Appendix 1

Traffic Impact Assessment

## Traffic Impact Assessment

For<br>Amendment of Plan to

Rezone from "Residential (Group D)" ("R(D)"), "Residential (Group E)" (" $R(E) ")$ and an area shown as 'Road' to "Residential (Group C)3) ("R(C)3")
on the Approved Ho Chung Outline Zoning Plan No. S/SK-HC/11
at Various Lots in Demarcation District 210 and Demarcation District 244 and Adjoining Government Land

Ho Chung, Sai Kung, New Territories, Hong Kong

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Appendix A Junction Analysis

## 1. Introduction

1.1.1 This Traffic Impact Assessment (TIA) is prepared as part of the Section 12A Application for the amendment of plan to rezone to "Residential (Group C) 3 " ("R(C)3") on the Approved Ho Chung Outline Zoning Plan No. S/SK-HC/11 (the Approved OZP) at various lots in Demarcation District 210 (D.D.210) and Demarcation District 244 (D.D.244) and adjoining government land, at Ho Chung, Sai Kung, New Territories (the Site) with a Site area about 3,190 sq.m. [Figure 1.1]
1.1.2 The TIA is required as part of the Section 12A planning application for the Proposed Development for rezone the Subject Site from "Residential (Group D)" ("R(D)"), "Residential (Group E)" ("R(E)") and an area shown as 'Road' to "Residential (Group C) 3 " ("R(C) 3 ") zoned with a maximum site coverage of $25 \%$ and a maximum building height of 12 m with 3 storeys over one storey of carport PR of 0.75 on the Approved OZP.
1.1.3 The owner of the Site has the intention to construct six individual houses with six ancillary car parking spaces of 2.5 m X 5 m , six accessible visitor parking space of 3.5 mX 5 m and one light goods vehicles (LGV) loading/unloading bay $3.5 \mathrm{~m} \mathrm{X} \mathrm{7m}$ in Parcel A \& B of the Site, and two individual houses with two ancillary car parking spaces of 2.5 m X 5 m , two accessible visitor parking space of 3.5 m X 5 m in Parcel C of the Site.
1.1.4 This traffic impact assessment (TIA) study is to support the proposed development. This report describes the traffic impact assessment undertaken.

### 1.2 Study Objectives

1.2.1 The objectives of this study can be summarised as follows:

- undertake traffic impact assessment to assess the traffic impact to be induced by the proposed development on the nearby road network in the vicinity of the Subject Site;
- design and conduct traffic surveys during peak hours in the vicinity of the Subject Site to supplement available information and traffic data;
- estimate the extra volumes of traffic that will be generated by the proposed development during the peak period (arrivals and departures);
- estimate the likely changes of circulation patterns and traffic flow in the future road network adjacent to the Subject Site;
- review the capacity of the critical links of the road networks adjacent to the Subject Site;
- provide traffic advice on the internal vehicular movements; and
- advise on the provision of internal parking and loading and unloading spaces based on relevant standards and requirements for residential development.


## 2. Proposed Development

2.1.1 The proposed development is to erect six individual houses in Parcel A \& B of the Site and two individual houses in Parcel C of the Site. The proposed gross floor area (GFA) of the houses are summarised in Table 2.1.

| Propose House | Gross Floor Area (GFA) (sqm) (about) |
| :--- | :---: |
| House 1 | 283 |
| House 2 | 283 |
| House 3 | 283 |
| House 4 | 283 |
| House 5 | 283 |
| House 6 | 283 |
| House 7 | 346 |
| House 8 | 346 |
| Total | 2,390 |
| Average Size | 299 |

Table 2.1 Proposed GFA of Houses
2.1.2 The proposed development would adopt a household size of 4 per house. In this connection, a total population of 32 would be used.

