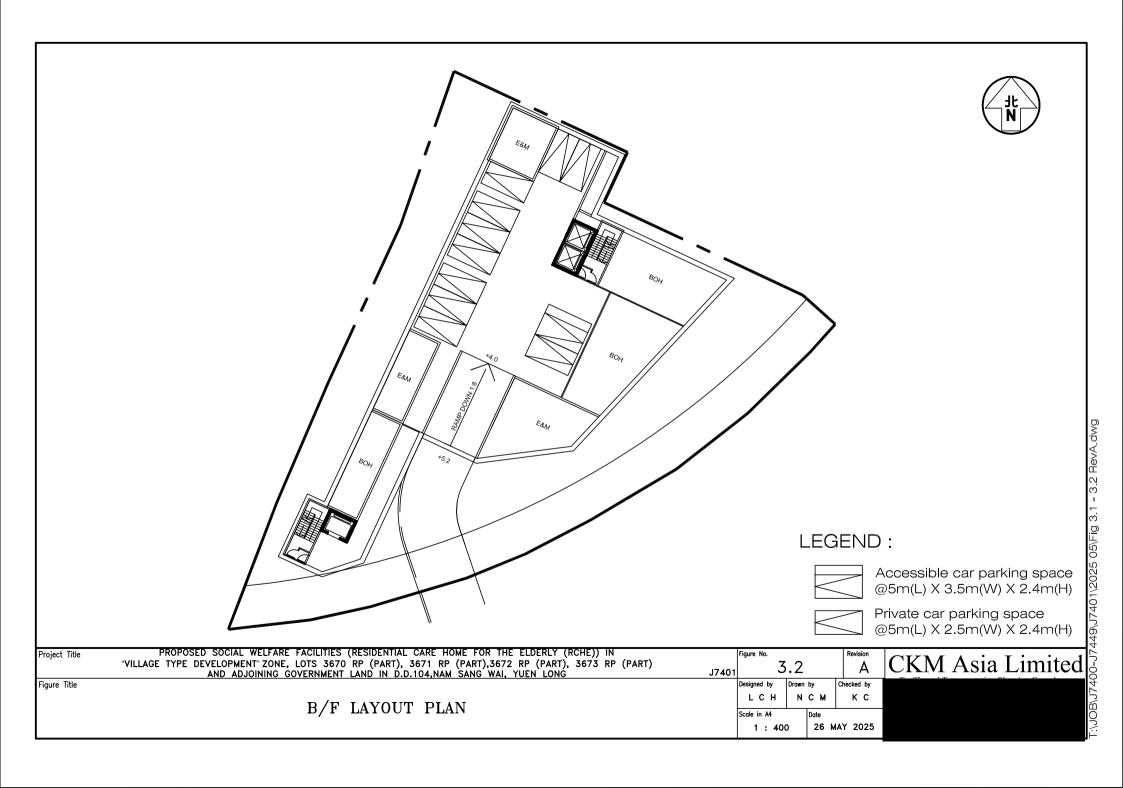


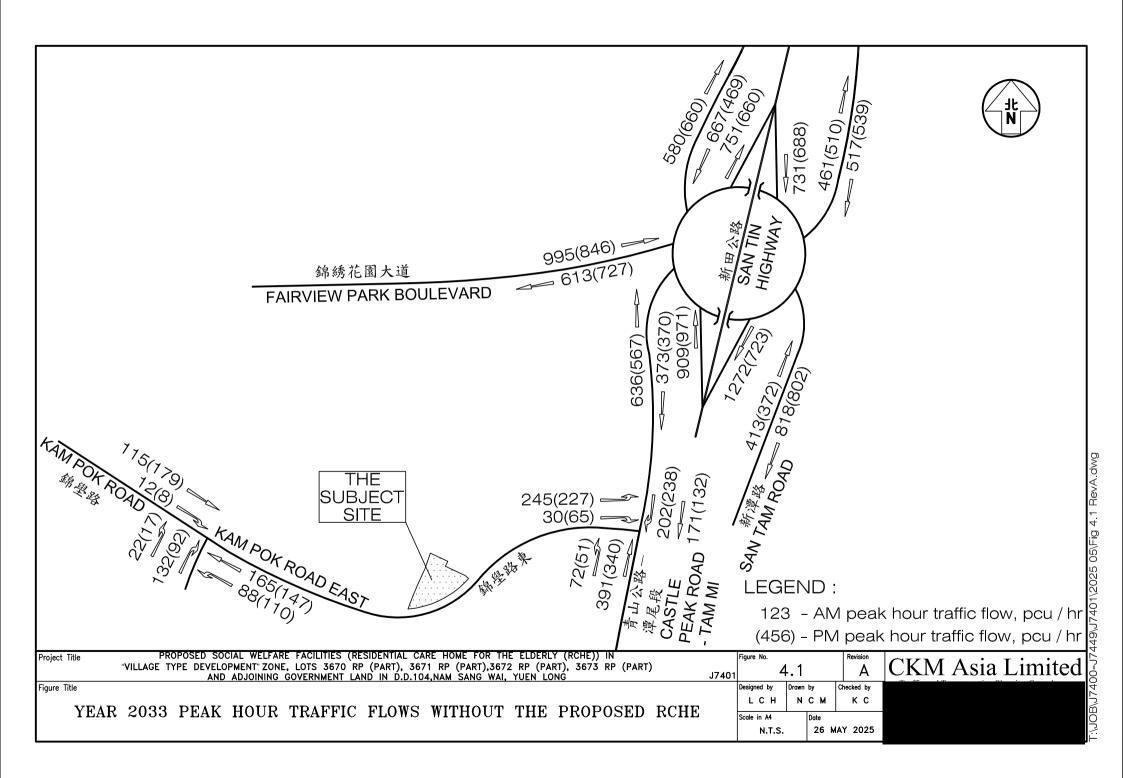


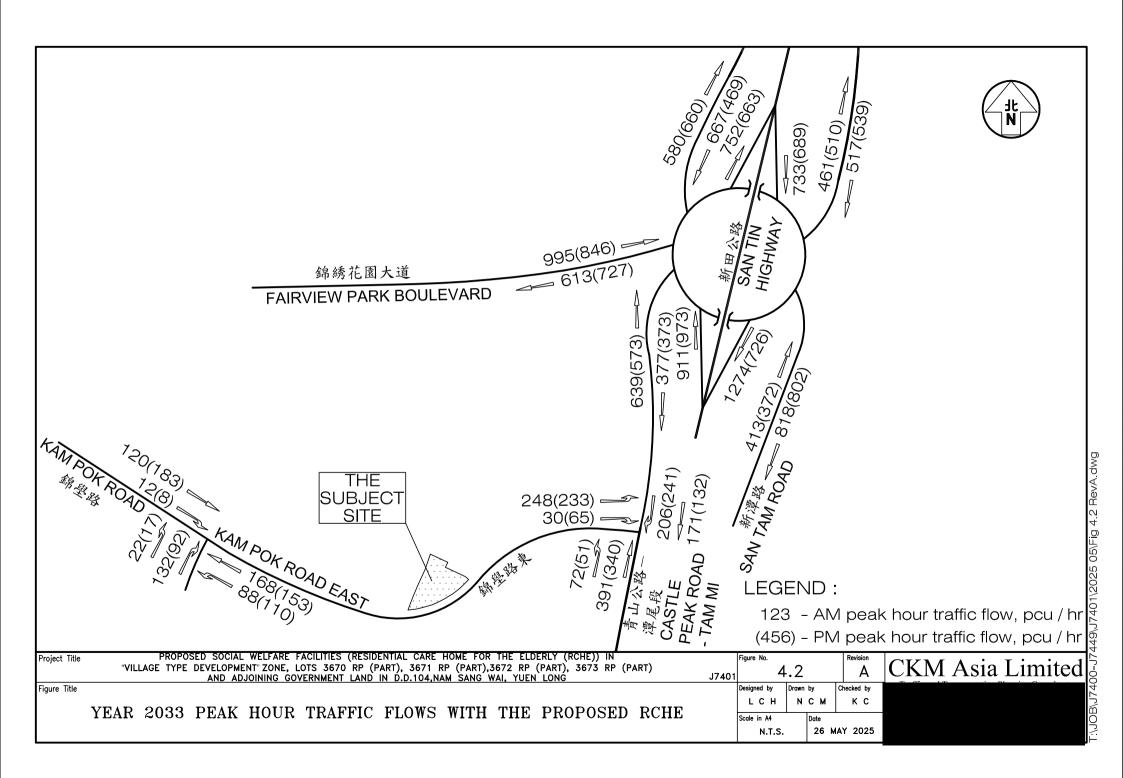












| | | Prior | ity Juncti | on Analy | /sis | | | | |
|--|--------------------|-------------|--------------|----------------|----------------|---------|---------|--------------|---|
| Junction: Kam F | Pok Road / Kai | m Pok R | oad East | | | | | | |
| Design Year: 2025 | _ | ob Numb | er: <u>J</u> | 7401 | D | ate: _ | 26 | May 2025 | |
| Scenario: <u>Existir</u> | ng Condition | | | | | | | Page | 1 |
| Kam Pok Road | EB (Arm C) | | | | Kam Po | ok Road | East WB | (Arm A) | |
| <u>167</u> 107 | , , | | | | | | | , | |
| <u>7</u> 11 | | | | | | _ | | | |
| | | 4 | | | | ← | 153 | <u>109</u> | |
| | | ੂੋ = : | | | _ | | 81 | <u>102</u> | |
| | - | 21 | 122 | | | Г | AM | PM | |
| | - H | 16 | 85 | | | L | Aivi | <u>r ivi</u> | |
| | L K | | Road NB (| (Arm B) | • | | | | |
| | | | | , | | | | | |
| The predictive equations | of capacity of | moveme | nt are: | | | | | | |
| Q-BA = D[627 + 14W-0 | | | 44q-AB + | 0.229q-0 | CA + 0.52q | -CB)] | | | |
| Q-BC = $E[745 - Y(0.364)]$ | | | | | | | | | |
| Q-CB = F[745 - 0.364Y | , , | - | _ | | | | | | |
| The geometric parameter | | | |)][1 | 006(\/ IB \ | 150\1 | | | |
| D = [1 + 0.094(w-B)] E = [1 + 0.094(w-B)] | | | | | 1000(V-IDA | - 150)] | | | |
