# **Appendix 4**

# **Traffic Impact Assessment**

Traffic Impact Assessment Final Report

15<sup>th</sup> August, 2025

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c/o KTA Planning Limited

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#### 1.0 INTRODUCTION

## **Background**

- 1.1 The Subject Site is located near Wo Hop Shek Village to the south of Wo Hing Road / Tai Wo Service Road West in Fanling, and its location is shown in **Figure 1.1**.
- 1.2 The Applicant, i.e. Sime Darby Motor Services Limited ("SDMS"), is a well-established motor vehicle dealer and distributor in Hong Kong, and has over 50 years of history in retail, distribution, assembly, servicing, and car rental businesses.
- 1.3 SDMS intends to develop the Subject Site, which is currently occupied by warehouses, into a Research and Development ("R&D") centre focusing on electric vehicle ("EV") technology, namely the "EV Mobility City" (hereinafter "Proposed EV Mobility City").
- 1.4 According to the Approved Fanling / Sheung Shui Outline Zoning Plan No. S/FSS/28 ("Approved OZP"), the Subject Site is zoned "Government, Institution or Community." To facilitate future development of the Subject Site, s12A Rezoning Application is being submitted.
- 1.5 Against this background, CKM Asia Limited, a traffic and transportation planning consultancy firm, was commissioned to conduct a Traffic Impact Assessment ("TIA") for the Proposed EV Mobility City in support of the s12A Rezoning Application.

### Structure of Report

- 1.6 After this introduction, the remaining chapters contain the following:
  - Chapter 2 Describes the existing situation;
  - Chapter 3 Provides details on the Proposed EV Mobility City:
  - Chapter 4 Describes the traffic impact analysis; and
  - Chapter 5 Gives the overall conclusion.

## 2.0 EXISTING SITUATION

## The Subject Site

2.1 The Subject Site is located to the south of Wo Hing Road / Tai Wo Service Road West near Wo Hop Shek Village in Fanling. It has a site area of approximately 5,480m², and is now being occupied by warehouses. The existing vehicular access to the Subject Site is from Wo Hing Road.

### The Road Network

- 2.2 Wo Hing Road is a Local Distributor which runs between the roundabout of Wah Ming Road / Lui Ming Road / Ming Yin Road / Wo Hing Road in the west, and continues as Tai Wo Service Road West in the east. It is a single carriageway 2 lane road.
- 2.3 Tai Wo Service Road West is a Rural Road which runs between Wo Hing Road to the north, and continues south towards Hong Lok Yuen Road. It is a single carriageway 2 lane road.
- 2.4 Wah Ming Road is a District Distributor which runs between the northern and southern junctions with Pak Ro Road. It is a single carriageway road with 3 to 4 traffic lanes between Pak Wo Road and the roundabout of Wah Ming Road / Lui Ming Road / Ming Yin Road / Wo Hing Road.
- 2.5 Pak Wo Road is a District Distributor which runs from Sheung Shui in the north, and Fanling in the south. It is generally a dual carriageway 2 lane road. It connects Fanling Highway at the Wo Hop Shek Interchange near the Subject Site providing regional access.

#### **Pedestrian and Cycling Facilities**

- 2.6 Footpaths are provided along the southern side of Tai Wo Service Road West fronting the Subject Site, and along both sides of other nearby roads, such as Wo Hing Road, Pak Wo Road and Wah Ming Road.
- 2.7 At-grade pedestrian crossings are provided along Wo Hing Road. Signalised pedestrian crossings, and grade separated crossings are provided across Pak Wo Road, Wah Ming Road and Fanling Highway.
- 2.8 Cycle track is provided along Wo Hing Road fronting the Subject Site connecting with Pak Wo Road and the network within Fanling, Sheung Shui, and to Tai Po.

#### **Existing Traffic Flows**

2.9 To quantify the existing traffic flows, manual classified counts were conducted during the AM and PM peak periods, i.e. from 0800 to 1000 hours and 1700 to 1900 hours, at selected junctions and road links found within the Area of Influence ("AOI") on Monday, 26<sup>th</sup> May 2025, and Tuesday, 27<sup>th</sup> May 2025. Table 2.1 presents the surveyed junctions and road links.

| TABLE 2.1         | SURVEYED | LUNCTINONS | AND ROAD LINKS |
|-------------------|----------|------------|----------------|
| 1/\DLL <b></b> .1 | JUNVLILD |            |                |

| Ref. | Survey Locations   |  |  |  |  |  |
|------|--|--|--|--|--|--|
|      | Junctions  |  |  |  |  |  |
| J01  | Junction of Tai Wo Service West / Kiu Tau Road                             |  |  |  |  |  |
| J02  | Junction of Wo Hing Road / Unnamed Road                                    |  |  |  |  |  |
| 103  | Roundabout of Wah Ming Road / Lui Ming Road / Ming Yin Road / Wo Hing Road |  |  |  |  |  |
| J04  | Southern Junction of Pak Wo Road / Yat Ming Road / Wah Ming Road           |  |  |  |  |  |
| J05  |  |  |  |  |  |  |
| J06  | Wo Hop Shek Interchange  |  |  |  |  |  |
| J07  | Wo Hing Road / Existing Site Access  |  |  |  |  |  |
|      |  |  |  |  |  |  |
|      | Road Links   |  |  |  |  |  |
| L01  | L01 Tai Wo Service Road West (Wo Hing Road – Kiu Tau Road)                 |  |  |  |  |  |
| L02  | LO2 Wo Hing Road (Pak Wo Road – Tai Wo Service Road West)                  |  |  |  |  |  |
| L03  | Pak Wo Road (Wo Hop Shek Interchange – Wah Ming Road)                      |  |  |  |  |  |
| L04  | Unnamed Road (Pak Wo Road – Wo Hing Road                                   |  |  |  |  |  |

- 2.10 **Figure 2.1** shows the Area of Influence ("AOI") and the locations of the surveyed junctions and road links. **Figures 2.2 2.7** shows the existing junction layouts.
- 2.11 The traffic counts were classified by vehicle type to enable traffic flows in passenger car units ("pcu") to be calculated. The AM peak hour is found to be 0730 to 0830 hours, and the PM peak hour is found to be 1730 to 1830 hours respectively. Figure 2.8 presents the existing AM and PM peak hour traffic flow established in pcu/hour.

## Performance of the Surveyed Junctions

2.12 Performance of the surveyed junctions were calculated based on the existing traffic flows, and the analyses were undertaken using the methods outlined in Volume 2 of Transport Planning and Design Manual ("TPDM"), which is published by the Transport Department. Table 2.2 summarises the analysis results, and the detailed calculations are found in **Appendix A**.

TABLE 2.2 EXISTING JUNCTION PERFORMANCE

| Ref. | Junctions  | Type of<br>Junction | Parameter | AM Peak<br>Hour | PM Peak<br>Hour |
|------|--|---------------------|-----------|-----------------|-----------------|
| J01  | Tai Wo Service West / Kiu Tau Road                                 | Priority            | RFC       | 0.033           | 0.038           |
| J02  | Wo Hing Road / Unnamed Road  | Priority            | RFC       | 0.373           | 0.268           |
| J03  | Wah Ming Road / Lui Ming Road / Ming<br>Yin Road / Wo Hing Road    | Roundabout          | RFC       | 0.306           | 0.253           |
| J04  | Pak Wo Road / Yat Ming Road / Wah<br>Ming Road (Southern Junction) | Signal              | RC        | 53%             | 77%             |
| J05  | Pak Wo Road / Yat Ming Road / Wah Ming Road (Northern Junction)    | Signal              | RC        | 63%             | 119%            |
| J06  | Wo Hop Shek Interchange  | Signal              | RC        | 32%             | 50%             |
| J07  | Wo Hing Road / Site Access   | Priority            | RFC       | 0.000           | 0.000           |

Note: RFC - Ratio of Flow to Capacity RC - Reserve Capacity

2.13 The above results indicate the surveyed junctions operate with capacities.

## Performance of the Surveyed Road Links

2.14 Performance of the surveyed road links, in terms of Peak Hourly Flows / Design Flow Ratio ("P/Df") is calculated, and the analysis results are summarized in Table 2.3.

TABLE 2.3 EXISTING P/Df OF SURVEYED ROAD LINKS

| Ref. | Ref. Road Link                       |          | Direction  | Design           | P/Df            |                 |
|------|--------------------------------------|----------|------------|------------------|-----------------|-----------------|
|      |                                      |          |            | Flow<br>(pcu/hr) | AM Peak<br>Hour | PM Peak<br>Hour |
| L01  | Tai Wo Service Road West (Wo Hing    | Single-2 | Northbound | 1,160            | 0.146           | 0.145           |
|      | Road – Kiu Tau Road)                 |          | Southbound | 1,160            | 0.138           | 0.136           |
| L02  | Wo Hing Road (Pak Wo Road – Tai Wo   | Single-2 | Northbound | 1,000            | 0.249           | 0.178           |
|      | Service Road West)                   |          | Southbound | 1,400            | 0.396           | 0.255           |
| L03  | Pak Wo Road (Wo Hop Shek Interchange | Dual-2   | Northbound | 3,050            | 0.372           | 0.305           |
|      | – Wah Ming Road)                     |          | Southbound | 3,050            | 0.275           | 0.242           |
| L04  | Unnamed Road (Pak Wo Road – Wo       | Single-2 | Eastbound  | 1,000            | 0.209           | 0.151           |
|      | Hing Road                            |          | Westbound  | 1,000            | 0.564           | 0.336           |

## **Existing Public Transport Services**

2.15 The Subject Site is located close to public transport services, including franchised bus and green mini-bus ("GMB") routes operate along Tai Wo Service Road West, Wo Hing Road, Pak Wo Road and Lui Ming Road. Table 2.4 presents the details.

TABLE 2.4 ROAD-BASED PUBLIC TRANSPORT SERVICES OPERATING IN VICINITY OF THE SUBJECT SITE

| Route    | Origin - Destination                                   |            |  |  |
|----------|--|------------|--|--|
| KMB 61S  | Tuen Mun City Centre ↔ Wo Hop Shek (Kiu Tau Road)      | (c)        |  |  |
| KMB 70K  | Fanling (Wah Ming) & Ching Ho                          |            |  |  |
| KMB 70S  | Hung Hom Station ↔ Wo Hop Shek                         |            |  |  |
| KMB 73   | Fanling (Wah Ming) ↔ Tai Po Industrial Estate          |            |  |  |
|          | Fanling (Wah Ming) ↔ Tai Po Central                    | (a)        |  |  |
| KMB 73A  | Fanling (Wah Ming) ↔ Yu Chui Court                     |            |  |  |
| KMB 73B  | Chuen On Road (Nethersole Hospital) U Sheung Shui      |            |  |  |
| KMB 73S  | Fanling Station ↔ Wo Hop Shek (Kiu Tau Road)           | (c)        |  |  |
| KMB 74S  | Ping Tin ↔ Wo Hop Shek                                 | (c)        |  |  |
| KMB 76S  | Fanling Station ↔ Wo Hop Shek                          | (c)        |  |  |
| KMB 78   | Sha Tau Kok → Sheung Shui (Tai Ping)                   | (a)        |  |  |
| KMB 78B  | Queen's Hill → Sheung Shui (Choi Yuen)                 | (a)        |  |  |
|          | Sheung Shui (Choi Yuen) → Queen's Hill                 | (a)        |  |  |
| KMB 78S  | Shueng Shui → Sha Tau Kok                              | (a)        |  |  |
|          | Sha Tau Kok → Shueng Shui                              | (a)        |  |  |
| KMB 261X | Fanling (Cheung Wah) ↔ So Kwun Wat                     | (a)        |  |  |
| KMB 264R | Tin Yiu ↔ Tai Po Market Station                        | (a)        |  |  |
| KMB 270A | Sheung Shui ↔ Tsim Sha Tsui East (Mody Road)           |            |  |  |
| KMB 270B | Sheung Shui ↔ Olympic Station                          |            |  |  |
|          | Sheung Shui → Charming Garden                          | (a)        |  |  |
|          | Charming Garden → Sheung Shui                          | (a)        |  |  |
| KMB 270C | Fanling (Luen Wo Hui) → Tsim Sha Tsu East (Mody Road)  | (a)        |  |  |
|          | Tsim Sha Tsu East (Mody Road) → Fanling (Luen Wo Hui)  | (a)        |  |  |
| KMB 270D | Fanling (Luen Wo Hui) → Sham Shui Po                   | (a)        |  |  |
|          | Sham Shui Po (Yen Chow Street) → Fanling (Luen Wo Hui) | (a)        |  |  |
| KMB 270P |  |            |  |  |
| KMB 270R | Hong Kong Coliseum → Fanling (Luen Wo Hui)             | (a)<br>(c) |  |  |
| KMB 270S | Tsim Sha Tsui East (Mody Road) → Fanling (Luen Wo Hui) | (a)        |  |  |

TABLE 2.4 ROAD-BASED PUBLIC TRANSPORT SERVICES OPERATING IN VICINITY OF THE SUBJECT SITE (CONT'D)

| ъ .  | 0 D  |       |  |  |
|--|--|-------|--|--|
| Route  | Origin - Destination   |       |  |  |
| KMB 273  | Fanling (Wah Ming) U Fanling Station                                 |       |  |  |
| KMB 273A   | Sheung Shui (Choi Yuen) & Fanling (Wah Ming)                         |       |  |  |
| KMB 273D   | Sheung Shui & Fanling (Wah Ming)                                     | ( )   |  |  |
| KMB 273S   | Fanling (Fai Ming Road) → Fanling Station                            | (a)   |  |  |
|  | Fanling Station → Fanling (Wah Ming)                                 | (a)   |  |  |
| KMB 274  |  |       |  |  |
| KMB 276C   | Tin Shui Wai Station ↔ Fanling (Cheung Wah)                          | (a)   |  |  |
| KMB 277A   | Sha Tau Kok ↔ Lam Tin Station  | (a)   |  |  |
| KMB 277E   | Sheung Shui (Tin Ping) ↔ Lam Tin Station                             |       |  |  |
| KMB 277P   | Sheung Shui (Tin Ping) → Lam Tin Station                             | (a)   |  |  |
|  | Lam Tin Station → Sheung Shui (Tin Ping)                             | (a)   |  |  |
| KMB 278A   | Queen's Hill ↔ Tsuen Wan (Nina Tower)                                |       |  |  |
| KMB 278P   | Sheung Shui (Tin Ping) → Tsuen Wan (Nina Tower                       | (a)   |  |  |
| KMB 278X   | Sheung Shui ↔ Tsuen Wan (Nina Tower)                                 |       |  |  |
| KMB 279S   | Tsing Yi (Cheung Ching Estate) ↔ Wo Hop Shek                         | (c)   |  |  |
| KMB 279X   | Fanling (Luen Wo Hui) ↔ Tsing Yi Station                             |       |  |  |
| KMB 373  | Fanling (Luen Wo Hui) → Central (Hong Kong Station)                  | (a)   |  |  |
|  | Central (Hong Kong Station) → Fanling (Luen Wo Hui)                  | (a)   |  |  |
| KMB 673A   | Sheung Shui → Central (Rumsey Street)                                | (a)   |  |  |
|  | Central (Rumsey Street) →Sheung Shui                                 | (a)   |  |  |
| KMB 673P   | Sheung Shui → Central (Rumsey Street)                                | (a)   |  |  |
| KMB/CTB 678  | Sheung Shui → Causeway Bay (Eastern Hospital Road)                   | (a)   |  |  |
|  | Causeway Bay (Eastern Hospital Road) → Sheung Shui                   | (a)   |  |  |
| KMB 978  | Fanling (Wah Ming) ↔ Exibition Centre Station                        |       |  |  |
| KMB W3   | Sheung Shui ↔ Jordan (West Kowloon Station)                          |       |  |  |
| KMB T270 Fanling (Cheung Wah) → Tsim Sha Tsui East (Mody Road) |  | (a)   |  |  |
|  | Tsim Sha Tsui East (Mody Road) → Fanling (Cheung Wah)                | (a)   |  |  |
| KMB T277   | Sheung Shui → Lam Tin Station  | (a)   |  |  |
|  | Lam Tin Station → Sheung Shui  | (a)   |  |  |
| KMB SP7  | Kai Tak Sports Park → Sheung Shui                                    | (c)   |  |  |
| KMB N73  | Shatin Central ↔ Lok Ma Chau   | (b)   |  |  |
| KMB N273   | Sheung Shui (Choi Yuen) O Fanling (Wah Ming)                         | (b)   |  |  |
| KMB N373   | Fanling (Luen Wo Hui) ↔ Central (Macau Ferry)                        | (b)   |  |  |
| LWB A43  | Fanling (Luen Wo Hui) ↔ Airport (Ground Transportation Centre)       | (2)   |  |  |
| LWB E43  | Fanling (Wah Ming) → Tung Chung Development Pier                     | (a)   |  |  |
| 2175 2 15  | Tung Chung Development Pier → Fanling (Wah Ming)                     | (a)   |  |  |
| LWB X43  | Asiaworld Expo → Fanling (Luen Wo Hui)                               | (c)   |  |  |
| LWB N42A   | Fanling (Luen Wo Hui) ↔ Tung Chung Station                           | (b)   |  |  |
| LWB NA43   | Fanling (Luen Wo Hui) ↔ HZMB Hong Kong Port                          | (b)   |  |  |
| CTB B7   | Sheung Shui Po Wan Road ↔ Heung Yuen Wai Port                        | (6)   |  |  |
| GMB 55K  | Sha Tau Kok → Sheung Shui Station                                    | (a)   |  |  |
| GMB 501A   | Yung Shing Court & Luen Wo Hui                                       | (a)   |  |  |
| GMB 501C Yung Shing Court & Luen Wo Hui                        |  | (a)   |  |  |
| GMB 501S   |  |       |  |  |
|  |  |       |  |  |
| GMB 502<br>GMB 505   | GMB 502 Ching Ho Estate ↔ Alice Ho Miu Ling Nethersole Hospital      |       |  |  |
|  | Sheung Shui Station → Yu Chui Court  Chi Fuk Circuit / 5 Ma Sik Boad |       |  |  |
| GMB 506  | Chi Fuk Circuit & Ma Sik Road  | /I_ \ |  |  |
| GMB 616S   | Mong Kok ↔ Lok Ma Chau Control Point                                 | (b)   |  |  |
| RMB<br>Note: KMR – Ko  | Mong Kok ↔ Sheung Shui   | (b)   |  |  |

Note: KMB – Kowloon Motor Bus GMB – Green Minibus CTB – Citybus RMB – Red Minibus LWB - Long Win Bus

(a) Regular special services during peak period.

(b) Overnight services.

(c) Special services on specific days only.

### Historic Traffic Growth

2.16 Annual averages daily traffic ("AADT") between 2016 and 2023 of roads located near the Subject Site was obtained from the Annual Traffic Census ("ATC") published by Transport Department, and are summarized in Table 2.5.

TABLE 2.5 HISTORIC TRAFFIC INFORMATION FROM THE ATC

|         | I        |             |                  |                   |                 | İ                |
|---------|----------|-------------|------------------|-------------------|-----------------|------------------|
| Station | 5302     | 5501        | 5702             | 6084              | 6206            | Overall          |
| Road    | Wo Hing  | Pak Wo      | Tai Wo Service   | Fanling           | Jockey Club     |                  |
|         | Road     | Road        | Road West        | Highway           | Road            |                  |
| From    | Unnamed  | Yat Ming    | Kau Lung Hang    | Wo Hop Shek       | Lok Yip Street  |                  |
|         | Road     | Road        | Flyover near Kiu | Intercahnge       |                 |                  |
|         |          |             | Tau Road         |                   |                 |                  |
| To      | Ming Yin | Wo Hop      | Wo Hing Road     | Kau Lung          | Wo Hop Shek     |                  |
|         | Road     | Shek        |                  | Hang Lo Wai       | Interchange     |                  |
|         |          | Interchange |                  |                   |                 |                  |
| Year    |          | Α           | verage Annual Da | ily Traffic ("AAD | T")             |                  |
| 2016    | 5,680    | 16,270      | 3,930            | 109,350           | 41,900          | 177,130          |
| 2017    | 5,590    | 16,010      | 3,870            | 101,920           | 38,380          | 165 <i>,77</i> 0 |
| 2018    | 5,760    | 16,410      | 3,960            | 106,100           | 41,730          | 173,960          |
| 2019    | 6,580    | 17,280      | 3,940            | 110,310           | 37,440          | 175,550          |
| 2020    | 6,310    | 19,060      | 3,400            | 105,020           | 36,370          | 170,160          |
| 2021    | 6,560    | 19,820      | 3,630            | 110,130           | 37,380          | 177,520          |
| 2022    | 6,360    | 19,210      | 3,520            | 100,940           | 36,240          | 166,270          |
| 2023    | 6,580    | 19,670      | 3,600            | 114,310           | 34,840          | 179,000          |
|         |          |             | Average          | Annual Growth     | (2016 - 2023) = | +0.2%            |

Note: \* - Estimated by Growth Factor

2.17 Table 2.5 shows that the traffic growth in vicinity is +0.2% per annum. It should be noted that the AADT for years 2020, 2021 and 2022 are disregarded due to the impact of the COVID-19 pandemic, but shown for reference only.

## 3.0 THE PROPOSED EV MOBILITY CITY

## **Proposed EV Mobility City**

- The Proposed EV Mobility City include EV R&D centre, showrooms, sales offices, after-sales servicing, training and testing units, ancillary offices, training centre, and other EV Related Business. In addition, ancillary staff quarter and residential institution, referred to as "talent housing" for qualified working staff and employees will also be provided.
- 3.2 Table 3.1 summarises development parameters of the Proposed EV Mobility City.

TABLE 3.1 PARAMETERS OF THE PROPOSED EV MOBILITY CITY

| Use  | Development Parameters                        |
|--|---|
| Staff Quarter (7/F – 12/F)                               | Gross Floor Area = 1,920m <sup>2</sup>        |
|  | Number of Units = 48 nos.                     |
|  | Average Unit Size = About 40m <sup>2</sup>    |
| Residential Institution (7/F – 18/F)                     | Gross Floor Area = 6,300m <sup>2</sup>        |
|  | Number of Units = 90 nos.                     |
|  | Average Unit Size = About 70m <sup>2</sup>    |
|  | Domestic Plot Ratio = 1.15                    |
| Conference / Seminars / Training Course / Administration | Gross Floor Area = 2,340m <sup>2</sup>        |
| & Accounting Office ("C/S/TC/AAO") (6/F)                 |   |
| EV Related Business (G/F – 5/F)                          | Gross Floor Area = About 14,040m <sup>2</sup> |

## **Proposed Internal Transport Facilities**

- 3.3 The internal transport facilities provided for the proposed uses comply with the recommendation of the Hong Kong Planning Standards and Guidelines ("HKPSG"). As for bicycle parking spaces, reference is made to the Transport Department's Guideline.
- 3.4 Staff Quarter is subsidized accommodation by the Applicant to support the development of the Proposed EV Mobility City. Hence, internal transport facilities are provided in accordance to the HKPSG recommendation for "Subsidised Housing", and the details are summarized in Table 3.2.
- 3.5 Residential Institution is accommodation for employees and personnel affiliated with the Applicant, and the average flat size is 70m² per unit. Hence, the HKPSG recommendation for "*Private Housing* 70m²" is adopted. Details are summarized in Table 3.3.
- 3.6 Conference / Seminars / Training Course / Administration & Accounting Office is assumed to be "office" space. Hence, the HKPSG recommendation for "Office" is adopted, and the details are summarized in Table 3.4.
- 3.7 EV Related Business is similar to "Vehicle Repair Workshops" defined in the HKPSG, and parking spaces are provided accordingly. For loading / unloading bays, the provision is as per HKPSG recommendation for "General Industrial Use". Table 3.5 summarises the details.

TABLE 3.2 PROVISION OF INTERNAL TRANSPORT FACILITIES FOR STAFF QUARTER

| Internal<br>Transport Facilities  | HKPSG / TD Recommendations   | Proposed Provision               |
|---|--|----------------------------------|
| Car Parking Space<br>(Residential)  | HKPSG Recommendation: Global Parking Standard ("GPS") = 1 space per 4 - 7 flats Demand Adjustment Ratio ("R1") = 0.52 Accessibility Adjustment Ratio ("R2") = 1.0 for Outside a 500m-radius of rail station Parking Requirement = GPS x R1 x R2 [see Note 1]  For 48 flats with 3 persons/flat: Minimum: 48 ÷ 7 x 0.52 x 1.0 = 3.6, say 4 nos.  Maximum: 48 ÷ 4 x 0.52 x 1.0 = 6.2, say 7 nos. | 7 nos.<br>= HKPSG<br>Maximum, OK |
| Car Parking Space<br>(Visitor)  | HKPSG Recommendation: Up to 5 spaces per block  For 1 block: Maximum: 1 x 5 = 5 nos.   | 5 nos.<br>= HKPSG<br>Maximum, OK |
| Motorcycle Parking<br>Space   | HKPSG Recommendation: 1 space per 110 – 250 flats [see Note 1]  For 48 flats with 3 persons/flat: Minimum: 48 ÷ 250 = 0.2, say 1 no. Maximum: 48 ÷ 110 = 0.4, say 1 no.  | 1 no.<br>= HKPSG<br>Maximum, OK  |
| "Shared-use" Light<br>Goods Vehicle and<br>Light Bus Parking<br>Space                                   | HKPSG Recommendation: 1 space per 260 flats [ see Note 1]  For 48 flats with 3 persons/flat: 48 ÷ 260 = 0.2, say 1 no.   | 1 no.<br>= HKPSG, OK             |
| "Shared-use" Medium /<br>Heavy Goods Vehicle<br>and Coach Parking<br>Space / Loading /<br>Unloading Bay | HKPSG Recommendation:  2 spaces around each residential blocks  For 1 block:  1 x 2 = 2 nos.   | 2 nos.<br>= HKPSG, OK            |
| Bicycle Parking Space   | Transport Department Guideline:  1 space per 5 flat for residents, and 1 space per 45 flat for visitors  For 48 flats: For Residents: $48 \div 5 = 9.6$ , say 10 nos. For Visitors: $48 \div 45 = 1.1$ , say 2 nos. TOTAL: $10 + 2 = 12$ nos.  | 12 nos.<br>= TD Guideline,<br>OK |

Note 1: "One person / two persons" flats, if any, can be excluded from the calculation of the overall parking provision of private car, motorcycle parking spaces and shared-use spaces for LGV and light bus.