## 3. Existing Traffic Situation

### 3.1 Existing Road Network

3.1.1 The Site is located at Ho Chung North Road (former Luk Mei Tsuen Road), which is a Feeder Road with single-two carriageway connecting to Hiram's Highway to the east.
3.1.2 The connecting section of Hiram's Highway was a Rural Road improved in 2020 year, from single-two carriageway to dual-two carriageway.
3.1.3 The critical road links and junctions in this study are, from north to south:

- J1 - Hiram's Highway / Marina Cove North Access
- J2 - Hiram's Highway / Marina Cove South Access
- L1 - Hiram's Highway between Ho Chung North Road (former Luk Mei Tsuen Road) and Ho Chung Road
- J3 - Hiram's Highway / Ho Chung Road
- L2 - Hiram's Highway between Ho Chung Road and Nam Pin Wai Road
- J4 - Hiram's Highway / New Hiram's Highway / Nam Pin Wai Road (Roundabout)
3.1.4 The Area of Influence (AoI) and Study Area are shown in Figure 1.1.


### 3.2 Public Transport

3.2.1 Public transport services include franchised bus, green minibus (GMB) and public light bus (PLB) in the vicinity are depicted in Figure 3.1 and summarised in Table 3.1.

Rezone from "Residential (Group D)" (" $R(D)$ "), ""Residential (Group E)" (" $R(E)$ ") and an area shown as 'Road' to
"Residential (Group C)3" (" $R(C) 3$ ") on the Approved Ho Chung Outline Zoning Plan No. S/SK-HC/11
Various Lots in Demarcation District 210 and Demarcation District 244 and Adjoining Government Land Ho Chung, Sai Kung, New Territories, Hong Kong

| Franchised Bus |  |  |
| :--- | :--- | :--- |
| Route | Destination | Frequency (min) |
| 92 | Sai Kung - Diamond Hill Station | $12-20$ |
| $92 R$ | Sai Kung - Star Ferry | 20 (Sunday and Holidays only) |
| $96 R$ | Wong Shek Pier - Diamond Hill <br> Station | $18-25$ (Sunday and Holidays <br> only) |
| $292 P$ | Sai Kung - Kwun Tong | $7: 30$ (Only one departure <br> Monday to Friday) |
| 792 M | Sai Kung - Tseung Kwan O Station | $15-20$ |
| Green Minibus (GMB) Services |  |  |
| 1 | Sai Kung - Kowloon Bay | $8-20$ |
| 1 A | Sai Kung - San Po Kong | 4 |
| $1 S$ | Sai Kung - San Po Kong | $10-15$ |
| 2 | Sai Kung - Ho Chung | $15-30$ |
| 12 | Sai Kung - Po Lam | $10-15$ |
| 101 M | Sai Kung - Hang Hau Station | $3-5$ |
| Public Light Bus (PLB) Services |  |  |
| -- | Sai Kung - Kwun Tong | $5-12$ |
| -- | Sai Kung -Mong Kok | Depart when fully loaded |
| -- | Sai Kung - Causeway Bay | $10-15$ |

Table 3.1 Service Provision of Public Transport

### 3.3 Future Road Network

3.3.1 To support the continued development and population growth in Sai Kung Area, Hiram's Highway Improvement is divided into two stages. Stage 1 between Clear Water Bay Road and Marina Cove has been completed in 2021. The works include improvement works that would relieve the traffic congestion on the road section near Marina Cove, enhance the safety of the road section and improve the local access to Ho Chung and Luk Mei Tsuen.
3.3.2 Stage 2 is to improve the section of Hiram's Highway, Po Tung Road and Tai Mong Tsai Road from Marina Cove to the south of Sha Ha. The proposed improvement works will relieve traffic congestion and enhance the safety of the road section at Sai Kung area. The project is currently under review and the commencement date is under review. The location of the improvements for Stage 2 are presented in Figure 3.2.

### 3.4 Traffic Count Surveys

3.4.1 In order to appraise the actual traffic demand for the proposed development, classified turning movement count surveys are carried out during peak hours, 07:00 to 10:00 and 17:00 to 20:00 on both Wednesday, 26 August 2020 and Sunday, 30 August 2020 at the key junctions of the study area as presented in Figure 3.3.
3.4.2 The traffic count survey data were recorded in a 15 minutes interval, and to be converted into pcu per hour. The highest hourly traffic volume is adopted as the peak hour traffic flow.
3.4.3 The morning and afternoon peak hours during weekday of the road network have been identified as 08:00 to 09:00 and 17:30 to 18:30 respectively. Meanwhile the peak hour of the weekend was observed to be 17:15 to 18:15. The observed traffic flows in the study area presented in Figure 3.4.