| F = [1 + 0.094(w-C)] | | | | | | | | | |
| where $Y = 1 - 0.0345$ V | , | | | . /1 | | | | | |
| q-AB, etc = the | | moveme | ent AB, etc | : | | | | | |
| W = major road | - | | , | | | | | | |
| W-CR = central | l reserve width | | | | | | | | |
| w-BA, etc = land | | | | | | | | | |
| v-rBA, etc = vis | | | - | | | С | | | |
| v-IBA, etc = visi | ibility to the lef | t for waiti | ng vehicle | s in strea | am BA, etc | | | | |
| Geometry : | Inpu | ıt | Inpu | ıt | Inpu | t | Calcu | lated | |
| Coomony . | W | | V-rBA | | w-BA | 2.70 | D | 0.7881 | |
| | W-CR | | V-IBA | | w-BC | 2.70 | Ē | 0.8492 | |
| | | | V-rBC | 45 | w-CB | 5.00 | F | 1.0356 | |
| | | | V-rCB | 30 | | | Υ | 0.6447 | |
| Analysis : | | | | | | | | | |
| Traffic Flows, pcu/hr | AM | PM | | | acity, pcu/l | nr | AM | PM | |
| q-CA | 107 | 167 | | | Q-BA | | 445 | 445 | |
| q-CB | 11 | 7 | | | Q-BC | | 596 | 603 | |
| q-AB | 81 | 102 | | | Q-CB | | 715 | 720 | |
| q-AC q-BA | 153 122 | 109 85 | | (| Q-BAC | | 462 | 464 | |
| q-вА q-вС | 21 | 65 16 | | | | | | | |
| q-BC f | 0.147 | 0.158 | | | | | | | |
| · | V.111 | 5.100 | | | | | | | |
| | Ratio-of-f | flow to C | apacity | AM | PM | | | | |
| | | 8-A | | 0.274 | 0.191 | | | | |
| | | B-C | | 0.035 | 0.027 | | | | |
| | | ` D | | | | | | | |
| | | C-B B-AC | | 0.015 0.310 | 0.010 0.217 | | | | |