TABLE 3.3 PROVISION OF INTERNAL TRANSPORT FACILITIES FOR RESIDENTIAL INSTITUTION

| Internal                                 | HKPSG / TD Recommendations   | Proposed Provision                |
|--|--|-----------------------------------|
| Transport Facilities                     |  | •                                 |
| Car Parking Space<br>(Residential)       | HKPSG Recommendation: Global Parking Standard ("GPS") = 1 space per $4-7$ flats Demand Adjustment Ratio ("R1") = 1.2 for $40 <$ Flat Size $\leq 70$ m² GFA Accessibility Adjustment Ratio ("R2") = 1.0 for Outside a 500m-radius of rail station Development Intensity Adjustment Ratio ("R3") = 1.1 for $1.00 <$ Plot Ratio $\leq 2.00$ Parking Requirement = GPS x R1 x R2 x R3 $\frac{\text{For } 90 \text{ flats } @ 70\text{m}^2 \text{ GFA and Plot Ratio } = 1.15:}{\text{Maximum:}}$ 90 ÷ 7 x 1.2 x 1.0 x 1.1 = 17.0, say 17 nos Maximum: 90 ÷ 4 x 1.2 x 1.0 x 1.1 = 29.7, say 30 nos. | 30 nos.<br>= HKPSG<br>Maximum, OK |
| Car Parking Space<br>(Visitor)           | HKPSG Recommendation: 5 spaces per block with more than 75 units per block  For 1 block 1 x 5 = 5 nos.   | 5 nos.<br>= HKPSG<br>Maximum, OK  |
| Motorcycle Parking<br>Space              | HKPSG Recommendation: 1 space per 100 – 150 flats  For 90 flats Minimum: 90 ÷ 150 = 0.6, say 1 no.  Maximum: 90 ÷ 100 = 0.9, say 1 no.   | 1 no.<br>= HKPSG<br>Maximum, OK   |
| Goods Vehicle Loading<br>/ Unloading Bay | HKPSG Recommendation: Minimum 1 loading / unloading bay for goods vehicles for every 800 flats or part thereof.  For 1 block: 1 x 1 = 1 no.  | 1 no.<br>= HKPSG, OK              |
| Bicycle Parking Space                    | Transport Department Guideline:  1 space per 5 flat for residents, and 1 space per 45 flat for visitors  For 90 flats: For Residents: $90 \div 5 = 18 \text{ nos.}$ For Visitors: $90 \div 45 = 2 \text{ nos.}$ TOTAL: $18 + 2 = 20 \text{ nos.}$  | 20 nos.<br>= TD Guideline,<br>OK  |

TABLE 3.4 PROVISION OF INTERNAL TRANSPORT FACILITIES FOR CONFERENCE / SEMINARS / TRAINING COURSE / ADMINISTRATION & ACCOUNTING OFFICE

| Internal Transport Facilities Car Parking Space | HKPSG / TD Recommendations  HKPSG Recommendation:  For the first 15,000 m <sup>2</sup> GFA: 1 space per 150 – 200 m <sup>2</sup> For 2,340 m <sup>2</sup> GFA:  Minimum: $2,340 \div 200 = 11.7$ , say 12 nos.  Maximum: $2,340 \div 150 = 15.6$ , say 16 nos.  | Proposed Provision  16 nos. = HKPSG Maximum, OK                 |
|---|---|---|
| Motorcycle Parking<br>Space                     | HKPSG Recommendation:  5% - 10% of car parking spaces  For 31 car parking spaces:  Minimum: 16 x 5% = 0.8, say 1 nos.  Maximum: 16 x 10% = 1.6, say 2 nos.  | 2 nos.<br>= HKPSG<br>Maximum, OK                                |
| Goods Vehicle Loading<br>/ Unloading Bay        | HKPSG Recommendation: 1 loading / unloading bay for goods vehicles for every 2,000 – 3,000 m² GFA  For 2,340 m² GFA: Minimum: 2,340 ÷ 3,000 = 0.8, say 1 nos. 35% HGV = 1 x 35% = 0.35, say 1 no. 65% LGV = 1 – 1 = 0 no.  Maximum: 2,340 ÷ 2,000 = 1.2, say 2 nos. 35% HGV = 2 x 35% = 0.7, say 1 no. 65% LGV = 2 – 1 = 1 nos. | 2 nos., including<br>1 HGV &<br>1 LGV<br>= HKPSG<br>Maximum, OK |
| Bicycle Parking Space                           | Transport Department Guideline:<br>1 space per $500 - 600\text{m}^2$ GFA  For 2,340 m <sup>2</sup> GFA:<br>Minimum: $2,340 \div 600 = 3.9$ , say 4 nos.<br>Maximum: $2,340 \div 500 = 4.7$ , say 5 nos.   | 5 nos.<br>= TD Guideline<br>Maximum, OK                         |

TABLE 3.5 PROVISION OF INTERNAL TRANSPORT FACILITIES FOR EV RELATED BUSINESS

| Internal<br>Transport Facilities                  | HKPSG / TD Recommendations   | Proposed Provision  |
|---|--|---|
| Parking Space                                     | HKPSG Recommendation: Minimum of 2 spaces for each workshop unit, or 0.75 space per workspace, or 150m² of GFA whichever is higher. ("Vehicle Repair Workshops," Ch12, HKPSG)  Proposed EV Mobility City with 14,040m² GFA Number of workshop unit and workspace are yet to be determined; hence, provision is calculated based on GFA.  For G/F with around 1,200m² GFA serving large commercial vehicles (HGV and Coach): 1,200 ÷ 150 = 8.0, say 8 nos. @ 12.0m (L) x 3.5m (W) x Min. 4.7m (H) (Shared-Use by HGV & Coach)  For remaining GFA = 14,040 - 1,200 = 12,840m² for light commercial vehicles, and light vehicles: 12,840 ÷ 150 = 85.6, say 86 nos. @ 8.0m (L) x 3.5m (W) x Min. 3.8m (H) (Shared-Use by LGV, Light Bus, Taxi and Private Car) | 8 nos. for HGV /<br>Coach, and<br>86 nos. for LGV /<br>Light Bus / Taxi /<br>Private Car<br>= HKPSG, OK |
| Goods Vehicle<br>Loading / Unloading<br>& Parking | HKPSG Recommendation:  1 goods vehicle bay per 700 - 900 m² GFA, 50% of which should be for parking of goods vehicles, and is divided into 65% LGV and 35% HGV (General Industrial Use (GIU)—Industrial (I), Ch8, HKPSG)  Proposed EV Mobility City with 14,040m² GFA Minimum:  14,040 ÷ 900 = 15.6, say 16 nos. 35% HGV = 16 x 35% = 5.6, say 6 nos. 65% LGV = 16 - 6 = 10 nos.  Maximum:  14,040 ÷ 700 = 20.1, say 21 nos. 35% HGV = 21 x 35% = 7.4, say 8 nos. 65% LGV = 21 - 8 = 13 nos.   | 21 nos., with<br>8 HGV, and<br>13 LGV<br>= HKPSG<br>maximum, OK   |
| Bicycle Parking<br>Space                          | Transport Department Guideline:<br>1 space per $2,500 - 2,700\text{m}^2$ GFA<br>For 14,040 $\frac{\text{m}^2}{\text{GFA}}$ :<br>Minimum: 14,040 ÷ 2,700 = 5.2, say 6 nos.<br>Maximum: 14,040 ÷ 2,500 = 5.6 say 6 nos.  | 6 nos.<br>= TD Guideline<br>Maximum, OK   |

#### Overall Provision of Internal Transport Facilities

3.8 Table 3.6 summarises the overall provision of internal transport facilities, which meets the high-end recommendation of the HKPSG and the Transport Department's Guideline.

TABLE 3.6 OVERALL PROVISION OF INTERNAL TRANSPORT FACILITIES

| Internal Transport Facilities        | TOTAL       |         | Num         | ber of Spaces |              |
|--------------------------------------|-------------|---------|-------------|---------------|--------------|
|                                      |             | Staff   | Residential | C/S/TC/AAO    | EV Related   |
|                                      | (Al-4-4)    | Quarter | Institution |               | Business Use |
| Car Parking Space (Residential) @    | 53 (Note 1) | 7       | 30          | 16            | /            |
| 5.0m (L) x 2.5m (W) x Min. 2.4m (H)  |             |         |             |               |              |
| Car Parking Space (Visitors) @ 5.0m  | 10 (Note 1) | 5       | 5           | /             | /            |
| (L) x 2.5m (W) x Min. 2.4m (H)       |             |         |             |               |              |
| Motorcycle Parking Space @ 2.4m (L)  | 4           | 1       | 1           | 2             | /            |
| x 1.0m (W) x Min. 2.4m (H)           |             |         |             |               |              |
| "Shared-use" LGV / Light Bus Parking | 87          | 1       | /           | /             | 86           |
| Space @ 8.0m (L) x3.5m (W) x Min.    |             |         |             |               |              |
| 3.6m (H)                             |             |         |             |               |              |
| "Shared-use" M/HGV & Coach           | 8           | /       | /           | /             | 8            |
| Parking Space @ 12.0m (L) x3.5m (W)  |             |         |             |               |              |
| x Min. 4.7m (H)                      |             |         |             |               |              |
| "Shared-use" M/HGV & Coach           | 2           | 2       | /           | /             | /            |
| Parking Space / L/UL Bay @ 12.0m (L) |             |         |             |               |              |
| x3.5m (W) x Min. 4.7m (H)            |             |         |             |               |              |
| LGV L/UL Bay-@ 7.0m (L) x3.5m (W)    | 14          | /       | /           | 1             | 13           |
| x Min. 3.6m (H)                      |             |         |             |               |              |
| HGV L/UL Bay-@ 11.0m (L) x 3.5m      | 10          | /       | 1           | 1             | 8            |
| (W) x Min. 4.7m (H)                  |             |         |             |               |              |
| Bicycle Parking Space                | 33          | 12      | 10          | 5             | 6            |

Note 1: Out the total of 63 car parking spaces, 2 nos. are accessible type @ 5.0m (L) x 3.5m (W) x Min. 2.4m (H) C/S/TC/AAO - Conference / Seminars / Training Course / Administration & Accounting Office

#### Vehicular Access

3.9 The existing vehicular access on Wo Hing Road serving the Subject Site will remain unchanged. **Figure 3.1** shows location of the vehicular access, and visibility assessment meeting the requirement as stipulated in the TPDM.

### **Internal Transport Layout**

3.10 The indicative internal transport layout is presented in Figures 3.2 - 3.8.

#### **Traffic Generation**

3.11 Traffic generation for various uses within the Proposed EV Mobility City is estimated based on (i) trip rates obtained from the TPDM, and (ii) trip rate derived from traffic survey at similar existing developments. Details are described in below paragraphs.

# Staff Quarter, Residential Institution and Conference / Seminars / Training Course / Administration & Accounting Office

3.12 Table 3.7 presents the trips rate for staff quarter, residential institution and conference / seminars / training course / administration & accounting office from the TPDM.

TABLE 3.7 ADOPTED TPDM TRIP RATES

| Proposed                | TPDM                         | Unit                     | Adopted Trip Rates     |            |            |            |
|-------------------------|------------------------------|--------------------------|------------------------|------------|------------|------------|
| Use                     | Category                     |                          | AM Peak Hour PM Peak H |            | k Hour     |            |
|                         |                              |                          | Generation             | Attraction | Generation | Attraction |
| Staff Quarter           | Subsidised<br>Housing (40m²) | pcu/hr/flat              | 0.0432                 | 0.0326     | 0.0237     | 0.0301     |
| Residential Institution | Private Housing (70m²)       | pcu/hr/flat              | 0.0888                 | 0.0515     | 0.0356     | 0.048      |
| C/S/TC/AAO              | Office                       | pcu/hr/100m <sup>2</sup> | 0.2361                 | 0.3257     | 0.1928     | 0.151      |

Note: C/S/TC/AAO - Conference / Seminars / Training Course / Administration & Accounting Office

3.13 For staff quarter and residential institution, the mean trip rates of TPDM are adopted in view that the residents are employees and does not involve external commuting. Hence, the use of mean trip rates is considered conservative. For conference / seminars / training course / administration & accounting office, to be conservative, the upper limit trip rates of TPDM are adopted.

#### EV Related Business

3.14 Since the TPDM does not provide trip rates for uses similar to the EV Related Business, or "Vehicle Repair Workshops", traffic generation surveys were conducted at selected existing standalone service centres ("SSC") operated by the Applicant, and the results are used to derive the appropriate trip rates. These existing service centres consist of showrooms, office, vehicle service centre etc. which are similar to the proposed EV Related Business. Table 3.8 summarizes the details of these surveyed standalone service centres.

TABLE 3.8 DETAILS OF THE SURVEYED STANDALONE SERVICE CENTRES

| Address  | Vehicle Type Served   | Approximate<br>Gross Floor Area | Operation Hours<br>(Monday – Friday) |
|--|---|---------------------------------|--------------------------------------|
| 374 Castle Peak Road – Tsuen<br>Wan, Tsuen Wan ("TWSSC") | Light Vehicles (Private Cars)                                 | 13,663m <sup>2</sup>            | 0800 – 1900                          |
| 33 & 96 Kam Pok Road, Yuen<br>Long ("YLSSC")             | Commercial Vehicles<br>(LGV, HGV, Light<br>Buses and Coaches) | 6,032m <sup>2</sup>             | 0845 - 1915                          |

- 3.15 In view that the TWSSC is located in Tsuen Wan town centre where there is good public transport service, its convenient location is a key attraction to car owners bringing their vehicles in for service, and it TWSSC has similar size to the EV Related Business.
- 3.16 The YLSSC is located in an area similar to the Subject Site, and is alike the EV Related Business.
- 3.17 Hence, the 2 surveyed locations are considered suitable reference to derive the trip rates for the EV Related Business. Table 3.9 summarizes the survey results, and the derived trip rates.

TABLE 3.9 RESULTS OF TRAFFIC GENERATION SURVEYS AND DERIVED TRIP RATES

| Survey  | Approximate          | Observed Number of Trips (pcu/hr) |            |            | 'nr)       |  |
|---|----------------------|-----------------------------------|------------|------------|------------|--|
| Location  | GFA                  | AM Peak Hour PM Pe                |            | PM Pea     | Peak Hour  |  |
|   |                      | Generation                        | Attraction | Generation | Attraction |  |
| TWSSC   | 13,663m <sup>2</sup> | 4                                 | 23         | 26         | 20         |  |
| YLSSC   | 6,032m <sup>2</sup>  | 4                                 | 10         | 13         | 10         |  |
| TOTAL   | 19,695m²             | 8                                 | 33         | 39         | 30         |  |
| Derived Trip Rates (pcu/hr/100 m <sup>2</sup> ) |                      | 0.0406                            | 0.1676     | 0.1980     | 0.1523     |  |

#### Overall Traffic Generation

3.18 Based on the development parameters presented in Table 3.1, and the trip rates presented in Tables 3.7 and 3.9, the estimated traffic generation for the Proposed EV Mobility City is summarised in Table 3.10.

TABLE 3.10 ESTIMATED TRAFFIC GENERATION OF THE PROPOSED EV MOBILITY CITY

| Use                     | Parameters           | Estimated Traffic Generation (pcu/hr)  AM Peak Hour PM Peak Hour |            |            | •          |
|-------------------------|----------------------|--|------------|------------|------------|
|                         |                      | Generation   | Attraction | Generation | Attraction |
| Staff Quarter           | 48 units             | 2  | 2          | 1          | 1          |
| Residential Institution | 90 units             | 8  | 5          | 3          | 4          |
| C/S/TC/AAO              | 2,340m <sup>2</sup>  | 6  | 8          | 5          | 4          |
| EV Business Related     | 14,040m <sup>2</sup> | 6  | 24         | 28         | 21         |
|                         | TOTAL                | 22   | 39         | 37         | 30         |
|                         |                      | 61 (2  | -way)      | 67 (2      | -way)      |

Note: C/S/TC/AAO - Conference / Seminars / Training Course / Administration & Accounting Office

### 4.0 TRAFFIC IMPACT

#### **Design Year**

4.1 The Proposed EV Mobility City is expected to be completed in 2031. Hence, the design year adopted is 2034, i.e. 3 years after completion.

#### **Traffic Forecasting**

- 4.2 Year 2034 traffic flows used for the capacity analysis are derived based on the following:
  - (i) the 2025 existing traffic flow,
  - (ii) with reference to the 2031 traffic flows from the NTE1 Base District Traffic Model ("BDTM") which is produced by Transport Department,
  - (iii) the estimated traffic growths from 2031 to 2034,
  - (iv) the expected traffic generation associated with other known planned / committed major developments,
  - (v) the planned traffic improvement works to be carried by other projects, and
  - (vi) the expected traffic generation associated to the Proposed EV Mobility City
- 4.3 Traffic growth from 2031 to 2034 are derived with reference to the "Hong Kong Population Projections" published by the Census and Statistics Department ("C&SD") available in the public domain and is presented in Table 4.1.

TABLE 4.1 POPULATION PROJECTIONS BY C&SD

| Year                                | HK Resident Population (in Thousands) |
|-------------------------------------|---------------------------------------|
| 2031                                | 7,820.2                               |
| 2034                                | 7,945.1                               |
| Average Annual Growth (2031 – 2034) | 0.5%                                  |

4.4 Table 4.1 shows an annual growth rate of 0.5% and this is adopted to develop the 2034 traffic model which is used to produce the 2034 traffic flows.

### Other Known Planned / Committed Major Developments in the Vicinity

4.5 Traffic generated by other known planned / committed major developments which are obtained from the available public domain including "Monthly Digest" published by Buildings Department, and the Town Planning Board's Statutory Planning Portal 3 by Planning Department, etc. included in the design year traffic flows. These developments are presented in Table 4.2.

TABLE 4.2 LIST OF OTHER KNOWN PLANNED / COMMITTED MAJOR DEVELOPMENTS

| Ref. | Developments                            | Development Parameters (Approx.)               |
|------|---|--|
| A.   | Fanling North New Development Area      | Public Housing: 15,939 flats                   |
|      | (including Proposed Minor Relaxation of | Private Housing: 8,990 flats                   |
|      | Plot Ratio and Building Height approved | G/IC: 32,837 m <sup>2</sup> GFA                |
|      | under TPB No. A/KTN/54, A/FLN/28, &     | Other non-domestic use (e.g. retail,           |
|      | A/FLN/30) (1)                           | kindergarten etc.): 129,657 m <sup>2</sup> GFA |
|      |   | Primary and Secondary Schools: 8 nos.          |
| B.   | Proposed Public Housing Development at  | Public Housing: 4,000 flats                    |
|      | Queen's Hill Extension (2)              | G/IC   |
| C.   | New Territories East Cultural Centre in | 67,000 m <sup>2</sup> CFA with 2,500 seats     |
|      | Area 11, Sha Tau Kok Road – Lung Yeuk   | Public Vehicle Park                            |
|      | Tau, Fanling (3)                        |  |

TABLE 4.2 LIST OF OTHER KNOWN PLANNED / COMMITTED MAJOR DEVELOPMENTS (CONT'D)

| Ref. | Developments  | Development Parameters (Approx.)   |
|------|---|--|
| D.   | Public Housing Development at San Wan<br>Road <sup>(4)</sup>  | Public Housing: 450 flats<br>G/IC, Kindergarten, Primary School and<br>Secondary School  |
| E.   | Mixed Housing Development Project at Pak Wo Road (TPB No. A/FSS/254) (5)(8)   | Public Housing: 510 flats Subsidized Sale Flat: 696 flats Elderly Housing: 261 flats RCHE: 210 beds Retail: 6,500 m² GFA Public Vehicle Park |
| F.   | Public Housing Development at Fanling Area 17 (7)   | Public Housing: 8,300 flats G/IC, Social Welfare Facilities, Kindergarten, Community Hall, Retail, Market                                    |
| G.   | Subsidized Sale Flats at Jockey Club Road (5)(7)  | Subsidized Sale Flat: 644 flats Retail: 3,000 m <sup>2</sup> CFA Public Vehicle Park   |
| H.   | Public Housing Development at Sheung<br>Shui Areas 4 and 30 Site 1 & 2 (including<br>Proposed Minor Relaxation of Plot Ratio<br>and Building Height approved under TPB<br>No. A/FSS/280) (7)(8) | Public Housing: 3,644 flats Retail: 1,100 m² CFA G/IC Public Vehicle Park  |
| I.   | Public Housing Development at Po Shek<br>Wu Road <sup>(7)</sup>   | Public Housing: 1,800 flats Retail: 3,000 m <sup>2</sup> CFA Kindergarten  |
| J.   | Proposed Flat Development and Social Welfare Facility (Residential Care Home for the Elderly) at Ma Sik Road, Fanling (TPB No. A/FSS/294) (8)   | Private Housing: 1,898 Flats<br>RCHE: 120 beds <sup>(9)</sup><br>Public Vehicle Park   |
| K.   | Proposed Social Welfare Facility (Residential Care Home for the Elderly) and Flat at Tin Ping Road, Sheung Shui (TPB No. A/FSS/279) (8)   | RCHE: 143 beds<br>Private Housing: 28 flats  |
| L.   | Proposed Minor Relaxation of Domestic<br>PR Restriction for Permitted Residential<br>Development with Commercial Uses at 1<br>Luen Fat Street, Fanling (TPB No.<br>A/FSS/282) (8)               | Private Housing: 119 flats Commercial: 161 m <sup>2</sup> GFA  |
| M.   | Proposed Shop and Services (Showroom) and Office (Wholesale Conversion of an Existing Industrial Building) at 5 Lok Yip Road, Fanling (TPB No. A/FSS/283) (8)                                   | Retail: 4,075 m <sup>2</sup> GFA   |
| N.   | Proposed Shop and Services, Eating Place<br>and Other Uses at 33 On Lok Mun Street,<br>Fanling (TPB No. A/FSS/284) (8)  | Retail: 2,392 m <sup>2</sup> GFA   |
| O.   | Public Housing Development at Ching<br>Hiu Road <sup>(9)</sup>  | Private Housing: 620 flats G/IC, & Social Welfare Facilities   |
| Р.   | Public Housing Development at Fanling Area 48 (TPB No. A/FSS/295) (8)(10)   | Public Housing: 4,620 flats Primary School Social Welfare Facilities, and Retail   |
| Q.   | Wo Hop Shek Cemetery Phases 2, 3 and 4 Columbarium, and Wo Hop Shek Crematorium Expansion (11)  | Columbarium: 280,000 niches<br>Cremators: 10 nos.  |

#### Source:

- (1) Rural and New Town Planning Committee ("RNTPC") Paper No. A/FLN/30
- (2) North Committees Meetings Discussion Paper 9/2022. "Proposed Public Housing Development at Queen's Hill Extension". Dated 15 May 2022. North District Council.
- (3) LC Paper No. CB(2)614/2022(01). Legislative Council.
- (4) Planning Brief. Hong Kong Housing Authority.
  - <a href="https://www.pland.gov.hk/pland\_en/access/pec/planning\_brief/San%20Wan%20Road%20PB.pdf">https://www.pland.gov.hk/pland\_en/access/pec/planning\_brief/San%20Wan%20Road%20PB.pdf</a>
- (5) HKHS Annual Report 2022. Hong Kong Housing Society.

- (6) Paper 2/2023. "粉嶺第 17 區公營房屋發展計劃". Dated 16 January 2023. North District Council.
- (7) North Committees Meetings Discussion Paper 5/2019. "Public Housing Development Programmes at Sites 1 and 2 in Sheung Shui Areas 4 and 30, a Site to the North of Po Shek Wu Road and a Site on Jockey Club Road, Fanling, and Proposed Amendments to the Approved Fanling/Sheung Shui Outline Zoning Plan No. S/FSS/22." Dated 21 January 2019. North District Council.
- (8) Statutory Planning Portal 2. Town Planning Board.
- (9) Paper 4/2023. "上水清曉路公營房屋發展之工地平整及基礎設施工程." Dated 16 January 2023. North District Council.
- (10) LC Paper No. CB(1)158/2022(03). Legislative Council.
- (11) Paper 24/2024. "和合石墳場興建火葬場、骨灰安置所第二期和第三期計劃及相關道路改善和排污設 施工程 (工務計劃項目第 5874TH 號)." Dated 9 July 2024. North District Council

### **Future Road Network**

4.6 Traffic improvement works have been planned for implementation within the AOI by the Government, and those identified are summarized in **Table 4.3**.

TABLE 4.3 PLANNED TRAFFIC IMPROVEMENT WORKS WITHIN THE AOI

| Planned Traffic Improvements                                      | Status             |
|---|--------------------|
| Fanling Bypass Eastern Section (1)                                | Under Construction |
| Realignment and upgrading of Tai Wo Service Road West (1)(2)      | Under Construction |
| Improvement at Southern Junction of Pak Wo Road / Yat Ming Road / | Under Planning     |
| Wah Ming Road (J04) (3)   |                    |

- (1) Project Number 7835CL. "Remaining Phase of Site Formation and Engineering Infrastructure Works at Kwu Tung North and Fanling North New Development Area - Detailed Design and Site Investigation" Civil Engineering and Development Department. <a href="https://www.cedd.gov.hk/eng/our-projects/major-projects/index-id-87.html">https://www.cedd.gov.hk/eng/our-projects/major-projects/index-id-87.html</a>
- (2) A/FSS/295. "Proposed Minor Relaxation of Maximum Gross Floor Area and Building Heigth for Proposed Public Housing Development at Fanling Area 48." Town Planning Board.
- (3) PWP Item No. 5874H. "Road Improvement Works at Wo Hop Shek Cemetery for Phases 2 and 3 Columbarium Development." Civil Engineering and Development Department.
- 4.7 The above listed traffic improvements are expected to be implemented prior to completion of the Proposed EV Mobility City, and are adopted in the 2034 traffic model. Information of the above traffic improvement works are found in Appendix B.

#### 2034 Traffic Flows

4.8 Year 2034 traffic flows with the Proposed EV Mobility City are derived as follows:

2034 Traffic Flows with the = 2034 Traffic Flows without the Proposed EV Proposed EV Mobility City + Traffic Generated by the Proposed EV Mobility City

4.9 **Figures 4.1 and 4.2** show the 2034 AM and PM peak hour traffic flows for the scenarios without and with the Proposed EV Mobility City respectively.

#### 2034 Junction Capacity Analysis

4.10 Year 2034 junction capacity analysis for the scenarios without and with the Proposed EV Mobility City are summarised in Table 4.4 and detailed calculations are found in the **Appendix A**.

TABLE 4.4 2034 JUNCTION PERFORMANCE

| Ref. | Junction  | Type<br>of<br>Junction | Parameter | Without the<br>Proposed EV<br>Mobility City |                    | With the<br>Proposed EV<br>Mobility City |                    |
|------|---|------------------------|-----------|---|--------------------|--|--------------------|
|      |   |                        |           | AM<br>Peak<br>Hour                          | PM<br>Peak<br>Hour | AM<br>Peak<br>Hour                       | PM<br>Peak<br>Hour |
| J01  | Tai Wo Service West / Kiu Tau<br>Road                                 | Priority               | RFC       | 0.035                                       | 0.184              | 0.035                                    | 0.184              |
| J02  | Wo Hing Road / Unnamed Road   | Priority               | RFC       | 0.557                                       | 0.413              | 0.587                                    | 0.438              |
| J03  | Wah Ming Road / Lui Ming Road /<br>Ming Yin Road / Wo Hing Road       | Round-<br>about        | RFC       | 0.415                                       | 0.348              | 0.428                                    | 0.356              |
| J04  | Pak Wo Road / Yat Ming Road /<br>Wah Ming Road (Southern Junction)    | Signal<br>(Note 1)     | RC        | 25%   | 31%                | 22%                                      | 28%                |
| J05  | Pak Wo Road / Yat Ming Road /<br>Wah Ming Road (Northern<br>Junction) | Signal                 | RC        | 24%   | 67%                | 23%                                      | 65%                |
| J06  | Wo Hop Shek Interchange   | Signal                 | RC        | 9%  | 24%                | 6%                                       | 21%                |
| J07  | Wo Hing Road / Site Access  | Priority               | RFC       | 0.000                                       | 0.000              | 0.050                                    | 0.055              |

Note 1: With planned traffic improvement works to be implemented by Others.

RFC - Ratio of Flow to Capacity RC - Reserve Capacity

- 4.11 Table 4.4 shows that, except for J06 during the AM peak hour, the junctions analyzed have capacity to accommodate the expected traffic growth to 2034, and the traffic generated by the Proposed EV Mobility City.
- 4.12 For J06, it is expected to operate unsatisfactory during the AM peak hour for both scenarios without and with the Proposed EV Mobility City.

## Proposed Traffic Improvement at J06

4.13 To improve the operational condition of J06, local traffic improvement is proposed, and is shown in **Figure 4.3**. Table 4.5 shows results of the junction capacity analyses for J06 with the proposed traffic improvement implemented for the scenario with the Proposed EV Mobility City.

TABLE 4.5 2034 JUNCTION PERFORMANCE FOR J06 WITH LOCAL TRAFFIC IMPROVEMENT

|   | Ref. | Junction                | Type of<br>Junction | Parameter | With the Proposed EV Mobility City AM Peak Hour   PM Peak Ho |                   |
|---|------|-------------------------|---------------------|-----------|--|-------------------|
| 1 |      |                         |                     |           | AWI I Cak I Ioui   | I WI I Cak I Ioui |
|   | J06  | Wo Hop Shek Interchange | Signal              | RC        | 16%  | 21%               |

#### 2034 Road Link Capacity Analysis

4.14 Year 2034 road link capacity analysis for the scenarios without and with the Proposed EV Mobility City are summarised in Table 4.6.