### 3.5 Existing Capacity Assessment

## Junction Capacity

3.5.1 Based on the observed traffic flows, the performance of the key junctions in the vicinity of the subject site during the morning and evening peak hours were assessed. The results area summarised and presented in Table 3.2 and the detailed calculation sheets are attached in Appendix A.
3.5.2 The Design Flow / Capacity (DFC) ratio is measured in evaluating the performance of a roundabout or priority junction. With reference to Ch4, Vol2, TPDM, a DFC ratio of 0.85 can be considered reasonable.
3.5.3 The performance of a traffic signalised junction is indicated by its reserved capacity (RC). A positive RC indicates that the junction is operating with spare capacity. A negative RC indicates that the junction is overloaded; resulting in traffic queues and longer delay.

| Jun <br> No. | Junction Location | Type/ Capacity <br> Index | AM Peak <br> Hour | PM Peak <br> Hour | Weekend <br> Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: |
| J1 | Luk Cheung Road <br> /Hiram's Highway <br> / Marina Cove <br> North Access | Priority / DFC | 0.12 | 0.07 | 0.07 |
| J2 | Luk Mei Tsuen <br> Road /Hiram's <br> Highway/ Marina <br> Cove South <br> Access | Signal / RC | $147 \%$ | $113 \%$ | $135 \%$ |
| J3 | Ho Chung Road <br> /Hiram's Highway | Signal / RC | $83 \%$ | $109 \%$ | $88 \%$ |
| J4 | Nam Pin Wai <br> Road / New <br> Hiram's Highway <br> / Hiram's <br> Highway | Roundabout / DFC | 0.71 | 0.64 | 0.69 |

Notes: RC=reserved capacity; DFC=Design Flow/ Capacity Ratio
Table 3.2 Existing Junction Performance
3.5.4 It can be observed in Table 3.2 that all of the key junctions perform satisfactorily during peak hours with adequate reserved capacities.
Link Capacity
3.5.5 Considering the routing of development traffic and construction traffic, link capacity of Sai Kung bound of L1 and L2, and Kowloon bound of L2 are assessed.
3.5.6 The result of road link capacity assessment is summarised in Table 3.3. With reference to para 10.6.4.5, Vol6, TPDM, the desirable limit of volume to capacity (V/C) ratio is less than 0.85 for links.

| Link No. | Section of <br> Hiram's <br> Highway | Link <br> Capacity <br> (veh/hr) | Reference Flow <br>  <br>  <br> (Saily Kung <br> Bound) |  | Between Ho <br> Chung Road <br> and Luk Mei <br> Tsuen Road | 2600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Weekend | Reference V/C Ratio <br> Peak | Weekend |  |  |  |
| L2 <br> (Sai Kung <br> Bound) | Between Ho <br> Chung Road <br> and Nam Pin <br> Wai Road | 2600 | 1336 | 1243 | 0.51 | 0.47 |
| L2 <br> (Kowloon <br> Bound) | Between Ho <br> Chung Road <br> and Nam Pin <br> Wai Road | 2600 | 1303 | 1143 | 0.50 | 0.44 |

Notes: Based on TPDM Volume 2 Chapter 2.4 - Design Flow Characteristics, it is assumed 2600 veh/hour for dual two-lane carriageway for one direction of flow.

Table 3.3 Existing Link Performance
3.5.7 It can be seen from Table 3.3 that all of the key links are within design capacities.

## 4. Future Traffic Situation

### 4.1 2028 Design Year Road Network

4.1.1 The anticipated year of completion for the proposed development is 2025. The design year is either 3 years after the completion year or 5 years after the application year, which ever longer. Therefore, Year 2028 is adopted as the design year of this study.