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| L 41 . | | PIIOI | ity Junction An | alysis | | | | |
|---|--|--|---|--|------------------------------|---|---|---|
| Junction: | Kam Pok Road / k | | | | | | | |
| Design Year: | 2033 | Job Numb | | [| Date: _ | 26 | May 2025 | |
| Scenario: | Future Condition (| Without Pr | oposed RCHE) | | | | Page | 2 |
| Kam Po | k Road EB (Arm C) | | | Kam F | ok Road | East WB | (Arm A) | |
| <u>179</u> | 115 | | | | | | | |
| <u>8</u> | 12 | | | | , r | 405 | 447 | |
| | | 5 | Ò | | | 165 88 | 147 110 | |
| | | ┲=╘=: | =='== | Г | • | | <u></u> | |
| | | 22 | 132 | | | AM | <u>PM</u> | |
| | | <u>17</u> | 92 | , I | | | | |
| | | Kam Pok | Road NB (Arm B |) | | | | |
| Q-BA = D[627 + Q-BC = E[745 - Q-CB = F[745 - The geometric pa D = [1 + 0.0 E = [1 + 0.0 F = [1 + 0.0 where Y = 1 - 0 q-AB, et W = maj W-CR = [1 + 0.0 where W = maj W-CR = [1 + 0.0 where W = maj w-CR = [1 + 0.0 where W = maj w-CR = [1 + 0.0 where w = maj w-CR = [1 + 0.0 where w = 1 | uations of capacity of capacity of 14W-CR - Y(0.364 Y(0.364q-AC + 0.14 0.364Y(q-AC + q-A rameters represente 94(w-BA - 3.65)][1 94(w-BC - 3.65)][1 94(w-CB - 3.65)][1 0.0345W c = the design flow jor road width central reserve width central reserve width | Iq-AC + 0.1 44q-AB)] B)] ed by D, E, + 0.0009(V + 0.0009(V + 0.0009(V of movement | F are: -rBA - 120)][1 + (-rBC - 120)] -rCB - 120)] ent AB, etc | | | | | |
| v-rBA, e | tc = visibility to the l tc = visibility to the l | | | | | | | |
| v-rBA, e v-IBA, e | tc = visibility to the I | eft for waiti | ing vehicles in st | eam BA, etc | ; | Calcu | lated | |
| v-rBA, e | tc = visibility to the I | eft for waiti put | ing vehicles in st | ream BA, etc Inpu | ut | Calcu D | | |
| v-rBA, e v-lBA, e | tc = visibility to the l In | eft for waiti put 10.30 | ing vehicles in st Input V-rBA 4 | eam BA, etc | ; | Calcu D E | lated 0.7881 0.8492 | |
| v-rBA, e v-lBA, e | tc = visibility to the I In W | eft for waiti put 10.30 | ing vehicles in st Input V-rBA 4 | ream BA, etc Inpo 5 w-BA 0 w-BC | e ut 2.70 | D | 0.7881 | |
| v-rBA, e v-lBA, e Geometry : | tc = visibility to the I In W | eft for waiti put 10.30 | Input V-rBA 4 V-IBA 3 | Inpu 5 w-BA 0 w-BC 5 w-CB | 2.70 2.70 | D E | 0.7881 0.8492 | |
| v-rBA, e v-lBA, e Geometry : Analysis : | tc = visibility to the I In W W-CR | eft for waiti put 10.30 0.00 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Inpu 5 w-BA 0 w-BC 5 w-CB | 2.70 2.70 2.70 5.00 | D E F Y | 0.7881 0.8492 1.0356 0.6447 | |
| v-rBA, e v-lBA, e Geometry : Analysis : Traffic Flows, | tc = visibility to the I In W W-CR pcu/hr AM | eft for waiti put 10.30 0.00 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Inpu Inpu 5 w-BA 0 w-BC 5 w-CB 0 | 2.70 2.70 2.70 5.00 | D E F Y | 0.7881 0.8492 1.0356 0.6447 | |
| v-rBA, e v-IBA, e Geometry : Analysis : Traffic Flows, q-CA | tc = visibility to the I In W W-CR pcu/hr AM 115 | eft for waiti put 10.30 0.00 PM 179 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Inpu 5 w-BA 0 w-BC 5 w-CB 0 apacity, pcu | 2.70 2.70 2.70 5.00 | D E F Y AM 441 | 0.7881 0.8492 1.0356 0.6447 PM 436 | |
| v-rBA, e v-IBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB | tc = visibility to the I In W W-CR pcu/hr AM 115 12 | eft for waiti put 10.30 0.00 PM 179 8 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Inpute the second secon | 2.70 2.70 2.70 5.00 | D E F Y AM 441 593 | 0.7881 0.8492 1.0356 0.6447 PM 436 595 | |
| v-rBA, e v-IBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB q-AB | tc = visibility to the I In W W-CR pcu/hr AM 115 12 88 | eft for waiti put 10.30 0.00 PM 179 8 110 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Input S w-BA W-CB W-CB apacity, pcur Q-BA Q-BC Q-CB | 2.70 2.70 2.70 5.00 | D E F Y AM 441 593 710 | 0.7881 0.8492 1.0356 0.6447 PM 436 595 709 | |
| v-rBA, e v-IBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB q-AB q-AC | tc = visibility to the I In W W-CR pcu/hr AM 115 12 88 165 | PM 179 8 110 147 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Inpute the second secon | 2.70 2.70 2.70 5.00 | D E F Y AM 441 593 | 0.7881 0.8492 1.0356 0.6447 PM 436 595 | |
| v-rBA, e v-lBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB q-AB q-AC q-BA | tc = visibility to the I In W W-CR pcu/hr AM 115 12 88 165 132 | PM 179 8 110 147 92 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Input S w-BA W-CB W-CB apacity, pcur Q-BA Q-BC Q-CB | 2.70 2.70 2.70 5.00 | D E F Y AM 441 593 710 | 0.7881 0.8492 1.0356 0.6447 PM 436 595 709 | |
| v-rBA, e v-IBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB q-AB q-AC | tc = visibility to the I In W W-CR pcu/hr AM 115 12 88 165 132 22 | PM 179 8 110 147 92 17 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Input S w-BA W-CB W-CB apacity, pcur Q-BA Q-BC Q-CB | 2.70 2.70 2.70 5.00 | D E F Y AM 441 593 710 | 0.7881 0.8492 1.0356 0.6447 PM 436 595 709 | |
| v-rBA, e v-lBA, e v-lBA, e Geometry : Analysis : Traffic Flows, q-CA q-CB q-AB q-AC q-BA q-BC | tc = visibility to the I In W W-CR pcu/hr AM 115 12 88 165 132 22 0.143 | PM 179 8 110 147 92 17 | Input V-rBA 4 V-IBA 3 V-rBC 4 V-rCB 3 | Input W-BA W-BC W-BC W-CB W-CB W-CB W-CB W-CB W-CB | 2.70 2.70 2.70 5.00 | D E F Y AM 441 593 710 | 0.7881 0.8492 1.0356 0.6447 PM 436 595 709 | |