TABLE 4.6 YEAR 2034 P/Df OF ROAD LINKS

| Ref.                                  | Road Link   | Config.    | Direction  | Design           | P/Df  |                 |  |                 |
|---------------------------------------|---|------------|------------|------------------|---|-----------------|--|-----------------|
|                                       |   |            |            | Flow<br>(pcu/hr) | Without the<br>Proposed EV<br>Mobility City |                 | With the<br>Proposed EV<br>Mobility City |                 |
|                                       |   |            |            |                  | AM Peak<br>Hour                             | PM Peak<br>Hour | AM Peak<br>Hour                          | PM Peak<br>Hour |
| L01                                   |   | Single-2   | Northbound | 1,160            | 0.332                                       | 0.265           | 0.351                                    | 0.297           |
| West (Wo Hing Road –<br>Kiu Tau Road) |   | Southbound | 1,160      | 0.287            | 0.276                                       | 0.320           | 0.302                                    |                 |
| L02                                   | L02 Wo Hing Road (Pak Wo<br>Road – Tai Wo Service<br>Road West) | Single-2   | Northbound | 1,000            | 0.334                                       | 0.234           | 0.341                                    | 0.245           |
|                                       |   |            | Southbound | 1,400            | 0.514                                       | 0.358           | 0.531                                    | 0.371           |
| L03                                   | Pak Wo Road (Wo Hop<br>Shek Interchange – Wah<br>Ming Road)     | Dual-2     | Northbound | 3,050            | 0.431                                       | 0.353           | 0.435                                    | 0.356           |
|                                       |   |            | Southbound | 3,050            | 0.296                                       | 0.267           | 0.296                                    | 0.267           |
| L04                                   | Unnamed Road (Pak   | Single-2   | Eastbound  | 1,000            | 0.295                                       | 0.227           | 0.309                                    | 0.239           |
|                                       | Wo Road – Wo Hing<br>Road                                       |            | Westbound  | 1,000            | 0.774                                       | 0.474           | 0.789                                    | 0.500           |

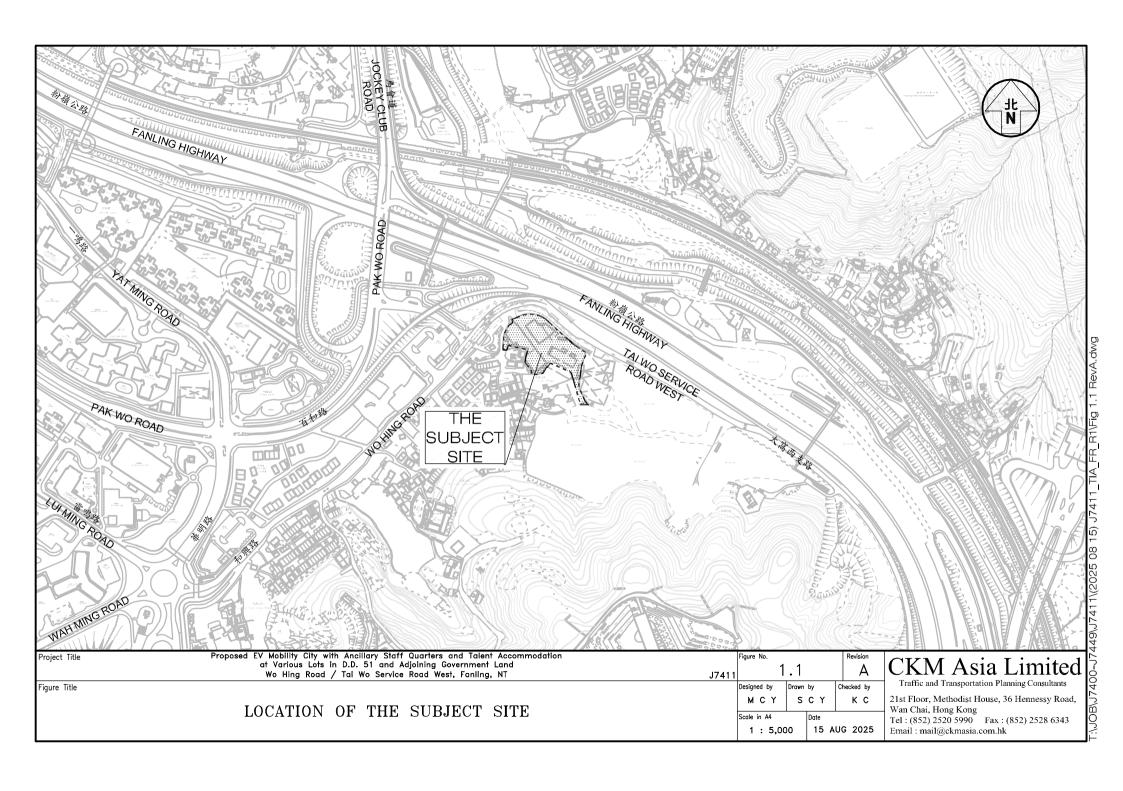
Config. – Configuration

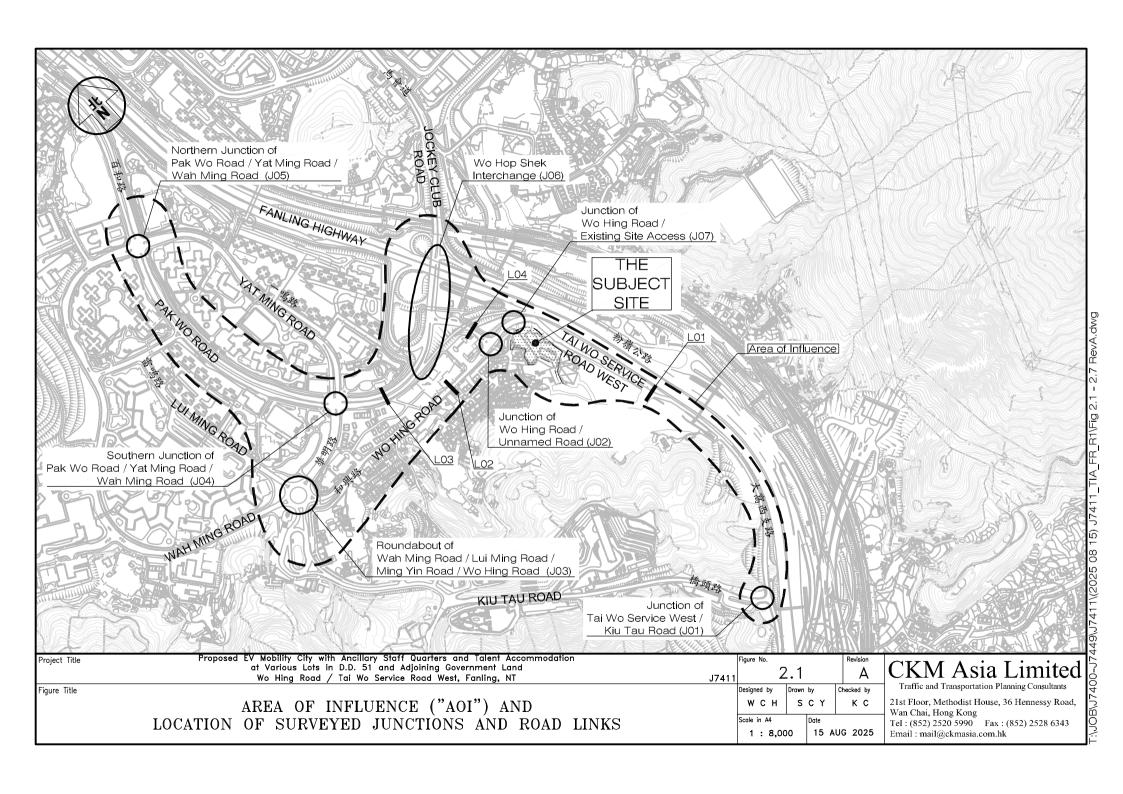
4.15 Table 4.6 shows that the road links analyzed have capacity to accommodate the expected traffic growth to 2034, and the traffic generated by the Proposed EV Mobility City.

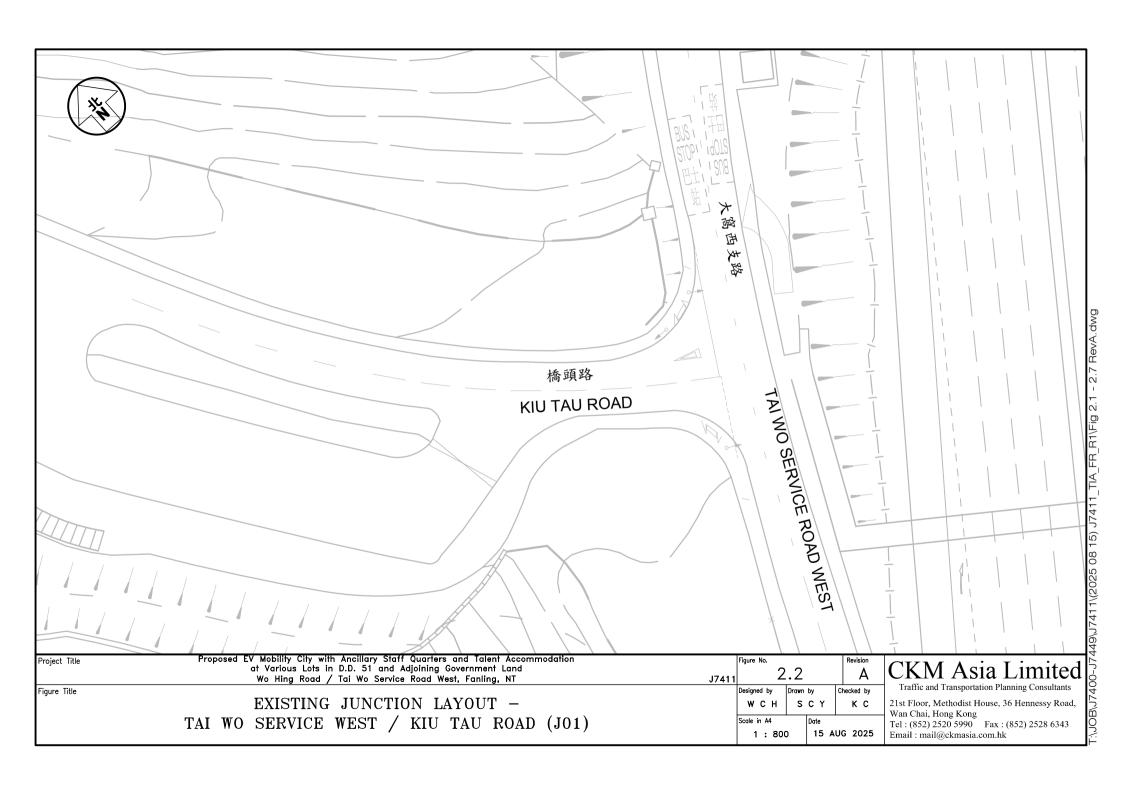
#### 5.0 SUMMARY

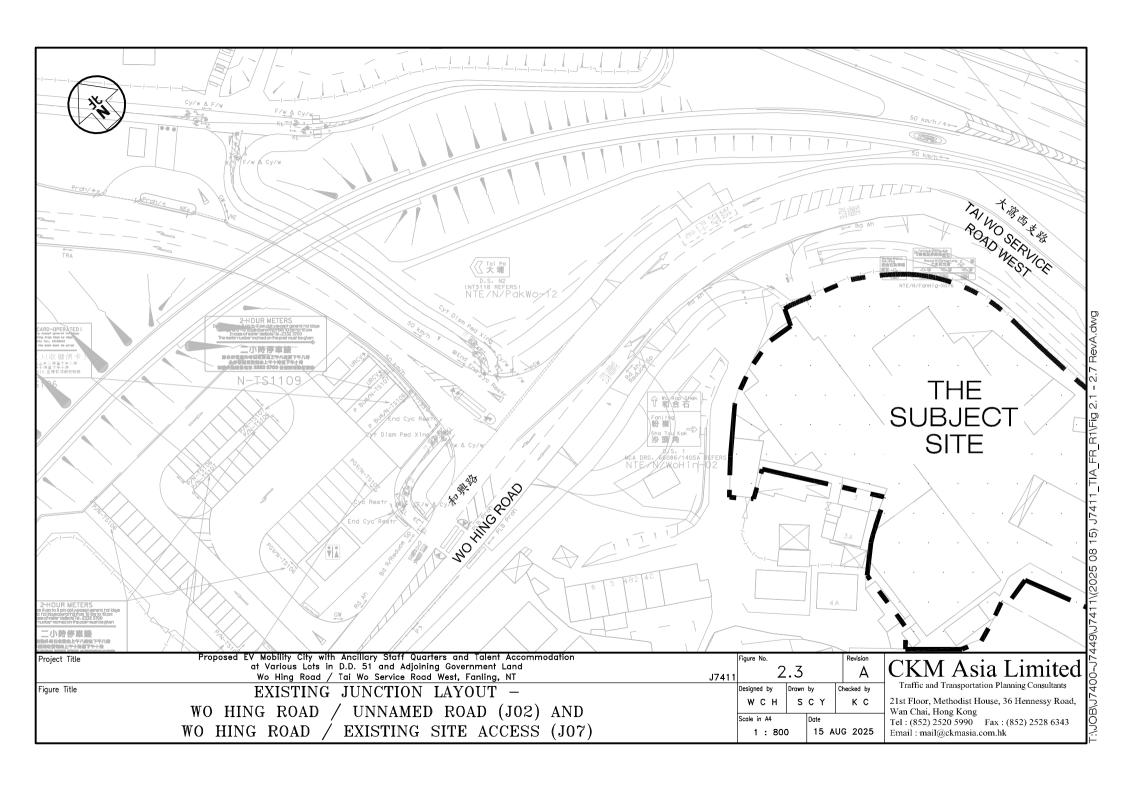
- 5.1 The Subject Site is located at Various Lots in D.D. 51 and Adjoining Government Lot in Fanling near Wo Hop Shek Village. It is currently occupied by warehouses.
- 5.2 The Applicant is a well-established vehicle dealer and distributor in Hong Kong, who intends to develop the Subject Site into a research and development centre focusing on electric vehicle technology, i.e. Proposed EV Mobility City, which also includes staff quarter, residential institution, ancillary office and training centre.
- 5.3 The proposed internal transport provision follows the high-end recommendation of the HKPSG, and TD's Guideline include the following:
  - i) 53 residential car parking spaces,
  - ii) 10 visitor car parking spaces,
  - iii) 4 motorcycle parking spaces,
  - iv) 87 "shared-use" LGV / light bus parking spaces,
  - v) 8 "shared-use" M/HGV / coach parking spaces,
  - vi) 2 "shared-use" M/HGV / coach parking spaces / loading / unloading bays,
  - vii) 14 LGV loading / unloading bays,
  - viii) 10 HGV loading / unloading bays, and
  - ix) 33 bicycle parking spaces.
- 5.4 Manual classified counts were conducted in May 2025 at selected junctions and road links located in the AOI to establish the existing traffic flows during the AM and PM peak hours. The design year 2034 traffic flows were derived with reference to the BDTM, and have also taken into account the traffic generation and planned traffic improvement works associated with other known planned / committed major developments located in the vicinity.
- 5.5 Traffic generation for the Proposed EV Mobility City is calculated based on the trip rates adopted from the TPDM, and derived trip rates from traffic generation surveys at referenced developments. The Proposed EV Mobility City is expected to generate some 61 and 67 pcu (2-way) during the AM and PM peak hours respectively.
- 5.6 The traffic analysis found the surveyed junctions and road links currently operate with capacity, and will have sufficient capacity to accommodate the expected traffic growth to 2034 and the traffic generated by the Proposed EV Mobility City, except Wo Hop Shek Interchange (J06).
- 5.7 The Wo Hop Shek Interchange (J06) is expected to operate unsatisfactorily in 2034 during the AM peak hour in both scenarios without and with the Proposed EV Mobility City. Traffic improvement is proposed which will enhance the operational condition to a satisfactory level.
- 5.8 In view of the above, it is concluded that the Proposed EV Mobility City is acceptable from traffic engineering viewpoint.