### 4.2 Traffic Generation

4.2.1 The proposed development is intended for eight single-family houses with an average size of 299 sq.m. It is proposed that there will only be 16 parking spaces.
4.2.2 The estimated average traffic generation and traffic attraction rate at peak hours are based on the trip rate based on the Transport Planning and Design Manual published by the Transport Department and are summarised in Table 4.1.

| Description | AM Peak |  | PM Peak |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Generation | Attraction | Generation | Attraction |
| Trip Rate (pcu/unit/hr) | 0.3252 | 0.2609 | 0.2835 | 0.4074 |

Rezone from "Residential (Group D)" ("R(D)"), ""Residential (Group E)" (" $R(E)$ ") and an area shown as 'Road' to
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Note 1: As the Site is used as a single-family house, the commutes would take place once in the morning and once in the afternoon to/from work/school.
Note 2: The pcu of a private car is taken as 1.
Note 3: Morning peak is defined as 8:00 a.m. to 9:00 a.m. whereas afternoon peak is defined as 6:00 p.m. to 7:00 p.m.

Table $4.1 \mathrm{AM} / \mathrm{PM}$ Peak Generation and Attraction
4.2.3 As shown in Table 4.1, the proposed development would generate 3(2) pcus and attract $2(3)$ pcus in the morning (evening) peak hours, which is considered negligible.
4.2.4 The development traffic was re-distributed and assigned onto the existing road network. Figure 4.1 show that resulting assignment of the proposed development traffic.

### 4.3 Regional Traffic Growth

4.3.1 For the estimation of traffic flows in the design year of 2028, it is proposed to adjust the existing traffic flows to take into account of the natural traffic growth which is related to the increase in car usage.

## Annual Traffic Census (ATC)

4.3.2 Reference has been made with uses of 2016 to 2021 (Latest) Annual Traffic Census Reports. The traffic data recorded at counting stations adjacent to the site are shown in Table 4.2.

| Station No./Road <br> Name | $\mathbf{2 0 1 6}$ | $\mathbf{2 0 1 7}$ | $\mathbf{2 0 1 8}$ | $\mathbf{2 0 1 9}$ | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 2 1}$ | Growth <br> per <br> Annum |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6055/ Hiram's <br> Highway | 25,610 | 24,050 | 24,450 | 24,280 | 23,360 | 24,460 | $\mathbf{- 0 . 9 1 \%}$ |
| 5017/ Clear Water <br> Bay Road | 29,370 | 26,910 | 28,450 | 28,980 | 28,900 | 29,100 | $\mathbf{- 0 . 1 8 \%}$ |
| 5466 / Clear Water <br> Bay Road | 18,770 | 18,650 | 18,950 | 20,240 | 19,110 | 20,020 | $\mathbf{1 . 3 0 \%}$ |
| 6056/ Sai Sha Road | 10,780 | 10,990 | 11,880 | 11,800 | 11,350 | 11,880 | $\mathbf{1 . 9 6 \%}$ |
| Total Growth per Annum |  |  | $\mathbf{0 . 2 2 \%}$ |  |  |  |  |

Source: Annual Traffic Census, Transport Department
Table 4.2: Traffic Data from Annual Traffic Census Reports
4.3.3 It is noted from Table 4.2 that $+0.22 \%$ annual growth is observed from the traffic flow record over the past five years.
Territory Population and Employment Data Matrices (TPEDM)
4.3.4 According to the latest 2019-based TPEDM from year 2019 to year 2031 in Southeast New Territories (Other Area) published on the PlanD website. The population growth from the base year 2019 to 2031 is $-1.18 \%$ as shown in Table 4.3.

Rezone from "Residential (Group D)" ("R(D)"), ""Residential (Group E)" (" $R(E)$ ") and an area shown as 'Road' to
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| Planning Data District | Year 2019 | Year 2026 | Year 2031 | Growth Rate <br> p.a. (\%) |
| :--- | :---: | :---: | :---: | :---: |
| Southeast New <br> Territories (Other Area) | 68,900 | 65,800 | 59,750 | $-1.18 \%$ |

Table 4.3 Projected Population by TPEDM, 2019-2031
4.3.5 After comparing the historical data and the future planning data, for conservative purpose, an annual growth rate of $+1.00 \%$ was adopted.