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| | | Prior | ity Junctio | on Analy | /sis | | | | |
|--------------------------|--|---------------|--------------|------------|----------------------|---|-----------|-------------------|---|
| Junction: | Kam Pok Road / Ka | am Pok R | oad East | | | | | | |
| Design Year: | | Job Numb | | 7401 | Da | ate: | 26 | May 2025 | |
| Scenario: | Future Condition (V | Vith Propo | sed RCHE | Ξ) | | | | Page | 3 |
| Kam Pok | Road EB (Arm C) | | | | Kam Po | k Road | East WB | (Arm A) | |
| <u>183</u> | 120 | | | | | | | | |
| <u>8</u> | 12 | | | | | | 400 | | |
| | | 5 | ð | | | | 168 88 | <u>153</u> 110 | |
| | | ===== | =='== | | | <u>, </u> | 00 | <u>110</u> | |
| | Ī | 22 | 132 | | | Γ | AM | <u>PM</u> | |
| | [| <u>17</u> | <u>92</u> | | | _ | - | | |
| | | Kam Pok | Road NB (| Arm B) | | | | | |
| The predictive equ | ations of capacity of | f moveme | nt are: | | | | | | |
| | 14W-CR - Y(0.364c | | | 0.229q-0 | CA + 0.52q- | CB)] | | | |
| Q-BC = $E[745 - $ | Y(0.364q-AC + 0.14 | 4q-AB)] | • | • | ' | /- | | | |
| - | 0.364Y(q-AC + q-AB | / - | | | | | | | |
| | ameters represente | | | | | | | | |
| | 94(w-BA - 3.65)][1 + | | | | 006(V-IBA | - 150)] | | | |
| | 94(w-BC - 3.65)][1 + 94(w-CB - 3.65)][1 + | | | | | | | | |
| where $Y = 1 - 0.03$ | , , | 0.0003(V | -100 - 120 | /1 | | | | | |
| | c = the design flow o | f moveme | ent AB. etc | | | | | | |
| _ | or road width | | , | | | | | | |
| W-CR = | central reserve widt | h | | | | | | | |
| | c = lane width to veh | | | | | | | | |
| | c = visibility to the ri | - | - | | | • | | | |
| V-IBA, etc | c = visibility to the le | ett for Walti | ing venicies | s in strea | am BA, etc | | | | |
| Geometry: | Inp | ut | Inpu | t | Input | | Calcu | lated | |
| , | w | | V-rBA | | w-BA | 2.70 | D | 0.7881 | |
| | W-CR | 0.00 | V-IBA | 30 | w-BC | 2.70 | Е | 0.8492 | |
| | | | V-rBC | 45 | w-CB | 5.00 | F | 1.0356 | |
| | | | V-rCB | 30 | | | Υ | 0.6447 | |
| Analysis : | oou/br AM | DI/I | | Can | acity paulh | r | A N 4 | DM | |
| Traffic Flows, p q-CA | ocu/hr AM 120 | PM 183 | | - | acity, pcu/h Q-BA | I | AM 439 | PM 434 | |
| q-CA q-CB | 120 | 8 | | | Q-BC | | 592 | 434 594 | |
| q-GB q-AB | 88 | 110 | | | Q-DC Q-CB | | 709 | 708 | |
| q-AB q-AC | 168 | 153 | | | Q-BAC | | 456 | 453 | |
| q-AC q-BA | 132 | 92 | | ` | G D/10 | | 730 | 700 | |
| q-BC | 22 | 17 | | | | | | | |
| f | 0.143 | 0.156 | | | | | | | |
| | Ratio of | -flow to C | anacity | AM | PM | | | | |
| | | B-A | арасну | 0.300 | 0.212 | | | | |
| | | B-C | | 0.037 | 0.029 | | | | |
| | | C-B | | 0.017 | 0.011 | | | | |
| | | B-AC | | 0.337 | 0.240 | | | | |
| | | | | | | | | | |

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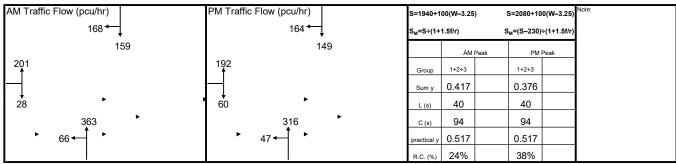
Signal Junction Analysis

 Junction:
 Castle Peak Road - Tam Mi / Kam Pok Road
 Job Number:
 J7401

 Scenario:
 Existing Condition
 P. 4

 Design Year:
 2025
 Designed By:
 Checked By:
 Date:
 26 May 2025

| Approach | Phase | Stage | Width (m) | Radius (m) | % Up-hill | Turning % | Sat. Flow | AM Peak Flow | y value | Critical y | Turning % | Sat. Flow | PM Peak Flow | y value | Critical |
|---------------------------------|-------|-------|-----------|------------|-----------|-----------|-----------|-----------------|---------|------------|-----------|-----------|-----------------|---------|----------|
| | | - | | , , | Gradient | | (pcu/hr) | (pcu/hr) | , | | | (pcu/hr) | (pcu/hr) | | |
| Castle Peak Road - LT+SA | A1 | 1 | 3.50 | 20.0 | | 17 | 1940 | 429 | 0.221 | 0.221 | 14 | 1945 | 363 | 0.187 | 0.187 |
| Tam Mi NB | | | | | | | | | | | | | | | |
| Castle Peak Road - Tam Mi SB SA | B1 | 2 | 3.30 | | | | 2085 | 159 | 0.076 | | | 2085 | 149 | 0.071 | |
| RT | B2 | 2 | 3.40 | 15.0 | | 100 | 1905 | 168 | 0.088 | 0.088 | 100 | 1905 | 164 | 0.086 | 0.086 |
| Kam Pok Road EB LT | C1 | 3 | 3.50 | 28.0 | | 100 | 1865 | 201 | 0.108 | 0.108 | 100 | 1865 | 192 | 0.103 | 0.103 |
| RT | C2 | 3 | 3.50 | 13.0 | | 100 | 1887 | 28 | 0.015 | | 100 | 1887 | 60 | 0.032 | |
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| pedestrian phase | D(p) | 4 | | min cr | ossing | time = | 13 | sec | GM + | 12 | sec F | GM = | 25 | sec | |
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| 1 | A1 ← | | | 2 | B2 B1 | | C1 C2 | | | 4 Dpi ↓ | | | | 5 | |
|-----------|-------------|-------|---|-----|-------|---|-------|-------|---|---------------|----|-------|---|-----|-------|
| AM G = | | I/G = | 6 | G = | I/G = | 5 | G = | I/G = | 5 | G = | 25 | I/G = | 2 | G = | I/G = |
| G = | | I/G = | | G = | I/G = | | G = | I/G = | | G = | | I/G = | | G = | I/G = |
| PM G = | | I/G = | 6 | G = | I/G = | 5 | G = | I/G = | 5 | G = | 25 | I/G = | 2 | G = | I/G = |
| G = | | I/G = | | G = | I/G = | | G = | I/G = | | G = | | I/G = | | G = | I/G = |