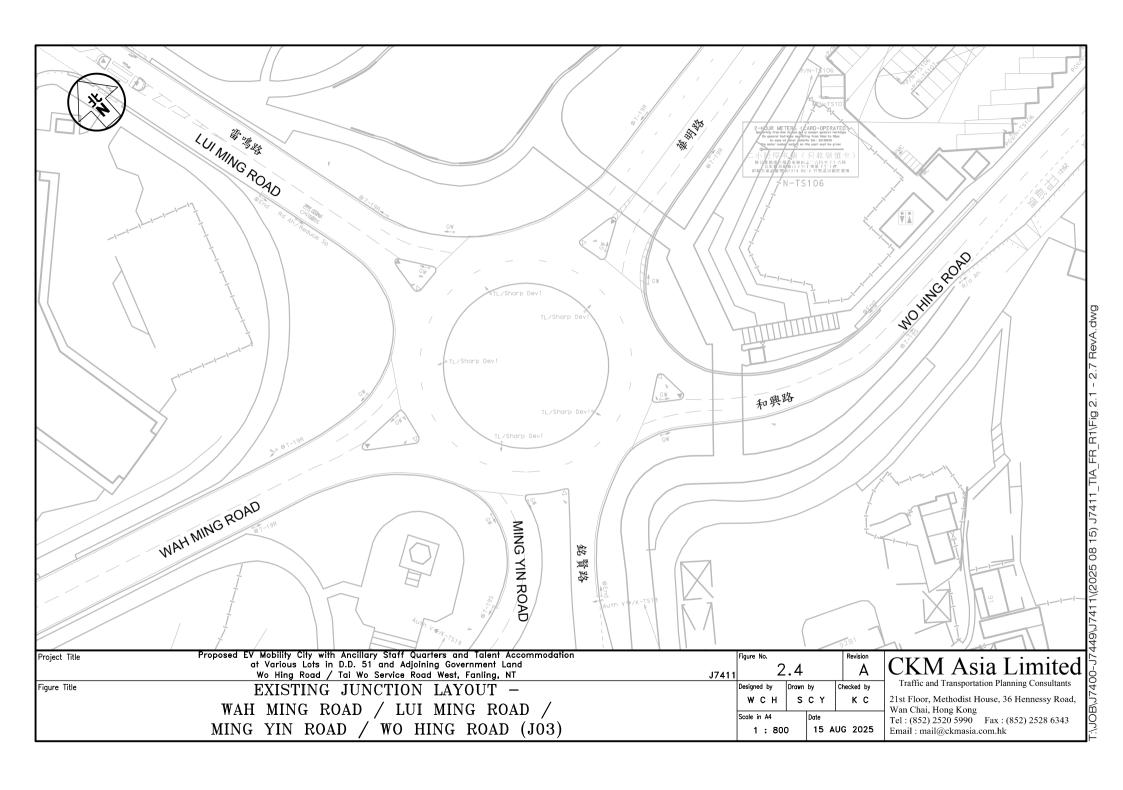


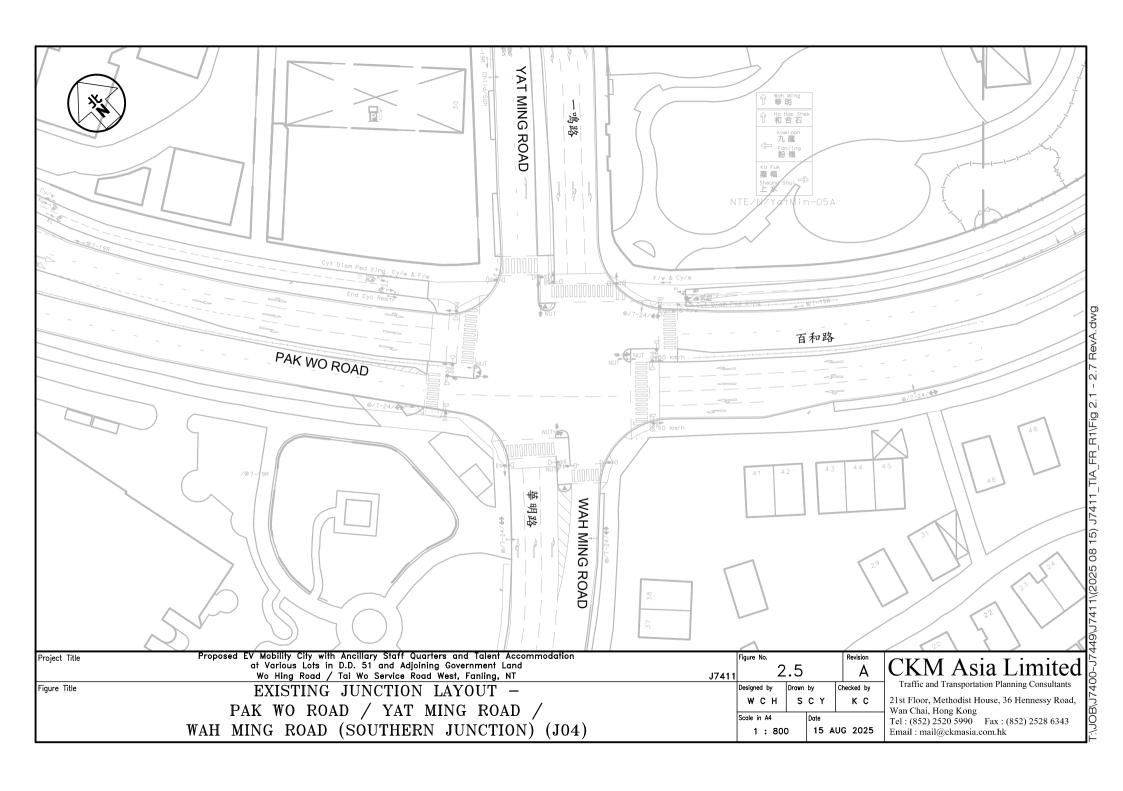


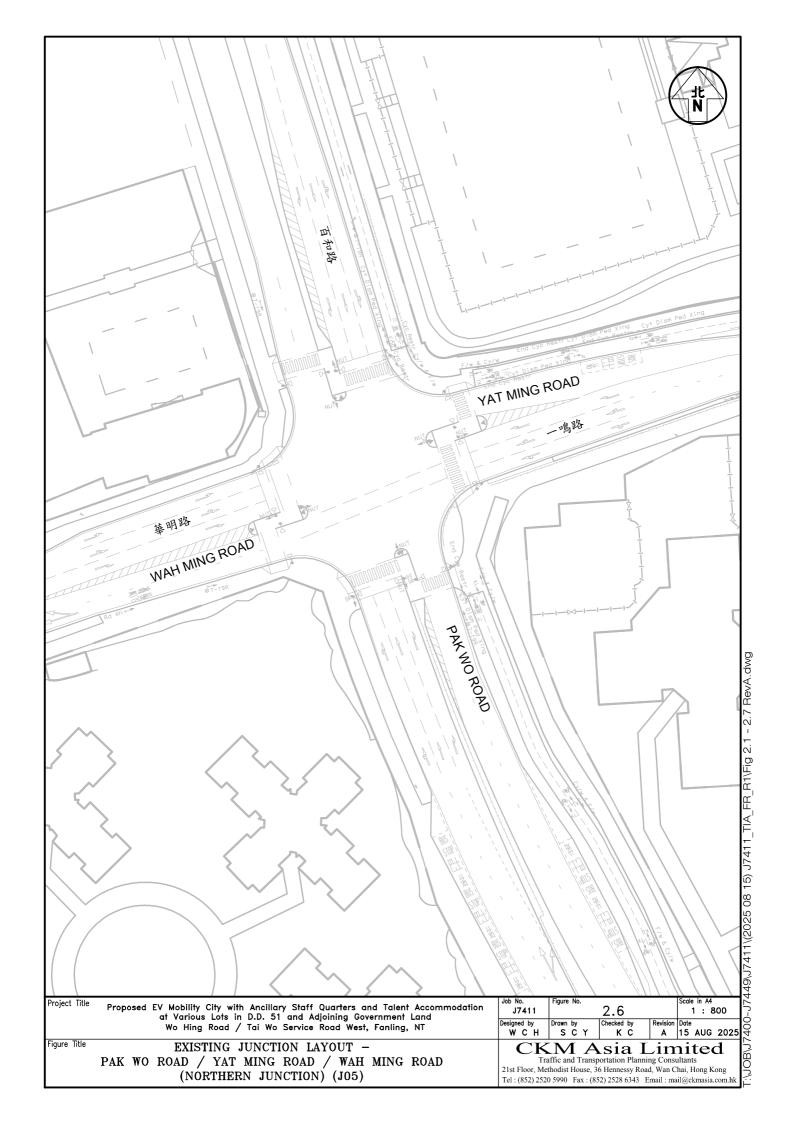


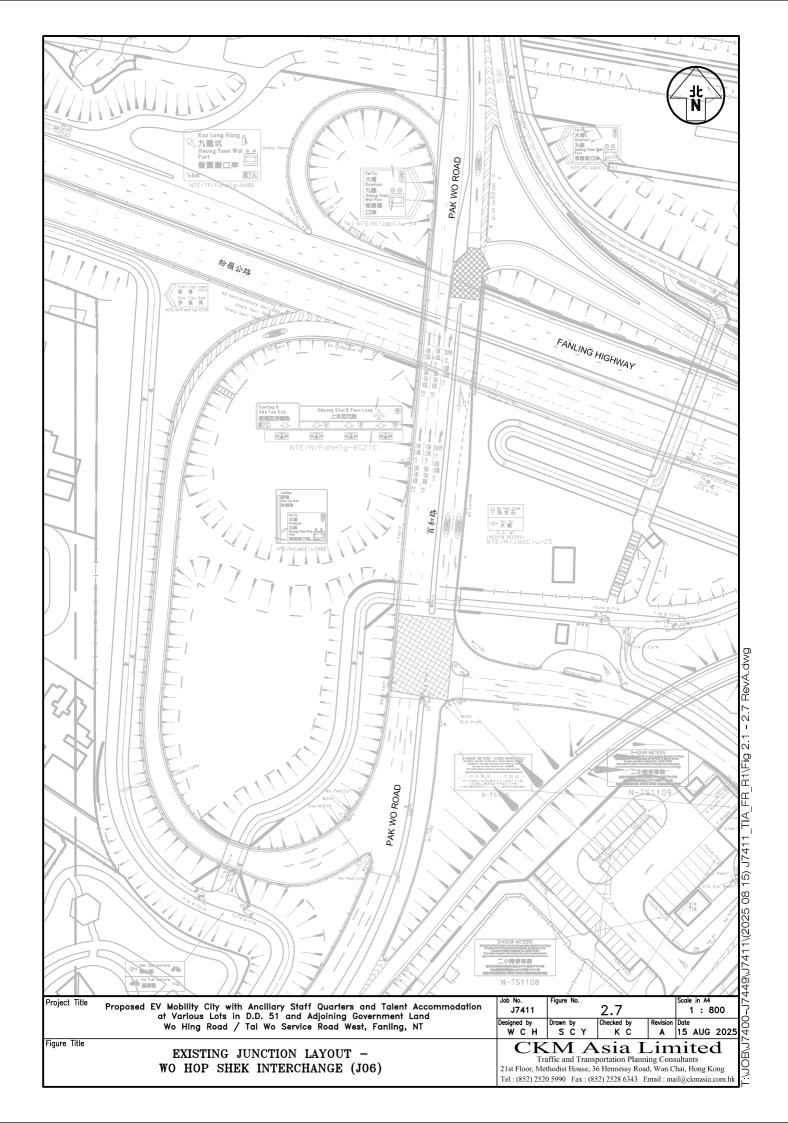


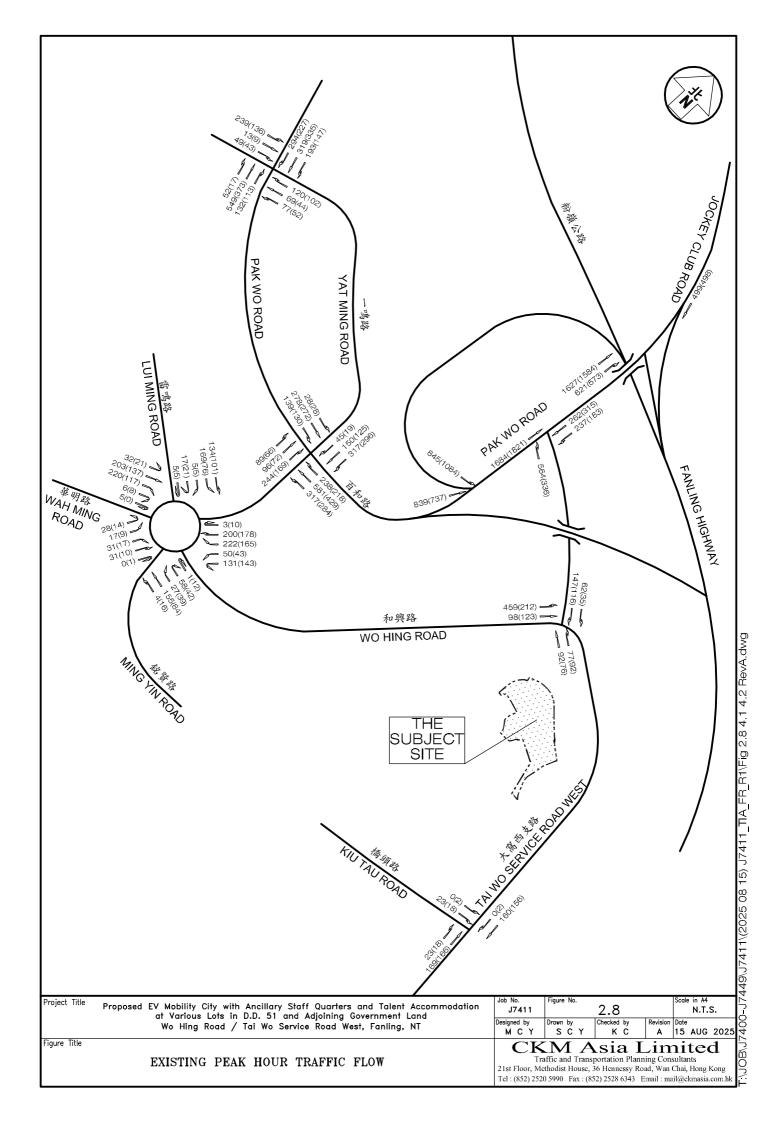


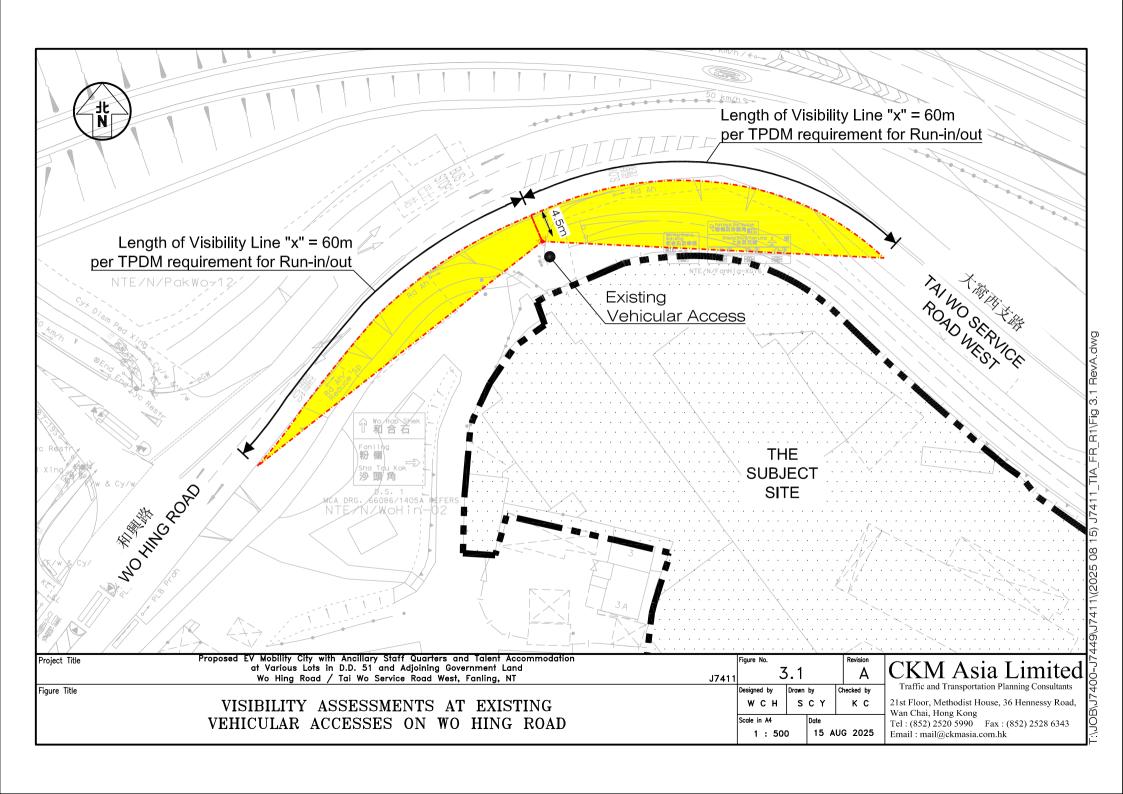


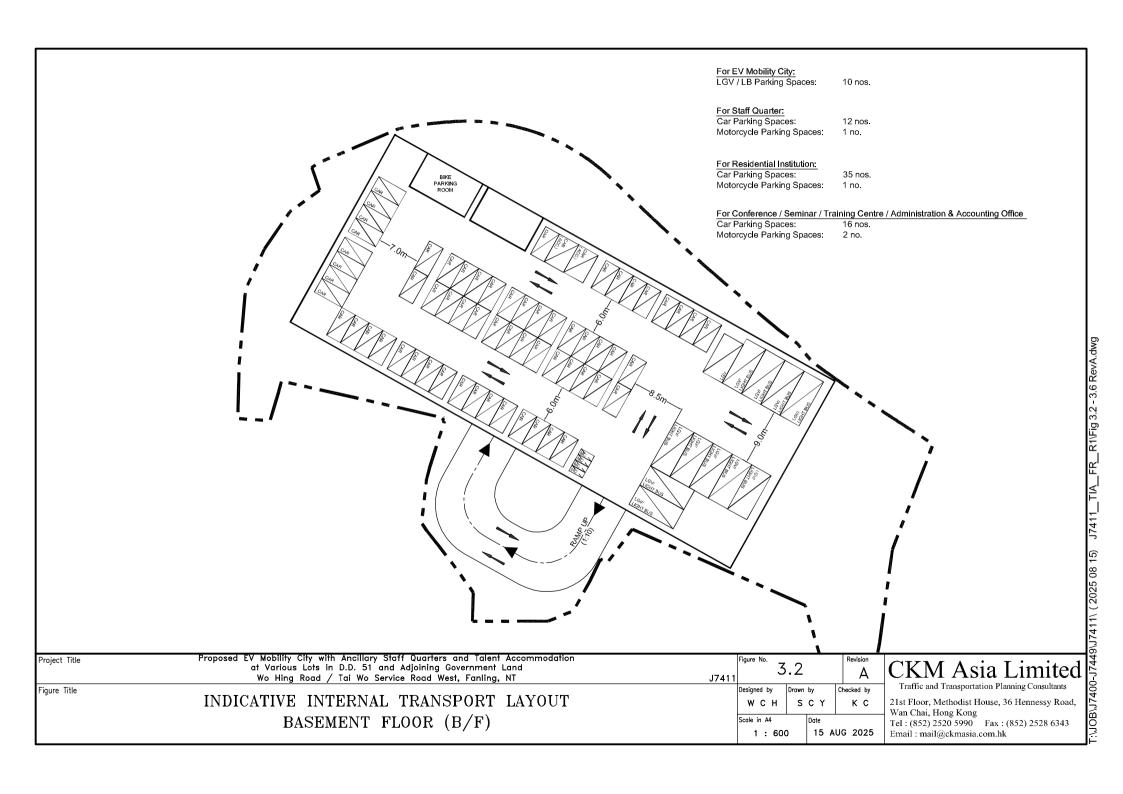


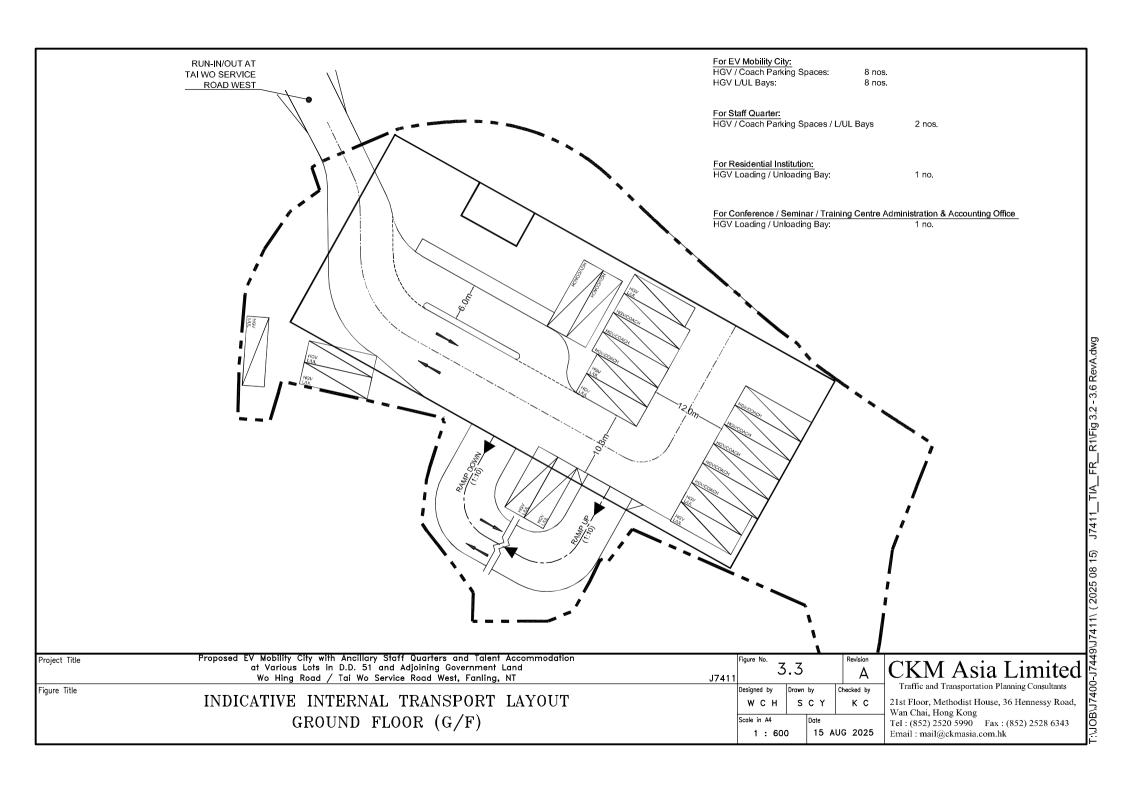


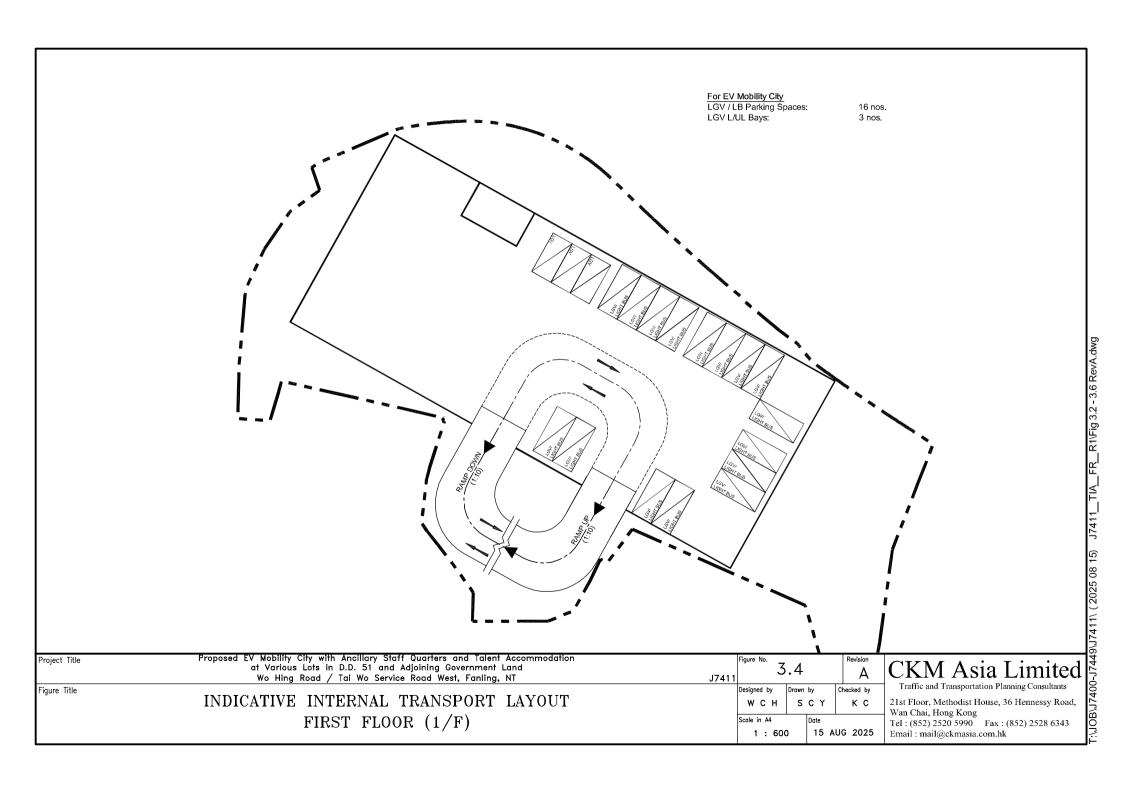


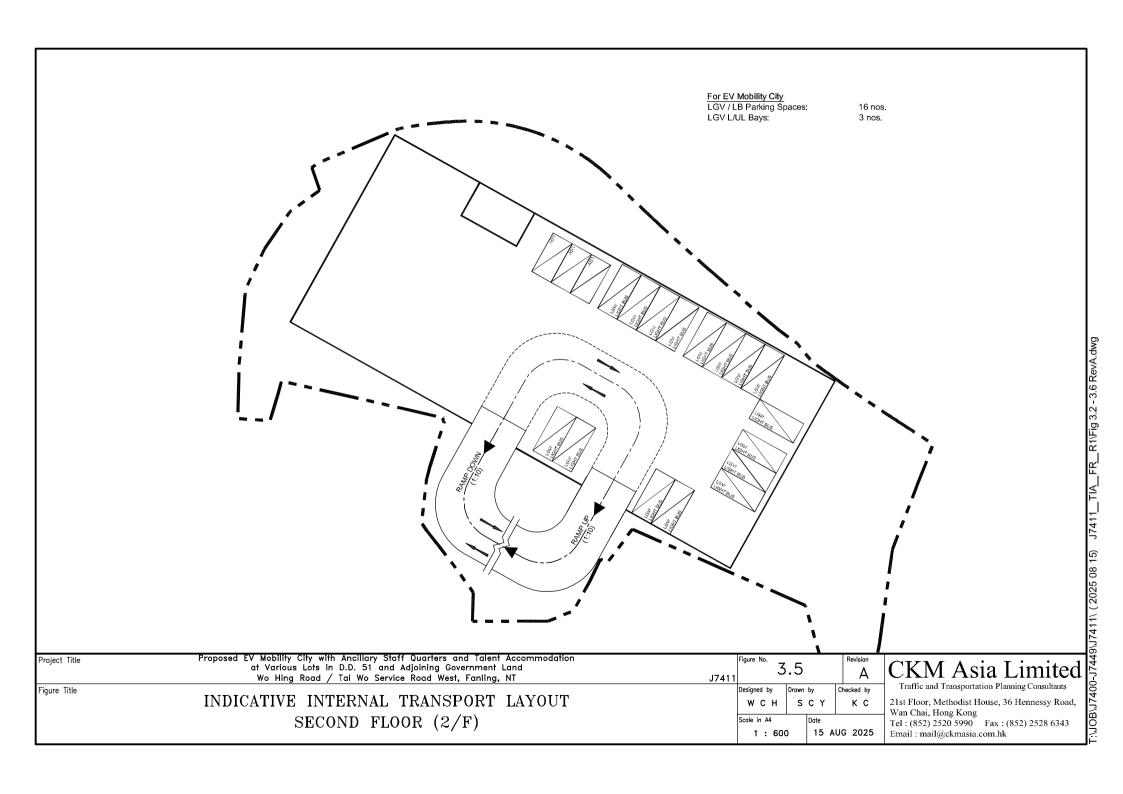


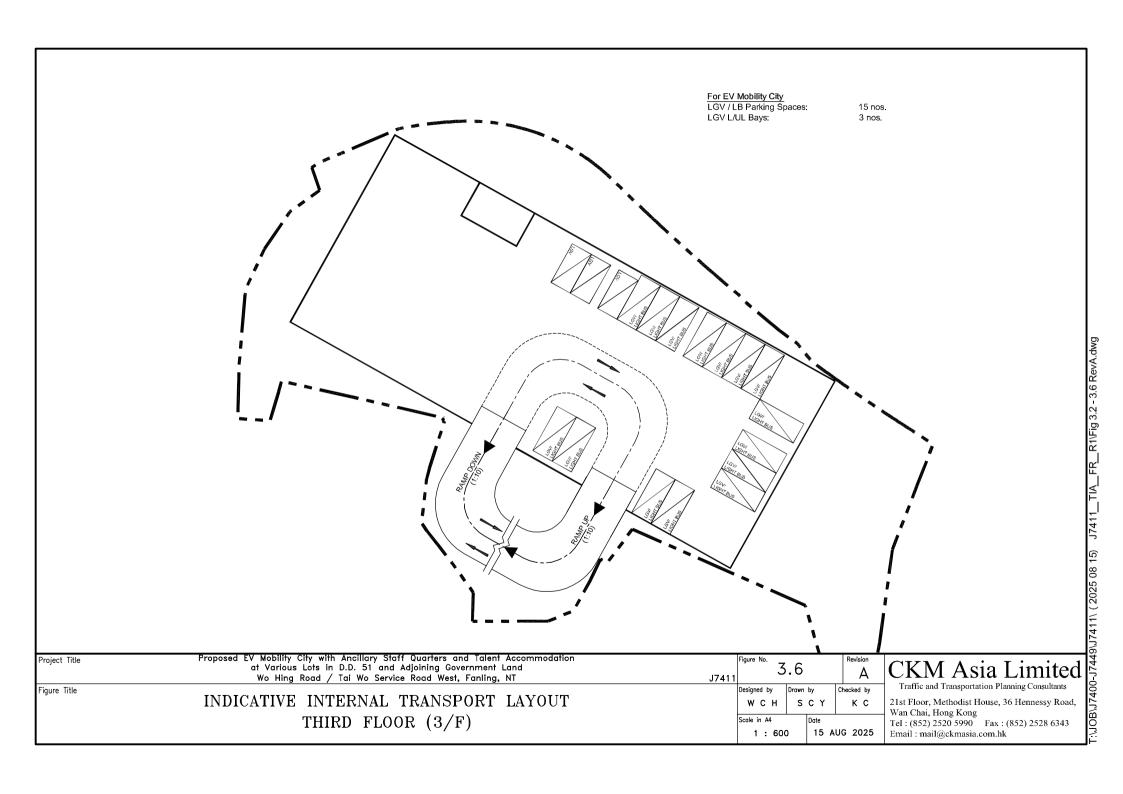


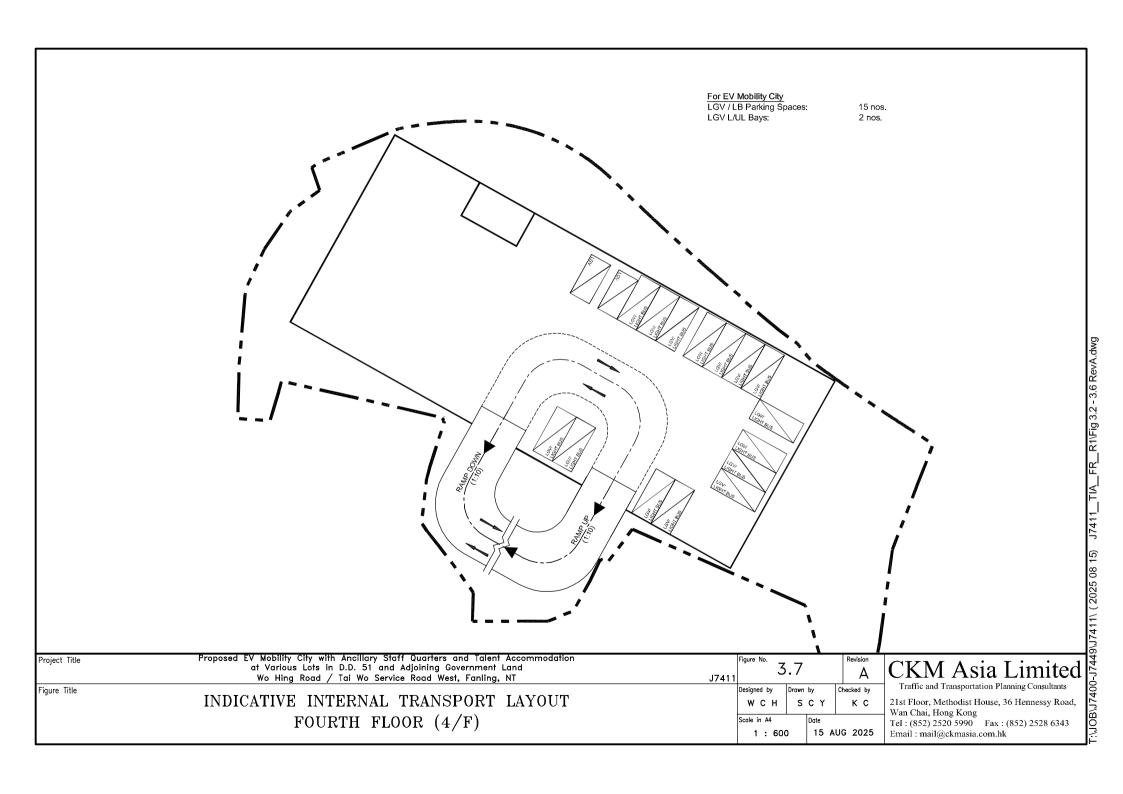


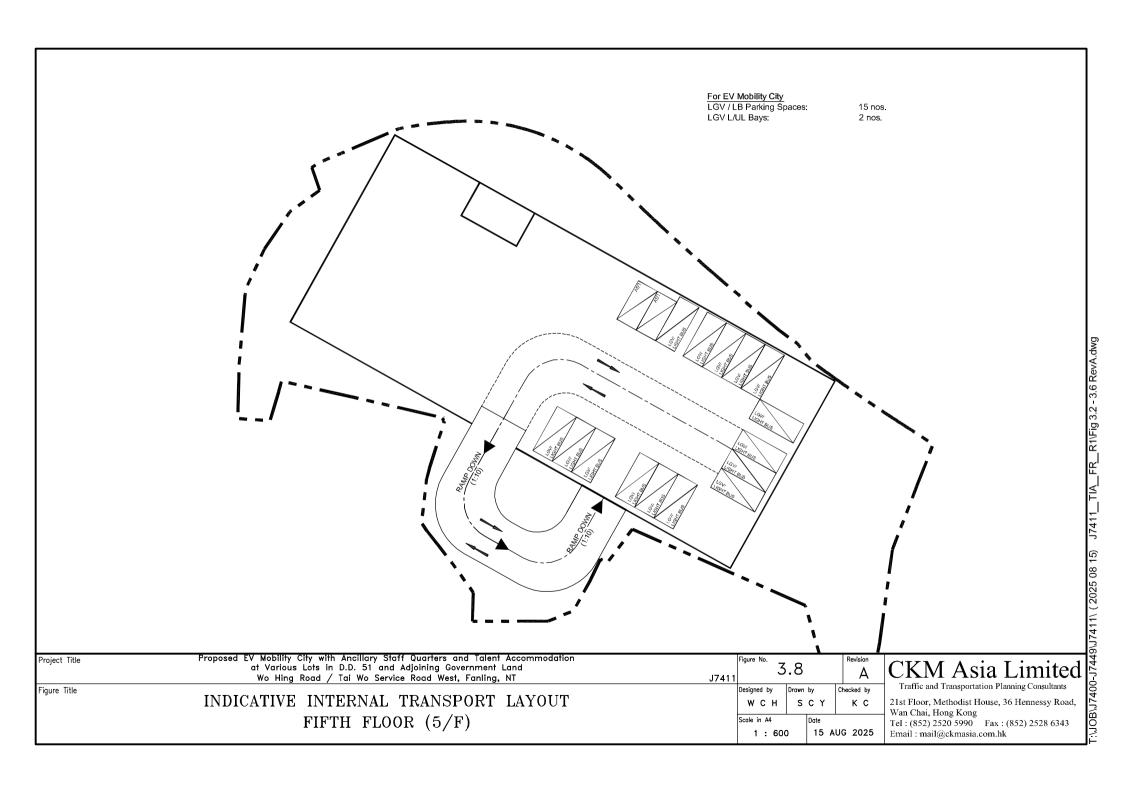


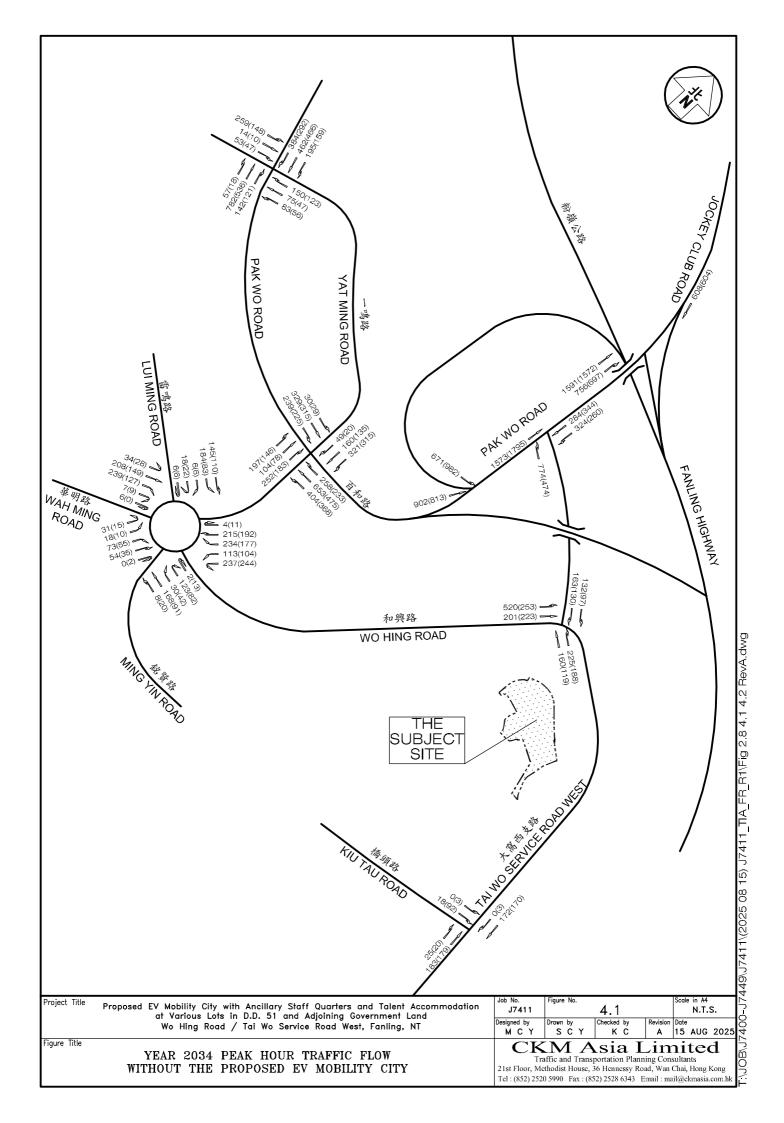


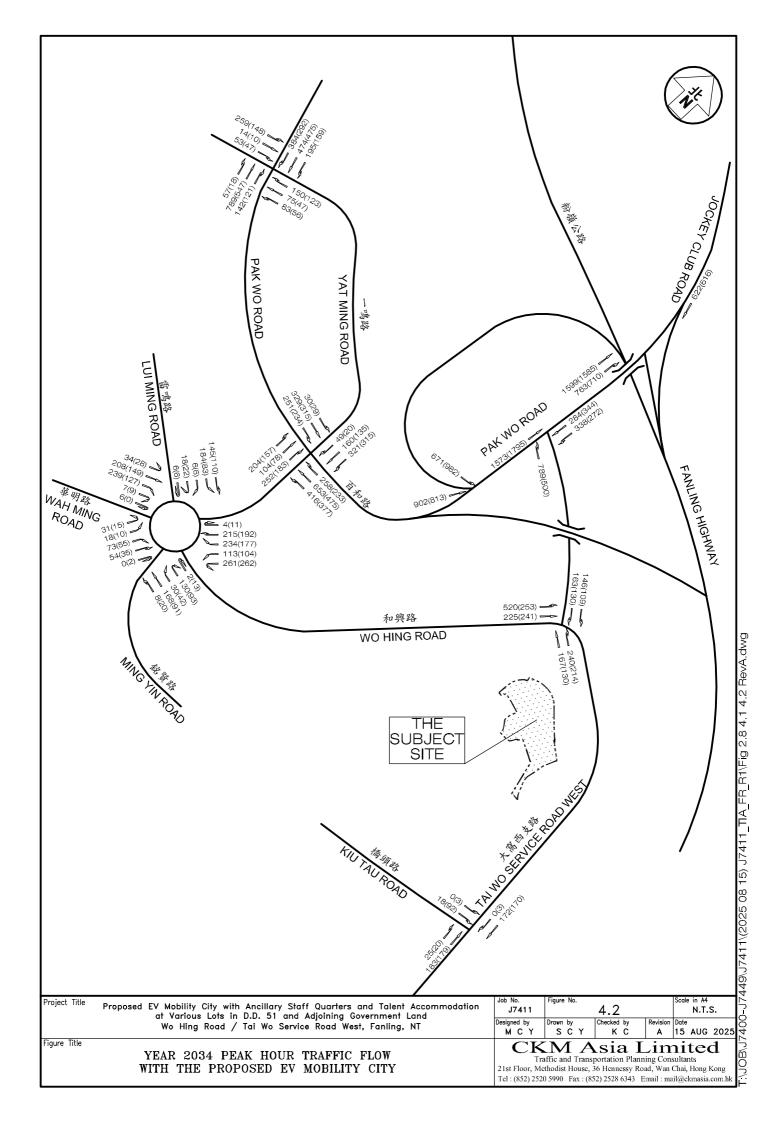


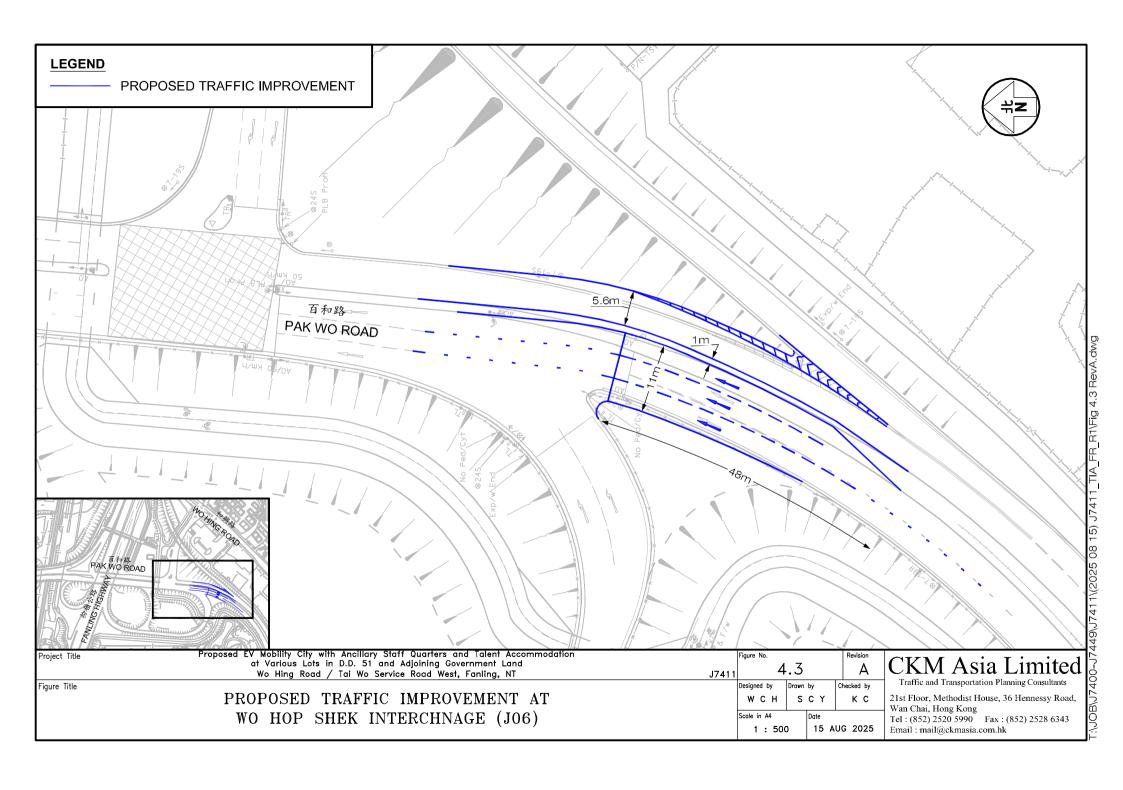




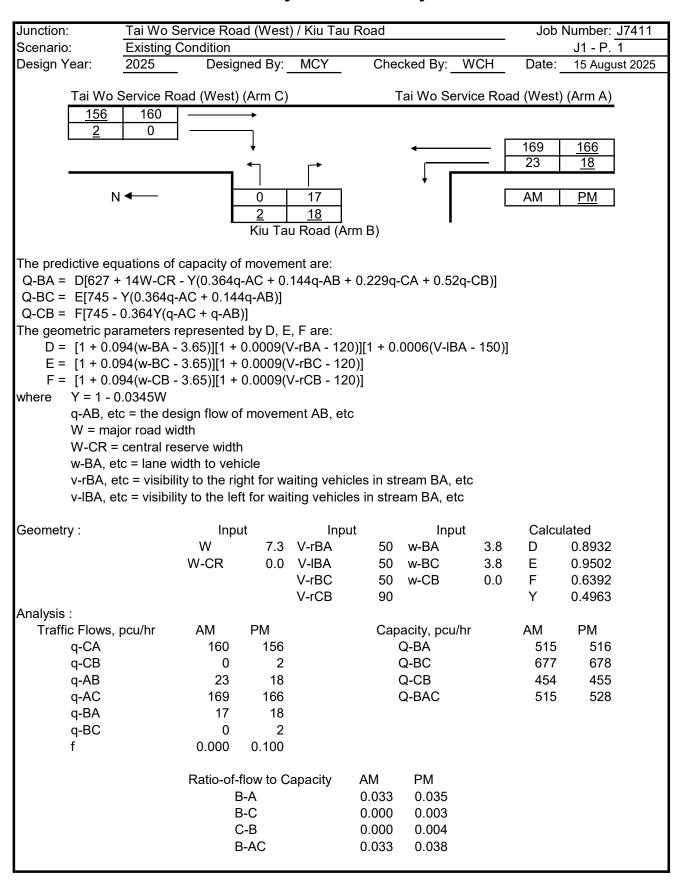


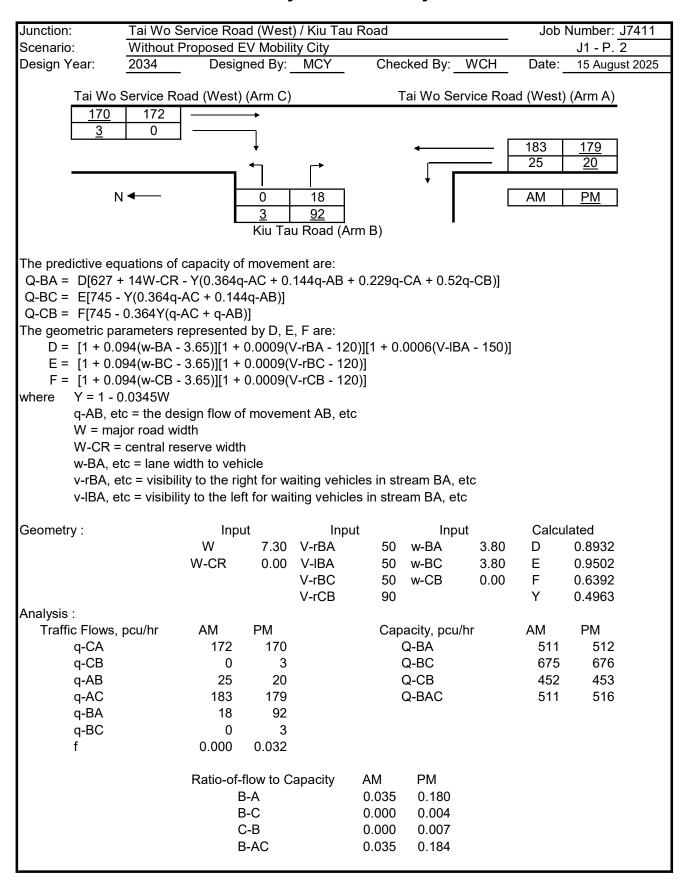


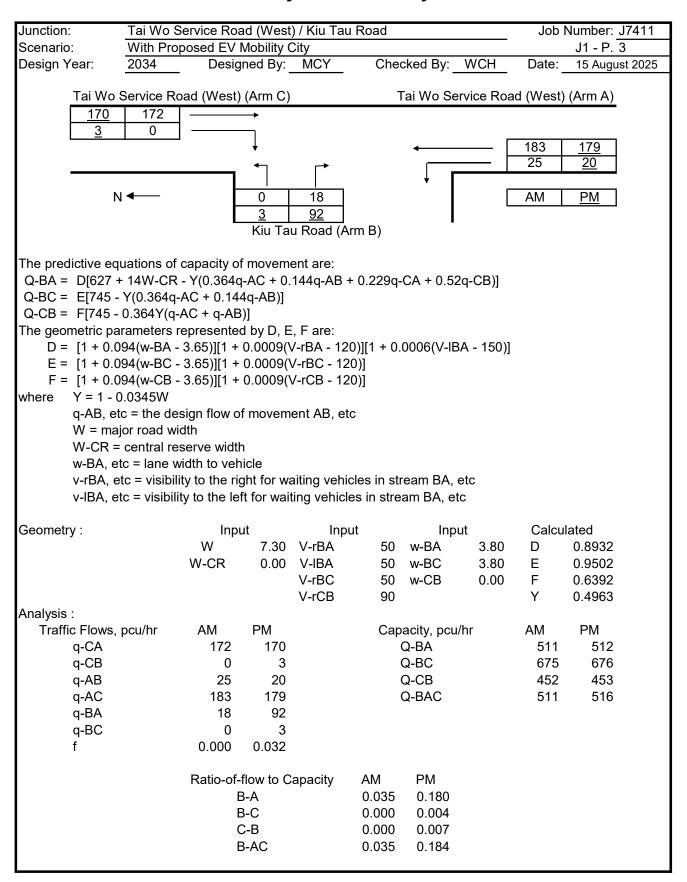


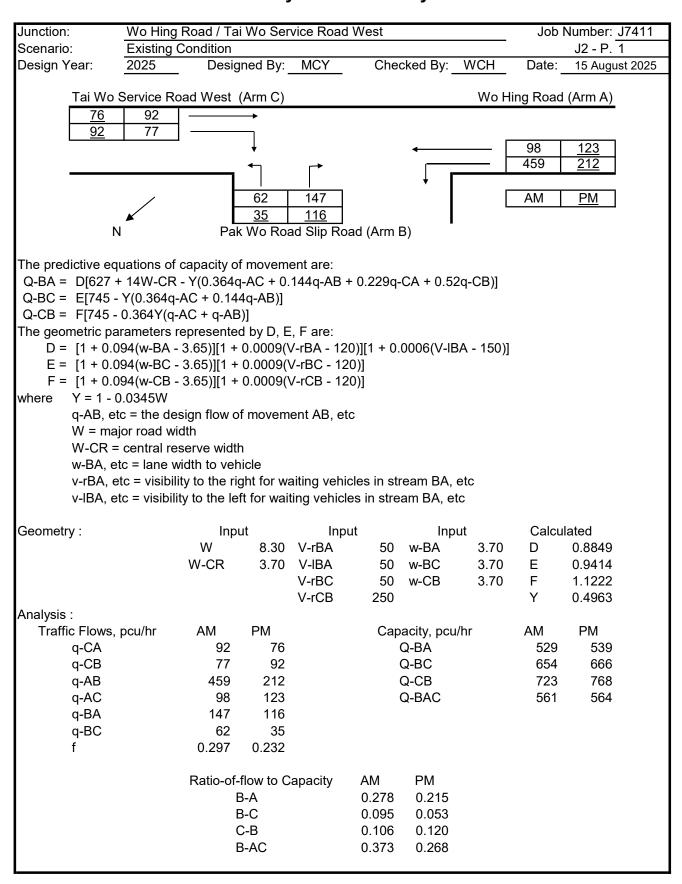


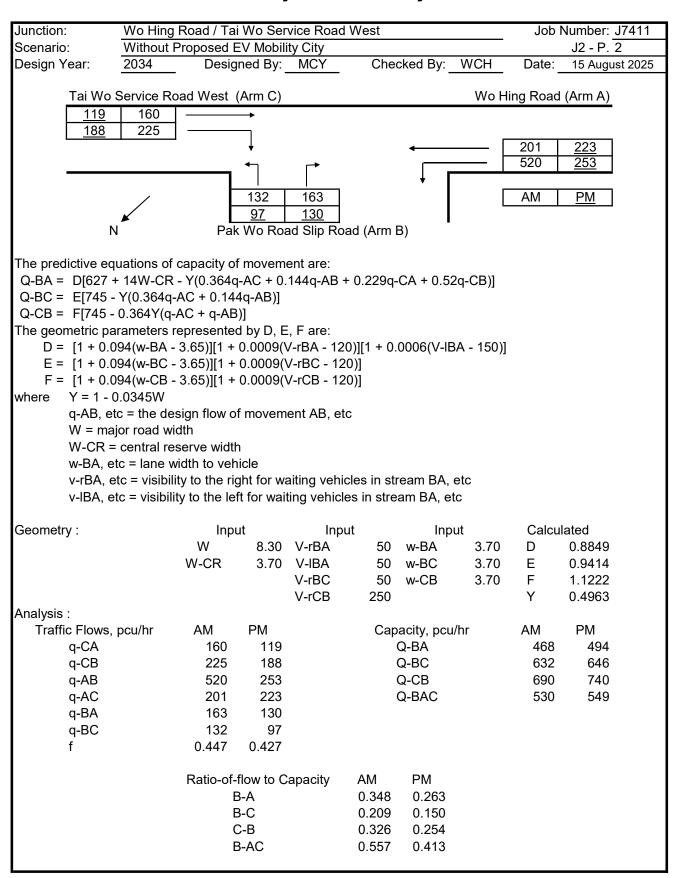


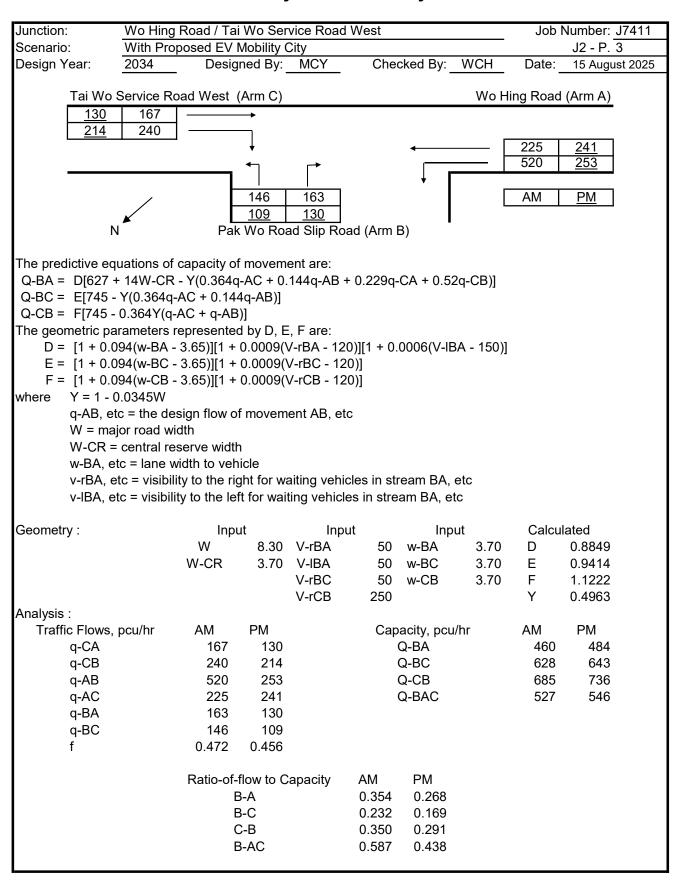












# **Roundabout Analysis**

 Junction:
 Wah Ming Road Roundabout
 Job Number: J7411

 Scenario:
 Existing Condition
 J3 - P. 1

 Design Year:
 2025 Designed By: MCY
 Checked By: WCH
 Date: 15 August 2025

#### AM Peak

| Arm    | To A | То В | To C | To D | To E | To F | To G | To H | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 3    | 131  | 50   | 222  | 200  |      |      |      | 606   | 459            |
| From B | 58   | 1    | 4    | 155  | 27   |      |      |      | 245   | 513            |
| From C | 31   | 31   | 0    | 28   | 17   |      |      |      | 107   | 693            |
| From D | 203  | 220  | 6    | 5    | 32   |      |      |      | 466   | 373            |
| From E | 134  | 169  | 5    | 17   | 5    |      |      |      | 330   | 558            |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 429  | 552  | 65   | 427  | 281  |      |      |      | 1754  |                |

#### PM Peak

| Arm    | To A | То В | To C | To D | To E | To F | To G | То Н | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 10   | 143  | 43   | 165  | 178  |      |      |      | 539   | 255            |
| From B | 42   | 12   | 16   | 84   | 39   |      |      |      | 193   | 436            |
| From C | 17   | 10   | 1    | 14   | 9    |      |      |      | 51    | 556            |
| From D | 137  | 117  | 8    | 0    | 21   |      |      |      | 283   | 772            |
| From E | 101  | 76   | 5    | 21   | 5    |      |      |      | 208   | 851            |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 307  | 358  | 73   | 284  | 252  |      |      |      | 1274  |                |

Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| Α   | Wah Ming Road SB          |
| В   | Wo Hing Road              |
| С   | Ming Yin Road             |
| D   | Wah Ming Road EB          |
| E   | Lui Ming Road             |
| F   | _                         |
| G   |                           |
| Н   |                           |

#### Geometric Parameters

| Geometri | ometric Parameters |       |       |       |       |       |     |  |  |
|----------|--------------------|-------|-------|-------|-------|-------|-----|--|--|
| Arm      | e (m)              | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |  |  |
| From A   | 9.0                | 7.0   | 42.0  | 8.0   | 45    | 54    | 0.4 |  |  |
| From B   | 7.5                | 4.0   | 21.5  | 6.0   | 45    | 54    | 0.9 |  |  |
| From C   | 8.0                | 8.0   | 15.0  | 7.5   | 45    | 61    | 0.0 |  |  |
| From D   | 8.0                | 6.0   | 22.0  | 11.0  | 45    | 50    | 0.3 |  |  |
| From E   | 8.5                | 5.0   | 22.0  | 9.0   | 45    | 38    | 0.6 |  |  |
| From F   |                    |       |       |       |       |       |     |  |  |
| From G   |                    |       |       |       |       |       |     |  |  |
| From H   |                    |       |       |       |       |       |     |  |  |

### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_{E}$               | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_c$                 | Circulating Flow across the Entry   |
| K                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_D(1+0.2x_2)$              |
| $t_D$                 | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| ٧ | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| s | Sharpness of Flare        | 0.0 - 3.0     |

### Ratio-of-Flow to Capacity (RFC)

|        |                |       |       |       |      |                | $Q_{E}$ |      | Entry Flow |     | RFC   |       |
|--------|----------------|-------|-------|-------|------|----------------|---------|------|------------|-----|-------|-------|
| Arm    | x <sub>2</sub> | M     | $t_D$ | K     | F    | f <sub>c</sub> | AM      | PM   | AM         | PM  | AM    | PM    |
| From A | 8.111          | 0.223 | 1.409 | 0.942 | 2458 | 0.776          | 1980    | 2130 | 606        | 539 | 0.306 | 0.253 |
| From B | 5.221          | 0.223 | 1.409 | 0.920 | 1582 | 0.605          | 1170    | 1213 | 245        | 193 | 0.209 | 0.159 |
| From C | 8.000          | 0.223 | 1.409 | 0.876 | 2424 | 0.769          | 1657    | 1749 | 107        | 51  | 0.065 | 0.029 |
| From D | 7.264          | 0.223 | 1.409 | 0.935 | 2201 | 0.726          | 1805    | 1534 | 466        | 283 | 0.258 | 0.184 |
| From E | 6.559          | 0.223 | 1.409 | 0.977 | 1988 | 0.684          | 1568    | 1373 | 330        | 208 | 0.210 | 0.152 |
| From F |                |       |       |       |      |                |         |      |            |     |       |       |
| From G |                |       |       |       |      |                |         |      |            |     |       |       |
| From H |                |       |       |       |      |                |         |      |            |     |       |       |

# **Roundabout Analysis**

 Junction:
 Wah Ming Road Roundabout
 Job Number: J7411

 Scenario:
 Without Proposed EV Mobility City
 J3 - P. 2

 Design Year:
 2034
 Designed By: MCY
 Checked By: WCH
 Date: 15 August 2025

#### AM Peak

| Arm    | To A | То В | To C | To D | To E | To F | To G | То Н | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 4    | 237  | 113  | 234  | 215  |      |      |      | 803   | 522            |