### 4.4 Reference and Design Flows

4.4.1 The anticipated year of completion and estimated year of population intake of the proposed development is 2025. The design year for assessment is 3 years after the completion year, i.e. Year 2028, is adopted as the design year of this study.
4.4.2 The growth factor derived in Section 4.3 will be applied to the traffic flows of 2020 observed peak hours, to estimate the 2028 reference flows.
4.4.3 The reference and design flows for design year 2028 are calculated from the following formulae:

2028 Reference Flows $=2020$ Observed Flows $x(1+1.00 \%)^{\wedge} 8$
2028 Design Flows $=2028$ Reference Flows + Proposed Development Traffic
4.4.4 Based on the observed traffic flows and pattern of existing and future road network, the 2028 peak hour Reference Flows at the critical junctions are presented in Figure 4.2. Meanwhile, the design Flows are presented in Figure 4.3.

### 4.5 Capacity Assessment Construction Stage and After Project Completion

## Construction Stage Junction Capacity

4.5.1 Based on similar projects, it is assumed that the development would generate 3(3) and attract 3(3) no. of construction vehicles (i.e. generate 6(6) and attract 6(6) pcus), in the morning (afternoon) peak hours throughout the week. The project is anticipated to be completed 2025. The reference peak hours traffic flows and design peak hours traffic flows are shown in Figures 4.4 and 4.5 respectively. The results are summarised and presented in Table 4.4 and shown in Figure 4.6.

| $\begin{aligned} & \text { Jun } \\ & \text { No. } \end{aligned}$ | Junction Location | Type/ Capacity Index | 2025 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Reference |  |  | Design |  |  |
|  |  |  | AM | PM | Week end | AM | PM | Week end |
| J1 | Luk Cheung <br> Road <br> /Hiram's <br> Highway / <br> Marina <br> Cove North | Priority / DFC | No Construction Traffic |  |  |  |  |  |

Traffic Impact Assessment for Amendment of Plan
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|  | Access |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Luk Mei <br> Tsuen Road <br> /Hiram's <br> Highway/ <br> Marina <br> Cove South <br> Access | Signal / RC | Construction Traffic Free Flow from Hiram's Highway <br> Northbound Left Turning to Luk Mei Tsuen Road |  |  |  |  |  |
|  | Ho Chung <br> Road <br> Hiram's <br> Highway | Signal /RC | $74 \%$ | $99 \%$ | $79 \%$ | $73 \%$ | $97 \%$ | $79 \%$ |
|  | Nam Pin <br> Wai Road / <br> New <br> Hiram's <br> Highway / <br> Hiram's <br> Highway | Roundabout DFC <br> / | 0.75 | 0.68 | 0.73 | 0.76 | 0.68 | 0.73 |

Notes: RC=reserved capacity; DFC=Design Flow/ Capacity Ratio
Table 4.4 2025 Construction Stage Junction Capacity
4.5.2 According to Table 4.4, the capacity of all the keys junctions would be performing satisfactorily during the peak periods for both the Reference and Design Scenarios.

## Construction Stage Link Capability

4.5.3 The link capacity assessment results with reference to the net development are summarised in Table 4.5.

| Link No. | Section of Hiram's Highwa y | Link <br> Capacit <br> y <br> (veh/hr) | Reference Flow |  | Reference V/C Ratio |  | Design Flow |  | $\begin{gathered} \hline \text { Design V/C } \\ \text { Ratio } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Daily Peak | Week end | Daily Peak | Week end | Daily Peak | Week end | Daily Peak | Week end |
| L1 <br> (Sai Kung Bound) | Between Ho Chung Road and Luk Mei Tsuen Road | 2600 | 1404 | 1306 | 0.54 | 0.50 | 1410 | 1312 | 0.54 | 0.50 |
| L2 <br> (Sai Kung Bound) | Between Ho Chung Road and Nam Pin | 2600 | 1059 | 1249 | 0.41 | 0.48 | 1065 | 1255 | 0.41 | 0.48 |

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|  | Wai <br> Road |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Between <br> Ho <br> L2 <br> (Kowloo <br> n Bound) |  |  |  |  |  |  |  |  |
| Road <br> and <br> Nam Pin <br> Wai <br> Road | 2600 | 1369 | 1201 | 0.53 | 0.46 | 1375 | 1207 | 0.53 | 0.46 |

Notes: Based on TPDM Volume 2 Chapter 2.4 - Design Flow Characteristics, it is assumed 2600 veh/hour for dual two-lane carriageway for one direction of flow.