Signal Junction Analysis

 Junction:
 Castle Peak Road - Tam Mi / Kam Pok Road
 Job Number:
 J7401

 Scenario:
 Future Condition (Without Proposed RCHE)
 P. 5

 Design Year:
 2033
 Designed By:
 Checked By:
 Date:
 26 May 2025

| Approach | Ph | ase Stage | Width (m) | Radius (m) | % Up-hill | Turning % | Sat. Flow | AM Peak Flow | y value | Critical y | Turning % | Sat. Flow | PM Peak Flow | y value | Critical |
|---|--------|-----------|------------|------------------|-------------------------|-----------|-----------|--|---|------------|-----------------------------|--------------------------|-----------------|---------|----------|
| | | | | | Gradient | | (pcu/hr) | (pcu/hr) | | | | (pcu/hr) | (pcu/hr) | | |
| Castle Peak Road - L1 | T+SA A | 1 1 | 3.50 | 20.0 | | 14 | 1945 | 463 | 0.238 | 0.238 | 10 | 1950 | 391 | 0.201 | 0.20 |
| Tam Mi NB | | | | | | | | | | | | | | | |
| Castle Peak Road - Tam Mi SB | SA E | 1 2 | 3.30 | | | | 2085 | 171 | 0.082 | | | 2085 | 132 | 0.063 | |
| | RT E | 2 2 | 3.40 | 15.0 | | 100 | 1905 | 202 | 0.106 | 0.106 | 100 | 1905 | 238 | 0.125 | 0.12 |
| | | | | | | | | | | | | | | | |
| Kam Pok Road EB | LT C | 1 3 | 3.50 | 28.0 | | 100 | 1865 | 245 | 0.131 | 0.131 | 100 | 1865 | 227 | 0.122 | 0.122 |
| | RT C | 2 3 | 3.50 | 13.0 | | 100 | 1887 | 30 | 0.016 | | 100 | 1887 | 65 | 0.034 | |
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| | | | | <u> </u> | | | | | | | | | | | |
| pedestrian phase | D | p) 4 | | min c | rossing t | ime = | 13 | sec (| GM + | 12 | sec F | GM = | 25 | sec | |
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| AM Traffic Flow (pcu/hr) | | PM Tr | affic Flov | v (pcu/hr | ·) | | | S=1940+1 | 00(W-3.25 |) : | S=2080+10 | 0(W-3.25) | Note: | | |
| AM Traffic Flow (pcu/hr) | | PM Tr | affic Flov | v (pcu/hr 238 | | | | S=1940+1 S _M =S÷(1+ | • | | | 0(W–3.25) ÷(1+1.5f/r) | Note: | | |
| | | PM Tr | affic Flov | | | | | | 1.5f/r) | s | S _M =(S-230) | ÷(1+1.5f/r) | Note: | | |
| 202 | | | affic Flov | | $\leftarrow \downarrow$ | | | S _M =S÷(1+ | 1.5f/r) | | S _M =(S-230) | | Note: | | |
| 202 ← ↓ 171 | | PM Tr | affic Flov | | $\leftarrow \downarrow$ | | | S _M =S÷(1+ | 1.5f/r) AM 1+2+3 | s | PM 1+2+3 | ÷(1+1.5f/r) | Note: | | |
| 202 ← 171 245 | | 227 | affic Flov | | $\leftarrow \downarrow$ | | | S _M =S÷(1+ | 1.5f/r) AM 1+2+3 0.475 | s | PM 1+2+3 0.447 | ÷(1+1.5f/r) | Note: | | |
| 202 171 | | | affic Flov | 238 | $\leftarrow \downarrow$ | | | S _M =S÷(1+ | 1.5f/r) AM 1+2+3 0.475 40 | s | PM 1+2+3 0.447 40 | ÷(1+1.5f/r) | Note: | | |
| 171 245 30 391 | | 227 | | 340 | $\leftarrow \downarrow$ | | | S _M =S÷(1+ Group Sum y L (s) C (s) | 1.5f/r) AM 1+2+3 0.475 40 120 | s | PM 1+2+3 0.447 40 120 | ÷(1+1.5f/r) | Note: | | |
| 202 171 | | 227 | affic Flov | 340 | $\leftarrow \downarrow$ | | | S _M =S÷(1+ Group Sum y L (s) C (s) practical y | 1.5f/r) AM 1+2+3 0.475 40 120 0.600 | s | PM 1+2+3 0.447 40 120 0.600 | ÷(1+1.5f/r) | Note: | | |
| 202 171 245 30 391 | | 227 | | 340 | $\leftarrow \downarrow$ | | | S _M =S÷(1+ Group Sum y L (s) C (s) | 1.5f/r) AM 1+2+3 0.475 40 120 | s | PM 1+2+3 0.447 40 120 | ÷(1+1.5f/r) | Note: | | |
| 202 171 245 30 391 | | 227 | | 340 | $\leftarrow \downarrow$ | | | S _M =S÷(1+ Group Sum y L (s) C (s) practical y | 1.5f/r) AM 1+2+3 0.475 40 120 0.600 | s | PM 1+2+3 0.447 40 120 0.600 | ÷(1+1.5f/r) | Note: | | |
| 202 171 245 30 391 72 1 | | 227 | ▶ 51 | 238 | $\leftarrow \downarrow$ | | | Group Sum y L (s) C (s) practical y R.C. (%) | 1.5f/r) AM 1+2+3 0.475 40 120 0.600 | s | PM 1+2+3 0.447 40 120 0.600 | ÷(1+1.5f/r) Peak | Note: | | |
| 202 171 245 30 391 72 1 | | 227 | ▶ 51 | 238 | $\leftarrow \downarrow$ | | | S _M =S+(1+ Group Sum y L (s) C (s) practical y R.C. (%) | 1.5f/r) AM 1+2+3 0.475 40 120 0.600 26% | s | PM 1+2+3 0.447 40 120 0.600 | ÷(1+1.5f/r) Peak | Note: | | |
| 202 171 245 30 391 72 1 | | 227 | ▶ 51 | 340 | 132 | | | Group Sum y L (s) C (s) practical y R.C. (%) | 1.5f/r) AM 1+2+3 0.475 40 120 0.600 26% | s | PM 1+2+3 0.447 40 120 0.600 | ÷(1+1.5f/r) Peak | Note: | | |