| From B | 123  | 2    | 8    | 168  | 30   |      |      |      | 331   | 609            |
| From C | 73   | 54   | 0    | 31   | 18   |      |      |      | 176   | 806            |
| From D | 208  | 239  | 7    | 6    | 34   |      |      |      | 494   | 525            |
| From E | 145  | 184  | 6    | 18   | 6    |      |      |      | 359   | 716            |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 553  | 716  | 134  | 457  | 303  |      |      |      | 2163  |                |

#### PM Peak

| Arm    | To A | ТоВ | To C | To D | To E | To F | To G | То Н | Total | q <sub>c</sub> |
|--------|------|-----|------|------|------|------|------|------|-------|----------------|
| From A | 11   | 244 | 104  | 177  | 192  |      |      |      | 728   | 303            |
| From B | 82   | 13  | 20   | 91   | 42   |      |      |      | 248   | 529            |
| From C | 55   | 35  | 2    | 15   | 10   |      |      |      | 117   | 636            |
| From D | 149  | 127 | 9    | 0    | 28   |      |      |      | 313   | 935            |
| From E | 110  | 83  | 6    | 22   | 6    |      |      |      | 227   | 967            |
| From F |      |     |      |      |      |      |      |      |       |                |
| From G |      |     |      |      |      |      |      |      |       |                |
| From H |      |     |      |      |      |      |      |      |       |                |
| Total  | 407  | 502 | 141  | 305  | 278  |      |      |      | 1633  |                |

### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| Α   | Wah Ming Road SB          |
| В   | Wo Hing Road              |
| С   | Ming Yin Road             |
| D   | Wah Ming Road EB          |
| E   | Lui Ming Road             |
| F   |                           |
| G   |                           |
| н   |                           |

#### **Geometric Parameters**

| 0001110111 | metric i didineters |       |       |       |       |       |     |  |  |  |
|------------|---------------------|-------|-------|-------|-------|-------|-----|--|--|--|
| Arm        | e (m)               | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |  |  |  |
| From A     | 9.0                 | 7.0   | 42.0  | 8.0   | 45    | 54    | 0.4 |  |  |  |
| From B     | 7.5                 | 4.0   | 21.5  | 6.0   | 45    | 54    | 0.9 |  |  |  |
| From C     | 8.0                 | 8.0   | 15.0  | 7.5   | 45    | 61    | 0.0 |  |  |  |
| From D     | 8.0                 | 6.0   | 22.0  | 11.0  | 45    | 50    | 0.3 |  |  |  |
| From E     | 8.5                 | 5.0   | 22.0  | 9.0   | 45    | 38    | 0.6 |  |  |  |
| From F     |                     |       |       |       |       |       |     |  |  |  |
| From G     |                     |       |       |       |       |       |     |  |  |  |
| From H     |                     |       |       |       |       |       |     |  |  |  |

### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_{E}$        | Entry Capacity                      |
|----------------|-------------------------------------|
| $q_c$          | Circulating Flow across the Entry   |
| K              | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F              | = 303x <sub>2</sub>                 |
| f <sub>c</sub> | $= 0.210t_D(1+0.2x_2)$              |
| $t_D$          | = 1+0.5/(1+M)                       |
| М              | $= \exp[(D-60)/10]$                 |
| $x_2$          | = v+(e-v)/(1+2S)                    |
| S              | W                                   |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| ٧ | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

#### Ratio-of-Flow to Capacity (RFC)

|        |                       |       |       |       |      |                | $Q_{E}$ |      | Entry Flow | •   | RFC   |       |
|--------|-----------------------|-------|-------|-------|------|----------------|---------|------|------------|-----|-------|-------|
| Arm    | <b>x</b> <sub>3</sub> | M     | $t_D$ | K     | F    | f <sub>c</sub> | AM      | PM   | AM         | PM  | AM    | PM    |
| From A | 8.111                 | 0.223 | 1.409 | 0.942 | 2458 | 0.776          | 1934    | 2094 | 803        | 728 | 0.415 | 0.348 |
| From B | 5.221                 | 0.223 | 1.409 | 0.920 | 1582 | 0.605          | 1117    | 1161 | 331        | 248 | 0.296 | 0.214 |
| From C | 8.000                 | 0.223 | 1.409 | 0.876 | 2424 | 0.769          | 1581    | 1695 | 176        | 117 | 0.111 | 0.069 |
| From D | 7.264                 | 0.223 | 1.409 | 0.935 | 2201 | 0.726          | 1702    | 1424 | 494        | 313 | 0.290 | 0.220 |
| From E | 6.559                 | 0.223 | 1.409 | 0.977 | 1988 | 0.684          | 1463    | 1295 | 359        | 227 | 0.245 | 0.175 |
| From F |                       |       |       |       |      |                |         |      |            |     |       |       |
| From G |                       |       |       |       |      |                |         |      |            |     |       |       |
| From H |                       |       |       |       |      |                |         |      |            |     |       |       |

# **Roundabout Analysis**

 Junction:
 Wah Ming Road Roundabout
 Job Number: J7411

 Scenario:
 With Proposed EV Mobility City
 J3 - P. 3

 Design Year:
 2034
 Designed By: MCY
 Checked By: WCH
 Date: 15 August 2025

#### AM Peak

| Arm    | To A | То В | To C | To D | To E | To F | To G | То Н | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 4    | 261  | 113  | 234  | 215  |      |      |      | 827   | 522            |
| From B | 130  | 2    | 8    | 168  | 30   |      |      |      | 338   | 609            |
| From C | 73   | 54   | 0    | 31   | 18   |      |      |      | 176   | 813            |
| From D | 208  | 239  | 7    | 6    | 34   |      |      |      | 494   | 532            |
| From E | 145  | 184  | 6    | 18   | 6    |      |      |      | 359   | 723            |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 560  | 740  | 134  | 457  | 303  |      |      |      | 2194  |                |