Table 4.5 2025 Construction Stage Link Capacity
4.5.4 It can be seen from Table 4.5 that all of the key links perform satisfactorily during the peak hours with adequate reserve capacities.

## Future Junction Capacity

4.5.5 After completion of the widening of Hiram's Highway, the new signalised junction at Ho Chung Road will be assessed. Capacity assessments were carried out for the major junctions in the local network for both the Reference and Design scenarios. The results are summarised and presented in Table 4.6 with detailed calculations sheets attached in Appendix A.

| $\begin{aligned} & \text { Jun } \\ & \text { No. } \end{aligned}$ | Junction Location | Type/ Capacity Index | 2028 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Reference |  |  | Design |  |  |
|  |  |  | AM | PM | Week end | AM | PM | Week end |
| J1 | Luk Cheung Road /Hiram's Highway / Marina Cove North Access | Priority / DFC | No Construction Traffic |  |  |  |  |  |
| J2 | Luk Mei <br> Tsuen Road <br> /Hiram's <br> Highway/ <br> Marina <br> Cove South <br> Access | Signal / RC | Construction Traffic Free Flow from Hiram's Highway Northbound Left Turning to Luk Mei Tsuen Road |  |  |  |  |  |
| J3 | Ho Chung Road /Hiram's Highway | Signal / RC | 69\% | 93\% | 74\% | 68\% | 92\% | 74\% |
| J4 | Nam Pin Wai Road/ | Roundabout / DFC | 0.78 | 0.70 | 0.75 | 0.78 | 0.70 | 0.75 |

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|  | New <br> Hiram's <br> Highway/ <br> Hiram's <br> Highway |  |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Notes: RC=reserved capacity; DFC=Design Flow/ Capacity Ratio
Table 4.62028 Junction Capacity Assessments
4.5.6 According to Table 4.6, the capacity of all the key junctions would be preforming satisfactory during the peak periods for bother the Reference and Design Scenarios.

## Future Link Capacity

4.5.7 The road link capacity assessment results with reference to the development traffic are summarised in Table 4.7.

| Link No. | Section of Hiram's Highwa y | Link Capacit y (veh/hr) | Reference Flow |  | Reference V/C Ratio |  | Design Flow |  | Design V/C Ratio |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Daily Peak | Week end | Daily <br> Peak | Week end | Daily <br> Peak | Week end | Daily <br> Peak | Week end |
| L1 <br> (Sai Kung Bound) | Between Ho Chung Road and Luk Mei Tsuen Road | 2600 | 1447 | 1346 | 0.56 | 0.52 | 1453 | 1352 | 0.56 | 0.52 |
| L2 <br> (Sai Kung Bound) | Between <br> Ho <br> Chung <br> Road <br> and <br> Nam Pin <br> Wai <br> Road | 2600 | 1092 | 1286 | 0.42 | 0.49 | 1098 | 1292 | 0.42 | 0.50 |
| L2 <br> (Kowloo <br> n Bound) | Between <br> Ho <br> Chung <br> Road <br> and <br> Nam Pin <br> Wai <br> Road | 2600 | 1411 | 1238 | 0.54 | 0.48 | 1417 | 1244 | 0.54 | 0.48 |

Notes: Based on TPDM Volume 2 Chapter 2.4 - Design Flow Characteristics, it is assumed 2600 veh/hour for dual two-lane carriageway for one direction of flow.

Table 4.72028 Link Capacity
4.5.8 Table 4.7 demonstrates that all of the key links perform satisfactorily during peak hours with adequate reserve capacities after completion of the improvement works.