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Signal Junction Analysis

 Junction:
 Castle Peak Road - Tam Mi / Kam Pok Road
 Job Number:
 J7401

 Scenario:
 Future Condition (With Proposed RCHE)
 P. 6

Design Year: 2033 Designed By: _____ Checked By: _____ Date: 26 May 2025

| Approach | | Phase | Stage | Width (m) | Radius (m) | % Up-hill Gradient | Turning % | Sat. Flow (pcu/hr) | AM Peak Flow (pcu/hr) | y value | Critical y | Turning % | Sat. Flow (pcu/hr) | PM Peak Flow (pcu/hr) | y value | Critical |
|------------------------------|------|-------|----------|-----------|----------------|-----------------------|-----------|-----------------------|-----------------------------|--------------|------------|-------------------------|-----------------------|-----------------------------|---------|----------|
| Castle Peak Road - L | T+SA | A1 | 1 | 3.50 | 20.0 | Oradion | 14 | 1945 | 463 | 0.238 | 0.238 | 10 | 1950 | 391 | 0.201 | 0.20 |
| Tam Mi NB | | | | | | | | | | | | | | | | |
| Castle Peak Road - Tam Mi SB | SA | B1 | 2 | 3.30 | | | | 2085 | 171 | 0.082 | | | 2085 | 132 | 0.063 | |
| | RT | B2 | 2 | 3.40 | 15.0 | | 100 | 1905 | 206 | 0.108 | 0.108 | 100 | 1905 | 241 | 0.127 | 0.12 |
| Kam Pok Road EB | LT | C1 | 3 | 3.50 | 28.0 | | 100 | 1865 | 248 | 0.133 | 0.133 | 100 | 1865 | 233 | 0.125 | 0.12 |
| | RT | C2 | 3 | 3.50 | 13.0 | | 100 | 1887 | 30 | 0.016 | | 100 | 1887 | 65 | 0.034 | |
| | | | | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | | | | |
| pedestrian phase | | D(p) | 4 | | min c | rossing | time = | 13 | sec (| GM + | 12 | sec F | GM = | 25 | sec | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| AM Traffic Flow (pcu/hr) | | | PM Tra | ffic Flow | / (pcu/hr | -) | | | S=1940+1 | 00(W-3.25 |) ; | S=2080+10 | 00(W-3.25) | Note: | | |
| 206← | | | | | 241 | ← ↓ | | | S _M =S÷(1+ | 1.5f/r) | s | 6 _M =(S-230) | ÷(1+1.5f/r) | | | |
| 171 | | | | | | 132 | | | | AM | Peak | PM | Peak | | | |
| 248 ↑ | | | 233 | | | | | | Group | 1+2+3 | | 1+2+3 | | | | |
| _ | | | | | | | | | Sum y | 0.479 | | 0.452 | | | | |
| 30 | | Þ | 65 | | ٠ | • | | | L (s) | 40 | | 40 | | | | |
| 391 | | | | | 340 1 | , | • | | C (s) | 120 | | 120 | | | | |
| ▶ 72 ← | | | , | 51 | ┥′ | | | | practical y | 0.600 25% | | 0.600 | | | | |
| 1 2 | | | <u> </u> | | 3 | | | | 4 | , =3,0 | | | 5 | | | |
| | | | B2 B1 | | c ₁ | | | | _ 4 | • | | | | | | |
| | | | | | C2 | | | | Dp | , | | | | | | |
| A1 | | | | | | | | | | | | | | | | |

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Roundabout Analysis

 Junction:
 The Fairview Park Roundabout
 Job Number: J7401

 Scenario:
 Existing Condition
 P. 7

 Design Year:
 2025
 Designed By:
 Checked By:
 Date:
 26 May 2025

AM Peak

| Arm | To A | То В | To C | To D | To E | to F | to G | Total | q_c |
|--------|------|------|------|------|------|------|------|-------|-------|
| From A | 34 | 53 | 373 | 138 | 72 | 120 | 68 | 858 | 1234 |
| From B | 30 | 11 | 137 | 32 | 52 | 205 | 97 | 564 | 1765 |
| From C | 205 | 41 | 42 | 128 | 127 | 68 | 99 | 710 | 1375 |
| From D | 29 | 17 | 72 | 14 | 51 | 117 | 13 | 313 | 1431 |
| From E | 62 | 34 | 131 | 108 | 10 | 46 | 32 | 423 | 1353 |
| From F | 155 | 86 | 110 | 84 | 25 | 29 | 83 | 572 | 1168 |
| From G | 52 | 85 | 89 | 150 | 54 | 23 | 19 | 472 | 1329 |
| | | | | | | | | | |
| Total | 567 | 327 | 954 | 654 | 391 | 608 | 411 | 3912 | |

PM Peak

| Arm | To A | То В | To C | To D | To E | to F | to G | - | Total | q _c |
|--------|------|------|------|------|------|------|------|---|-------|----------------|
| From A | 28 | 53 | 151 | 97 | 95 | 251 | 63 | | 738 | 1147 |
| From B | 67 | 16 | 76 | 44 | 77 | 110 | 118 | | 508 | 1572 |
| From C | 223 | 75 | 22 | 140 | 76 | 35 | 97 | | 668 | 1546 |
| From D | 66 | 17 | 48 | 24 | 63 | 70 | 17 | | 305 | 1524 |
| From E | 99 | 21 | 127 | 133 | 14 | 37 | 33 | | 464 | 1409 |
| From F | 124 | 73 | 54 | 146 | 51 | 25 | 109 | | 582 | 1321 |
| From G | 60 | 58 | 56 | 106 | 44 | 24 | 13 | | 361 | 1453 |
| | | | | | | | | | | |
| Total | 667 | 313 | 534 | 690 | 420 | 552 | 450 | : | 3626 | |

Legend

| Arm | Road (in clockwise order) |
|-----|----------------------------|
| Α | Fairview Park Boulevard EB |
| В | Castle Peak Road NB |
| С | San Tin Road NB |
| D | San Tam Road NB |
| E | San Tam Road SB |
| F | San Tin Road SB |
| G | Castle Peak Road SB |
| Н | |

Geometric Parameters

| | o i aiaiiiote | | | | | | |
|--------|---------------|-------|-------|-------|-------|-------|-----|
| Arm | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S |
| From A | 11.0 | 7.0 | 22.0 | 14.0 | 142 | 35 | 0.5 |
| From B | 9.0 | 5.5 | 20.0 | 10.0 | 142 | 35 | 0.6 |
| From C | 8.5 | 6.4 | 23.0 | 7.5 | 142 | 30 | 0.4 |
| From D | 8.5 | 6.5 | 20.0 | 10.0 | 142 | 25 | 0.3 |
| From E | 8.0 | 6.0 | 20.0 | 9.5 | 142 | 35 | 0.3 |
| From F | 8.5 | 6.0 | 25.0 | 6.5 | 142 | 40 | 0.6 |
| From G | 6.0 | 5.0 | 22.0 | 7.0 | 142 | 30 | 0.2 |
| From H | | | | | | | |

Predictive Equation $Q_E = K(F - f_cq_c)$

| Q_{E} | Entry Capacity |
|----------------|-------------------------------------|
| q _c | Circulating Flow across the Entry |
| К | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F | = 303x ₂ |
| f _c | $= 0.210t_D(1+0.2x_2)$ |
| t_{D} | = 1+0.5/(1+M) |
| М | = exp[(D-60)/10] |
| x_2 | = v+(e-v)/(1+2S) |
| s | = 1.6(e-v)/L |

Limitation

| е | Entry Width | 4.0 - 15.0 m |
|---|---------------------------|---------------|
| v | Approach Half Width | 2.0 - 7.3 m |
| r | Entry Radius | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m |
| Ø | Entry Angle | 10° - 60° |
| S | Sharpness of Flare | 0.0 - 3.0 |