#### PM Peak

| Arm    | To A | То В | To C | To D | To E | To F | To G | То Н | Total | q <sub>c</sub> |
|--------|------|------|------|------|------|------|------|------|-------|----------------|
| From A | 11   | 262  | 104  | 177  | 192  |      |      |      | 746   | 303            |
| From B | 93   | 13   | 20   | 91   | 42   |      |      |      | 259   | 529            |
| From C | 55   | 35   | 2    | 15   | 10   |      |      |      | 117   | 647            |
| From D | 149  | 127  | 9    | 0    | 28   |      |      |      | 313   | 946            |
| From E | 110  | 83   | 6    | 22   | 6    |      |      |      | 227   | 967            |
| From F |      |      |      |      |      |      |      |      |       |                |
| From G |      |      |      |      |      |      |      |      |       |                |
| From H |      |      |      |      |      |      |      |      |       |                |
| Total  | 418  | 520  | 141  | 305  | 278  |      |      |      | 1662  |                |

### Legend

| Arm | Road (in clockwise order) |
|-----|---------------------------|
| Α   | Wah Ming Road SB          |
| В   | Wo Hing Road              |
| С   | Ming Yin Road             |
| D   | Wah Ming Road EB          |
| E   | Lui Ming Road             |
| F   |                           |
| G   |                           |
| н   |                           |

#### **Geometric Parameters**

| Ocomenia | c i arainete | ,13   |       |       |       |       |     |
|----------|--------------|-------|-------|-------|-------|-------|-----|
| Arm      | e (m)        | v (m) | r (m) | L (m) | D (m) | Ø (°) | S   |
| From A   | 9.0          | 7.0   | 42.0  | 8.0   | 45    | 54    | 0.4 |
| From B   | 7.5          | 4.0   | 21.5  | 6.0   | 45    | 54    | 0.9 |
| From C   | 8.0          | 8.0   | 15.0  | 7.5   | 45    | 61    | 0.0 |
| From D   | 8.0          | 6.0   | 22.0  | 11.0  | 45    | 50    | 0.3 |
| From E   | 8.5          | 5.0   | 22.0  | 9.0   | 45    | 38    | 0.6 |
| From F   |              |       |       |       |       |       |     |
| From G   |              |       |       |       |       |       |     |
| From H   |              |       |       |       |       |       |     |

### Predictive Equation $Q_E = K(F - f_cq_c)$

| $Q_{E}$               | Entry Capacity                      |
|-----------------------|-------------------------------------|
| $q_c$                 | Circulating Flow across the Entry   |
| K                     | = 1-0.00347(Ø-30)-0.978[(1/r)-0.05] |
| F                     | = 303x <sub>2</sub>                 |
| f <sub>c</sub>        | $= 0.210t_D(1+0.2x_2)$              |
| $t_D$                 | = 1+0.5/(1+M)                       |
| М                     | = exp[(D-60)/10]                    |
| <b>x</b> <sub>2</sub> | = v+(e-v)/(1+2S)                    |
| S                     | = 1.6(e-v)/L                        |

#### Limitation

| е | Entry Width               | 4.0 - 15.0 m  |
|---|---------------------------|---------------|
| ٧ | Approach Half Width       | 2.0 - 7.3 m   |
| r | Entry Radius              | 6.0 - 100.0 m |
| L | Effective Length of Flare | 1.0 - 100.0 m |
| D | Inscribed Circle Diameter | 15 - 100 m    |
| Ø | Entry Angle               | 10° - 60°     |
| S | Sharpness of Flare        | 0.0 - 3.0     |

### Ratio-of-Flow to Capacity (RFC)

|        |                |       |       |       |      |                            | $Q_{E}$ |      | Entry Flow |     | RFC   |       |
|--------|----------------|-------|-------|-------|------|----------------------------|---------|------|------------|-----|-------|-------|
| Arm    | X <sub>4</sub> | М     | $t_D$ | K     | F    | $f_{\scriptscriptstyle C}$ | AM      | PM   | AM         | PM  | AM    | PM    |
| From A | 8.111          | 0.223 | 1.409 | 0.942 | 2458 | 0.776                      | 1934    | 2094 | 827        | 746 | 0.428 | 0.356 |
| From B | 5.221          | 0.223 | 1.409 | 0.920 | 1582 | 0.605                      | 1117    | 1161 | 338        | 259 | 0.303 | 0.223 |
| From C | 8.000          | 0.223 | 1.409 | 0.876 | 2424 | 0.769                      | 1576    | 1688 | 176        | 117 | 0.112 | 0.069 |
| From D | 7.264          | 0.223 | 1.409 | 0.935 | 2201 | 0.726                      | 1697    | 1416 | 494        | 313 | 0.291 | 0.221 |
| From E | 6.559          | 0.223 | 1.409 | 0.977 | 1988 | 0.684                      | 1458    | 1295 | 359        | 227 | 0.246 | 0.175 |
| From F |                |       |       |       |      |                            |         |      |            |     |       |       |
| From G |                |       |       |       |      |                            |         |      |            |     |       |       |
| From H |                |       |       |       |      |                            |         |      |            |     |       |       |

Pak Wo Road / Yat Ming Road / Wah Ming Road Junction: Job Number: <u>J7411</u> Scenario: Existing Condition J4 - P. 1

| Design Year: 2025 Design |         |                          | ed By:       |              | MCY           |              | -                         | Checked By: WCH |                       |                             |               |                           | Date: 15 August 2025 |                       |                             |                |            |
|--------------------------|---------|--------------------------|--------------|--------------|---------------|--------------|---------------------------|-----------------|-----------------------|-----------------------------|---------------|---------------------------|----------------------|-----------------------|-----------------------------|----------------|------------|
| Aj                       | pproach |                          | Phase        | Stage        | Width (m)     | Radius (m)   | % Up-hill<br>Gradient     | Turning %       | Sat. Flow<br>(pcu/hr) | AM Peak<br>Flow<br>(pcu/hr) | y value       | Critical y                | Turning %            | Sat. Flow<br>(pcu/hr) | PM Peak<br>Flow<br>(pcu/hr) | y value        | Critical y |
| Pak Wo Road EB           |         | LT+SA                    | A1           | 1            | 3.40          | 15.0         |                           | 16              | 1924                  | 147                         | 0.076         | 0.076                     | 23                   | 1911                  | 143                         | 0.075          |            |
|                          |         | SA                       | A2           | 1            | 3.30          |              |                           |                 | 2085                  | 159                         | 0.076         |                           |                      | 2085                  | 157                         | 0.075          |            |
|                          |         | RT                       | А3           | 1            | 3.30          | 15.0         |                           | 100             | 1895                  | 139                         | 0.073         |                           | 100                  | 1895                  | 130                         |                | 0.069      |
| Pak Wo Road WE           | 3       | LT                       | B1           | 2            | 3.00          | 15.0         |                           | 100             | 1741                  | 317                         | 0.182         | 0.182                     | 100                  | 1741                  | 284                         | 0.163          | 0.163      |
|                          |         | SA                       | B2           | 2            | 3.00          |              |                           |                 | 2055                  | 282                         | 0.137         |                           |                      | 2055                  | 223                         | 0.109          |            |
|                          |         | SA+RT                    | В3           | 2            | 3.00          | 20.0         |                           | 0               | 2055                  | 299                         | 0.145         |                           | 7                    | 2044                  | 222                         | 0.109          |            |
|                          |         | RT                       | B4           | 2            | 3.00          | 15.0         |                           | 100             | 1868                  | 238                         | 0.127         |                           | 100                  | 1868                  | 202                         | 0.108          |            |
| Yat Ming Road SE         | <br>3   | LT                       | C1           | 3            | 3.40          | 15.0         |                           | 100             | 1777                  | 218                         | 0.123         | 0.123                     | 100                  | 1777                  | 196                         | 0.110          | 0.110      |
|                          |         | LT+SA                    | C2           | 3            | 3.30          | 20.0         |                           | 40              | 2024                  | 249                         | 0.123         |                           | 32                   | 2036                  | 225                         | 0.111          |            |
|                          |         | RT                       | СЗ           | 3            | 3.30          | 15.0         |                           | 100             | 1895                  | 45                          | 0.024         |                           | 100                  | 1895                  | 19                          | 0.010          |            |
| Wah Ming Road N          | NB      | LT+SA                    | D1           | 4            | 3.40          | 15.0         |                           | 65              | 1836                  | 136                         | 0.074         | 0.074                     | 68                   | 1831                  | 97                          | 0.053          | 0.053      |
| , , , ,                  |         | SA+RT                    | D2           | 4            | 3.30          | 25.0         |                           | 67              | 2004                  | 149                         | 0.074         |                           | 62                   | 2010                  | 107                         | 0.053          |            |
|                          |         | RT                       | D3           | 4            | 3.30          | 20.0         |                           | 100             | 1940                  | 144                         | 0.074         |                           | 100                  | 1940                  | 103                         | 0.053          |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       |                             |               |                           |                      |                       |                             |                |            |
| pedestrian phase         |         |                          | E(p)         | 1            |               |              | rossing                   |                 | 6                     |                             | GM +          | 12                        |                      | GM =                  | 18<br>18                    | sec            |            |
|                          |         |                          | F(p)<br>G(p) | 2,3,4        |               |              | rossing rossing           |                 | 6<br>5                |                             | GM +<br>GM +  | 12<br>8                   | sec F                |                       | 13                          | sec            |            |
|                          |         |                          | H(p)         | 1,2,4        |               |              | rossing                   |                 | 8                     |                             | GM +          | 15                        | sec F                |                       | 23                          | sec            |            |
|                          |         |                          | I(p)         | 2            |               |              | rossing                   |                 | 5                     |                             | GM +          | 7                         | sec F                |                       | 12                          | sec            |            |
|                          |         |                          | J(p)         | 1,3,4<br>4   |               |              | rossing rossing           |                 | 9<br>5                |                             | GM +<br>GM +  | 17<br>6                   | sec F                | GM =<br>GM =          | 26<br>11                    | sec            |            |
|                          |         |                          | K(p)         | 1,2,3        |               |              | rossing                   |                 | 5                     |                             | GM +          | 10                        |                      | GM =                  | 15                          | sec            |            |
| AM Traffic Flow (pcu/hr) | ī       |                          |              | PM Traffic F | low (pcu/hr)  |              |                           |                 | N                     | S=1940+                     | 100(W–3.:     | 25) S=                    | 2080+100             | )(W-3.25)             | Note:                       |                |            |
| 45 ←                     | 317     |                          | N<br>↑       |              | 19            | $\leftarrow$ | 296                       |                 | N<br>↑                | S <sub>M</sub> =S÷(1        |               |                           | =(S-230)=            |                       |                             |                |            |
|                          | 150     |                          |              |              |               | ↓<br>125     |                           |                 | l                     |                             | AM Pe         | ak Hour                   | PM Pe                | ak Hour               |                             |                |            |
| 28                       |         | 238                      |              |              | 28            |              |                           | 218             |                       |                             | 1+2+3+4       |                           | 1+2+3+4              |                       |                             |                |            |
| → 278                    | 581     | -                        | -            |              | 272           |              | 429 ◀                     | 1               | _                     | Sum y                       | 0.455         |                           | 0.395                |                       |                             |                |            |
| <b>†</b> 139             |         | <b>↓</b><br>317          |              | •            | 130           |              |                           | <b>↓</b><br>284 |                       | L (s)                       | 27            |                           | 27                   |                       |                             |                |            |
|                          | 96      |                          |              |              |               | 72           |                           |                 |                       | C (s)                       | 120           |                           | 120                  |                       |                             |                |            |
| 89 ←                     | 244     |                          |              |              | 66            | $\leftarrow$ | 169                       |                 |                       | practical y                 | 0.698         |                           | 0.698                |                       |                             |                |            |
|                          |         |                          |              |              |               |              |                           |                 |                       | R.C. (%)                    | 53%           |                           | 77%                  |                       |                             |                |            |
| 1                        | H(p)    | 2                        |              | H(p)         | _ <del></del> | 3            | G(p)                      | C3 C2 C1        |                       | 4                           |               | H(p)                      |                      |                       |                             |                |            |
| <b>.</b>                 | -       |                          |              |              | I(p)          |              | •                         | C3 C2 C1        |                       |                             |               |                           |                      |                       |                             |                |            |
| A1<br>A2<br>A3           | I       | <b>▼</b> <sup>F(p)</sup> |              |              | B4<br>B3<br>♣ | F(p)         |                           |                 | J(p)                  | ₩ F(p)                      |               |                           | A I                  |                       |                             |                |            |
| E(p)                     | J(p) 🛊  |                          |              |              | B2◀<br>B1♥    |              |                           |                 | σ(P) <b>ψ</b>         |                             | D1 D2 D3      |                           | →(P) <b>*</b>        |                       |                             |                |            |
| <b>↓</b>                 |         |                          | <b>←</b>     |              |               |              | <b>←</b> T(b) <b>&gt;</b> |                 |                       |                             | <u> 14</u> ₱₽ | <b>←</b> R(b)L - <b>→</b> |                      |                       |                             |                |            |
| AM<br>G=                 | I/G =   | 9 G=                     |              | I/G =        | 6             | G =          |                           | I/G =           | 7                     | G =                         |               | I/G =                     | 9                    | G =                   |                             | I/G =          |            |
| PM<br>G=                 | I/G =   | 9 G=                     |              | I/G =        | 6             | G =          |                           | I/G =           | 7                     | G =                         |               | I/G =                     | 9                    | G =                   |                             | I/G =          |            |
|                          |         | =                        |              | . =          | Ü             | -            |                           |                 |                       | -                           |               |                           | ŭ                    | -                     |                             | · <del>-</del> |            |

Junction: Pak Wo Road / Yat Ming Road / Wah Ming Road Job Number: <u>J7411</u> Scenario: Without Proposed EV Mobility City J4 - P. 2

| Design Year: 2034       | ned By: MCY |                       |                |                |                       | Checke                    | ed By:          |                  | Date: 15 August 2025  |              |                        | 2025               |                  |                 |         |          |
|-------------------------|-------------|-----------------------|----------------|----------------|-----------------------|---------------------------|-----------------|------------------|-----------------------|--------------|------------------------|--------------------|------------------|-----------------|---------|----------|
| Approach                |             | Phase                 | Stage          | Width (m)      | Radius (m)            | % Up-hill<br>Gradient     | Turning %       | Sat. Flow        | AM Peak<br>Flow       | y value      | Critical y             | Turning %          | Sat. Flow        | PM Peak<br>Flow | y value | Critical |
| Pak Wo Road EB          | LT+SA       | A1                    | 1              | 3.40           | 15.0                  | Gradient                  | 15              | (pcu/hr)<br>1926 | (pcu/hr)<br>172       | 0.089        | 0.089                  | 21                 | (pcu/hr)<br>1915 | (pcu/hr)<br>165 | 0.086   |          |
|                         | SA          | A2                    | 1              | 3.30           | 0.0                   |                           |                 | 2085             | 187                   | 0.090        |                        |                    | 2085             | 179             | 0.086   |          |
|                         | RT          | A3                    | 1              | 3.30           | 15.0                  |                           | 100             | 1895             | 239                   | 0.126        |                        | 100                | 1895             | 225             | 0.119   | 0.11     |
| Pak Wo Road WB          | LT          | B1                    | 2              | 3.00           | 15.0                  |                           | 100             | 1741             | 404                   | 0.232        | 0.232                  | 100                | 1741             | 368             | 0.211   | 0.21     |
|                         | SA          | B2                    | 2              | 3.00           |                       |                           |                 | 2055             | 313                   | 0.152        |                        |                    | 2055             | 244             | 0.119   |          |
|                         | SA+RT       | В3                    | 2              | 3.00           | 20.0                  |                           | 0               | 2055             | 340                   | 0.165        |                        | 7                  | 2044             | 248             | 0.121   |          |
|                         | RT          | B4                    | 2              | 3.00           | 15.0                  |                           | 100             | 1868             | 258                   | 0.138        |                        | 100                | 1868             | 216             | 0.116   |          |
| ⁄at Ming Road SB        | LT          | C1                    | 3              | 3.40           | 15.0                  |                           | 100             | 1777             | 225                   | 0.127        | 0.127                  | 100                | 1777             | 210             | 0.118   | 0.11     |
|                         | LT+SA       | C2                    | 3              | 3.30           | 20.0                  |                           | 40              | 2024             | 256                   | 0.126        |                        | 33                 | 2035             | 240             | 0.118   |          |
|                         | RT          | C3                    | 3              | 3.30           | 15.0                  |                           | 100             | 1895             | 49                    | 0.026        |                        | 100                | 1895             | 20              | 0.011   |          |
| Vah Ming Road NB        | LT+SA       | D1                    | 4              | 3.40           | 15.0                  |                           | 100             | 1777             | 197                   | 0.111        | 0.111                  | 100                | 1777             | 146             | 0.082   | 0.08     |
|                         | SA+RT       | D2                    | 4              | 3.30           | 25.0                  |                           | 48              | 2027             | 195                   | 0.096        |                        | 46                 | 2029             | 144             | 0.071   |          |
|                         | RT          | D3                    | 4              | 3.30           | 20.0                  |                           | 100             | 1940             | 161                   | 0.083        |                        | 100                | 1940             | 117             | 0.060   |          |
|                         |             |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
|                         |             |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
|                         |             |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
|                         |             |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
|                         |             |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
|                         |             |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
| edestrian phase         |             | E(P)                  | 1              |                | min c                 | rossing                   | time =          | 6                | sec                   | GM +         | 12                     | sec F              | GM =             | 18              | sec     |          |
|                         |             | F(P)                  | 2,3,4          |                | min c                 | rossing                   | time =          | 6                | sec                   | GM +         | 12                     | sec F              | GM =             | 18              | sec     |          |
|                         |             | G(P)                  | 3              |                |                       | rossing .                 |                 | 5                |                       | GM +         | 8                      | sec F              |                  | 13              | sec     |          |
|                         |             | H(P)                  | 1,2,4          |                |                       | rossing                   |                 | 8<br>5           |                       | GM +<br>GM + | 15<br>7                | sec F              |                  | 23<br>12        | sec     |          |
|                         |             | J(P)                  | 1,3,4          |                |                       | rossing                   |                 | 9                |                       | GM +         | 17                     | sec F              |                  | 26              | sec     |          |
|                         |             | K(P)                  | 4              |                | min c                 | rossing                   | time =          | 5                | sec                   | GM+          | 6                      | sec F              | GM =             | 11              | sec     |          |
|                         |             | L(P)                  | 2,3,4          |                | min c                 | rossing                   | time =          | 5                | sec                   | GM +         | 10                     | sec F              | GM =             | 15              | sec     |          |
| M Traffic Flow (pcu/hr) |             | N<br>•                | PM Traffic F   | Flow (pcu/hr)  |                       |                           |                 | N<br>•           |                       | 100(W-3.2    |                        | 2080+100           |                  | Note:           |         |          |
| 49 321                  |             |                       |                | 20             | $\top$                | 315                       |                 |                  | S <sub>M</sub> =S÷(1· | AM Pe        |                        | =(S-230)+<br>PM Pe |                  |                 |         |          |
| 30                      | 258         |                       |                | 29             | 135                   |                           | 233             |                  |                       | 1+2+3+4      |                        | 1+2+3+4            |                  |                 |         |          |
| 329 653                 | ₃ ♣         | -                     | -              | 315            |                       | 475 ◀                     | Ť               | _                | Sum y                 | 0.559        |                        | 0.530              |                  |                 |         |          |
| <b>★</b> 239            | ↓<br>404    |                       | 1              | 225            |                       |                           | <b>↓</b><br>368 |                  | L (s)                 | 27           |                        | 27                 |                  |                 |         |          |
| 104<br><b>↑</b>         |             |                       |                |                | 78<br><b>∱</b>        |                           |                 |                  | C (s)                 | 120          |                        | 120                |                  |                 |         |          |
| 197 252                 |             |                       |                | 146            | $\longleftrightarrow$ | 183                       |                 |                  | practical y           | 0.698        |                        | 0.698              |                  |                 |         |          |
|                         |             |                       |                |                | ļ                     |                           |                 |                  | R.C. (%)              | 25%          |                        | 31%                |                  |                 |         |          |
| <b>4 →</b>              | 2           |                       | <b>← H</b> (p) | . ,            | 3                     | G(p)                      | C3 C2 C1        |                  | 4                     |              | H(p)                   |                    |                  |                 |         |          |
| <b>‡</b> A1             |             |                       |                | I(p)           | <b>≜</b><br>F(p)      |                           |                 |                  | F(p)                  |              |                        |                    |                  |                 |         |          |
| A2<br>A3                | • "         |                       |                | B4<br>B3<br>B2 | <b>*</b> "            |                           |                 | J(p)             | * "                   |              |                        | J(p) ↓             |                  |                 |         |          |
| E(p)  ← ½(p) →          |             | <b>4</b> <u>L</u> (₽) |                | B1.<br>▼       |                       | <b>4</b> 1(0) <b>&gt;</b> |                 |                  |                       | D1 D2 D3     | <b>4</b> K(p) <b>▲</b> |                    |                  |                 |         |          |
|                         | 1           |                       |                |                |                       |                           |                 |                  |                       |              |                        |                    |                  |                 |         |          |
| M = VG =                | 9 G=        |                       | I/G =          | 6              | G =                   |                           | I/G =           | 7                | G =                   |              | I/G =                  | 9                  | G =              |                 | I/G =   |          |
|                         | 9 G=        |                       | I/G =          | 6              | G =                   |                           | I/G =           | 7                | G =                   |              | I/G =                  | 9                  | G =              |                 | I/G =   |          |

Job Number: <u>J7411</u> Junction: Pak Wo Road / Yat Ming Road / Wah Ming Road J4 - P. 3

WCH Date: \_\_\_\_15 August 2025

Scenario: With Proposed EV Mobility City

Design Year: 2034 Designed By:

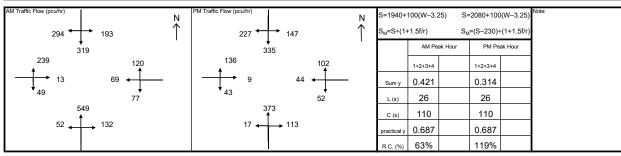
| Design Year: 2034 Designed By: MCY |              |                  |                   |              |                 | Checked By: WCH Date: 15 August 202 |                           |           |                       |                       |             |             | 2025      |                       |                  |         |            |
|------------------------------------|--------------|------------------|-------------------|--------------|-----------------|-------------------------------------|---------------------------|-----------|-----------------------|-----------------------|-------------|-------------|-----------|-----------------------|------------------|---------|------------|
|                                    |              |                  |                   |              | ı               | l                                   |                           | Ι         |                       | AM Peak               |             |             | <u> </u>  |                       | PM Peak          |         |            |
|                                    | Approach     |                  | Phase             | Stage        | Width (m)       | Radius (m)                          | % Up-hill<br>Gradient     | Turning % | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr)      | y value     | Critical y  | Turning % | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr) | y value | Critical y |
| Pak Wo Road                        | EB           | LT+SA            | A1                | 1            | 3.40            | 15.0                                |                           | 15        | 1926                  | 172                   | 0.089       |             | 21        | 1915                  | 165              | 0.086   |            |
|                                    |              | SA               | A2                | 1            | 3.30            | 0.0                                 |                           |           | 2085                  | 187                   | 0.090       | 0.090       |           | 2085                  | 179              | 0.086   |            |
|                                    |              | RT               | А3                | 1            | 3.30            | 15.0                                |                           | 100       | 1895                  | 251                   | 0.132       |             | 100       | 1895                  | 234              | 0.123   | 0.123      |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
| Pak Wo Road                        | WB           | LT<br>SA         | B1<br>B2          | 2            | 3.00            | 15.0                                |                           | 100       | 1741<br>2055          | 416<br>313            | 0.239       | 0.239       | 100       | 1741<br>2055          | 377<br>244       | 0.217   | 0.217      |
|                                    |              | SA+RT            | B3                | 2            | 3.00            | 20.0                                |                           | 0         | 2055                  | 340                   | 0.132       |             | 7         | 2044                  | 248              | 0.119   |            |
|                                    |              | RT               | B4                | 2            | 3.00            | 15.0                                |                           | 100       | 1868                  | 258                   | 0.138       |             | 100       | 1868                  | 216              | 0.116   |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
| Yat Ming Road                      | SB           | LT               | C1                | 3            | 3.40            | 15.0                                |                           | 100       | 1777                  | 225                   | 0.127       | 0.127       | 100       | 1777                  | 210              | 0.118   | 0.118      |
|                                    |              | LT+SA            | C2                | 3            | 3.30            | 20.0                                |                           | 40        | 2024                  | 256                   | 0.126       |             | 33        | 2035                  | 240              | 0.118   |            |
|                                    |              | RT               | C3                | 3            | 3.30            | 15.0                                |                           | 100       | 1895                  | 49                    | 0.026       |             | 100       | 1895                  | 20               | 0.011   |            |
| Wah Ming Roa                       | ad NP        | 1 T±6 V          | D1                | 4            | 3.40            | 15.0                                |                           | 100       | 1777                  | 204                   | 0.115       | 0.115       | 100       | 1777                  | 157              | 0.000   | 0.088      |
| vvan wiing Koa                     | מע ואט       | SA+RT            | D1<br>D2          | 4            | 3.40            | 25.0                                |                           | 48        | 1777<br>2027          | 198                   | 0.115       | 0.115       | 47        | 2028                  | 157<br>148       | 0.088   | 0.000      |
|                                    |              | RT               | D3                | 4            | 3.30            | 20.0                                |                           | 100       | 1940                  | 158                   | 0.081       |             | 100       | 1940                  | 113              | 0.073   |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
| pedestrian pha                     | ase          |                  | E(P)              | 1            |                 | min c                               | rossing                   | time =    | 6                     | sec                   | GM +        | 12          | sec F     | GM =                  | 18               | sec     |            |
|                                    |              |                  | F(P)              | 2,3,4        |                 |                                     | rossing                   |           | 6                     |                       | GM +        | 12          |           | GM =                  | 18               | sec     |            |
|                                    |              |                  | G(P)              | 3            |                 | min c                               | rossing                   | time =    | 5                     | sec                   | GM +        | 8           | sec F     | GM =                  | 13               | sec     |            |
|                                    |              |                  | H(P)              | 1,2,4        |                 | min c                               | rossing                   | time =    | 8                     | sec                   | GM+         | 15          | sec F     | GM =                  | 23               | sec     |            |
|                                    |              |                  | I(P)              | 2            |                 | min c                               | rossing                   | time =    | 5                     | sec                   | GM +        | 7           | sec F     | GM =                  | 12               | sec     |            |
|                                    |              |                  | J(P)              | 1,3,4        |                 | min c                               | rossing                   | time =    | 9                     | sec                   | GM +        | 17          | sec F     | GM =                  | 26               | sec     |            |
|                                    |              |                  | K(P)              | 4            |                 |                                     | rossing                   |           | 5                     |                       | GM +        | 6           |           | GM =                  | 11               | sec     |            |
|                                    |              |                  | L(P)              | 2,3,4        |                 |                                     | rossing                   | time =    | 5                     |                       | GM +        | 10          |           | GM =                  | 15               | sec     |            |
| AM Traffic Flow (pcu/hr            | r)           |                  | N                 | РМ ТГАПІСТ   | low (pcu/hr)    |                                     |                           |           | N                     |                       |             | 25) S=      |           |                       | Note:            |         |            |
| 49                                 | 321          |                  | T                 |              | 20              | 7                                   | 315                       |           |                       | S <sub>M</sub> =S÷(1· |             |             |           | +(1+1.5f/r)           |                  |         |            |
| 30                                 | 160          | 258              |                   |              | 29              | 135                                 |                           | 233       |                       |                       |             | ak Hour     |           | ak Hour               | l                |         |            |
| 329                                | 9 65         | 3 4              | _                 |              | 315             |                                     | 475 -                     | . 1       | _                     |                       | 1+2+3+4     |             | 1+2+3+4   |                       |                  |         |            |
| 251                                | 5 00         | 416              |                   | 1            | 234             |                                     | 470                       | +         |                       | Sum y                 | 0.570<br>27 |             | 0.547     |                       |                  |         |            |
|                                    | 104          | 410              |                   |              |                 | 78                                  |                           | 377       |                       | L (s)                 | 120         |             | 27<br>120 |                       |                  |         |            |
| 204                                | 252          |                  |                   |              | 157             | $\leftarrow$                        | 183                       |           |                       | practical y           | 0.698       |             | 0.698     |                       |                  |         |            |
|                                    |              |                  |                   |              |                 |                                     |                           |           |                       | R.C. (%)              | 22%         |             | 28%       |                       |                  |         |            |
| 1                                  | H(n)         | 2                |                   | H(a)         |                 | 3                                   | G(n)                      | Ш         |                       | 4                     |             | H(n)        |           |                       |                  |         |            |
|                                    | <b>H</b> (p) |                  |                   | <b>H</b> (p) | (p)             |                                     | <b>◆&gt;</b>              | C3 C2 C1  |                       |                       |             | <b>◆</b>    |           |                       |                  |         |            |
| <b>1</b> A1                        |              | <b>▲</b><br>F(p) |                   |              | ₽4 <b>†</b>     | F(p)                                |                           |           |                       | <b>≜</b><br>F(p)      |             |             |           |                       |                  |         |            |
| A2<br>A3                           | J(p)         | '                |                   |              | B3.<br>B2.<br>■ | '                                   |                           |           | J(p)                  | '                     |             |             | J(p)      |                       |                  |         |            |
| E(p)                               | •            |                  |                   |              | B1 <b></b> ₩    |                                     |                           |           | *                     |                       | D1 D2 D3    |             | •         |                       |                  |         |            |
| <b>◆</b> L(p)                      | <b>+</b>     |                  | ← <sup>L(p)</sup> |              |                 |                                     | <b>←</b> 1(0) <b>&gt;</b> | -         |                       |                       | 111         | ◆ R(b)r - ▶ |           |                       |                  |         |            |
| AM<br>G=                           | I/G =        | 9 G=             |                   | I/G =        | 6               | G =                                 |                           | I/G =     | 7                     | G =                   |             | I/G =       | 9         | G =                   |                  | I/G =   |            |
| PM<br>G=                           |              |                  |                   |              |                 |                                     |                           |           |                       |                       |             |             |           |                       |                  |         |            |
| G=                                 | I/G =        | 9 G=             |                   | I/G =        | 6               | G =                                 |                           | I/G =     | 7                     | G =                   |             | I/G =       | 9         | G =                   |                  | I/G =   |            |