## 5. Transport Provision

### 5.1 Parking and Loading/Unloading Provision

5.1.1 With reference to the proposed plan, 12 car parking spaces ( 6 ancillary carparking spaces and 6 accessible/visitor parking space) and one LGV loading/unloading bay for the residential development are proposed to serve the needs occupants in Parcel A \& B and 4 car parking spaces ( 2 ancillary carparking spaces and 2 accessible/visitor parking space) are proposed to serve the needs occupants in Parcel C. This is summarised in Table 5.1.

| Type of Parking Space/Bay | Provision |
| :--- | :---: |
| Parcel A \& B for 6 Houses |  |
| Private Car (2.5m X 5m) | 6 |
| Accessible Visitor (3. 5X 5m) | 6 |
| Loading/Unloading Bay (3.5 X 7m) | 1 |
| Parcel C for 2 Houses |  |
| Private Car (2.5m X 5m) |  |
| Accessible Visitor (3.5X 5m) | 2 |

Table 5.1 Provision of Internal Transport

### 5.2 Hong Kong Planning Standards and Guidelines (HKPSG)

5.2.1 The car parking requirements and loading/unloading provisions for the proposed development in accordance with the HKPSG are listed in Table 5.2.

| Development | Facility | HKPSG Standard | Required | Provision |
| :---: | :---: | :---: | :---: | :---: |
| Residential (8 units with avg. size of 299 sqm) | Car Parking | Global Parking Standard (GPS) = 1 <br> Car space per 4-7 <br> flats <br> R1 $=7.0$ for avg. flat <br> size over 160 sqm <br> R2 = 1 (outside a <br> 500 m radius of rail <br> station) <br> R3 = 1.3 of domestic <br> plot ratio 0.00-1.00 | 11-19 | 16 |

\(\left.$$
\begin{array}{|l|l|l|l|}\hline & \begin{array}{l}\text { Loading/Unloading } \\
\text { Bay }\end{array}
$$ \& \begin{array}{l}Minimum of 1 <br>
Loading/Unloading <br>
Bay for goods <br>
vehicles within the <br>
site for every 800 <br>
flats or part thereof, <br>
subject to a <br>
minimum of 1 bay <br>
for each housing <br>
block or as <br>
determined by the <br>

Authority.\end{array} \& 1\end{array}\right\} 1\)|  |
| :--- |

Table 5.2 HKPSG Requirement and Provision

### 5.3 Ingress/Egress Points and Internal Manoeuvring

5.3.1 The proposed ingress and egress point to all Parcels of the Site will be from Ho Chung North Road. In all Parcels of the Site, adequate maneuvering space is proposed for the maneuvering within the Site for the vehicles such that no vehicle queuing outside the Site would occur as a result of the proposed developments. In addition, there will be no reverse onto/from Ho Chung North Road to the Site. [Figure 5.1]

## 6. Conclusions

6.1.1 The traffic generation from the proposed development (including the construction period) is minimal in nature and will have will have minimal traffic impact to the surrounding network.
6.1.2 The proposed development would provide a total of 16 carparking spaces and 1 loading/unloading bay which fulfills the requirements of HKPSG.
6.1.3 The proposed development will provide adequate maneuvering space within all Parcels of the Site. Therefore, no queuing or reversing motion will occur at the street level.
6.1.4 As a result, it is concluded that the proposed development would not generate any significant adverse impact to the traffic of the surrounding vicinity of the Site.

Figures













Appendix A
Junction Analysis











| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1207 | 138 | 1521 | 47 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 116 | 1253 | 194 | 1477 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2278 | 1312 | 2129 | 743 | Total In Sum = | 2913 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.53 | 0.11 | 0.71 | 0.06 | DFC of Critical Approach = | 0.71 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1453 | 74 | 1306 | 52 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 148 | 1513 | 157 | 1157 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2260 | 1180 | 2149 | 879 | Total In Sum = | 2885 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.64 | 0.06 | 0.61 | 0.06 | DFC of Critical Approach = | 0.64 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1289 | 55 | 1516 | 61 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 125 | 1336 | 84 | 1325 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2273 | 1270 | 2189 | 808 | Total In Sum = | 2921 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.57 | 0.04 | 0.69 | 0.08 | DFC of Critical Approach = | 0.69 |  |









| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1268 | 145 | 1599 | 49 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 122 | 1317 | 203 | 1553 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2275 | 1279 | 2124 | 710 | Total In Sum = | 3061 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.56 | 0.11 | 0.75 | 0.07 | DFC of Critical Approach = | 0.75 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1526 | 77 | 1373 | 54 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 155 | 1589 | 164 | 1216 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2256 | 1142 | 2145 | 854 | Total In Sum = | 3030 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.68 | 0.07 | 0.64 | 0.06 | DFC of Critical Approach = | 0.68 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1355 | 57 | 1593 | 63 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 130 | 1403 | 87 | 1392 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2270 | 1236 | 2188 | 779 | Total In Sum = | 3068 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.60 | 0.05 | 0.73 | 0.08 | DFC of Critical Approach = | 0.73 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1274 | 145 | 1605 | 49 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 122 | 1323 | 203 | 1559 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2275 | 1276 | 2124 | 708 | Total In Sum = | 3073 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.56 | 0.11 | 0.76 | 0.07 | DFC of Critical Approach = | 0.76 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1532 | 77 | 1379 | 54 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 155 | 1595 | 164 | 1222 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2256 | 1139 | 2145 | 852 | Total In Sum = | 3042 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.68 | 0.07 | 0.64 | 0.06 | DFC of Critical Approach = | 0.68 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1361 | 57 | 1599 | 63 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 130 | 1409 | 87 | 1398 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2270 | 1233 | 2188 | 777 | Total In Sum = | 3080 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.60 | 0.05 | 0.73 | 0.08 | DFC of Critical Approach = | 0.73 |  |









| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1306 | 148 | 1648 | 50 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 125 | 1356 | 208 | 1599 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2273 | 1260 | 2121 | 691 | Total In Sum = | 3152 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.57 | 0.12 | 0.78 | 0.07 | DFC of Critical Approach = | 0.78 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1572 | 79 | 1414 | 55 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 159 | 1637 | 168 | 1252 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2254 | 1117 | 2143 | 839 | Total In Sum = | 3120 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.70 | 0.07 | 0.66 | 0.07 | DFC of Critical Approach = | 0.70 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1395 | 58 | 1641 | 65 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 134 | 1446 | 89 | 1433 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2268 | 1214 | 2186 | 762 | Total In Sum = | 3159 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.62 | 0.05 | 0.75 | 0.09 | DFC of Critical Approach = | 0.75 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1308 | 148 | 1651 | 50 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 125 | 1358 | 208 | 1602 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | $=$ | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | $=$ | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | = | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2273 | 1259 | 2121 | 689 | Total In Sum = | 3157 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.58 | 0.12 | 0.78 | 0.07 | DFC of Critical Approach = | 0.78 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1575 | 79 | 1416 | 55 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 159 | 1640 | 168 | 1254 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2254 | 1116 | 2143 | 838 | Total In Sum = | 3125 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.70 | 0.07 | 0.66 | 0.07 | DFC of Critical Approach = | 0.70 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.5 | 6.0 | 7.6 | 3.5 |  |  |  |
|  | $=$ | Entry width (m) | 8.5 | 7.0 | 7.6 | 6.0 |  |  |  |
|  | $=$ | Effective length of flare (m) | 13.5 | 6.0 | 0.0 | 6.0 |  |  |  |
|  | $=$ | Entry radius (m) | 20.0 | 20.0 | 22.5 | 17.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 78.0 | 78.0 | 78.0 | 78.0 |  |  |  |
|  | $=$ | Entry angle (degree) | 50.0 | 40.0 | 40.0 | 30.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 1397 | 58 | 1643 | 65 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 134 | 1448 | 89 | 1435 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.12 | 0.27 | 0.00 | 0.67 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 0.93 | 0.97 | 0.97 | 0.99 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 8.31 | 6.65 | 7.60 | 4.57 |  |  |  |
|  | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 6 | 6 | 6 | 6 |  |  |  |
| F | $=$ | 303*X2 | 2517 | 2016 | 2303 | 1385 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.07 | 1.07 | 1.07 | 1.07 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.60 | 0.52 | 0.57 | 0.43 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2268 | 1213 | 2186 | 761 | Total In Sum = | 3163 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.62 | 0.05 | 0.75 | 0.09 | DFC of Critical Approach = | 0.75 |  |