Ratio-of-Flow to Capacity (RFC)

| | | | | | | | Q_E | | Entry Flow | | RFC | |
|--------|-----------------------|---------|---------|------|---------|----------------|---------|------|------------|-----|------|------|
| Arm | X ₂ | M | t_{D} | K | F | f _c | AM | PM | AM | PM | AM | PM |
| From A | 9.09 | 3640.95 | 1.00 | 0.99 | 2754.13 | 0.59 | 1997.68 | 2049 | 858 | 738 | 0.43 | 0.36 |
| From B | 7.15 | 3640.95 | 1.00 | 0.98 | 2166.74 | 0.51 | 1243.90 | 1341 | 564 | 508 | 0.45 | 0.38 |
| From C | 7.51 | 3640.95 | 1.00 | 1.01 | 2274.80 | 0.53 | 1562.29 | 1472 | 710 | 668 | 0.45 | 0.45 |
| From D | 7.72 | 3640.95 | 1.00 | 1.02 | 2339.01 | 0.53 | 1601.76 | 1551 | 313 | 305 | 0.20 | 0.20 |
| From E | 7.19 | 3640.95 | 1.00 | 0.98 | 2180.08 | 0.51 | 1461.19 | 1433 | 423 | 464 | 0.29 | 0.32 |
| From F | 7.12 | 3640.95 | 1.00 | 0.98 | 2157.57 | 0.51 | 1523.95 | 1448 | 572 | 582 | 0.38 | 0.40 |
| From G | 5.69 | 3640.95 | 1.00 | 1.00 | 1722.94 | 0.45 | 1131.38 | 1075 | 472 | 361 | 0.42 | 0.34 |
| From H | | | | | | | | | | | | |

Roundabout Analysis

 Junction:
 The Fairview Park Roundabout
 Job Number: J7401

 Scenario:
 Future Condition (Without Proposed RCHE)
 P. 8

 Design Year:
 2033
 Designed By:
 Checked By:
 Date:
 26 May 2025

AM Peak

| Arm | To A | То В | To C | To D | To E | to F | to G | Total | q_c |
|--------|------|------|------|------|------|------|------|-------|-------|
| From A | 36 | 58 | 444 | 156 | 79 | 148 | 74 | 995 | 1652 |
| From B | 32 | 12 | 165 | 37 | 57 | 229 | 104 | 636 | 2274 |
| From C | 222 | 55 | 55 | 139 | 167 | 75 | 196 | 909 | 1638 |
| From D | 31 | 20 | 78 | 15 | 61 | 180 | 28 | 413 | 1729 |
| From E | 67 | 36 | 194 | 126 | 11 | 49 | 34 | 517 | 1681 |
| From F | 168 | 100 | 120 | 161 | 27 | 32 | 123 | 731 | 1447 |
| From G | 57 | 92 | 216 | 184 | 59 | 38 | 21 | 667 | 1598 |
| | | | | | | | | | |
| Total | 613 | 373 | 1272 | 818 | 461 | 751 | 580 | 4868 | |

PM Peak

| Arm | To A | То В | To C | To D | To E | to F | to G | | Total | q _c |
|--------|------|------|------|------|------|------|------|---|-------|----------------|
| From A | 30 | 58 | 191 | 110 | 103 | 286 | 68 | | 846 | 1436 |
| From B | 73 | 17 | 94 | 49 | 83 | 125 | 126 | | 567 | 1912 |
| From C | 245 | 106 | 36 | 155 | 134 | 42 | 253 | | 971 | 1756 |
| From D | 72 | 20 | 52 | 26 | 71 | 103 | 28 | | 372 | 1925 |
| From E | 107 | 22 | 170 | 150 | 15 | 40 | 35 | | 539 | 1787 |
| From F | 134 | 85 | 60 | 188 | 56 | 30 | 135 | | 688 | 1666 |
| From G | 66 | 62 | 120 | 124 | 48 | 34 | 15 | | 469 | 1694 |
| | | | | | | | | | | |
| Total | 727 | 370 | 723 | 802 | 510 | 660 | 660 | • | 4452 | |

Legend

| Arm | Road (in clockwise order) |
|-----|----------------------------|
| Α | Fairview Park Boulevard EB |
| В | Castle Peak Road NB |
| С | San Tin Road NB |
| D | San Tam Road NB |
| Е | San Tam Road SB |
| F | San Tin Road SB |
| G | Castle Peak Road SB |
| Н | |

Geometric Parameters

| | o i aiaiiiote | | | | | | |
|--------|---------------|-------|-------|-------|-------|-------|-----|
| Arm | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S |
| From A | 11.0 | 7.0 | 22.0 | 14.0 | 142 | 35 | 0.5 |
| From B | 9.0 | 5.5 | 20.0 | 10.0 | 142 | 35 | 0.6 |
| From C | 8.5 | 6.4 | 23.0 | 7.5 | 142 | 30 | 0.4 |
| From D | 8.5 | 6.5 | 20.0 | 10.0 | 142 | 25 | 0.3 |
| From E | 8.0 | 6.0 | 20.0 | 9.5 | 142 | 35 | 0.3 |
| From F | 8.5 | 6.0 | 25.0 | 6.5 | 142 | 40 | 0.6 |
| From G | 6.0 | 5.0 | 22.0 | 7.0 | 142 | 30 | 0.2 |
| From H | | | | | | | |

Predictive Equation $Q_E = K(F - f_cq_c)$

| Q_{E} | Entry Capacity |
|----------------|-------------------------------------|
| q _c | Circulating Flow across the Entry |
| К | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F | $= 303x_2$ |
| f _c | $= 0.210t_D(1+0.2x_2)$ |
| t _D | = 1+0.5/(1+M) |
| М | = exp[(D-60)/10] |
| x ₂ | = v+(e-v)/(1+2S) |
| s | = 1.6(e-v)/L |

Limitation

| е | Entry Width | 4.0 - 15.0 m |
|---|---------------------------|---------------|
| V | Approach Half Width | 2.0 - 7.3 m |
| r | Entry Radius | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m |
| Ø | Entry Angle | 10° - 60° |
| S | Sharpness of Flare | 0.0 - 3.0 |

Ratio-of-Flow to Capacity (RFC)

| | | | | | | | Q_{E} | | Entry Flow | | RFC | |
|--------|-----------------------|---------|---------|------|---------|-------|---------|------|------------|-----|------|------|
| Arm | X ₂ | M | t_{D} | K | F | f_c | AM | PM | AM | PM | AM | PM |
| From A | 9.09 | 3640.95 | 1.00 | 0.99 | 2754.13 | 0.59 | 1753 | 1880 | 995 | 846 | 0.57 | 0.45 |
| From B | 7.15 | 3640.95 | 1.00 | 0.98 | 2166.74 | 0.51 | 989 | 1170 | 636 | 567 | 0.64 | 0.48 |
| From C | 7.51 | 3640.95 | 1.00 | 1.01 | 2274.80 | 0.53 | 1423 | 1361 | 909 | 971 | 0.64 | 0.71 |
| From D | 7.72 | 3640.95 | 1.00 | 1.02 | 2339.01 | 0.53 | 1440 | 1333 | 413 | 372 | 0.29 | 0.28 |
| From E | 7.19 | 3640.95 | 1.00 | 0.98 | 2180.08 | 0.51 | 1296 | 1243 | 517 | 539 | 0.40 | 0.43 |
| From F | 7.12 | 3640.95 | 1.00 | 0.98 | 2157.57 | 0.51 | 1385 | 1277 | 731 | 688 | 0.53 | 0.54 |
| From G | 5.69 | 3640.95 | 1.00 | 1.00 | 1722.94 | 0.45 | 1010 | 967 | 667 | 469 | 0.66 | 0.49 |
| From H | | | | | | | | | | | | |