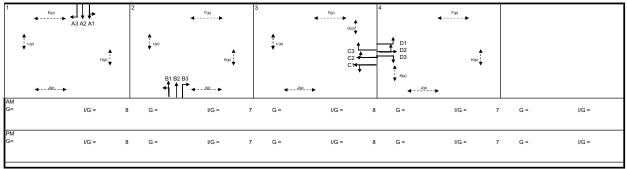
 Junction:
 Pak Wo Road / Yat Ming Road / Wah Ming Road
 Job Number:
 J7411

 Scenario:
 Existing Condition
 J5 - P. 1

Design Year: 2025 Designed By: MCY Checked By: WCH Date: 15 August 2025

| Design real. 2025        | Designi | еи Бу.       |       | IVICT         |            | -                     | Checke    | зи Бу.                |                             | WCH          |            |           | Date.                 | 157                         | August 2 | 1025     |
|--------------------------|---------|--------------|-------|---------------|------------|-----------------------|-----------|-----------------------|-----------------------------|--------------|------------|-----------|-----------------------|-----------------------------|----------|----------|
| Approach                 |         | Phase        | Stage | Width (m)     | Radius (m) | % Up-hill<br>Gradient | Turning % | Sat. Flow<br>(pcu/hr) | AM Peak<br>Flow<br>(pcu/hr) | y value      | Critical y | Turning % | Sat. Flow<br>(pcu/hr) | PM Peak<br>Flow<br>(pcu/hr) | y value  | Critical |
| Pak Wo Road SB           | LT+SA   | A1           | 1     | 3.50          | 15.0       | Gradient              | 61        | 1852                  | 291                         | 0.157        | 0.157      | 61        | 1852                  | 266                         | 0.144    | 0.14     |
|                          | SA      | A2           | 1     | 3.00          |            |                       |           | 2055                  | 322                         | 0.157        |            |           | 2055                  | 296                         | 0.144    |          |
|                          | RT      | А3           | 1     | 3.00          | 20.0       |                       | 100       | 1912                  | 294                         | 0.154        |            | 100       | 1912                  | 227                         | 0.119    |          |
| Pak Wo Road NB           | LT+SA   | B1           | 2     | 3.50          | 15.0       |                       | 18        | 1930                  | 288                         | 0.149        | 0.149      | 9         | 1947                  | 188                         | 0.097    | 0.09     |
|                          | SA      | B2           | 2     | 3.40          |            |                       |           | 2095                  | 313                         | 0.149        |            |           | 2095                  | 202                         | 0.096    |          |
|                          | RT      | B3           | 2     | 3.40          | 20.0       |                       | 100       | 1949                  | 132                         | 0.068        |            | 100       | 1949                  | 113                         | 0.058    |          |
| Yat Ming Road WB         | LT+SA   | C1           | 3     | 3.50          | 15.0       |                       | 92        | 1799                  | 84                          | 0.047        | 0.047      | 83        | 1814                  | 63                          | 0.035    | 0.03     |
|                          | SA+RT   | C2           | 3     | 3.00          | 25.0       |                       | 34        | 2014                  | 94                          | 0.047        |            | 52        | 1993                  | 69                          | 0.035    |          |
|                          | RT      | C3           | 3     | 3.00          | 20.0       |                       | 100       | 1912                  | 88                          | 0.046        |            | 100       | 1912                  | 66                          | 0.035    |          |
| Wah Ming Road EB         | LT      | D1           | 4     | 3.40          | 15.0       |                       | 100       | 1777                  | 121                         | 0.068        | 0.068      | 100       | 1777                  | 70                          | 0.039    | 0.03     |
|                          | LT+SA   | D2           | 4     | 3.30          | 15.0       |                       | 90        | 1913                  | 131                         | 0.068        |            | 88        | 1916                  | 75                          | 0.039    |          |
|                          | RT      | D3           | 4     | 3.30          | 20.0       |                       | 100       | 1940                  | 49                          | 0.025        |            | 100       | 1940                  | 43                          | 0.022    |          |
|                          |         |              |       |               |            |                       |           |                       |                             |              |            |           |                       |                             |          |          |
|                          |         |              |       |               |            |                       |           |                       |                             |              |            |           |                       |                             |          |          |
|                          |         |              |       |               |            |                       |           |                       |                             |              |            |           |                       |                             |          |          |
|                          |         |              |       |               |            |                       |           |                       |                             |              |            |           |                       |                             |          |          |
| pedestrian phase         |         | E(p)         | 1     |               | min c      | rossing               | time =    | 5                     | sec                         | GM+          | 9          | sec F     | GM =                  | 14                          | sec      |          |
|                          |         | F(p)         | 2,3,4 |               | min c      | rossing               | time =    | 5                     | sec                         | GM +         | 10         | sec F     | GM =                  | 15                          | sec      |          |
|                          |         | G(p)         | 3     |               |            | rossing               |           | 5                     |                             | GM +         | 6          |           | GM =                  | 11                          | sec      |          |
|                          |         | H(p)         | 1,2,4 |               |            | rossing               |           | 5<br>5                |                             | GM +<br>GM + | 10<br>6    |           | GM =                  | 15<br>11                    | sec      |          |
|                          |         | J(p)         | 1,3,4 |               |            | rossing<br>rossing    |           | 5                     |                             | GM +         | 10         |           | GM =<br>GM =          | 15                          | sec      |          |
|                          |         | J(p)<br>K(p) | 4     |               |            | rossing               |           | 5                     |                             | GM +         | 6          |           | GM =                  | 11                          | sec      |          |
|                          |         | L(p)         | 1,2,3 |               |            | rossing               |           | 5                     |                             | GM+          | 10         |           | GM =                  | 15                          | sec      |          |
| AM Traffic Flow (pcu/hr) |         | N<br>↑       |       | Flow (pcu/hr) |            | 447                   |           | N                     | S=1940+                     | 100(W–3.:    | 25) S=     | 2080+100  |                       | Note:                       |          |          |





 Junction:
 Pak Wo Road / Yat Ming Road / Wah Ming Road
 Job Number:
 J7411

 Scenario:
 Without Proposed EV Mobility City
 J5 - P. 2

Design Year: 2034 Designed By: MCY Checked By: WCH Date: 15 August 2025

| Fig.   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   | Design Year: 2034        | Design | ed By:       |              | MCY          |              | -                     | Checke    | ed By:                       |                       | WCH                               |            |           | Date:       | 15 /  | August 2 | 2025       |
|---|--------------------------|--------|--------------|--------------|--------------|--------------|-----------------------|-----------|------------------------------|-----------------------|-----------------------------------|------------|-----------|-------------|-------|----------|------------|
| Pak Wo Road SB  | i                        |        |              |              |              |              |                       |           |                              | ****                  |                                   |            |           |             | DMD 1 |          |            |
| Pack Wo Road SB  LT-SA At 1 1 3.50 15.0 48 482 401 0.217 0.217 47 1877 362 0.193 0.193  RT A3 1 3.00 20.0 100 1912 384 0.201 100 1912 205 386 0.193  Pak Wo Road NB  LT-SA B1 2 3.50 15.0 14 1938 403 0.206 0.208 7 1951 267 0.137 0.137  RT B3 2 3.40 20.0 150 1949 142 0.073 100 1949 121 0.065 27 0.137 0.137  RT B3 2 3.40 20.0 100 1994 142 0.073 100 1994 121 0.065 27 0.039  Yet Ming Road WB  LT-SA C1 3 3.50 15.0 86 1989 97 0.054 78 1823 72 0.039  RT C3 3 3.00 20.0 100 1912 103 0.054 0.054 100 1912 76 0.040 0.040  Wah Ming Road EB  LT D1 4 3.40 13.0 100 1953 142 0.074 88 1916 83 0.043  LT+SA D2 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 3.30 20.0 100 1940 153 0.077 100 1950 175 860 0.040 0.040  RT D3 4 3.30 20.0 100 1940 153 0.077 100 1940 175 860 0.044 0.044 0.040  Wah Ming Road EB  LT D1 4 3.40 13.0 100 1953 142 0.074 88 1916 83 0.043  RT D3 4 3.30 20.0 100 1940 153 0.077 100 1950 175 860 0.043 0.043  RT D3 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5   | Approach                 |        | Phase        | Stage        | Width (m)    | Radius (m)   |                       | Turning % |                              | Flow                  | y value                           | Critical y | Turning % |             | Flow  | y value  | Critical y |
| SA A2 1 1 3.00 20 20.0 100 1912 384 02.01 100 1912 222 0155 155 176 187 187 187 187 187 187 187 187 187 187   | Dok We Bood SP           | LTICA  | Λ1           | 1            | 2 50         | 15.0         | Gradient              | 40        |                              |                       | 0.217                             | 0.217      | 47        |             |       | 0.102    | 0.402      |
| RT A3 1 3.00 20.0 100 1912 384 0.201 100 1912 222 0.163   Pak Wo Road NB  | Pak WO Road 35           |        |              |              |              | 15.0         |                       | 40        |                              |                       |                                   | 0.217      | 47        |             |       |          | 0.193      |
| Pak Wo Road NB  |                          |        |              |              |              | 20.0         |                       | 400       |                              |                       |                                   |            | 100       |             |       |          |            |
| SA B2 2 3.40  |                          | KI     | A3           | 1            | 3.00         | 20.0         |                       | 100       | 1912                         | 384                   | 0.201                             |            | 100       | 1912        | 292   | 0.153    |            |
| SA B2 2 3.40 20.0 100 1949 142 0.073 100 1949 121 0.062    Nat Ming Road WB LT-SA C1 3 3.50 15.0 86 1809 97 0.054   RT C2 3 3 3.00 25.0 44 2002 108 0.054   RT C3 3 3.00 25.0 100 1912 103 0.054   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 100 1912 103 0.054   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 100 1912 103 0.054   RT C3 3 3.00 15.0 0 0 0 1912 103 0.054   RT C3 3 3.00 15.0 0 0 0 1913 102 0.075   RT C3 3 3.00 100 1753 100 1753 100 1914   RT C3 3 3.00 100 1912 103 100 1914   RT C3 3 3.00 100 1912 103 100 1914   RT C3 3 3.00 100 1912 103 100 1914   RT C3 3 3.00 100 1912 103 100 1914   RT C3 3 3.00 100 1912 103 100 1914   RT C3 3 3.00 100 1912 103 100 1914   RT C3 3 3.00 100 1913 100 1912 100 1914   RT C3 3 3 3 0 0.00 1 100 1912 100 1912 100 1914   RT C3 3 3 0.00 100 1 100 1912 100 1 10  | Dalawa Baad NB           | 1.7.04 | D4           |              | 0.50         | 45.0         |                       | 44        | 4000                         | 400                   | 0.000                             | 0.000      |           | 4054        | 007   | 0.407    | 0.407      |
| RT   B3   2   3.40   20.0   100   1949   142   0.073   100   1949   121   0.082   | Pak Wo Road NB           |        |              |              |              | 15.0         |                       | 14        |                              |                       |                                   | 0.208      |           |             |       |          | 0.137      |
| Yat Ming Road WB  |                          |        |              |              |              | 00.0         |                       | 400       |                              |                       |                                   |            | 400       |             |       |          |            |
| SA-RT C2 3 3 3.00 25.0 44 2002 108 0.054 0.054 100 1984 78 0.039 0.040 0  |                          | - RI   | B3           | 2            | 3.40         | 20.0         |                       | 100       | 1949                         | 142                   | 0.073                             |            | 100       | 1949        | 121   | 0.062    |            |
| SA-RT C2 3 3.00 25.0 44 2002 108 0.054 0.054 100 1984 78 0.039 0.040 0.0  | V-4 Min in Dirichland    | 1.7.04 | 04           | _            | 0.50         | 45.0         |                       |           | 4000                         | 0.7                   | 0.054                             |            | 70        | 4000        | 70    | 0.000    |            |
| RT C3 3 3.00 2.00 100 1912 103 0.054 0.054 100 1912 76 0.040 0.040  Wah Ming Road EB LT D1 4 3.40 13.0 100 1753 131 0.075 0.075 100 1753 75 0.043 0.043  LT+SA D2 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 3.30 20.0 100 1940 53 0.027 100 1940 47 0.024  RT D3 4 3.30 20.0 100 1940 53 0.027 100 1940 47 0.024  Pedestrian phase 690 1 min crossing time = 5 sec GM + 9 sec FCM = 11 sec GM + 10 sec FCM = 15 sec GM + 10 sec FCM = 11 sec GM   | Yat Ming Road WB         |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| Wah Ming Road EB LT D1 4 3.40 13.0 100 1753 131 0.075 0.075 100 1753 75 0.043 0.043   LT+SA D2 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043   RT D3 4 3.30 20.0 100 1940 53 0.027 100 1940 47 0.024   RT D3 4 3.30 20.0 100 1940 53 0.027 100 1940 47 0.024   RT D3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| LT+SA D2 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RTI D3 4 3.30 20.0 100 1940 53 0.027 100 1940 47 0.024  Pedestrian phase E <sub>E(B)</sub> 1 1 min crossing time = 5 sec GM+ 9 sec FGM = 14 sec GPM = 15 sec GM+ 10 sec FGM = 11 sec GPM = 15 sec GM+ 10 sec FGM = 15 sec GM+ 10 sec FGM = 15 sec GM+ 10 sec FGM = 1  |                          | RT     | C3           | 3            | 3.00         | 20.0         |                       | 100       | 1912                         | 103                   | 0.054                             | 0.054      | 100       | 1912        | 76    | 0.040    | 0.040      |
| LT+SA D2 4 3.30 15.0 90 1913 142 0.074 88 1916 83 0.043  RT D3 4 3.30 20.0 100 1940 53 0.027 100 1940 47 0.024  Pedestrian phase Egp 1 1 min crossing time = 5 sec GM + 9 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 10 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 10 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 10 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 10 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 2.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 15 sec GM = 10 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 sec GM + 6 sec FGM = 11 sec Gp 3.34 min crossing time = 5 se  |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| Pedestrian phase  | vvah Ming Road EB        |        |              |              |              |              |                       |           |                              |                       |                                   | 0.075      |           |             |       |          | 0.043      |
| pedestrian phase  E <sub>(0)</sub> 1 min crossing time = 5 sec GM + 9 sec FGM = 14 sec  F <sub>(0)</sub> 2,3.4 min crossing time = 5 sec GM + 10 sec FGM = 115 sec  G <sub>(0)</sub> 3 min crossing time = 5 sec GM + 10 sec FGM = 115 sec  H <sub>(0)</sub> 1,2.4 min crossing time = 5 sec GM + 10 sec FGM = 115 sec  H <sub>(0)</sub> 2 min crossing time = 5 sec GM + 10 sec FGM = 115 sec  H <sub>(0)</sub> 1,3.4 min crossing time = 5 sec GM + 10 sec FGM = 11 sec  H <sub>(0)</sub> 1,3.4 min crossing time = 5 sec GM + 10 sec FGM = 11 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 11 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 11 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 5 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 15 sec GM + 10 sec FGM = 15 sec  H <sub>(0)</sub> 1,2.3 min crossing time = 15 sec GM + 10 sec FGM = 15 |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| Fig.   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          | RT     | D3           | 4            | 3.30         | 20.0         |                       | 100       | 1940                         | 53                    | 0.027                             |            | 100       | 1940        | 47    | 0.024    |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| Fig.   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| F(p)   2,3,4   min crossing time   5   sec GM + 10   sec FGM   15   sec   |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| Cop   3   | pedestrian phase         |        | E(p)         |              |              | min c        | rossing               | time =    |                              |                       |                                   | 9          |           |             |       | sec      |            |
| H(p) 1,2,4 min crossing time = 5 sec GM + 10 sec FGM = 15 sec M + 10 sec FGM = 11 sec M + 10 sec FGM = 15 sec M + 10 sec FGM =  |                          |        | F(p)         |              |              | min c        | rossing               | time =    |                              |                       |                                   |            |           |             |       | sec      |            |
| No   1   1   1   1   1   1   1   1   1  |                          |        | G(p)         |              |              | min c        | rossing               | time =    |                              |                       |                                   | 6          |           |             |       | sec      |            |
| Jp  |                          |        | H(p)         |              |              | min c        | rossing               | time =    | 5                            |                       |                                   | 10         | sec F     | GM =        | 15    | sec      |            |
| K(p)   4   min crossing time =   5   sec GM +   6   sec FGM =   11   sec  |                          |        | l(p)         | 2            |              | min c        | rossing               | time =    | 5                            | sec                   | GM +                              | 6          | sec F     | GM =        | 11    | sec      |            |
| L(p)   1,2,3   min crossing time   5   sec GM + 10   sec FGM = 15   sec   |                          |        | J(p)         | 1,3,4        |              | min c        | rossing               | time =    | 5                            | sec                   | GM +                              | 10         | sec F     | GM =        | 15    | sec      |            |
| AM Traffic Flow (pcultr)  384  195  462  159  466  148  75  144  75  10  47  56  123  58=1940+100(W-3.25)  5=2080+100(W-3.25)   |                          |        | K(p)         | 4            |              |              |                       |           |                              |                       |                                   | 6          | sec F     | GM =        | 11    | sec      |            |
| 384 + 195   |                          |        | L(p)         | 1,2,3        |              | min c        | rossing               | time =    | 5                            | sec                   | GM +                              | 10         | sec F     | GM =        | 15    | sec      |            |
| 384 195   | AM Traffic Flow (pcu/hr) |        | N            | PM Traffic F | low (pcu/hr) |              |                       |           | N                            | S=1940+               | 100(W-3.2                         | 25) S=     | 2080+100  | D(W-3.25)   | Note: |          |            |
| AM Peak Hour   PM Peak Hour   | 384 + 195                |        |              |              | 292          | $\leftarrow$ | 159                   |           |                              | S <sub>M</sub> =S÷(1- | +1.5f/r)                          | $S_M$      | =(S-230)- | ÷(1+1.5f/r) |       |          |            |
| 259 150 148 123 123 124344 1424344 1553 0.412 153 142 156 157 142 158 159 159 159 159 159 159 159 159 159 159   | 462                      |        | '            |              | 202          | *            | .00                   |           | 1                            |                       |                                   | ak Hour    | PM Pe     | ak Hour     | 1     |          |            |
| 14 75   |                          | 150    |              |              | 148          | 400          |                       | 123       |                              |                       | 1+2+3+4                           |            | 1+2+3+4   |             |       |          |            |
| 53 83 47 56 L(s) 26 26 C(s) 110 110 practically 0.687 0.687 RC. (%) 24% 67%   | 14 75                    | •      | _            |              | 10           |              | 47 🔻                  |           | _                            | Cum v                 |                                   |            |           |             | l     |          |            |
| 782<br>57<br>142<br>18<br>121<br>100<br>110<br>110<br>110<br>110<br>110<br>110  | ↓ <sub>53</sub>          | ,<br>, |              | +            | 47           |              |                       | 56        |                              |                       |                                   |            |           |             | l     |          |            |
| Practically 0.007 R.C. (%) 24% 67%  R.C. (%) 24% 67%  A3 A2 A1  F(p)  A4 A2 A1  F(p)  A5 A2 A1  F(p)  | 782                      | 782    |              |              |              |              |                       | 30        |                              |                       |                                   |            |           |             |       |          |            |
| RC. (%) 24% 67%   | 57 🕕 142                 |        |              |              | 18           | $\leftarrow$ | 121                   |           |                              |                       |                                   |            |           |             |       |          |            |
| A3 A2 A1    C3  |                          |        |              |              |              |              |                       |           |                              |                       |                                   |            |           |             |       |          |            |
| High Liph Liph Liph C3 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1   |                          | In .   |              |              |              | I<br>Ia      |                       |           |                              | R.U. (%)              | <u>∠</u> + /0                     |            | 07 /0     |             |       |          |            |
| High Liph Liph Liph C3 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1   | 1 E(p)                   | 2      |              | F(p)         |              | 3            |                       | F(p)      |                              | 4                     |                                   | F(p)       |           |             |       |          |            |
| Min   | A3 A2 A1                 |        |              |              |              |              |                       |           | G(p)                         |                       |                                   |            |           |             |       |          |            |
| B1 B2 B3  | ↓ L(p)                   | Ŭ L(p) |              |              |              | L(p)         |                       |           | сз ू                         | D1                    |                                   |            | •         |             |       |          |            |
| ←30\> ←30\> ←30\> ←30\>   | H(p) ₩                   |        |              |              | H(p)         |              |                       |           | C2 <b>₹</b><br>C1 <b>∢</b> 1 | D3                    |                                   |            | H(p) ₩    |             |       |          |            |
| AM  |                          |        | B1 B2 B3     |              |              |              |                       |           | •                            | ₩ K(p)                |                                   |            |           |             |       |          |            |
| vun<br>G=   |                          |        | <b>↑</b> [ ] | < J(₽) →     |              |              | 4 ¬ <sub>1</sub> (5)▶ |           |                              |                       | <b>←</b> <sup>J(p)</sup> <b>→</b> |            |           |             |       |          |            |
|   | M<br>=                   |        |              |              |              |              |                       |           |                              |                       |                                   | I/G =      | 7         | G =         |       | I/G =    |            |

 Junction:
 Pak Wo Road / Yat Ming Road / Wah Ming Road
 Job Number:
 J7411

 Scenario:
 With Proposed EV Mobility City
 J5 - P. 3

Design Year: 2034 Designed By: MCY Checked By: WCH Date: 15 August 2025

| Design Year: 2034                            | Design   | ed By:      |              | MCY          |              |                | Checke         | d By:  |                       | WCH                 |                |           | Date:            | 15 /            | August 2 | 2025       |
|--|----------|-------------|--------------|--------------|--------------|----------------|----------------|--|-----------------------|---------------------|----------------|-----------|------------------|-----------------|----------|------------|
|  |          |             |              |              |              |                |                |  | ****                  |                     |                |           |                  | DIAD 1          |          |            |
| Approach                                     |          | Phase       | Stage        | Width (m)    | Radius (m)   | % Up-hill      | Turning %      | Sat. Flow  | AM Peak<br>Flow       | y value             | Critical y     | Turning % | Sat. Flow        | PM Peak<br>Flow | y value  | Critical y |
| Pak Wo Road SB                               | LT+SA    | A1          | 1            | 3.50         | 15.0         | Gradient       | 48             | (pcu/hr)<br>1852   | (pcu/hr)<br>407       | 0.220               | 0.220          | 46        | (pcu/hr)<br>1879 | (pcu/hr)<br>366 | 0.195    | 0.195      |
| Fak Wo Road Sb                               | SA       | A2          | 1            | 3.00         | 13.0         |                | 40             | 2055   | 451                   | 0.219               | 0.220          | 40        | 2055             | 401             | 0.195    | 0.193      |
|  | RT       | A3          | 1            | 3.00         | 20.0         |                | 100            | 1912   | 384                   | 0.219               |                | 100       | 1912             | 292             | 0.153    |            |
|  | IXI      | 7.5         | '            | 3.00         | 20.0         |                | 100            | 1312   | 304                   | 0.201               |                | 100       | 1312             | 232             | 0.155    |            |
| Pak Wo Road NB                               | LT+SA    | B1          | 2            | 3.50         | 15.0         |                | 14             | 1938   | 407                   | 0.210               | 0.210          | 7         | 1951             | 272             | 0.139    | 0.139      |
| FAK WO ROAU ND                               | SA       | B2          | 2            | 3.40         | 13.0         |                | 14             | 2095   | 439                   | 0.210               | 0.210          |           | 2095             | 293             | 0.139    | 0.139      |
|  | RT       | B3          | 2            | 3.40         | 20.0         |                | 100            | 1949   | 142                   | 0.210               |                | 100       | 1949             | 121             | 0.062    |            |
|  | 131      |             |              | 3.40         | 20.0         |                | 100            | 1343   | 142                   | 0.073               |                | 100       | 1343             | 121             | 0.002    |            |
| Yat Ming Road WB                             | LT+SA    | C1          | 3            | 3.50         | 15.0         |                | 86             | 1809   | 97                    | 0.054               |                | 78        | 1823             | 72              | 0.039    |            |
| Tat Willing Road WD                          | SA+RT    | C2          | 3            | 3.00         | 25.0         |                | 44             | 2002   | 108                   | 0.054               |                | 60        | 1984             | 78              | 0.039    | 0.039      |
|  | RT       | C3          | 3            | 3.00         | 20.0         |                | 100            | 1912   | 103                   | 0.054               | 0.054          | 100       | 1912             | 76              | 0.039    | 0.000      |
|  | KI       |             | 3            | 3.00         | 20.0         |                | 100            | 1912   | 103                   | 0.034               | 0.054          | 100       | 1912             | 70              | 0.040    |            |
| Mah Mina Bood EB                             | 1.7      | D1          | 4            | 2 40         | 12.0         |                | 100            | 1752   | 121                   | 0.075               | 0.075          | 100       | 1752             | 75              | 0.043    | 0.042      |
| Wah Ming Road EB                             | LT+SA    | D1          | 4            | 3.40         | 13.0         |                | 100            | 1753   | 131                   |                     | 0.075          | 100       | 1753             | 75              | 0.043    | 0.043      |
|  |          | D2          | 4            | 3.30         | 15.0         |                | 90             | 1913   | 142                   | 0.074               |                | 88        | 1916             | 83              | 0.043    |            |
|  | RT       | D3          | 4            | 3.30         | 20.0         |                | 100            | 1940   | 53                    | 0.027               |                | 100       | 1940             | 47              | 0.024    |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
| pedestrian phase                             |          | E(p)        | 1            |              |              | rossing        |                | 5  | sec (                 |                     | 9              |           | GM =             | 14              | sec      |            |
|  |          | F(p)        | 2,3,4        |              |              | rossing        |                | 5  | sec (                 |                     | 10             |           | GM =             | 15              | sec      |            |
|  |          | G(p)        | 3            |              |              | rossing        |                | 5  | sec (                 |                     | 6              |           | GM =             | 11              | sec      |            |
|  |          | H(p)        | 1,2,4        |              |              | rossing        |                | 5  | sec (                 |                     | 10             |           | GM =             | 15              | sec      |            |
|  |          | l(p)        | 2            |              |              | rossing        |                | 5  |                       | GM +                | 6              |           | GM =             | 11              | sec      |            |
|  |          | J(p)        | 1,3,4        |              |              | rossing        |                | 5  |                       | GM +                | 10             |           | GM =             | 15              | sec      |            |
|  |          | K(p)        | 4            |              |              | rossing        |                | 5  |                       | 3M +                | 6              |           | GM =             | 11              | sec      |            |
|  |          | L(p)        | 1,2,3        |              | min c        | rossing        | time =         | 5  | sec (                 | GM +                | 10             | sec F     | GM =             | 15              | sec      |            |
| AM Traffic Flow (pcu/hr)                     |          | N           | PM Traffic F | low (pcu/hr) |              |                |                | N  | S=1940+               | 100(W-3.2           | 25) S=         | 2080+100  | )(W-3.25)        | Note:           |          |            |
| 384 ← 195                                    |          | $\uparrow$  |              | 292          | +            | 159            |                | $\uparrow$   | S <sub>M</sub> =S÷(1+ | -1.5f/r)            | S <sub>M</sub> | =(S-230)- | +(1+1.5f/r)      |                 |          |            |
| <b>↓</b><br>474                              |          | '           |              |              | ↓<br>475     |                |                | '  |                       | AM Pe               | ak Hour        | PM Pe     | ak Hour          |                 |          |            |
| 259  | 150      |             |              | 148          |              |                | 123            |  |                       | 1+2+3+4             |                | 1+2+3+4   |                  |                 |          |            |
| 14 75  | <b>←</b> | _           |              | → 10         |              | 47 🔻           | 1              | •  | Sum y                 | 0.558               |                | 0.416     |                  |                 |          |            |
| <sup>♦</sup> 53                              | .↓<br>83 |             | +            | 47           |              |                | <b>↓</b><br>56 |  | L (s)                 | 26                  |                | 26        |                  |                 |          |            |
| 789  | 789      |             |              |              |              |                |                |  | C (s)                 | 110                 |                | 110       |                  |                 |          |            |
| 57 142                                       |          |             |              | 18           | $\leftarrow$ | 121            |                |  | practical y           | 0.687               |                | 0.687     |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  | R.C. (%)              | 23%                 |                | 65%       |                  |                 |          |            |
| 1 111  | 12       |             |              |              | 3            |                |                |  | 14                    |                     |                | -3,0      |                  |                 |          |            |
| E(p) A3 A2 A1                                | 2        |             | <b>←</b>     |              | 3            |                | F(p)           |  | 4                     |                     | <b>←</b>       |           |                  |                 |          |            |
| A3 A2 A1                                     |          |             |              |              |              |                |                | G(p)   | .                     |                     |                |           |                  |                 |          |            |
| L(p)   | ↓ L(p)   |             |              | •            | L(p)         |                |                | С3 ू   | D1                    |                     |                | •         |                  |                 |          |            |
| H(p)   |          |             |              | H(p)         |              |                |                | C2 <del>▼</del> C1 <del>1</del> C1 | D3                    |                     |                | H(p) ₩    |                  |                 |          |            |
|  |          | B1 B2 B3    |              |              |              |                |                | •  | ₩ K(p)                |                     |                |           |                  |                 |          |            |
|  |          |             |              |              |              |                |                |  |                       |                     |                |           |                  |                 |          |            |
| <b>4</b> <sup>J(Q)</sup> <b>▶</b> AM G= VG = |          | <b>⁴</b> ∏′ | ← J(E) ►     |              |              | <b>←</b> ∃(E)▶ |                |  |                       | < <sup>J(p)</sup> → |                |           |                  |                 |          |            |