Roundabout Analysis

 Junction:
 The Fairview Park Roundabout
 Job Number: J7401

 Scenario:
 Future Condition (With Proposed RCHE)
 P. 9

 Design Year:
 2033
 Designed By:
 Checked By:
 Date:
 26 May 2025

AM Peak

| Arm | To A | То В | To C | To D | To E | to F | to G | Total | q_c |
|--------|------|------|------|------|------|------|------|-------|-------|
| From A | 36 | 58 | 444 | 156 | 79 | 148 | 74 | 995 | 1656 |
| From B | 32 | 12 | 167 | 37 | 57 | 230 | 104 | 639 | 2274 |
| From C | 222 | 57 | 55 | 139 | 167 | 75 | 196 | 911 | 1639 |
| From D | 31 | 20 | 78 | 15 | 61 | 180 | 28 | 413 | 1732 |
| From E | 67 | 36 | 194 | 126 | 11 | 49 | 34 | 517 | 1684 |
| From F | 168 | 102 | 120 | 161 | 27 | 32 | 123 | 733 | 1449 |
| From G | 57 | 92 | 216 | 184 | 59 | 38 | 21 | 667 | 1602 |
| | | | | | | | | | |
| Total | 613 | 377 | 1274 | 818 | 461 | 752 | 580 | 4875 | |

PM Peak

| Arm | To A | То В | To C | To D | To E | to F | to G | Total | q _c |
|--------|------|------|------|------|------|------|------|-------|----------------|
| From A | 30 | 58 | 191 | 110 | 103 | 286 | 68 | 846 | 1439 |
| From B | 73 | 17 | 97 | 49 | 83 | 128 | 126 | 573 | 1912 |
| From C | 245 | 108 | 36 | 155 | 134 | 42 | 253 | 973 | 1759 |
| From D | 72 | 20 | 52 | 26 | 71 | 103 | 28 | 372 | 1930 |
| From E | 107 | 22 | 170 | 150 | 15 | 40 | 35 | 539 | 1792 |
| From F | 134 | 86 | 60 | 188 | 56 | 30 | 135 | 689 | 1668 |
| From G | 66 | 62 | 120 | 124 | 48 | 34 | 15 | 469 | 1697 |
| | | | | | | | | | |
| Total | 727 | 373 | 726 | 802 | 510 | 663 | 660 | 4461 | |

Legend

| | Arm | Road (in clockwise order) |
|---|-----|----------------------------|
| | Α | Fairview Park Boulevard EB |
| | В | Castle Peak Road NB |
| | С | San Tin Road NB |
| | D | San Tam Road NB |
| | Е | San Tam Road SB |
| | F | San Tin Road SB |
| | G | Castle Peak Road SB |
| ı | Н | |

Geometric Parameters

| | o i aiaiiiote | | | | | | |
|--------|---------------|-------|-------|-------|-------|-------|-----|
| Arm | e (m) | v (m) | r (m) | L (m) | D (m) | Ø (°) | S |
| From A | 11.0 | 7.0 | 22.0 | 14.0 | 142 | 35 | 0.5 |
| From B | 9.0 | 5.5 | 20.0 | 10.0 | 142 | 35 | 0.6 |
| From C | 8.5 | 6.4 | 23.0 | 7.5 | 142 | 30 | 0.4 |
| From D | 8.5 | 6.5 | 20.0 | 10.0 | 142 | 25 | 0.3 |
| From E | 8.0 | 6.0 | 20.0 | 9.5 | 142 | 35 | 0.3 |
| From F | 8.5 | 6.0 | 25.0 | 6.5 | 142 | 40 | 0.6 |
| From G | 6.0 | 5.0 | 22.0 | 7.0 | 142 | 30 | 0.2 |
| From H | | | | | | | |

Predictive Equation $Q_E = K(F - f_cq_c)$

| Q_{E} | Entry Capacity |
|----------------|-------------------------------------|
| q _c | Circulating Flow across the Entry |
| K | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F | = 303x ₂ |
| f _c | $= 0.210t_D(1+0.2x_2)$ |
| t_D | = 1+0.5/(1+M) |
| М | $= \exp[(D-60)/10]$ |
| x_2 | = v+(e-v)/(1+2S) |
| s | = 1.6(e-v)/L |

Limitation

| е | Entry Width | 4.0 - 15.0 m |
|---|---------------------------|---------------|
| V | Approach Half Width | 2.0 - 7.3 m |
| r | Entry Radius | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m |
| Ø | Entry Angle | 10° - 60° |
| S | Sharpness of Flare | 0.0 - 3.0 |

Ratio-of-Flow to Capacity (RFC)

| | | | | | | | Q_{E} | | Entry Flow | | | |
|--------|-----------------------|---------|---------|------|---------|-------|---------|------|------------|-----|------|------|
| Arm | X ₂ | M | t_{D} | K | F | f_c | AM | PM | AM | PM | AM | PM |
| From A | 9.09 | 3640.95 | 1.00 | 0.99 | 2754.13 | 0.59 | 1751 | 1878 | 995 | 846 | 0.57 | 0.45 |
| From B | 7.15 | 3640.95 | 1.00 | 0.98 | 2166.74 | 0.51 | 989 | 1170 | 639 | 573 | 0.65 | 0.49 |
| From C | 7.51 | 3640.95 | 1.00 | 1.01 | 2274.80 | 0.53 | 1423 | 1359 | 911 | 973 | 0.64 | 0.72 |
| From D | 7.72 | 3640.95 | 1.00 | 1.02 | 2339.01 | 0.53 | 1438 | 1331 | 413 | 372 | 0.29 | 0.28 |
| From E | 7.19 | 3640.95 | 1.00 | 0.98 | 2180.08 | 0.51 | 1295 | 1240 | 517 | 539 | 0.40 | 0.43 |
| From F | 7.12 | 3640.95 | 1.00 | 0.98 | 2157.57 | 0.51 | 1384 | 1276 | 733 | 689 | 0.53 | 0.54 |
| From G | 5.69 | 3640.95 | 1.00 | 1.00 | 1722.94 | 0.45 | 1008 | 965 | 667 | 469 | 0.66 | 0.49 |
| From H | | | | | | | | | | | | |