 Junction:
 Wo Hop Shek Interchange
 Job Number:
 J7411

 Scenario:
 Existing Condition
 J6 - P. 1

 Design Year:
 2025
 Designed By:
 MCY
 Checked By:
 WCH
 Date:
 15 August 2025

| Design Year: 2025        | Design           | ed By:        |              | MCY             |             | -         | Checke    | ed By:       |                 | WCH      |            | -         | Date:        | 15 /            | August 2 | 2025       |
|--------------------------|------------------|---------------|--------------|-----------------|-------------|-----------|-----------|--------------|-----------------|----------|------------|-----------|--------------|-----------------|----------|------------|
| Approach                 |                  | Phase         | Stage        | Width (m)       | Radius (m)  | % Up-hill | Turning % |              | AM Peak<br>Flow | y value  | Critical y | Turning % |              | PM Peak<br>Flow | y value  | Critical y |
| Dok We Bood NB           | SA               | Λ1            |              | 2 20            |             | Gradient  |           | (pcu/hr)     | (pcu/hr)<br>404 | 0.208    |            |           | (pcu/hr)     | (pcu/hr)        | 0.102    |            |
| Pak Wo Road NB           | SA               | A1<br>A2      | 1            | 3.30            |             |           |           | 1945<br>2095 | 435             | 0.208    |            |           | 1945<br>2095 | 355<br>382      | 0.183    |            |
|                          | 0/1              | ,,,,          | ·            | 0.10            |             |           |           | 2000         | 100             | 0.200    |            |           | 2000         | 002             | 0.102    |            |
| Fanling Highway          | LT               | B1            | 2,3          | 4.00            | 30.0        |           | 100       | 1919         | 407             | 0.212    |            | 100       | 1919         | 522             | 0.272    |            |
| Slip Road NB             | LT               | B2            | 2,3          | 4.00            | 35.0        |           | 100       | 2066         | 438             | 0.212    |            | 100       | 2066         | 562             | 0.272    |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
| Pak Wo Road NB           | SA               | C1            | 1,2          | 3.00            |             |           |           | 1915         | 535             | 0.279    |            |           | 1915         | 579             | 0.302    |            |
|                          | SA               | C2            | 1,2          | 3.00            |             |           |           | 2055         | 574             | 0.279    |            |           | 2055         | 621             | 0.302    |            |
|                          | SA               | C3            | 1,2          | 3.00            |             |           |           | 2055         | 575             | 0.280    |            |           | 2055         | 621             | 0.302    |            |
| Pak Wo Road NB           | RT               | D3            | 1,3          | 3.00            | 15.0        |           | 100       | 1868         | 621             | 0.332    | 0.332      | 100       | 1868         | 573             | 0.307    | 0.307      |
|                          |                  | -             | ,-           |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
| Jockey Club Road SB      | SA               | E1            | 2            | 4.50            |             |           |           | 2065         | 499             | 0.242    | 0.242      |           | 2065         | 498             | 0.241    | 0.241      |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
| Pak Wo Road SB           | LT               | F1            | 1,2          | 3.40            | 20.0        |           | 100       | 1819         | 237             | 0.130    |            | 100       | 1819         | 183             | 0.101    |            |
|                          | SA               | F2            | 1,2          | 3.30            |             |           |           | 2085         | 262             | 0.126    |            |           | 2085         | 315             | 0.151    |            |
|                          |                  |               | _            |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
| Wo Hing Road WB          | RT               | G1            | 3            | 3.30            | 20.0        |           | 100       | 1809         | 275             | 0.152    |            | 100       | 1809         | 164             | 0.091    |            |
|                          | RT               | G2            | 3            | 3.30            | 15.0        |           | 100       | 1895         | 289             | 0.153    |            | 100       | 1895         | 172             | 0.091    |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              |                 |          |            |           |              |                 |          |            |
| AM Traffic Flow (pcu/hr) | I                | ,             | PM Traffic I | low (pcu/hr)    |             | Ī         | N         |              | S=1940+         | 100(W_3  | 25) S=     | =2080+100 | O(W-3.25)    | Note:           |          |            |
| 564⁴                     | N                | $\leftarrow$  |              |                 |             | 336◀      | N         | $\leftarrow$ |                 | +1.5f/r) |            |           | ÷(1+1.5f/r)  |                 |          |            |
| 237                      |                  |               |              |                 | 183         | 000       |           |              |                 | AM Pe    | ak Hour    |           | ak Hour      |                 |          |            |
| → 499 → 262              |                  |               |              | 498             |             | 315       |           |              |                 | 1,3+2    | 1+2+3      | 1,3+2     | 1+2+3        |                 |          |            |
| 621                      |                  |               |              | 573<br><b>↑</b> |             |           |           |              | Sum y           | 0.574    | 0.601      | 0.548     | 0.514        |                 |          |            |
| 1627 1684                | — <sub>839</sub> |               | 1584         | ़ ←             | 1821        | •—        | 737       | •—           | L(s)            | 12       | 17         | 12        | 17           |                 |          |            |
|                          | 845              | $\overline{}$ |              |                 |             |           | 1084      | $\neg$       | C (s)           | 140      | 140        | 140       | 140          |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              | practical y     | 0.823    | 0.791      | 0.823     |              |                 |          |            |
|                          |                  |               |              |                 |             |           |           |              | R.C. (%)        | 43%      | 32%        | 50%       | 54%          |                 |          |            |
| 1                        | 2                |               |              |                 | 3           |           |           |              |                 |          |            |           |              |                 |          |            |
| <b>↑</b> F1              |                  |               |              |                 |             |           | 1 1       |              |                 |          |            |           |              |                 |          |            |
| —                        | <b>■</b> E1      |               |              |                 | D1 <b>†</b> | _         | G2 G1     |              |                 |          |            |           |              |                 |          |            |
| C3 ← A2 ←                | 4                |               | C3 ←         | -               | _           |           |           |              |                 |          |            |           |              |                 |          |            |
| C1 ← A1 ←                | 7                |               | C1 <b>←</b>  | B1 B2           |             |           |           | B1 B2        |                 |          |            |           |              |                 |          |            |

|          | C3 ← — — — — — — — — — — — — — — — — — — | 2 | → E1 <del>- ↑</del> F | 2     | D1 11 B2 1 ■ 1 | <u>t_</u> | G2 G1 | - 1 |     |       |     |       |
|----------|--|---|-----------------------|-------|----------------|-----------|-------|-----|-----|-------|-----|-------|
| AM<br>G= | I/G =                                    | 8 | G =                   | I/G = | 6              | G =       | I/G = |     | G = | I/G = | G = | I/G = |
| AMG=     | I/G =                                    | 8 | G =                   | I/G = | 6              | G =       | I/G = | 6   | G = | I/G = | G = | I/G = |
| PM<br>G= | I/G =                                    | 8 | G =                   | I/G = | 6              | G =       | I/G = |     | G = | I/G = | G = | I/G = |
| G =      | I/G =                                    | 8 | G =                   | I/G = | 6              | G =       | I/G = | 6   | G = | I/G = | G = | I/G = |

 Junction:
 Wo Hop Shek Interchange
 Job Number:
 J7411

 Scenario:
 Without Proposed EV Mobility City
 J6 - P. 2

| Design Year: 2034       | Designe      | ed By:       |              | MCY           |            |                       | Checke    | ed By:                |                                  | WCH          |             |              | Date:                 | 15 /                        | August 2 | 2025    |
|-------------------------|--------------|--------------|--------------|---------------|------------|-----------------------|-----------|-----------------------|----------------------------------|--------------|-------------|--------------|-----------------------|-----------------------------|----------|---------|
| Approach                |              | Phase        | Stage        | Width (m)     | Radius (m) | % Up-hill<br>Gradient | Turning % | Sat. Flow<br>(pcu/hr) | AM Peak<br>Flow<br>(pcu/hr)      | y value      | Critical y  | Turning %    | Sat. Flow<br>(pcu/hr) | PM Peak<br>Flow<br>(pcu/hr) | y value  | Critica |
| Pak Wo Road NB          | SA           | A1           | 1            | 3.30          |            |                       |           | 1945                  | 434                              | 0.223        |             |              | 1945                  | 391                         | 0.201    |         |
|                         | SA           | A2           | 1            | 3.40          |            |                       |           | 2095                  | 468                              | 0.223        |             |              | 2095                  | 422                         | 0.201    |         |
| -<br>anling Highway     | LT           | B1           | 2,3          | 4.00          | 30.0       |                       | 100       | 1919                  | 323                              | 0.168        |             | 100          | 1919                  | 473                         | 0.246    |         |
| Slip Road NB            | LT           | B2           | 2,3          | 4.00          | 35.0       |                       | 100       | 2066                  | 348                              | 0.168        |             | 100          | 2066                  | 509                         | 0.246    |         |
| Pak Wo Road NB          | SA           | C1           | 1,2          | 3.00          |            |                       |           | 1915                  | 500                              | 0.261        |             |              | 1915                  | 571                         | 0.298    |         |
|                         | SA           | C2           | 1,2          | 3.00          |            |                       |           | 2055                  | 537                              | 0.261        |             |              | 2055                  | 612                         | 0.298    |         |
|                         | SA           | C3           | 1,2          | 3.00          |            |                       |           | 2055                  | 536                              | 0.261        |             |              | 2055                  | 612                         | 0.298    |         |
| Pak Wo Road NB          | RT           | D3           | 1,3          | 3.00          | 15.0       |                       | 100       | 1868                  | 756                              | 0.405        | 0.405       | 100          | 1868                  | 697                         | 0.373    | 0.37    |
| Jockey Club Road SB     | SA           | E1           | 2            | 4.50          |            |                       |           | 2065                  | 608                              | 0.294        | 0.294       |              | 2065                  | 604                         | 0.292    | 0.29    |
| Pak Wo Road SB          | LT           | F1           | 1,2          | 3.40          | 20.0       |                       | 100       | 1819                  | 324                              | 0.178        |             | 100          | 1819                  | 260                         | 0.143    |         |
|                         | SA           | F2           | 1,2          | 3.30          |            |                       |           | 2085                  | 284                              | 0.136        |             |              | 2085                  | 344                         | 0.165    |         |
| Wo Hing Road WB         | RT           | G1           | 3            | 3.30          | 20.0       |                       | 100       | 1809                  | 378                              | 0.209        |             | 100          | 1809                  | 231                         | 0.128    |         |
|                         | RT           | G2           | 3            | 3.30          | 15.0       |                       | 100       | 1895                  | 396                              | 0.209        |             | 100          | 1895                  | 243                         | 0.128    |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
|                         |              |              |              |               |            |                       |           |                       |                                  |              |             |              |                       |                             |          |         |
| M Traffic Flow (pcu/hr) | N            | $\leftarrow$ | PM Traffic I | Flow (pcu/hr) |            |                       | N         | $\leftarrow$          | S=1940+<br>S <sub>M</sub> =S÷(1- |              |             | =(S-230)÷    |                       | Note:                       |          |         |
| 774 <b>~</b><br>324     | 4            |              |              |               | 260        | 474                   |           |                       | JM 0.(1                          | AM Pe        |             | PM Pe        |                       |                             |          |         |
| 608                     | 324          |              |              | 604           | <b>A</b>   | 344                   |           |                       |                                  | 1,3+2        | 1+2+3       | 1,3+2        | 1+2+3                 |                             |          |         |
| 756<br>1591 1573 1573   | 1573 - 902 - |              |              | 697           | 1795       | •—                    | 813       | •—                    | Sum y                            | 0.699        | 0.727<br>17 | 0.666        | 0.622                 |                             |          |         |
|                         | 671          | _            | 1572         |               |            |                       | 982       |                       | C (s)                            | 140          | 140         | 140          | 140                   |                             |          |         |
|                         | _            | <u> </u>     |              |               |            |                       |           |                       | practical y                      | 0.823<br>18% | 0.791<br>9% | 0.823<br>24% | 0.791<br>27%          |                             | _        |         |
| ı                       | 2            |              |              |               | 3          |                       |           |                       |                                  |              |             |              |                       |                             |          |         |

| 1        | c3 ←<br>C2 ← A2 ←<br>C1 ← A1 ← | 2 | → E1 → F2 | α ←<br>α ←<br>α ←<br>α ← B1 | - 1 | <u>†</u> |       | B2<br><b>★</b> |     |       |     |       |
|----------|--------------------------------|---|-----------|-----------------------------|-----|----------|-------|----------------|-----|-------|-----|-------|
| AM<br>G= | I/G =                          | 8 | G =       | I/G =                       | 6   | G =      | I/G = |                | G = | I/G = | G = | I/G = |
| G =      | I/G =                          | 8 | G =       | I/G =                       | 6   | G =      | I/G = | 6              | G = | I/G = | G = | I/G = |
| PM<br>G= | I/G =                          | 8 | G =       | I/G =                       | 6   | G =      | I/G = |                | G = | I/G = | G = | I/G = |
| G =      | I/G =                          | 8 | G =       | I/G =                       | 6   | G =      | I/G = | 6              | G = | VG =  | G = | I/G = |

Junction: Wo Hop Shek Interchange Job Number: <u>J7411</u> With Proposed EV Mobility City J6 - P. 3 Scenario: De

| Design Year: | 2034 | Designed By: | MCY | Checked Bv: | WCH | Date: | 15 August 2025 |
|--------------|------|--------------|-----|-------------|-----|-------|----------------|
|              |      |              |     |             |     |       |                |

| Design Year: 2034        | Designed By: MCY |  | MCY          |                 | -               | Checke                | ed By:           |                       | WCH                  |           |            | Date:     | 15 /                  | August 2         | 2025    |            |
|--------------------------|------------------|--|--------------|-----------------|-----------------|-----------------------|------------------|-----------------------|----------------------|-----------|------------|-----------|-----------------------|------------------|---------|------------|
|                          |                  |  |              | ı               | I               | <u> </u>              | 1                |                       | AM Peak              |           |            |           |                       | PM Peak          |         |            |
| Approach                 |                  | Phase                                      | Stage        | Width (m)       | Radius (m)      | % Up-hill<br>Gradient | Turning %        | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr)     | y value   | Critical y | Turning % | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr) | y value | Critical y |
| Pak Wo Road NB           | SA               | A1   | 1            | 3.30            |                 |                       |                  | 1945                  | 434                  | 0.223     |            |           | 1945                  | 391              | 0.201   |            |
|                          | SA               | A2   | 1            | 3.40            |                 |                       |                  | 2095                  | 468                  | 0.223     |            |           | 2095                  | 422              | 0.201   |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| Fanling Highway          | LT               | B1   | 2,3          | 4.00            | 30.0            |                       | 100              | 1919                  | 323                  | 0.168     |            | 100       | 1919                  | 473              | 0.246   |            |
| Slip Road NB             | LT               | B2   | 2,3          | 4.00            | 35.0            |                       | 100              | 2066                  | 348                  | 0.168     |            | 100       | 2066                  | 509              | 0.246   |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| Pak Wo Road NB           | SA               |  | 1,2          | 3.00            |                 |                       |                  | 1915                  | 500                  | 0.261     |            |           | 1915                  | 571              | 0.298   |            |
|                          | SA               | C2   | 1,2          | 3.00            |                 |                       |                  | 2055                  | 537                  | 0.261     |            |           | 2055                  | 612              | 0.298   |            |
|                          | SA               | C3   | 1,2          | 3.00            |                 |                       |                  | 2055                  | 536                  | 0.261     |            |           | 2055                  | 612              | 0.298   |            |
| D-I-W- D IND             | DT               | Do   | 4.0          | 0.00            | 45.0            |                       | 400              | 4000                  | 700                  | 0.400     | 0.400      | 400       | 4000                  | 740              | 0.000   | 0.000      |
| Pak Wo Road NB           | RT               | D3   | 1,3          | 3.00            | 15.0            |                       | 100              | 1868                  | 763                  | 0.408     | 0.408      | 100       | 1868                  | 710              | 0.380   | 0.380      |
| Jackey Club Boad SB      | SA               | E1   | 2            | 4 50            |                 |                       |                  | 2065                  | 622                  | 0.301     | 0.201      |           | 2065                  | 616              | 0.298   | 0.200      |
| Jockey Club Road SB      | - SA             | <u> </u>                                   | 2            | 4.50            |                 |                       |                  | 2003                  | 622                  | 0.301     | 0.301      |           | 2005                  | 010              | 0.296   | 0.290      |
| Pak Wo Road SB           | LT               | F1   | 1,2          | 3.40            | 20.0            |                       | 100              | 1819                  | 338                  | 0.186     |            | 100       | 1819                  | 272              | 0.150   |            |
|                          | SA               | F2   | 1,2          | 3.30            |                 |                       | 1.00             | 2085                  | 284                  | 0.136     |            | 100       | 2085                  | 344              | 0.165   |            |
|                          |                  |  | ,-           |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| Wo Hing Road WB          | RT               | G1   | 3            | 3.30            | 15.0            |                       | 100              | 1768                  | 390                  | 0.221     |            | 100       | 1768                  | 247              | 0.140   |            |
|                          | RT               |  | 3            | 3.30            | 10.0            |                       | 100              | 1813                  | 399                  | 0.220     |            | 100       | 1813                  | 253              | 0.140   |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| AM Traffic Flow (pcu/hr) |                  | $\leftarrow$                               | PM Traffic F | Flow (pcu/hr)   |                 |                       | N                | $\leftarrow$          |                      | 100(W-3.2 | 25) S=     | 2080+100  | O(W-3.25)             | Note:            |         |            |
| 789 <sup>&lt;</sup>      |                  |  |              |                 |                 | 500◀                  |                  |                       | S <sub>M</sub> =S÷(1 |           |            |           | ÷(1+1.5f/r)           |                  |         |            |
| 338                      |                  |  |              |                 | 272<br><b>•</b> |                       |                  |                       |                      | AM Pe     | ak Hour    | PM Pe     | ak Hour               |                  |         |            |
| 622 284                  |                  |  |              | 616             |                 | 344                   |                  |                       |                      | 1,3+2     | 1+2+3      | 1,3+2     | 1+2+3                 |                  |         |            |
| 763<br><b>↑</b>          |                  |  |              | 710<br><b>↑</b> |                 |                       |                  |                       | Sum y                | 0.710     |            | 0.678     | 0.639                 |                  |         |            |
| 1599 1573                | 902              | _  | 1585         | ←—              | 1795            | •                     | 813              |                       | L (s)                | 12        | 17         | 12        | 17                    |                  |         |            |
|                          | 671              |  |              |                 |                 |                       | 982              |                       | C (s)                | 140       | 140        | 140       | 140                   |                  |         |            |
|                          |                  | l  |              |                 |                 |                       |                  | ļ                     | practical y          | 0.823     | 0.791      | 0.823     | 0.791                 |                  |         |            |
|                          |                  |  |              |                 |                 |                       |                  |                       | R.C. (%)             | 16%       | 6%         | 21%       | 24%                   |                  |         |            |
| 1                        | 2                |  |              |                 | 3               |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| <b>_</b> F1              |                  |  |              |                 |                 |                       | 1 1              |                       |                      |           |            |           |                       |                  |         |            |
| → F2<br>D3 ♠             | E1               | F1<br>———————————————————————————————————— |              |                 | D1 <b>†</b>     | _                     | <b>4 4</b> G2 G1 |                       |                      |           |            |           |                       |                  |         |            |
| C3 ← A2 ←                | _                |  | C3 <b>←</b>  | -               |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| c1 ← A1 ←                | $\neg$           |  | C1 <b>←</b>  | B1 B2           |                 |                       |                  | B1 B2                 |                      |           |            |           |                       |                  |         |            |
| AM                       |                  |  |              | 11              |                 |                       |                  |                       |                      |           |            |           |                       |                  |         |            |
| G= VG =                  | 8 G=             |  | I/G =        | 6               |                 |                       | I/G =            |                       | G =                  |           | I/G =      |           | G =                   |                  | I/G =   |            |
| G = I/G =<br>PM          | 8 G=             |  | I/G =        | 6               |                 |                       | I/G =            | 6                     |                      |           | I/G =      |           | G =                   |                  | I/G =   |            |
| G= I/G =                 | 8 G=             |  | I/G =        | 6               |                 |                       | I/G =            |                       | G =                  |           | I/G =      |           | G =                   |                  | I/G =   |            |
| G = VG =                 | 8 G=             |  | I/G =        | 6               | G =             |                       | I/G =            | 6                     | G =                  |           | I/G =      |           | G =                   |                  | I/G =   |            |

 Junction:
 Wo Hop Shek Interchange
 Job Number:
 J7411

 Scenario:
 With Proposed EV Mobility City (With Traffic Improvement)
 J6 - P. 4

Design Year: 2034 Designed By: MCY Checked By: WCH Date: 15 August 2025

|                       |     |       | _     |           |            |                       |           |                       | AM Peak          |         |            |           |                       | PM Peak          |         |            |
|-----------------------|-----|-------|-------|-----------|------------|-----------------------|-----------|-----------------------|------------------|---------|------------|-----------|-----------------------|------------------|---------|------------|
| Approach              |     | Phase | Stage | Width (m) | Radius (m) | % Up-hill<br>Gradient | Turning % | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr) | y value | Critical y | Turning % | Sat. Flow<br>(pcu/hr) | Flow<br>(pcu/hr) | y value | Critical y |
| Pak Wo Road NB        | SA  | A1    | 1     | 3.75      |            |                       |           | 1990                  | 288              | 0.145   |            |           | 1990                  | 260              | 0.131   |            |
|                       | SA  | A2    | 1     | 3.65      |            |                       |           | 2120                  | 307              | 0.145   |            |           | 2120                  | 277              | 0.131   |            |
|                       | SA  | А3    | 1     | 3.65      |            |                       |           | 2120                  | 307              | 0.145   |            |           | 2120                  | 276              | 0.130   |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
| Fanling Highway       | LT  | B1    | 2,3   | 4.00      | 30.0       |                       | 100       | 1919                  | 323              | 0.168   |            | 100       | 1919                  | 473              | 0.246   |            |
| Slip Road NB          | LT  | B2    | 2,3   | 4.00      | 35.0       |                       | 100       | 2066                  | 348              | 0.168   |            | 100       | 2066                  | 509              | 0.246   |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
| Pak Wo Road NB        | SA  | C1    | 1,2   | 3.00      |            |                       |           | 1915                  | 500              | 0.261   |            |           | 1915                  | 571              | 0.298   |            |
|                       | SA  | C2    | 1,2   | 3.00      |            |                       |           | 2055                  | 537              | 0.261   |            |           | 2055                  | 612              | 0.298   |            |
|                       | SA  | C3    | 1,2   | 3.00      |            |                       |           | 2055                  | 536              | 0.261   |            |           | 2055                  | 612              | 0.298   |            |
|                       |     |       | ,     |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
| Pak Wo Road NB        | RT  | D3    | 1,3   | 3.00      | 15.0       |                       | 100       | 1868                  | 763              | 0.408   | 0.408      | 100       | 1868                  | 710              | 0.380   | 0.380      |
| T dit VVO Ttodd TVD   |     |       | 1,0   | 0.00      | 10.0       |                       | 100       | 1000                  | 700              | 0.100   | 0.100      | 100       | 1000                  | 7.10             | 0.000   | 0.000      |
| Jockey Club Road SB   | SA  | E1    | 2     | 4.50      |            |                       |           | 2065                  | 622              | 0.301   | 0 301      |           | 2065                  | 616              | 0.298   | 0.298      |
| occitor class read ob | 0/1 |       |       | 1.00      |            |                       |           | 2000                  | ULL              | 0.001   | 0.001      |           | 2000                  | 010              | 0.200   | 0.200      |
| Pak Wo Road SB        | LT  | F1    | 1,2   | 3.40      | 20.0       |                       | 100       | 1819                  | 338              | 0.186   |            | 100       | 1819                  | 272              | 0.150   |            |
| T ak WO Noad OB       | SA  | F2    | 1,2   | 3.40      | 20.0       |                       | 100       | 2095                  | 284              | 0.136   |            | 100       | 2095                  | 344              | 0.164   |            |
|                       | OA  | 12    | 1,2   | 0.40      |            |                       |           | 2000                  | 204              | 0.100   |            |           | 2000                  | 044              | 0.104   |            |
| Wo Hing Road WB       | RT  | G1    | 3     | 3.30      | 15.0       |                       | 100       | 1768                  | 390              | 0.221   |            | 100       | 1768                  | 247              | 0.140   |            |
| Wo Tilling Road WB    | RT  | G2    | 3     | 3.30      | 10.0       |                       | 100       | 1813                  | 399              | 0.220   |            | 100       | 1813                  | 253              | 0.140   |            |
|                       | 111 | 02    |       | 0.00      | 10.0       |                       | 100       | 1010                  | 000              | 0.220   |            | 100       | 1010                  | 200              | 0.140   |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |
|                       |     |       |       |           |            |                       |           |                       |                  |         |            |           |                       |                  |         |            |

